

Theory of Polymer Dynamics

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Chapter 1

1.1 Introduction

This document summarizes information related to the construction of theoretical models representing polymers. It is mainly drawn from the books by Doi [4][3], and Bird [2].

1.2 The elastic dumbbell model

Taken from [2] chapter 13 The dumbbell model is an idealized toy model composed of two beads of mass m connected by a Hookian spring. The position of the beads in space will be labeled r_1 and r_2 . The connector vector $Q = r_1 - r_2$ describes the orientation and configuration of the dumbbell.

The define the configuration-space distribution function $\Psi(r_1, r_2, t)$ as

$$F(r_1, r_2, \dot{r}_1, \dot{r}_2, t) = \Psi(r_1, r_2, t) \Xi(\dot{r}_1, \dot{r}_2, r_2, r_2, t)$$

with Ξ the velocity-space distribution function, which satisfies $\int \int \Xi d\dot{r}_1 d\dot{r}_2 = 1$. We further assume that the configuration-space distribution can be factored, to be independent of the position, as $\Psi(r_1, r_2, t) = n\psi(Q, t)$. The distribution function $\psi(Q, t)$ satisfies $\int \psi dQ = 1$.

The Brownian force $F_v^{(b)}$ and the elastic force $F_v^{(\phi)}$, acting upon each bead will be defined as

$$\begin{aligned} F_v^{(b)} &= -KT(\partial \ln \Psi / \partial r_v) \quad v = 1, 2 \\ F_v^{(\phi)} &= -\frac{\partial}{\partial r_v} \phi \end{aligned}$$

The **equation of continuity** for the dumbbell is given by

$$\frac{\partial \psi}{\partial t} = -\left(\frac{\partial}{\partial Q} [\dot{Q}] \psi \right)$$

The **configuration distribution** is given by

$$\Psi(Q, t) = \frac{(H/2\pi KT)^{3/2}}{\sqrt{\det \alpha}} \exp(-H/2KT \alpha^{-1} : QQ)$$

1.3 The freely jointed chain

From [4]. We start with a simple model: a chain consisting of N links, each of length b_0 and able to point in any direction independently of each other. The conformation of the model is represented by $(N + 1)$ position vectors $\{R_n\} = \{R_0, R_1, \dots, R_N\}$, or by the set of bond vectors $\{r_n\} = (r_1, r_2, \dots, r_N)$, where $r_n = R_n - R_{n-1}$.

Since the bonds are independent, the configuration distribution is defined as

$$\Psi(\{\vec{r}_n\}) = \prod_{n=1}^N \psi(\vec{r}_n)$$

for vector of constant length b_0

$$\psi(\vec{r}) = \frac{1}{4\pi b_0^2} \delta(|\vec{r}| - b_0)$$

we then normalize such that

$$\int \psi(\vec{r}) d\vec{r} = 1$$

If the bond vectors are presented using spherical coordinates with angles θ and ϕ , then the configuration distribution of the chain is given by

$$\psi(\theta^N, \phi^N) = \left(\frac{1}{4\pi}\right)^N \prod_{i=1}^N \sin(\theta_i)$$

This is due to the fact that the surface element of the sphere is given by the determinant of the Jacobi matrix, J , of spherical transformation for each $R_i = (x, y, z)$, namely

$$\begin{aligned} x &= b_0 \sin(\theta) \cos(\phi) \\ y &= b_0 \sin(\theta) \sin(\phi) \\ z &= b_0 \cos(\theta) \end{aligned}$$

which is $|J| = b_0^2 \sin(\theta)$, to get the probability that a bond vector is in the range $d\theta d\phi$, we divide $|J|$ by the surface area of the sphere which is $4\pi b_0^2$ to get $\sin(\theta)/4\pi$ for each bond vector. Since the bond vectors are independent, we get the multiplicative expression for ψ .

