

substitution

$$\tilde{\phi}^{n+1} = 2\tilde{\phi}^{n+1/2} - \tilde{\phi}^n \quad (60a)$$

$$h^{n+1} = 2h^{n+1/2} - h^n \quad (60b)$$

$$W^{n+1} = 2W^{n+1/2} - W^n \quad (60c)$$

$$Z^{n+1} = 2Z^{n+1/2} - Z^n \quad (60d)$$

is made such that the coupled system is solved in terms of the (five) midpoint variables. Once these are solved, the update to (discrete) time level  $n + 1$  is made using the above relations (60). To numerically solve the system at rest in order to establish the initial condition, the following VP can be employed

$$0 = \delta \left[ \int_0^{L_x} g h^{n+1/2} V^{n+1/2} \left( \frac{1}{2} h^{n+1/2} - H_0 \right) - \frac{1}{2} g V^{n+1/2} H_0^2 + V^{n+1/2} F \left( \frac{h_b(Z^{n+1/2}, x) - h^{n+1/2}}{\alpha} \right) dx + m g Z^{n+1/2} \right] \quad (61)$$

for  $n = 0$  and with  $V^{n+1/2} = L_w$ . Variational derivatives with respect to  $\{h^{n+1/2}, Z^{n+1/2}\}$  will establish the weak formulations to be solved.

For reference, Achimedes' law yields the following based on geometric considerations. The position of the keel is  $Z - K$ . Assuming a rest water level  $H_0$ , the submerged buoy depth at  $x = L_x$  is  $H_0 + K - Z$ . The width of the buoy at the water line is then

$$L_x - L_b = (H_0 + K - Z)/\tan \theta. \quad (62)$$

Hence, the submerged volume is  $V_b = \frac{1}{2} L_y (H_0 + K - Z)^2 / \tan \theta$ . The displaced water mass equals the mass of the buoy. Hence, the rest reference level  $Z$  is

$$\begin{aligned} \rho V_b &= \rho \frac{1}{2} L_y (H_0 + K - Z)^2 / \tan \theta = M \\ \implies Z &= H_0 + K - \sqrt{2m \tan \theta} \end{aligned} \quad (63)$$

with water density  $\rho$ , which results can be used as reference for the numerical solution using the soft-boundary method. For example, when  $L_y = H_0 = Z = 1\text{m}$ ,  $K = 0.5\text{m}$  and  $\tan \theta = 1$  we find that  $m = (1/8)\text{m}$  such that the mass of the buoy  $M = 125\text{kg}$ .

Alternatively, the VP using the exact constraint  $h - h_b(Z, x) = 0$  between free surface and buoy reads

$$\begin{aligned} 0 = \delta \int_0^T \int_0^{L_x} & \phi \partial_t h - \frac{1}{2} h (\partial_x \phi)^2 - g h \left( \frac{1}{2} h - H_0 \right) + \frac{1}{2} g H_0^2 \\ & + \lambda (h_b(Z, x) - h) \Theta(x - x_p) dx \\ & + m W \dot{Z} - \frac{1}{2} m W^2 - m g Z dt. \end{aligned} \quad (64)$$

with Lagrange multiplier  $\lambda$  and Heaviside function  $\Theta(\cdot)$ . Its

variations are

$$\begin{aligned} 0 = \int_0^T \int_0^{L_x} & \delta \phi (\partial_t h + \partial_x (h \partial_x \phi)) \\ & - \delta h \left( \partial_t \phi + \frac{1}{2} (\partial_x \phi)^2 + g(h - H_0) + \lambda \Theta(x - x_p) \right) dx \\ & + m \delta W (\dot{Z} - W) \\ & - \delta Z (m \dot{W} + m g - \int_{x_b}^{L_x} \lambda dx) dt \end{aligned} \quad (65)$$

with  $x_p$  the dynamic waterline point.

Hence, at rest, the following system needs to be solved

$$g(h - H_0) = -\lambda \Theta(x - L_b) \quad (66a)$$

$$h - h_b(Z, x) = 0 \quad (66b)$$

$$h_b(Z, x) = Z - K + \theta(L_x - x) \quad (66c)$$

$$m g = \int_{L_b}^{L_x} \lambda dx \quad (66d)$$

where at rest  $x_b = L_b$  is as before the function of  $Z$  and  $H_0$  in (62). An interim step in the solution of the above system is  $\lambda = g(H_0 - h_b(Z, x))$ , which substitution into the last equation while using the expression for  $h_b(Z, x)$  again yields (63).

Comparison of the two VPs (53) and (64) provides an interpretation of the buffer potential  $\mu F(s)$ , in that

$$\lambda (h_b(Z, x) - h) \Theta(x - x_b) \approx -\mu F \left( \frac{h_b(Z, x) - h}{\alpha} \right) \quad (67a)$$

$$\lambda \Theta(x - x_b) \approx -\frac{\mu}{\alpha} F' \left( \frac{h_b(Z, x) - h}{\alpha} \right). \quad (67b)$$

We can therefore attempt to tune  $\alpha, \beta, \mu$  for sufficiently small values towards the exact rest-state solution in order to improve the numerical solution of the rest state using the buffer potential  $\mu F(s)$  instead of the constraint and its Lagrange multiplier.

