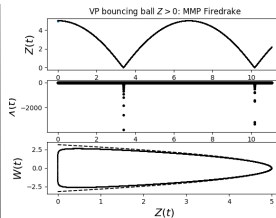
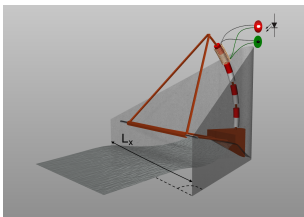


# Building a wave-to-wire finite-element wave-energy model in Firedrake

Onno Bokhove [et al.], Oxford, Firedrake 18-09-2024  
£€: EU Eagre GA859983 & CDT Fluid Dynamics

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# Outline

Ongoing build-up to complete (nonlinear) wave-to-wire FEM within Firedrake using (time-discrete) VPs with nontrivial damping of the electric circuits and energy-harvesting load:

- ▶ Grand continuum variational principle (VP) entire model plus non-conservative terms.

## Implementation hierarchy:

- ▶ time-discrete VP for (hanging and driven) nonlinear buoy-generator model
- ▶ (time-discrete VP with inequality constraint for bouncing ball under gravity with  $Z \geq 0$ )
- ▶ time-discrete VP for water and buoy at rest, in hydrostatic balance
- ▶ time-discrete VP for water waves and buoy in motion
- ▶ then **full coupled model should work** ... ?

## Why variational principles (VPs)? Advantages:

- ▶ When the (main) dynamics has a VP, multiple coupled equations are **succintly** described by one space-time VP.
- ▶ Associated with a VP are **conservation properties** of the resulting PDEs/ODEs.
- ▶ Within the (*finite-element*) *environment Firedrake*, the time-discrete VP can be implemented directly, with automated generation of (complicated 3D+1D) weak forms of the equations.
- ▶ **Advantages**: enormous reduction in development time, efficient, flexible, higher-order spectrally-accurate space discretisations plus (automatic) preservation of discrete forms of conservation properties.
- ▶ **VP for 3D+1D** nonlinear water waves as potential flow: implemented and tested (Choi et al. 2024, Lu et al. 2024).

# Grand VP of wave-to-wire model

Equations of motion follow from variational principle (**red**=waves, **blue**=buoy, **green**=EM-generator, coupling, B. et al. 2019):

$$0 = \delta \int_0^T \int_0^{L_x} \int_{R(t)}^{l_y(x)} \int_0^h -(\partial_t \phi + \frac{1}{2} |\nabla \phi|^2) dz - gh(\frac{1}{2}h - H_0) \\ - \frac{1}{2\gamma} \left( F_+ (\gamma(h - h_b) - \lambda)^2 - \lambda^2 \right) dy dx \\ \underline{MW\dot{Z} - \frac{1}{2}MW^2 - MgZ + (L_i I - \underline{K(Z)})\dot{Q} - \frac{1}{2}L_i I^2} dt \quad (1)$$

velocity  $u = \nabla \phi(x, y, z, t)$ , depth  $h(x, y, t)$ , rest depth  $H_0$ , buoy  $h_b(Z, y) = Z - K_h - \tan \theta (L_y - y)$ , piston  $R(t)$ , coupling function  $\gamma_m G(Z) = K'(Z)$ , buoy mass  $M$ , keel height  $K_h$ , buoy coordinate  $Z(t)$ , buoy velocity  $W(t) = \dot{Z}$ , charge  $Q(t)$ , current  $I(t) = \dot{Q}$ .