Any average quantity $B(\theta, \phi)$ that depends on the configuration of the chain in equilibrium will be written as

$$\langle B \rangle = \int \int B \psi d\theta^N d\phi^N$$

The above property of expected value of a quantity $g(x)$ given that we know only the distribution function $f(x)$ is the called the **Law of the unconscious statistician**.

$$E[g(x)] = \int_{-\infty}^{\infty} g(x) f(x) dx = \int_{-\infty}^{\infty} g(x) dF(x) dx$$

were $F(x)$ is the cdf (if known).

1.3.1 The end-to-end vector

We define the end-to-end vector as $\vec{R} = \vec{R}_N - \vec{R}_0 = \sum_{n=1}^N \vec{r}_n$. The quantity $\langle R^2 \rangle$ characterizes the length of the chain. The standard deviation of the end-to-end vector

$$\bar{R} = \langle R^2 \rangle^{0.5} = \langle (R_N - R_0)^2 \rangle^{0.5} = \sqrt{N}b_0$$

since

$$\langle R^2 \rangle = \left\langle \left(\sum_{n=1}^N r_n \right)^2 \right\rangle = \sum_{n=1}^N \sum_{m=1}^N \langle r_n r_m \rangle + \sum_{n=1}^N \langle r_n^2 \rangle + 2 \sum_{m>n}^N \langle r_n r_m \rangle = \sum_{n=1}^N \langle r_n^2 \rangle = Nb_0^2$$

therefore, $\langle R^2 \rangle^{0.5} = \sqrt{N}b_0$. Here we used $\langle r_n r_m \rangle = \langle r_n \rangle \langle r_m \rangle = 0$. Note that this is just the sum of variances of the bond vectors (each of which has variance of b_0^2).

1.3.2 Distribution of the end-to-end vector

We denote $\Phi(R, N)$ as the probability distribution function that the end-to-end vector of a chain of N beads is R .

$$\Phi(R, N) = \int \int \int \dots \int \delta(R - \sum_{n=1}^N r_n) \Psi(\{r_n\}) dr_1 dr_2 \dots dr_N$$

in short, we take all chain configurations for which the end-to-end vector is exactly R . Using the Fourier transform identity for the delta function

$$\delta(r) = \frac{1}{(2\pi)^3} \int e^{ikr} dk$$

see wikipedia. where, after some manipulation and using polar coordinates for solving the integral, we get

$$\Phi(R, N) = \frac{1}{(2\pi)^3} \int e^{ikR} \left(\frac{\sin(kb)}{kb} \right)^N dk$$

Continuing with a series of approximations to the integral above, we get

$$\Phi(R, N) = (3/2\pi Nb^2)^{1.5} \exp\left(-\frac{3R^2}{2Nb^2}\right)$$

1.4 The freely rotating chain

In this model the n -th bond is connected to the $(n-1)$ -th bond with a fixed angle θ_0 and can rotate freely around the $(n-1)$ -th bond. We calculate $\langle r_m \cdot r_n \rangle$.

If the average of r_n is taken with the rest of the chain $r_m, r_{m+1}, r_{m+2}, \dots, r_{n-1}$ with $n > m$, we get

$$\langle r_n \rangle_{r_m, r_{m+1}, r_{m+2}, \dots, r_{n-1}} = \cos(\theta_0) r_{n-1}$$

We multiply both sides by r_m and take the average over $r_m, r_{m+1}, r_{m+2}, \dots, r_{n-1}$ we get

$$\langle r_n \cdot r_m \rangle = \cos(\theta_0) \langle r_{n-1} \cdot r_m \rangle$$

We get a recursion relation with the initial condition $\langle r_m^2 \rangle = b^2$, which can be solved by $\langle r_n, r_m \rangle = b^2 \cos(\theta_0)^{n-m}$

