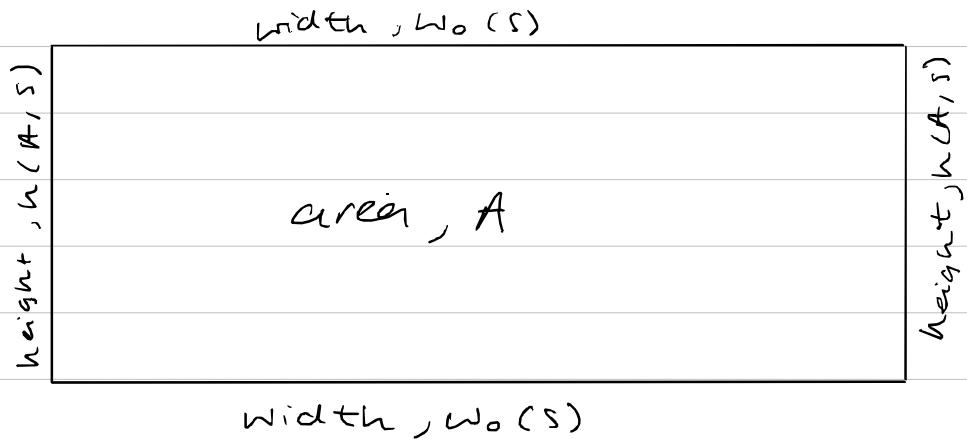


1. Rectangular cross section



Given rectangular model, Area = width \times height

$$\Rightarrow A = w_0(s) \times h(A, s)$$

$$\Rightarrow h(A, s) = \frac{A}{w_0(s)}$$

Wetted perimeter, $P(A, s) = \sum_{\text{all edges with}} \text{exception of river surface}$

$$\Rightarrow P = w_0 + h + h$$

$$\text{given } h(A, s) = \frac{A}{w_0(s)}$$

$$\Rightarrow P(A, s) = w_0 + 2 \left(\frac{A}{w_0(s)} \right)$$

$$\frac{A^{5/3} \sqrt{-\omega_0 b}}{C_m P(A, s)^{2/3}}$$

$$= A^{5/3} P(A, s)^{-2/3} \cdot G(s)$$

where $G(s) \equiv \sqrt{\frac{\omega_0 b}{C_m}}$ (only dependent on $s \Rightarrow$ only a constant in $\frac{\partial F}{\partial A}$)

$$\frac{\partial F}{\partial A} = G(s) \cdot \frac{\partial}{\partial A} \left(A^{5/3} P^{-2/3} \right)$$

$$= G(s) \cdot \left(\frac{5}{3} A^{2/3} P^{-2/3} + A^{5/3} (-2/3) P^{-5/3} \frac{\partial P}{\partial A} \right)$$

$$= G(s) \cdot \left(\frac{5}{3} A^{2/3} P^{-2/3} - \frac{2}{3} A^{5/3} P^{-5/3} \cdot \frac{2}{\omega_0} \right)$$

$$\frac{\partial F}{\partial A} = \frac{5 \sqrt{-\omega_0 b}}{3 C_m} \cdot \frac{A^{2/3}}{P^{2/3}} - \frac{2 \sqrt{-\omega_0 b}}{3 C_m} \cdot \frac{2 A^{5/3}}{\omega_0 P^{5/3}}$$

$$\text{given } P = \omega_0 + 2A/\omega_0$$

$$\Rightarrow \frac{\partial F}{\partial A} = \frac{5 \sqrt{-\omega_0 b}}{3 C_m} \cdot \frac{A^{2/3}}{(A/\omega_0 + 2)^{2/3}} - \frac{2 \sqrt{-\omega_0 b}}{3 C_m} \cdot \frac{2 A^{5/3}}{(A/\omega_0 + 2)^{5/3}}$$