# Grand VP: PDEs

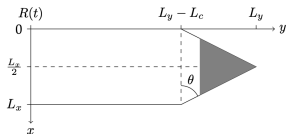
- Potential-flow water-wave dynamics (Laplace equation in interior, kinematic & Bernoulli equations at free surface):

$$\delta\phi: \quad \nabla^2\phi = 0 \quad \text{in} \quad \Omega$$

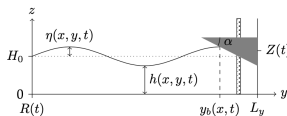
$$(\delta\phi)|_{z=h}: \quad \partial_t h + \nabla\phi \cdot \nabla h = \phi_z \quad \text{at} \quad z = h$$

$$\delta h: \quad \partial_t\phi + \frac{1}{2}|\nabla\phi|^2 + g(z - H_0) - \lambda = 0 \quad \text{at} \quad z = h.$$

- Coupled **elliptic Laplace equation** to **hyperbolic free-surface equations**, plus a (Lagrange) **multiplier**  $\lambda$ .



(b) Top view of the tank and buoy, outlining the tank's dimensions and how the buoy fits the shape of the contraction.



(c) Side view at time  $t$ , with the buoy constrained to move vertically.

# Grand VP: inequality constraint & ODEs

- **Karush-Kuhn-Tucker inequality conditions** satisfied at every space-time  $x, y, t$ -position are (Burman et al. 2023):

$$\delta\lambda : \lambda = -[\gamma(h - h_b) - \lambda]_+ = -F_+(\gamma(h - h_b) - \lambda) \\ \implies \underline{h(x, y, t) - h_b(Z, y) \leq 0, \lambda \leq 0, \lambda(h - h_b) = 0.}$$

- Add **resistance  $R_i, R_c$  & Shockley load  $V_s(|I|)$**  to submodel:

$$\delta W : \dot{Z} = W,$$

$$\delta Z : M\dot{W} = - Mg - \underline{\gamma_m G(Z)I} - \int_0^{L_x} \int_0^{l_y(x)} \lambda dy dx$$

$$\delta I : \dot{Q} = I,$$

$$\delta Q; \quad L_i \dot{I} = \underline{\gamma_m G(Z)\dot{Z}} - (R_i + R_c)I - \frac{I}{|I|} V_s(|I|).$$

## VP buoy-motor

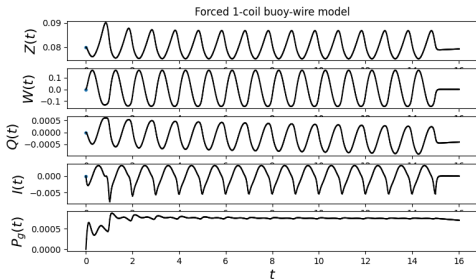
The full modified midpoint time-discrete variational principle for the single-coil model reads

$$\begin{aligned}
 0 = & \delta \left( MW^{n+1/2} \frac{(Z^{n+1} - Z^n)}{\Delta t} - MZ^{n+1/2} \frac{(W^{n+1} - W^n)}{\Delta t} \right. \\
 & - \frac{1}{2} M (W^{n+1/2})^2 - \underline{MW}^{n+1/2} \underline{\dot{f}}^{n+1/2} - \frac{1}{2} k (Z^{n+1/2} - \bar{Z} - \underline{f}^{n+1/2})^2 \\
 & + (L_i I^{n+1/2} - K(Z^{n+1/2})) \frac{(Q^{n+1} - Q^n)}{\Delta t} \\
 & \left. - Q^{n+1/2} \left( L_i \frac{(I^{n+1} - I^n)}{\Delta t} - \frac{K(Z^{n+1}) - K(Z^n)}{\Delta t} \right) - \frac{1}{2} L_i (I^{n+1/2})^2 \right)
 \end{aligned}$$

Terms stemming from  $K(Z)$  (implementation ito VP does not work in FD) implemented into two weak equations.