1.5 The Gaussian Chain

From [4]. We consider a chain whose bond length has a Gaussian distribution

$$\psi(r) = \left[\frac{3}{2\pi b^2} \right]^{3/2} \exp \left(-\frac{3r^2}{2b^2} \right)$$

in 3D, with bond-length variance $\langle r^2 \rangle = b^2$. The Gaussian chain represent the model of beads on a strings, with the harmonic potential energy

$$U_0(\{R_n\}) = \frac{3k_B T}{2b^2} \sum_{n=1}^N (R_n - R_{n-1})^2$$

Since the sum of two Gaussian random variables is again a random variable, it turns out that the distribution of the bond between any two beads m and n is Gaussian with

$$\Phi(R_n - R_m, n - m) = \left[\frac{3}{2\pi b^2 |n - m|} \right]^{3/2} \exp \left[-\frac{3(R_n - R_m)^2}{2|n - m|b^2} \right]$$

and for any m and n

$$\langle (R_n - R_m)^2 \rangle = |n - m|b^2$$

From the formula of the distribution, we can immediately see that setting $R_N = R_m$, meaning placing two beads at the same position, gives us the encounter probability at steady state, namely $A|n-m|^{(3/2)}$, with A some constant of normalization.

We can thus immediately see that when setting $R_n = R_m$ we get

$$\Phi(0, |n - m|) = (3/2\pi b^2 |n - m|)^{1.5}$$

which is the steady state probability of encounter, which drops with the distance

1.5.1 Extensibility of the chain

A Gaussian chain can be extended to any length provided that enough force was invested. In reality, the chain must oppose the stretching force. To take this into account modified force laws have been proposed. One useful law is the Warner law

$$F(r_i - r_j) = \frac{3KT(r_i - r_j)/((N-1)b_0^2)}{(1 - ((r_i - r_j)/((N-1)b_0^2))^2)}$$

Chains obeying a stretching law as shown above are called FENE chains (Finite extensible nonlinear elastic)

1.6 The Rouse Chain

From [4] Chap. 4. The Rouse model was suggested as the basis for polymer dynamics in dilute solution. Let $\{R\} = \{R_1, R_2, \dots, R_N\}$ be the coordinates of the beads of the chain. The motion of the beads is described using the Smoluchowski equation

$$\frac{\partial \Psi}{\partial t} = \sum_n \frac{\partial}{\partial R_n} H_{nm} \left[k_B T \frac{\partial \Psi}{\partial R_m} + \frac{\partial U}{\partial R_m} \Psi \right]$$

1.6.1 The source of the Hookian behavior

From [2]. Let us look at the probability density function of the end-to-end vector being length r at equilibrium

$$P_{eq}(r) = \left(\frac{3}{2\pi(N-1)b^2} \right) \exp(-3r^2/2(N-1)b^2)$$

The Helmholtz free energy $A = U - TS$, with U the internal energy and S the entropy, of the system in equilibrium at temperature T is given by

$$A = -KT \ln(Z)$$

with Z the partition function, which is defined as

$$Z = c \int e^{(\mathbb{K} + \phi)/(KT)}$$

with c some constant, \mathbb{K} is the kinetic energy of the system, ϕ is the potential energy, over the phase space of the system.

When the length of the chain is changed by a small amount, the change in the Helmholtz free energy is

$$dA = -KT d \ln P_{eq} = \frac{3KT}{(N-1)b^2} (r \cdot dr)$$

We also know that the change in the Helmholtz free energy is related to the tension F^c of the chain by

$$dA = (F^c \cdot dr)$$

equating these two quantities we get

$$F^c(r) = -\frac{3KT}{(N-1)b^2}r \quad N - large$$

therefore, we see that the tension behaves as a Hookian spring. If we set $N = 2$ we get the spring constant between any two beads.

We can therefore write the probability density function for the end to end vector using the Hookian spring constant

$$P(r) = \left(\frac{k}{2\pi KT}\right)^{1.5} \exp\left(-\frac{kr^2}{2KT}\right)$$

1.6.2 The center of mass

The center of mass is defined as the mean bead position over time

$$cm(t) = \frac{1}{N+1} \sum_{i=0}^N R_n(t)$$

therefore, the differential equation for the center of mass is

$$\frac{dcm}{dt} = \frac{1}{N+1} \sum_{i=0}^N \frac{dR_i}{dt} = \frac{1}{N+1} \sum_{i=0}^N f_n(t)$$

1.6.3 Central bead is closest to the center-of-mass

In this subsection we show that on average the central beads of the chain are closest to the center of mass of the chain. This result will be useful in future sections when we calculate the encounter probability between beads in the chain with beads outside of it, to be the multiplication of the probability of an encounter between a bead outside the loop with a phantom bead in the center of mass of the loop and the encounter between beads in the loop and its center of mass.