## APPENDIX G. 3D POTENTIAL FLOW VIA VP

The VP (a simplification of expression (8) in [21]) for 3D potential flow without wavemaker (in an  $x$ -periodic) domain is

$$\begin{aligned} 0 = \delta \int_0^T \left\{ \int_{\Omega_{x,y}} \left[ \int_0^{H_0} \left[ \frac{1}{2} \frac{L_w^2}{W} h (\phi_x - \frac{1}{h} (H_0 b_x + z h_x) \phi_z)^2 \right. \right. \right. \\ \left. \left. + \frac{1}{2} W h \left( \phi_y - \frac{1}{h} (H_0 b_y + z h_y) \phi_z \right)^2 \right. \right. \\ \left. \left. + \frac{1}{2} W \frac{H_0^2}{h} (\phi_z)^2 \right] dz \right. \\ \left. + H_0 \left( g W h \left( \frac{1}{2} h - H_0 \right) - \phi W h_t \right) \right|_{z=H_0} dx dy \right\} dt \end{aligned} \quad (68)$$

with

$$W = L_w, \quad (69)$$

noting that  $W$  is more complicated when there is a piston wave-maker present. In addition, topography  $b$  needs to be periodic in the  $x$ -direction. **Implemented and seems to be working on**

initialisation with linear waves; soliton in periodic channel next, then SP2 and SP3; then wavebreaking. parameterisation.

Upon making the splitting  $\phi(x, y, z, t) = \psi(x, y, t)\hat{\phi}(z) + \varphi(x, y, z, t)$  with  $\hat{\phi}(H_0 = 1)$  and  $\varphi(x, y, H_0, t) = 0$ , the MMP time discretisation of (69) reads

$$\begin{aligned}
0 = \int_{\Omega_{x,y}} & \left[ \left( -H_0 W \psi^{n+1/2} \frac{(h^{n+1} - h^n)}{\Delta t} + H_0 h^{n+1/2} \frac{(W \psi^{n+1} - W \psi^n)}{\Delta t} \right. \right. \\
& \left. \left. + H_0 g W h^{n+1/2} \left( \frac{1}{2} h^{n+1/2} - H_0 \right) \right) \right. \\
& + \int_0^{H_0} \left[ \frac{1}{2} \frac{L_w^2}{W} h^{n+1/2} (\psi_x^{n+1/2} \hat{\phi} + \varphi_x^{n+1/2} - \frac{1}{h^{n+1/2}} (H_0 b_x + z h_x^{n+1/2}) (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2}))^2 \right. \\
& + \frac{1}{2} W h^{n+1/2} \left( \psi_y^{n+1/2} \hat{\phi} + \varphi_y^{n+1/2} - \frac{1}{h^{n+1/2}} (H_0 b_y + z h_y^{n+1/2}) (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2}) \right)^2 \\
& \left. \left. + \frac{1}{2} W \frac{H_0^2}{h^{n+1/2}} (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2})^2 \right] dz \right] dx dy. \quad (70)
\end{aligned}$$

The time-discrete VP corresponding to SV reads

$$\begin{aligned}
0 = \int_{\Omega_{x,y}} & \left[ \left( -H_0 W \psi^{n+1/2} \frac{(h^{n+1} - h^n)}{\Delta t} + H_0 W \psi^{n+1} \frac{h^{n+1}}{\Delta t} - H_0 W \psi^n \frac{h^n}{\Delta t} \right. \right. \\
& \left. \left. + \frac{1}{2} H_0 g W (h^{n+1} (\frac{1}{2} h^{n+1} - H_0) + h^n (\frac{1}{2} h^n - H_0)) \right) \right. \\
& + \frac{1}{2} \int_0^{H_0} \left[ \frac{1}{2} \frac{L_w^2}{W} h^{n+1} (\psi_x^{n+1/2} \hat{\phi} + \varphi_x^{n+1/2} - \frac{1}{h^{n+1}} (H_0 b_x + z h_x^{n+1}) (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2}))^2 \right. \\
& + \frac{1}{2} W h^{n+1} \left( \psi_y^{n+1/2} \hat{\phi} + \varphi_y^{n+1/2} - \frac{1}{h^{n+1}} (H_0 b_y + z h_y^{n+1}) (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2}) \right)^2 \\
& \left. \left. + \frac{1}{2} W \frac{H_0^2}{h^{n+1}} (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2})^2 \right] dz \right. \\
& + \frac{1}{2} \int_0^{H_0} \left[ \frac{1}{2} \frac{L_w^2}{W} h^n (\psi_x^{n+1/2} \hat{\phi} + \varphi_x^{n+1/2} - \frac{1}{h^n} (H_0 b_x + z h_x^n) (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2}))^2 \right. \\
& + \frac{1}{2} W h^n \left( \psi_y^{n+1/2} \hat{\phi} + \varphi_y^{n+1/2} - \frac{1}{h^n} (H_0 b_y + z h_y^n) (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2}) \right)^2 \\
& \left. \left. + \frac{1}{2} W \frac{H_0^2}{h^n} (\psi^{n+1/2} \hat{\phi}_z + \varphi_z^{n+1/2})^2 \right] dz \right] dx dy. \quad (71)
\end{aligned}$$

Variations herein are taken with respect to  $\{h^n, \varphi^{n+1/2}\}$  to update  $\{\psi^{n+1/2}, \varphi^{n+1/2}\}$  in unison, then  $\psi^{n+1/2}$  to update  $h^{n+1}$ , and finally  $h^{n+1}$  to update to  $\psi^{n+1}$ .