## VP buoy-motor

- ▶ Variations taken wrt  $\{Z^{n+1/2}, Q^{n+1/2}, W^{n+1/2}\}$ , augmented with  $z^{n+1} = Z^{n+1/2} - Z^n$ ,  $w^{n+1} = 2W^{n+1/2} - W^n$ ,  $l^{n+1} = 2I^{n+1/2} - I^n$  (“replace”) plus  $q^{n+1} = Q^n + \Delta t l^{n+1/2}$ , (Gagarina 2014, Choi et al. 2024).
- ▶ So,  $\{Z^{n+1}, W^{n+1}, I^{n+1}\}$  eliminated after variations have been taken using mid-point definitions. SE & MMP same:





## VP code buoy-motor

```

VPn1 = (1/Lx)*( Mm*W12*(Z1-Z0)/dt - Mm*Z12*(W1-W0)/dt - Mm*W12*force12dt \
        - 0.5*Mm*W12**2 - rfac*0.5*kspring*(Z12-Zbar-force12)**2 \
        + (Li*Ic12)*(Q1-Q0)/dt - Q12*Li*(I1-I0)/dt - 0.5*Li*Ic12**2 ) *fd.dx(degree=vpolyp
Z_expr = fd.derivative(VPn1, W12, du=vvmc2) # du=v_R eqn for Z1
Z_expr = fd.replace(Z_expr, {Z1: 2*Z12-Z0})
W_expr = fd.derivative(VPn1, Z12, du=vvmc0) # du=v_R eqn for W1
W_expr = W_expr + (1/Lx)*( -vvmc0*(gamma*GZZ12*Ic12 ) ) *fd.dx(degree=vpolyp) # Add buoy
W_expr = fd.replace(W_expr, {W1: 2*W12-W0}) # W1 = 2*W12-W0

I_expr = fd.derivative(VPn1, Q12, du=vvmc1) # du=v_R eqn for I1
I_expr = I_expr - (1/Lx)*( vvmc1*((Rc+Ri+lfac*Rl)*Ic12 + tfac*fd.conditional(AbsI<small
) ) *fd.dx(degree=vpolyp)
I_expr = fd.replace(I_expr, {Z1: 2*Z12-Z0})
I_expr = fd.replace(I_expr, {I1: 2*Ic12-I0})

Fexpr = Z_expr+W_expr+I_expr

solver_parameters6 = {'sns_type': 'newtonls', 'sns_atol': 1e-19, 'mat_type': 'aij'}
solve1coil_1 = fd.NonlinearVariationalSolver(fd.NonlinearVariationalProblem(Fexpr, \
        result_mixedmpc), solver_parameters=solver_parameters6)

```

# Vertically-falling ball under gravity with $Z(t) \geq 0$

Continuous in time:

- ▶ **VP of falling ball** with unit mass  $M = 1$  without constraint:

$$0 = \delta \mathcal{F} = \delta \int_0^T L(Z, W) dt \equiv \delta \int_0^T W \dot{Z} - \frac{1}{2} W^2 - Z dt,$$

$$\equiv \lim_{\epsilon \rightarrow 0} \int_0^T \frac{L(Z + \epsilon \delta Z, W + \epsilon \delta W) - L(Z, W)}{\epsilon} dt$$

time  $t$ , acceleration  $g = 1$ , kinetic & potential energy  $MgZ$ .

- ▶ **Minimisation problem** with *virtual* changes  $z_p = \delta Z$  and  $w_p = \delta W$ , i.e.  $\delta Z(0) = \delta Z(T) = 0$ .
- ▶ **Newton's equations** for position  $Z(t)$  and velocity  $W(t) \equiv \dot{Z}$ :

$$0 = \int_0^T (\dot{Z} - W) \delta W - (\dot{W} + 1) \delta Z dt : \dot{Z} = W, \quad \dot{W} = -1.$$

# Vertically-falling ball under gravity with $Z(t) \geq 0$

Continuous in time:

- **VP** of falling ball with inequality constraint:

$$\begin{aligned}
 0 &= \delta \int_0^T L(Z, W) dt \\
 &\equiv \delta \int_0^T W \dot{Z} - \frac{1}{2} W^2 - Z - \frac{1}{2\gamma} (F_+(-\gamma Z - \lambda)^2 - \lambda^2) dt,
 \end{aligned}$$