Let our chain be defined as a sequence of N uncorrelated and independent random variables in the following way

$$p_1 = n_1$$

$$p_2 = p_1 + n_2 = n_1 + n_2$$

$$p_3 = p_2 + n_3 = n_1 + n_2 + n_3$$

.

.

$$p_N = \sum_{i=1}^{i=N} n_i$$

where $n_i \sim N(0,1) \forall i = 1..N$ and N is an odd integer.

We define the chain center of mass as:

$$p_{cm} = \frac{1}{N} \sum_{i=1}^{i=N} p_i = \frac{1}{N} (Nn_1 + (N-1)n_2 + (N-3)n_3 + \dots n_N) = \sum_{i=1}^N \left(\frac{N-i+1}{N} \right) n_i$$

The question we address here is for which index $k \in [1..N]$ does the point p_k is closest to p_{cm} ?

Each p_i is distributed normally with mean $\mu_i = 0$ (since the sum of means of the preceding points is zero) and $\sigma_i = \sqrt{\sigma_{i-1}^2 + 1 + 2\rho\sigma_{i-1}}$, where ρ is the correlation coefficient. Since each two subsequent points are uncorrelated, by definition $\rho = 0$. More specifically, the ρ in the expression for the standard deviation of point i is given by $E[(n_i - \mu_i)(p_{i-1} - \mu_{i-1})] / \sigma_{n_i} \sigma_{i-1} = E[n_i p_{i-1}] / \sigma_j$, where E is the expectation. Since n_i is independent of p_{i-1} , we get

$$E[n_i p_{i-1}] = E[n_i] E[p_{i-1}] = 0$$

Therefore we get

$$\sigma_i = \sqrt{i}$$

The center of mass p_{cm} has mean $\mu_{cm} = 0$ and standard deviation that can be written as

$$\sigma_{cm} = \sum_{i=1}^{i=N} \left(\frac{N-i+1}{N} \right)^2 = \frac{N(N+1)(2N+1)}{6N^2}$$

We now look for the point p_j for which the distribution of the random variable

$$Y(j) = p_{cm} - p_j$$

is the most 'concentrated' around zero. In this sense, the standard deviation of $Y(j)$ should be the smallest among all $i = 1..N$.

the random variable $Y(j)$ can be written as

$$Y(j) = \sum_{k=1}^N \left(1 + \frac{1-k}{N} \right) n_k - \sum_{k=1}^j n_k = \sum_{k=1}^j \frac{1-k}{N} n_k + \sum_{k=j+1}^N \left(1 + \frac{1-k}{N} \right) n_k$$

The standard deviation of Y_j is

$$\sigma_{Y(j)} = \sqrt{\sum_{k=1}^j \left(\frac{1-k}{N} \right)^2 + \sum_{k=j+1}^N \left(\frac{N+1-k}{N} \right)^2} = \frac{1}{N} \sqrt{\sum_{k=1}^{j-1} k^2 + \sum_{k=1}^{N-j} k^2}$$

To find the j that minimizes this expression, we can disregard the square root, and denote $Q(j) = \sum_{k=1}^{j-1} k^2$, so $Q(N-j+1) = \sum_{k=1}^{N-j} k^2$. Differentiate to find $Q'(j) - Q'(N-j+1) = 0$ we see that when $j = \frac{N+1}{2}$

$$Q'\left(\frac{N+1}{2}\right) - Q'\left(N - \frac{N+1}{2} + 1\right) = Q'\left(\frac{N+1}{2}\right)$$