Can also be written as

$$\frac{\sqrt{-\omega_0 b}}{3 C_m} \cdot A^{2/3} \left(\omega_0 + 2A/\omega_0 \right)^{-5/3} \left(5 \left(\omega_0 + 2A/\omega_0 \right) - \frac{4A}{\omega_0} \right)$$

$$= \frac{\sqrt{-ds_b}}{3 \text{ cm}} A^{2/3} \left(\omega_0 + \frac{2A}{\omega_0} \right)^{-5/3} \left(5\omega_0 + \frac{10A}{\omega_0} - \frac{4A}{\omega_0} \right)$$

$$= \frac{\sqrt{-ds_b}}{3 \text{ cm}} A^{2/3} \left(\omega_0 + \frac{2A}{\omega_0} \right)^{-5/3} \left(5\omega_0 + \frac{6A}{\omega_0} \right)$$

$$= \frac{\sqrt{-ds_b}}{3 \text{ cm}} \cdot \frac{\left(5\omega_0 A^{2/3} + 6A^{5/3}/\omega_0 \right)}{\left(\omega_0 + 2A/\omega_0 \right)^{5/3}}$$

ω_0, A, cm - real scalar quantities $\Rightarrow > 0$

$-ds_b$ is positive else the expressions are not valid
hence $\sqrt{-ds_b}$ hence all values

$$\frac{\partial F}{\partial A} > 0$$

$$\frac{\partial F}{\partial S} = \frac{\partial}{\partial S} \left(G(S) \cdot A^{5/3} P^{-2/3} \right)$$

Assuming A is independent of S

$$\rightarrow \frac{\partial F}{\partial S} = A^{5/3} \cdot \frac{\partial}{\partial S} \left(G(S) \cdot P^{-2/3} \right)$$

$$= A^{5/3} \left(G'(S) \cdot P^{-2/3} - \frac{2}{3} G(S) \cdot P^{-5/3} \frac{\partial P}{\partial S} \right)$$

$$= A^{5/3} \left[G'(S) P^{-2/3} - \frac{2}{3} G(S) P^{-5/3} \left(\frac{\partial}{\partial S} \left(\omega_0 + \frac{2A}{\omega_0} \right) \right) \right]$$

$$= A^{5/3} \left(G'(s) \bar{P}^{2/3} - \frac{2}{3} G(s) \bar{P}^{-5/3} \left(\frac{d\omega_0}{ds} - \frac{2A}{\omega_0^2} \frac{d\omega_0}{ds} \right) \right)$$

$G'(s)$ will be much less than the second term and is considered negligible

$$\Rightarrow \frac{\partial F}{\partial s} = - \frac{2\sqrt{dsb}}{3cm} A^{5/3} \bar{P}^{-5/3} \left(1 - \frac{2A}{\omega_0^2} \right) \frac{d\omega_0}{ds}$$

$$\text{given } P = \omega_0 + \frac{2A}{\omega_0}$$

$$\rightarrow \frac{\partial F}{\partial s} = - \frac{2\sqrt{dsb}}{3cm} \cdot \frac{A^{5/3}}{(\omega_0 + 2A/\omega_0)^{5/3}} \left(1 - \frac{2A}{\omega_0^2} \right) \frac{d\omega_0}{ds}$$

with $s=0$, equation (2) becomes

$$dt A + ds F(A, s) = 0$$

which can be expressed as

$$dt A + \frac{\partial F}{\partial A} \partial_s A + \frac{\partial F}{\partial s} = 0$$

2. Where $\omega_0(s)$ is independent of s , or varying very slowly the PDE (3) :
 $\partial_t A + \partial_s F(A, s) = 0$ can be treated as a scalar conservation law where

$$\lambda(A) = \frac{\partial F}{\partial A} = \frac{1}{3} \sqrt{f_{sb}} \cdot \frac{s \omega_0 + 6A/\omega_0}{(s \omega_0 + 2A/\omega_0)^{5/3}}$$

Initial data

$$A(s, 0) = \begin{cases} A_L, & s < 0 \\ A_R, & s > 0 \end{cases}$$

$\frac{df}{dA} > 0 \Rightarrow \lambda(A) > 0$ hence characteristics move downstream

Given monotonicity of $\lambda(A)$ (A, ω_0 are physical scalar quantities) solutions of type :