- **Resulting equations:**

$$\delta W : \quad \dot{Z} = W$$

$$\delta Z : \quad \dot{W} = -1 - \lambda$$

$$\begin{aligned}
 \delta \lambda : \quad \lambda &= -F_+(-\gamma Z - \lambda) F'_+(-\gamma Z - \lambda) \\
 &= -F_+(-\gamma Z - \lambda) \iff \underline{-Z \leq 0}, \lambda \leq 0, \lambda Z = 0.
 \end{aligned}$$

## Vertically-falling ball: smoothing

For  $b > 0$ , approximations of  $F_+$  include:

$$F_+(q) = \frac{1}{2}q + \sqrt{b^2 + \frac{1}{4}q^2} \rightarrow_{b \rightarrow 0} \max(q, 0) \quad \text{with}$$

$$F'_+(q) = \frac{1}{2} + \frac{\frac{1}{4}q}{\sqrt{b^2 + \frac{1}{4}q^2}} \rightarrow_{b \rightarrow 0} \Theta(q) \quad \text{or}$$

$$F_+(q) = \ln(1 + e^{bq})/b \rightarrow_{b \rightarrow 0} \max(q, 0). \quad (2)$$

Hence,

$$\begin{aligned} \lambda &= -F_+(-\gamma Z - \lambda) = -\left(-\frac{1}{2}(\gamma Z + \lambda) + \sqrt{b^2 + (\gamma Z + \lambda)^2/4}\right) \\ &\iff \frac{1}{2}(\lambda - \gamma Z) = -\sqrt{b^2 + (\gamma Z + \lambda)^2/4} \implies \\ &-\gamma Z \lambda = b^2 \quad \text{for } Z \geq 0 \iff \lambda = -\frac{b^2}{\gamma Z} \quad \text{for } Z \geq 0. \end{aligned}$$

## Vertically-falling ball: phase plot

Therefore, equations become as follows and can be solved

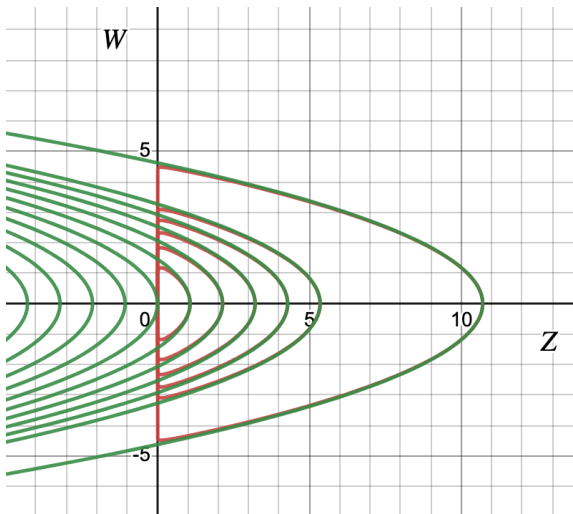
$$\dot{Z} = W, \dot{W} = -1 + \frac{b^2}{\gamma Z} \iff \ddot{Z} = -1 + \frac{b^2}{\gamma Z} \implies$$

$$\frac{d}{dt} \left( \frac{1}{2} W^2 + Z - \frac{b^2}{\gamma} \ln Z \right) = 0 \iff$$

$$\frac{1}{2} W^2 + Z - \frac{b^2}{\gamma} \ln Z = H_0$$

with integration constant/energy  $H_0 = H(t)$ . When  $W = 0$  maximum  $Z = Z_{max}$  satisfies  $Z_{max} - b^2/(\gamma Z_{max}) = H_0$  with as first approximation  $Z_{max} \approx H_0 = H_1 - b^2/(\gamma) \ln H_1$ , where  $\frac{1}{2} W^2 + Z = H_1$ . Make **phase plot** in  $(Z, W)$ -plane:

# Vertically-falling ball: phase plot



# Vertically-falling ball under gravity with $Z(t) \geq 0$

Time discrete VP:

- **2<sup>nd</sup>-order modified mid-point VP** of falling ball with constraint:

$$0 = \delta \left( W^{n+1/2} \frac{Z^{n+1} - Z^n}{\Delta t} - Z^{n+1/2} \frac{W^{n+1} - W^n}{\Delta t} - \frac{1}{2} (W^{n+1/2})^2 - Z^{n+1/2} - \frac{1}{2\gamma} \left( F_+ (-\gamma Z^{n+1/2} - \lambda)^2 - \lambda^2 \right) \right)$$

with additional relations

$$Z^{n+1} = 2Z^{n+1/2} - Z^n \text{ and } W^{n+1} = 2W^{n+1/2} - W^n.$$

# Vertically-falling ball under gravity with $Z(t) \geq 0$

- Resulting **time-discrete equations** (variations wrt  $Z^{n+1/2}, W^{n+1/2}$ ):

$$\delta W^{n+1/2} : Z^{n+1} = Z^n + \Delta t W^{n+1/2} \implies$$

$$Z^{n+1/2} = Z^n + \frac{1}{2} \Delta t W^{n+1/2}$$

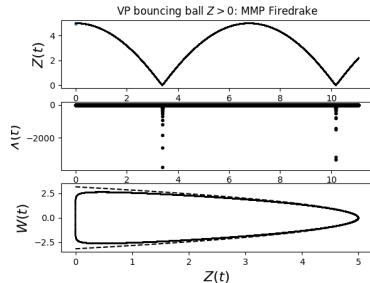
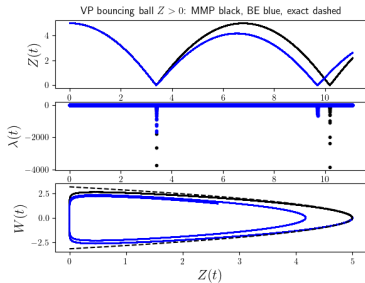
$$\delta Z^{n+1/2} : W^{n+1} = W^n - \Delta t(1 + \lambda)$$

$$\implies \frac{4(Z^{n+1/2} - Z^n)}{\Delta t} = 2W^n - \Delta t(1 + \lambda)$$

$$\delta \lambda : \lambda = -F_+(-\gamma Z^{n+1/2} - \lambda) F'_+(-\gamma Z^{n+1/2} - \lambda).$$



# Vertically-falling ball under gravity with $Z(t) \geq 0$



# VP buoy and water at rest

Strategy on rest-flow buoy-water surface coupling:

- **Goal** is to solve Bernoulli & KKT inequality equations:

$$\delta h : g(z - H_0) - \lambda = 0 \quad \text{at} \quad z = h.$$

$$\delta Z : \int_0^{L_x} \int_0^{l_y(x)} \lambda dy dx + Mg = 0$$

$$\delta \lambda : \lambda = -[\gamma(h - h_b(Z, y)) - \lambda]_+ = -F_+(\gamma(h - h_b(Z, y)) - \lambda)$$

$$\implies \underline{h(y, t) - h_b(Z, y) \leq 0}, \lambda \leq 0, \lambda(h - h_b(Z, y)) = 0.$$

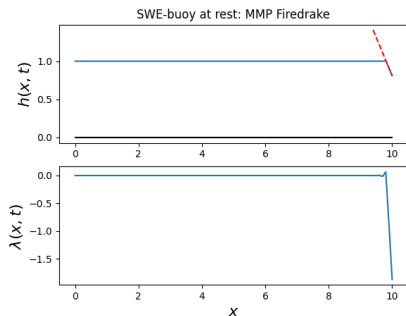
with  $h_b(Z, y) = Z - K_h - \tan \theta (L_y - y)$ .