1.6.4 The distribution of the bond lengths

[UNFINISHED]

The bond length behaves like the central χ^2 with d degrees of freedom, where d is the dimension of the problem. In $3D$, since each $\vec{r}_i = [x_i, y_i, z_i]$ has 3 coordinates, each i.i.d normally distributed with $\langle x_i^2 \rangle = \langle y_i^2 \rangle = \langle z_i^2 \rangle = \frac{b^2}{3}$, the length squared $\|\vec{r}_i\|^2 = x_i^2 + y_i^2 + z_i^2 \sim \chi^2(3)$ with variance $\mu = b^2/3 + b^2/3 + b^2/3 = b^2$ which is the sum of variances.

To calculate the cumulative distribution function (CDF) of the bond length, we use result from the analysis of quadratic forms [6] (chapter 3). From the CDF we will obtain the *survival probability*, which its first moment is the *mean first passage time* for the two ends of the polymer.

For the polymer chain, the bond length is a random variable, $b \sim \mathcal{N}(0, \sigma_b)$

1.6.5 Eigenvalues of the Rouse Matrix

In this subsection we derive the eigenvalues of the Rouse matrix. The Rouse matrix defines the connection between beads as a harmonic potential. The system of differential equation governing the dynamics of the chain comprised of N beads is

$$\frac{d[X(t)]}{dt} = -k[R][X(t)] + [g(t)] \quad (1.1)$$

where the $[.]$ notation represents a matrix (vector), $[g(t)]$ is an N by 1 vector of normally distributed numbers with mean 0 and STD =1, k is a constant and the matrix $[R]$ is defined as:

$$R = \begin{bmatrix} 1 & -1 & 0 & 0 & \dots & 0 \\ -1 & 2 & -1 & 0 & \dots & 0 \\ 0 & -1 & 2 & -1 & \dots & 0 \\ . & & & . & & . \\ . & & & . & & . \\ 0 & & & & -1 & 2 & -1 \\ 0 & & & & 0 & -1 & 1 \end{bmatrix} \quad (1.2)$$

The Rouse matrix is also called the Kirchhoff matrix of the chain's graph.

To find the eigenvalues we calculate

$$D_N = |[R] - \lambda[I]| = 0$$

which gives us a matrix of the form

$$R = \begin{bmatrix} y & -1 & 0 & 0 & \dots & 0 \\ -1 & x & -1 & 0 & \dots & 0 \\ 0 & -1 & x & -1 & \dots & 0 \\ . & & & . & & . \\ . & & & . & & . \\ 0 & & & & -1 & x & -1 \\ 0 & & & & 0 & -1 & y \end{bmatrix}$$

with $x = 2 - \lambda$, and $y = x - 1$.

Developing the determinant by the last column we find a recursion relation as follows

$$D_N = yD_{N-1} - D_{N-2}$$

Since the recursion relation is slightly different for D_{N-1} , bt remains the same for all $j \leq N - 1$, we solve the recursion relation for D_{N-1} and then return to define the last term D_N using the relation above.

The recurrence relation is:

$$D_z = xD_{z-1} - D_{z-2}$$

with the boundary conditions

$$D_1 = y$$

$$D_2 = xy - 1$$

We note that according to the Rouse matrix $x = y + 1$.

The particular solution to the recursion relation is

$$D_z = e^{iz\theta}$$

substituting it into the recursion relation gives

$$e^{iz\theta} = xe^{i(z-1)\theta} - e^{i(z-2)\theta}$$

hence

$$x = 2\cos(\theta)$$

The general solution can then be defined as

$$D_z = Ae^{iz\theta} + Be^{-iz\theta}$$

where A and B are some constants to be defined.