$A_L < A_R$ characteristics diverge \rightarrow rarefaction fan

$A_L > A_R$ characteristics converge \rightarrow shock formation

$A_L = A_R$ constant solution

Rarefaction ($A_L < A_R$)

Self-similar solution depending on $S (= s/t)$

Inside a centred rarefaction fan, the solution
satisfies the self-similar relation

$$\xi = \lambda(A(\xi))$$

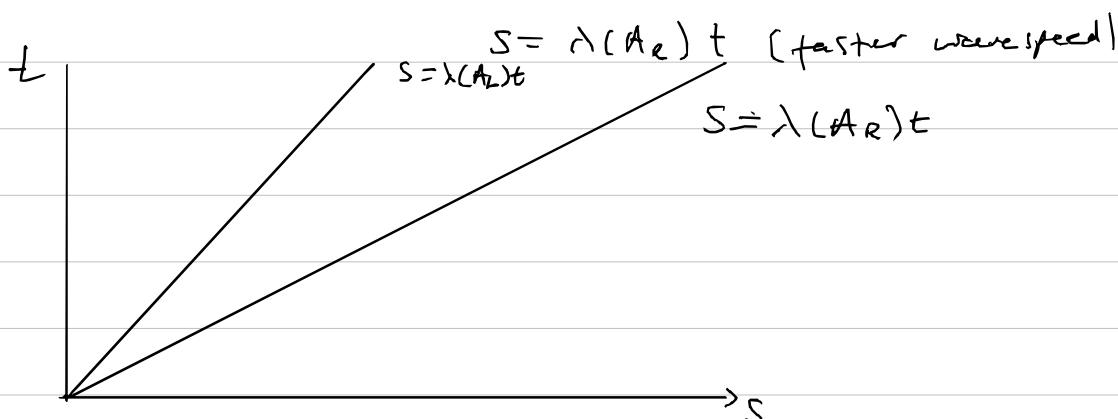
Because λ is strictly increasing ($A_L < A_R$ and $A > 0$) relation can be inverted to give

$$A(s, t) = \lambda^{-1}(s/t) \text{ for } \lambda(A_L) \leq s/t \leq \lambda(A_R)$$

Providing the Riemann solution

$$A(s, t) = \begin{cases} A_L, & s/t < \lambda(A_L) \\ \lambda^{-1}(s/t), & \lambda(A_L) \leq s/t \leq \lambda(A_R) \\ A_R, & s/t > \lambda(A_R) \end{cases}$$

Characteristic lines: $s = \lambda(A_i)t$ ('slower wave speed')



Shock ($A_L > A_R$)

Shock moves with Rankine-Hugoniot speed:

$$\sigma = \frac{f(A_R) - f(A_L)}{A_R - A_L}$$

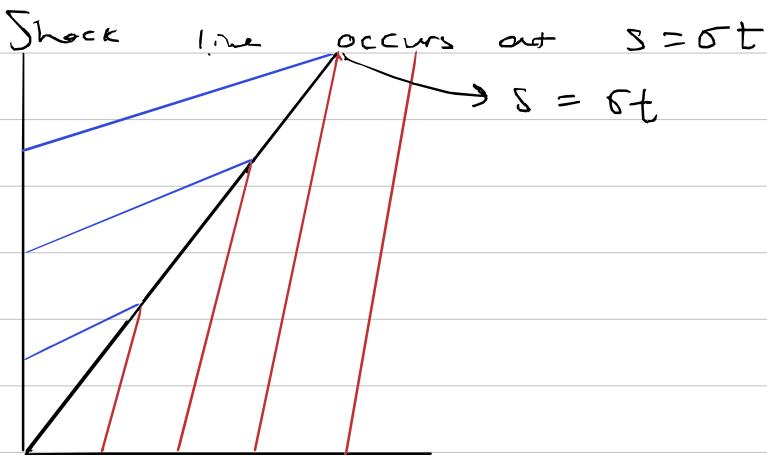
Entropy condition for a compressive shock
enforces that

$$\lambda(A_R) \leq \sigma < \lambda(A_L)$$

Meaning: characteristics left of the shock
impinge upon it and characteristics leave
right of it.