# VP buoy and water at rest

- **Solve** VP for  $h(x, y)$ ,  $Z$  and  $\lambda$ -equation with  $F_+(q) = \ln(1 + e^{aq})/b$  (buoy of finite extent  $L_w$ ):

$$0 = \delta \left( \int_0^{L_x} \int_0^{l_y(x)} gh \left( \frac{1}{2} h - H_0 \right) + \lambda (h_b(Z, y) - h) dy dx + MgZ \right)$$

$$\delta \lambda : 0 = \int_0^{L_x} \int_0^{l_y(x)} \left( \lambda + \begin{cases} F_+(\gamma(h - h_b) - \lambda) & L_y - L_w < y < L_y \\ 0 & y \leq L_y - L_w \end{cases} \right) \delta \lambda dy dx$$



# VP dynamic buoy and water motion (BLE for dispersion)

Strategy on buoy-water surface coupling (work in progress):

- **Goal** is to solve Bernoulli & KKT inequality equations:

$$\delta h: \quad \partial_t \phi + \dots + \frac{1}{2} |\nabla \phi|^2 + g(z - H_0) - \lambda = 0 \quad \text{at} \quad z = h.$$

$$\delta \phi: \quad \partial_t h + \dots + \nabla \cdot (h \nabla \phi) = 0, \dots$$

$$\delta Z: \quad M \dot{W} + \int_0^{L_x} \int_0^{l_y(x)} \lambda dy dx + Mg = 0$$

$$\delta \lambda: \quad \lambda = -[\gamma(h - h_b(Z, y)) - \lambda]_+ = -F_+(\gamma(h - h_b(Z, y)) - \lambda) \\ \implies \underline{h(x, y, t) - h_b(Z, y) \leq 0}, \lambda \leq 0, \lambda(h - h_b(Z, y)) = 0.$$

$$\text{with } h_b(Z, y) = Z - K_h - \tan \theta (L_y - y).$$

# VP dynamic buoy and water motion (BLE for dispersion)

Strategy on buoy-water surface coupling (work in progress):

- **Solve** VP for  $h(x, y)$ ,  $Z$  and imposed, solved, separated  $\lambda$ -solution (buoy has been given finite extent  $L_w$ ;  $R(t) = 0$ ):

$$\begin{aligned}
 0 = & \delta \left( \int_0^{L_x} \int_0^{l_y(x)} \int_0^{h^{n+1/2}} -\frac{1}{2} |\nabla \phi^{n+1/2}|^2 dz + \phi_s^{n+1/2} \frac{(h^{n+1} - h^n)}{\Delta t} - h^{n+1/2} \frac{(\phi_s^{n+1} - \phi_s^n)}{\Delta t} + \dots \right. \\
 & - gh^{n+1/2} \left( \frac{1}{2} h^{n+1/2} - H_0 \right) - \lambda (h_b(Z^{n+1/2}, y) - h^{n+1/2}) dy dx \\
 & \left. + MW^{n+1/2} \frac{(Z^{n+1} - Z^n)}{\Delta t} - MZ^{n+1/2} \frac{(W^{n+1} - W^n)}{\Delta t} - \frac{1}{2} M(W^{n+1/2})^2 - MgZ^{n+1/2} \right) \\
 \delta \lambda : 0 = & \int_0^{L_x} \int_0^{l_y(x)} \left( \lambda + \left\{ \begin{array}{ll} F_+(\gamma(h^{n+1/2} - h_b(y, Z^{n+1/2})) - \lambda) & L_y - L_w < y < L_y \\ 0 & y \leq L_y - L_w \end{array} \right. \right) \delta \lambda dy dx
 \end{aligned}$$

with  $F_+(q) = \ln(1 + e^{aq})/b$ . Rest flow in dynamic case stays rest flow!