Using the boundary conditions we get

$$y = Ae^{i\theta} + Be^{-i\theta}$$

$$\begin{aligned} A &= \frac{y - Be^{-i\theta}}{e^{i\theta}} = (2\cos(\theta) - 1)e^{-i\theta} - Be^{-2i\theta} \\ &= \frac{1 - e^{i\theta}}{e^{-i\theta} - e^{i\theta}} = e^{i\theta/2} \frac{e^{-i\theta/2} - e^{i\theta/2}}{-2i\sin(\theta)} \\ &= \frac{e^{i\theta/2}}{2\cos(\theta/2)} \end{aligned}$$

and

$$B = \frac{e^{-i\theta} - 1}{e^{-i\theta} - e^{i\theta}} = \frac{e^{-i\theta/2}}{2\cos(\theta/2)}$$

The general solution is now

$$D_z = \frac{e^{i\theta/2}}{2\cos(\theta/2)}e^{iz\theta} + \frac{e^{-i\theta/2}}{2\cos(\theta/2)}e^{-iz\theta} = \frac{\cos((z+1/2)\theta)}{\cos(\theta/2)} \quad (1.3)$$

Since the determinant must vanish, we have

$$D_N = yD_{N-1} - D_{N-2} = 0$$

substituting the expressions for D_{N-1} and D_{N-2} into the equation above yields

$$\begin{aligned} yD_{N-1} - D_{N-2} &= D_1D_{N-1} - D_{N-2} = \\ \frac{\cos(3\theta/2)}{\cos(\theta/2)} \frac{\cos((N-1/2)\theta)}{\cos(\theta/2)} - \frac{\cos((N-3/2)\theta)}{\cos(\theta/2)} &= 0 \end{aligned}$$

therefore

$$\cos(3\theta/2) \cos((N-1/2)\theta) = \cos((N-3/2)\theta) \cos(\theta/2)$$

displaying the trigonometric functions as sum of exponentials we can get

$$\cos((N+1)\theta) - \cos((N-1)\theta) = 0$$

which gives

$$-2\sin(N\theta)\sin(\theta) = 0$$

therefore

$$\theta = \frac{p\pi}{N}$$

$p = 0, 1, \dots, N-1$ (since we have N solutions)

The eigenvalues are then

$$\lambda_p = 2 - x = 2 - 2\cos(\theta_p) = 2 \left(1 - \cos\left(\frac{p\pi}{N}\right)\right) = 4\sin^2\left(\frac{p\pi}{2N}\right)$$

$p = 0, 1, \dots, (N-1)$.

1.6.6 Eigenvectors of the Rouse Matrix

[Show Full derivation]

The k^{th} entry in the p^{th} eigenvector is

$$c_k = \sqrt{\frac{2}{N}} \sin\left(\frac{k\pi p}{N}\right)$$

with $k = 1, 2, \dots, N$ and $p = 0, 1, \dots, N-1$

1.6.7 Centralizing the chain

[UNFINISHED]

The differential equation describing the dynamics R_n in 3D is

$$\frac{dR_n}{dt} = -\frac{3D}{b^2} (2R_n(t) - R_{n-1}(t) - R_{n+1}(t)) + f_n(t)$$

If we shift the chain so that its new center of mass always lays at the origin, we get

$$\frac{d(R_n - cm)}{dt} = -\frac{3D}{b^2} (2R_n - R_{n-1} - R_{n+1}) + f_n - \frac{1}{N+1} \sum_{i=0}^N f_i$$

for such a new system, the new center of mass, cm^* should have zero derivative, indeed.

$$\frac{dcm^*}{dt} = \frac{1}{N+1} \left[\sum_{i=1}^N \frac{dR_i}{dt} - (N+1) \sum_{i=0}^N \frac{1}{N+1} f_i \right] = \vec{0}$$

Of course, this process is only valid post simulation. It seems not plausible to simulate a random process such that its center of mass remains in one point.