Riemann solution:

$$A(s, t) = \begin{cases} A_L, & s < \sigma t \\ A_R, & s > \sigma t \end{cases}$$



If $w_0(s)$ is slowly varying, the solution can
be treated as locally constant, therefore

the Riemann solution is still valid locally.

Over longer distances / times, the characteristics will curve since t weakly depends on s due to $w_0(s)$ causing small differences in the rarefaction or shock speed over large distance / time.

$$3. \quad \partial_t A(s, t) + \partial_s F(A, s) = 0$$

Integrate over cell K $(s_{k-1/2}, s_{k+1/2})$ and over time interval (t_n, t_{n+1})

$$\int_{t_n}^{t_{n+1}} \int_{s_{k-1/2}}^{s_{k+1/2}} (\partial_t A + \partial_s F) ds dt = 0$$

Swapping integrals and using divergence theorem for 1D:

$$\Rightarrow \int_{s_{k-1/2}}^{s_{k+1/2}} (A(s, t^{n+1}) - A(s, t^n)) ds + \int_{t_n}^{t_{n+1}} (F(A, s)|_{s_{k+1/2}} - F(A, s)|_{s_{k-1/2}}) dt = 0$$

Defining cell average:

$$\hat{A}_K = \frac{1}{\Delta s_K} \int_{s_{k-1/2}}^{s_{k+1/2}} A(s, t^n) ds \quad [\text{where } \Delta s_K = \text{cell width}]$$

Then the update formula becomes

$$\bar{A}_k^{n+1} - \bar{A}_k^n = \frac{1}{\Delta s_k} \int_{t_n}^{t_{n+1}} (F(A, s)|_{s_{k+1/2}} - F(A, s)|_{s_{k-1/2}}) dt = c$$

$$\Rightarrow \bar{A}_k^{n+1} = \bar{A}_k^n + \frac{1}{\Delta s_k} \int_{t_n}^{t_{n+1}} (F(A, s)|_{s_{k+1/2}} - F(A, s)|_{s_{k-1/2}}) dt$$

In Godunov's method, the solution is represented as piecewise constant

states equal to cell averages:

$$A(s, t^n) \approx \begin{cases} \bar{A}_k^n, & s \in (s_{k-1/2}, s_{k+1/2}) \\ \bar{A}_{k+1}^n, & s \in (s_{k+1/2}, s_{k+3/2}) \end{cases}$$

At each interface $s_{k+1/2}$ solve the Riemann problem with left state \bar{A}_k^n and right state

$$\bar{A}_{k+1}^n$$

$$\Rightarrow A(s, t^n) = \begin{cases} \bar{A}_k^n, & s \leq s_{k+1/2} \\ \bar{A}_{k+1}^n, & s > s_{k+1/2} \end{cases}$$

The Riemann solution is self-similar: $A(s, t) = A(\xi)$

with $\xi = \frac{s - s_{k+1/2}}{t - t^n}$. The state exactly at the interface corresponds to $\xi = 0$ and is determined entirely by the cell averaged values $\bar{A}_k^n, \bar{A}_{k+1}^n$

$$\Rightarrow A_{k+1/2}^* = A(0; \bar{A}_k^n, \bar{A}_{k+1}^n)$$

Since Riemann solution is self-similar, flux out
to interface $t \in (t_{k+1}, t_{k+2})$ is constant in time
and given by $F(A^*_{k+1/2}, S_{k+1/2})$ therefore
the time integral reduces to $\Delta t \cdot F(A^*_{k+1/2}, S_{k+1/2})$

Godunov numerical flux given by

$$F_{k+1/2}(\bar{A}_k^n, \bar{A}_{k+1}^n) = f(A^*_{k+1/2}, S_{k+1/2})$$

Update becomes

$$\bar{A}_{k+1}^n = \bar{A}_k^n - \frac{\Delta t}{\Delta S_k} \left[F_{k+1/2}(\bar{A}_k^n, \bar{A}_{k+1}^n) - F_{k-1/2}(\bar{A}_{k-1}^n, \bar{A}_k^n) \right]$$

(all averages are used as !)