## VP code buoy-waves

```

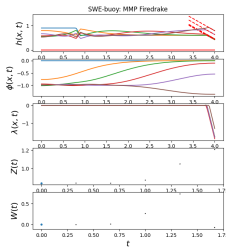
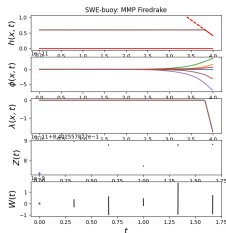
VPn1 = ( facs*phi12*(h1-h0)/dt-facs*h12*(phi1-phi0)/dt -0.5*h12*(phi12.dx(0))**2 \
- gg*h12*(0.5*h12-H0) + 0.5*gg*H0**2 -(0.5/gamm)*(Fplus**2-lamb12**2) ) \
*fd.dx(degree=vpolyp)
VPn1 = VPn1 - facs*( 0.5*muu*h12.dx(0)*(phi1.dx(0)-phi0.dx(0))/dt \
-0.5*muu*phi12.dx(0)*(h1.dx(0)-h0.dx(0))/dt )*fd.dx(degree=vpolyp)
VPn1 = VPn1 - ( muu*(q12.dx(0)*phi12.dx(0)-0.75*q12**2) )*fd.dx(degree=vpolyp)
VPn1 = VPn1 + (1/Lx)*( facs2*mm*W12*(Z1-Z0)/dt-facs2*mm*Zh12*(W1-W0)/dt \
-0.5*mm*W12**2-mm*gg*Zh12)*fd.dx(degree=vpolyp)
phi_expr = fd.derivative(VPn1, h12, du=vvmpec0) #
phi_expr = fd.replace(phi_expr, {phi1: 2*phi12-phi0})
h_expr = fd.derivative(VPn1, phi12, du=vvmpec1) #
h_expr = fd.replace(h_expr, {h1: 2*h12-h0})
W_expr = fd.derivative(VPn1, Zh12, du=vvmpec3) #
W_expr = fd.replace(W_expr, {W1: 2*W12-W0}) #
Z_expr = fd.derivative(VPn1, W12, du=vvmpec4) #
Z_expr = fd.replace(Z_expr, {Z1: 2*Zh12-Z0}) #
Fexpr = h_expr+phi_expr+lamb_expr+Z_expr+W_expr

solvelamb_n10 = fd.NonlinearVariationalSolver(fd.NonlinearVariationalProblem(Fexpr0, res
solver_parameters=solver_parameters1s)
solvelamb_n1 = fd.NonlinearVariationalSolver(fd.NonlinearVariationalProblem(Fexpr, resul

```

# To do/Firedrake Questions

- ▶ time-discrete VP for water waves and buoy in motion
- ▶ then **then full coupled model should work ...?**
- ▶ ■■■: Use the in-build Firedrake inequality solvers? Not geometric in time. Other (non-■■■) time integrators?
- ▶ How should one manage and deal with these solver-parameter settings?



# Thank you very much for your attention ...

- ▶ B., Zweers 2013: Proof of principle 2013 [https://www.youtube.com/watch?v=SZhe\\_S0xBWo&t=254s](https://www.youtube.com/watch?v=SZhe_S0xBWo&t=254s)
- ▶ B., Kalogirou, Zweers 2019: From bore-soliton-splash to a new wave-to-wire wave-energy model. *Water Waves* 1 10.1007/s42286-019-00022-9 Bore-soliton-splash: <https://www.youtube.com/watch?v=YSXsXNX4zW0&list=FL6mc7mUa6M4Bo2VkD970urw>
- ▶ Choi, Kalogirou, Lu, B., Kelmanson 2024: A study of extreme water waves using a hierarchy of models based on potential-flow theory. *Water Waves* <https://doi.org/10.1007/s42286-024-00084-4>
- ▶ B., Bolton, Thompson, Geometric power optimisation of a rogue-wave energy device in a (breakwater) contraction. 8<sup>th</sup> IEEE Conference on Control Technology & Applications (CCTA) (2024) 6 pp. Preprint <https://eartharxiv.org/repository/view/7260/>
- ▶ Lu, Gidel, Choi, B., Kelmanson 2024: Submitted. *J. Comp. Phys.*.