Robot Control Equations

Table 1: MuJoCo Controller Key Bindings

Category	Key Binding and Description
General	
ESC	Exit simulation
ENTER	Reset simulation
Gripper Control	
Z	Close gripper (jaw)
X	Open gripper (jaw)
С	Side gripper outward
V	Side gripper inward
В	Tip gripper open
N	Tip gripper close
Arm Movement	
W / S	Forward / Backward
A / D	Left / Right
Q / E	Up / Down
Base Movement (relative to orientation)	
\uparrow/\downarrow	Forward / Backward
\rightarrow / \leftarrow	Right / Left
T / R	Rotate Counterclockwise / Clockwise
Camera Control (Free Mode)	
Mouse Left Drag	Rotate camera
Mouse Right Drag	Pan camera
Mouse Middle Drag	Zoom
Mouse Scroll	Zoom

1 Control for Mobile Base (control_base)

This method drives a mobile robot base to a target position $(x_{\rm target}, y_{\rm target})$ and orientation $\theta_{\rm target}$ using PID control. Errors are transformed into the robot's local frame, and PID gains compute linear $(v_{x_{\rm local}}, v_{y_{\rm local}})$ and angular (ω) velocities.

These are mapped to wheel velocities for a four-wheeled differential drive, with small commands clipped to zero to avoid unnecessary actuation. The key bindings (e.g., †/\pu for forward/backward, T/R for rotation) allow manual control of the base movement, complementing the automated PID control.

Position and Orientation Errors 1.1

The errors in position and yaw angle are calculated as:

$$\Delta x = x_{\text{target}} - x_{\text{current}} \tag{1}$$

$$\Delta y = y_{\text{target}} - y_{\text{current}} \tag{2}$$

$$\Delta \theta = \arctan 2 \left(\sin(\theta_{\text{target}} - \theta_{\text{current}}), \cos(\theta_{\text{target}} - \theta_{\text{current}}) \right)$$
 (3)

where θ_{target} and θ_{current} are derived from quaternions using:

$$\theta = \arctan 2 \left(2(wz + xy), 1 - 2(y^2 + z^2) \right) \tag{4}$$

for quaternion [w, x, y, z].

Local Frame Transformation 1.2

Errors are transformed into the robot's local frame:

$$\Delta x_{\text{local}} = \cos(\theta_{\text{current}}) \Delta x + \sin(\theta_{\text{current}}) \Delta y$$
 (5)

$$\Delta y_{\text{local}} = -\sin(\theta_{\text{current}})\Delta x + \cos(\theta_{\text{current}})\Delta y$$
 (6)

Integral Terms 1.3

The integral terms accumulate errors over time:

$$I_x = I_x + \Delta x_{\text{local}} \cdot \Delta t \tag{7}$$

$$I_y = I_y + \Delta y_{\text{local}} \cdot \Delta t \tag{8}$$

$$I_{\theta} = I_{\theta} + \Delta\theta \cdot \Delta t \tag{9}$$

where Δt is the simulation timestep.

Derivative Terms with Smoothing

Derivative terms are computed and smoothed with a low-pass filter ($\alpha = 0.7$):

$$D_{x_{\text{local}}} = \frac{\Delta x_{\text{local}} - \Delta x_{\text{prev}}}{\Delta t}$$

$$D_{y_{\text{local}}} = \frac{\Delta y_{\text{local}} - \Delta y_{\text{prev}}}{\Delta t}$$
(10)

$$D_{y_{\text{local}}} = \frac{\Delta y_{\text{local}} - \Delta y_{\text{prev}}}{\Delta t} \tag{11}$$

$$D_{\theta} = \frac{\Delta \theta - \Delta \theta_{\text{prev}}}{\Delta t} \tag{12}$$

$$D_x = \alpha D_x + (1 - \alpha) D_{x_{\text{local}}}$$
(13)

$$D_y = \alpha D_y + (1 - \alpha) D_{y_{\text{local}}}$$
(14)

$$D_{\theta} = \alpha D_{\theta} + (1 - \alpha)D_{\theta} \tag{15}$$

1.5 Control Velocities

The control velocities are computed using PID gains ($k_p = 3.0$, $k_i = 0.02$, $k_d = 0.3$ for position; $k_{p_{\theta}} = 3.0$, $k_{i_{\theta}} = 0.03$, $k_{d_{\theta}} = 0.3$ for orientation):

$$v_{x_{\text{local}}} = k_p \Delta x_{\text{local}} + k_i I_x + k_d D_x \tag{16}$$

$$v_{y_{\text{local}}} = k_p \Delta y_{\text{local}} + k_i I_y + k_d D_y \tag{17}$$

$$\omega = k_{p_{\theta}} \Delta \theta + k_{i_{\theta}} I_{\theta} + k_{d_{\theta}} D_{\theta}$$
(18)