- Godunov reconstructs solution based on piecewise constant values from previous cell, defining the Riemann problem at each interface.
- Self similarity of the Riemann solution means at each interface only the left and right initial states are required.
- Explicit time stepping means \bar{A}^{n+1} is not solved within each step \Rightarrow fluxes are known.

4. Because for the Manning flux $\lambda(A) = F(A) > 0$ for all physically admissible $A \geq 0$, every characteristic at an interface points downstream. Therefore the Godunov flux is purely upwind.

$$F_{k+1/2} = f(A_L, S_{k+1/2}) = F(\bar{A}_k^+, S_{k+1/2})$$

$$\lambda(A) = F'(A) = \frac{1}{3} \frac{\sqrt{g_0}}{C_{\text{mu}}} \cdot \frac{(S_{w_0} A^{2/3} + 6 A^{1/3} / w_0)}{(w_0 + 2 A / w_0)^{5/3}}$$

$\lambda(A) > 0$ for all $A \geq 0 \Rightarrow$ every characteristic travels downstream. In case of last centred reposition and clock, left value should be used.

$$\text{Flux} : F_{k+1/2}(\bar{A}_k^+, \bar{A}_{k+1}^-) - F_{k-1/2}(\bar{A}_k^-, \bar{A}_k^+)$$

$$5. \bar{A}_k^{n+1} = \bar{A}_k^n + \frac{\Delta t}{\Delta S_k} (F_{k+1/2} - F_{k-1/2})$$

$$\text{Cell width } \Delta S_k = h_k :$$

For the numerical scheme to be stable, numerical information must not travel beyond a single cell during a time step, providing the

CFL condition :

$$\max_k \frac{|A_{k,l}| \Delta t}{h_k} \leq CFL \quad 0 < CFL < 1$$

for time step, $\Delta t \leq CFL \min_k \frac{h_k}{|A_{k,l}|}$

Linearized conservation law

$$\rightarrow \partial_t A + \lambda(A_k) \partial_x A.$$

$$\text{where } \lambda(A) = \frac{\partial F}{\partial A}$$

(consider $\lambda(A)$ to be a constant coefficient

at an interface $\Rightarrow \lambda(A_k)$. Applying

this for every cell interface allows the global condition to be enforced as

would be the case for a linear system.

$$\lambda(A, s) = \frac{1/\sqrt{F_{\text{diff}}}}{3 \text{ cm}} \cdot \frac{s w_0 A^{2/3} + 6 A^{5/3} / w_0}{(w_0 + 2h/w_0)^{5/3}}$$

Given $h = A/w_0$, this can be expressed as

$$\lambda(h, s) = \frac{1/\sqrt{F_{\text{diff}}}}{3 \text{ cm}} \cdot \frac{s w_0^{5/3} h^{2/3} + 6 h^{5/3} w_0^{2/3}}{(w_0 + 2h)^{5/3}}$$

$\Delta t \leq CFL \min_k \frac{h_k}{\lambda(h_k, s_k)}$ which can be expressed as

$$\Delta t \leq CFL \min_k \frac{1/\sqrt{F_{\text{diff}}}}{3 \text{ cm}} \cdot \frac{s w_0^{5/3} h^{2/3} + 6 h^{5/3} w_0^{2/3}}{(w_0 + 2h)^{5/3}}$$

Simplified to give

$$\Delta t \leq (FL_{\min_k} \left[3 \frac{C_m}{\sqrt{-\partial_{\delta} b(s_k)}} \cdot \frac{h_k^{1/3} (w_0(s_k) + 2h_k)^{5/3}}{5w_0(s_k)^{5/3} + 6h_k w_0(s_k)^{2/3}} \right])$$

6. Convective flux determines interface state from the incoming characteristic direction.
Since $\partial_A F(A) > 0$ at all points in the stream, all characteristics point downstream.

- Meaning at $s=0$, characteristics enter the domain, so inflow should be defined here by use of the left ghost cell \bar{A}_{-1} .
- And upstream at $s=L_c$, the solution will be determined from the interior values of the domain so no flux should be imposed.

All fine.