1.6 Wheel Velocities

The velocities are mapped to four wheels of a differential drive robot, where D is the distance from the robot's center to the wheels and r is the wheel radius:

$$v_{\text{target}}[0] = \frac{v_{x_{\text{local}}} - v_{y_{\text{local}}} - \omega D}{r}$$
(19)

$$v_{\text{target}}[1] = \frac{v_{x_{\text{local}}} + v_{y_{\text{local}}} + \omega D}{r}$$
 (20)

$$v_{\text{target}}[2] = \frac{v_{x_{\text{local}}} + v_{y_{\text{local}}} - \omega D}{r}$$
 (21)

$$v_{\text{target}}[3] = \frac{v_{x_{\text{local}}} - v_{y_{\text{local}}} + \omega D}{r}$$
 (22)

2 Inverse Kinematics Solver (ik_solution)

The ik_solution method solves an inverse kinematics problem to position a robotic arm's end-effector by optimizing joint parameters h_1 , h_2 , and θ .

It optimizes joint parameters h_1 , h_2 , and θ to minimize the angle between vectors from two vertical links points to the target, subject to length, angle, and z-height constraints. The solution ensures the arm's configuration is feasible and avoids singularities or ground penetration.

2.1 Base to End-Effector Transformation

The end-effector's position is transformed into the base frame:

$$\mathbf{R}_{base} = quaternion_to_matrix(\mathbf{q}_{base}) \tag{23}$$

$$ee_{base} = R_{base}^{T}(ee_{world} - p_{arm_base})$$
 (24)

$$target = ee_{base} + err_{base}$$
 (25)

2.2 Base Points Calculation

Two base points are defined for the arm segments:

$$\mathbf{b}_{1} = \begin{bmatrix} -\frac{D_{2}}{2}\cos(\theta) \\ -\frac{D_{2}}{2}\sin(\theta) \\ h_{1} \end{bmatrix}, \quad \mathbf{b}_{2} = \begin{bmatrix} \frac{D_{2}}{2}\cos(\theta) \\ \frac{D_{2}}{2}\sin(\theta) \\ h_{2} \end{bmatrix}$$
(26)

where $D_2 = 0.2$.

Objective Function 2.3

The objective is to minimize the negative angle between vectors $\mathbf{v}_1 = \mathbf{target} - \mathbf{b}_1$ and $v_2 = target - b_2$:

$$l_1 = \|\mathbf{v}_1\|, \quad l_2 = \|\mathbf{v}_2\|$$
 (27)

$$\cos(\theta_{\text{angle}}) = \frac{\mathbf{v}_1 \cdot \mathbf{v}_2}{\max(l_1 l_2, 10^{-12})}$$
(28)

$$obj(\mathbf{x}) = -\arccos(\cos(\theta_{angle})) \tag{29}$$

2.4 **Constraints**

The optimization is subject to the following constraints:

• Length constraints:

$$l_{1,\min}^2 \le \|\mathbf{target} - \mathbf{b}_1\|^2 \le l_{1,\max}^2$$
 (30)
 $l_{2,\min}^2 \le \|\mathbf{target} - \mathbf{b}_2\|^2 \le l_{2,\max}^2$ (31)

$$l_{2,\min}^2 \le \|\mathbf{target} - \mathbf{b}_2\|^2 \le l_{2,\max}^2$$
 (31)

where $l_{1,min} = 0.4$, $l_{1,max} = 1.0$, $l_{2,min} = 0$, $l_{2,max} = 0.6$.

• Angle constraint:

$$\theta_{\rm angle} \ge 20^{\circ}$$
 (32)

• Projection constraints:

$$tol \ge target[0](-\sin(\theta)) + target[1]\cos(\theta)$$
 (33)

$$tol < target[0](-\sin(\theta)) + target[1]\cos(\theta)$$
 (34)

where tol = 10^{-3} .

Z-height constraints:

$$l_{1end}[2] \ge -z_{threshold} \tag{35}$$

$$l_{2\text{end}}[2] \ge -z_{\text{threshold}}$$
 (36)

where:

$$\mathbf{l}_{1\text{end}} = \mathbf{b}_1 - \frac{\mathbf{v}_1}{\|\mathbf{v}_1\|} (\text{arm_length} - l_1) \tag{37}$$

$$\mathbf{l}_{2\text{end}} = \mathbf{b}_2 - \frac{\mathbf{v}_2}{\|\mathbf{v}_2\|} (\text{arm_length} - l_2)$$
 (38)

with arm_length = 1.15, $z_{\text{threshold}} = 0.05$.

Optimization 2.5

The optimization problem is:

$$\min_{\mathbf{x}} \mathbf{obj}(\mathbf{x}), \quad \mathbf{x} = [h_1, h_2, \theta]$$
(39)

subject to the constraints, with bounds:

$$0.0 \le h_1 \le 1.0 \tag{40}$$

$$0.0 \le h_2 \le 1.0 \tag{41}$$

$$-3.14 \le \theta \le 3.14 \tag{42}$$

The SLSQP algorithm is used with a tolerance of 10^{-5} and a maximum of 15 iterations.