Subtracting the center of mass from the position of each bead should not affect the distribution of bond lengths, and it is indeed obvious to see it by subtracting two consecutive beads equation that the center of mass cancels out. However, the distribution of bead position is affected.

since each f_n is normally distributed with std $\sqrt{2D}$ and mean 0, the random variable $\frac{1}{N} \sum_{i \neq n}^N f_n(t)$

1.6.8 Mean First End To end Encounter Time Of the Rouse Chain

From [1]. [UNFINISHED]

1.6.9 The Pair Correlation function

According to [3]. To investigate the spatial distribution of segments in the Rouse polymer we introduce the segment pair correlation function, $g(r)$, defined as follows. If we focus on the n^{th} segment, we define $g_n(r)$ to be the average segment density at position r from segment n . If we write $R_n (n = 1, 2, 3, \dots, N)$ for the position vectors of the segments, then we can express $g_n(r)$ as

$$g_n(r) = \sum_{m=1}^N \langle \delta(r - (R_m - R_n)) \rangle$$

The average is a spatial average, so in 3D we have to divide by the volume $r + \delta r$ to get the concentration. The time correlation function, $g(r)$, is then defined as the average of the segment pair correlation function, $g_n(r)$.

$$g(r) = \frac{1}{N} \sum_{n=1}^N g_n(r)$$

In addition, we define $g(q)$, the Fourier transform of $g(r)$

$$g(q) = \int e^{iqr} g(r) dr = \frac{1}{N} \sum_{n=1}^N \sum_{m=1}^N \langle \exp([iq(R_m - R_n)]) \rangle$$

The pair correlation function is thus also called the radial distribution function. In the simplest terms it is a measure of probability of finding a particle at a distance r away from a given reference particle.

1.6.10 Radius of Gyration

[UNFINISHED]

From the definition of the Fourier transform of the pair correlation function for small q , we can define the length called radius of gyration.

1.7 Equilibrium properties of generalized chain

1.8 Chain conformation under an external field

Taken from [4]. If an external field $U_e(r)$ acts on each segment of the chain, the chain's equilibrium distribution is modified by the Boltzmann factor

$$\exp \left[-\frac{1}{k_B T} \int_0^N U_e(R_n) dn \right]$$

1.9 The Rouse ring

Construction of the Rouse ring is done by setting the first and last beads at position $x_0 = 0$. This forms a discrete **Brownian bridge**, which is defined using the standard random walk, $w(t)$, with $\langle w(t)^2 \rangle = 1$, $\langle w(t) \rangle = 0$, of N steps (between $N + 1$ beads).

$$B(t) = w(t) - \frac{t}{N} w(N) \quad t = 1, \dots, N$$

In the context of polymer dynamics we will refer to the bridge as a *Rouse ring*. The expectation $E[B(t)]$ can be shown to be 0 due to the properties of the Brownian paths

$$E[B(t)] = E[w(t) - \frac{t}{N} w(N)] = E[w(t)] - (t/N) E[w(N)] = 0$$

The covariance, C_B , of $B(t)$ is

$$\begin{aligned}
C_B &= E((B(t) - E[B(t)])(B(s) - E[B(s)])) \\
&= E[B(t)B(s)] = E[(w(t) - (t/N)w(N))(w(s) - (s/N)w(N))] \\
&= E[w(s)w(t) - w(N)(sw(t) + tw(s))/N + (st/N^2)w(N)^2] \\
&= \min(s, t) - (s/N)\min(N, t) - (t/N)\min(N, s) + st/N^2 \\
&= \min(s, t) - 2st/N + st/N^2 \\
&= \min(s, t) - (st/N^2)(2N - 1)
\end{aligned}$$

We therefore see that the position of the Rouse ring are dependent. The variance is given by setting $s = t$ to be

$$\sigma_B^2 = t - (t/N)^2(2N - 1)$$

The Rouse ring is a Gaussian process with a joint probability density function given by

$$f_B(x) = \frac{1}{\sqrt{((2\pi)^N |C_B|)}} \exp(-0.5x^T C_B^{-1} x)$$

Derivation of the probability density of the Rouse ring

The Rouse ring is a tied-down random walk, with $w(N) = w(0)$. Without loss of generality, we set $w(0) = 0$, as in the classical random walk.

The probability density function of the random walk in 3D is given by the Weiner measure as

$$f(w(x), N) = \left(\frac{1}{2\pi N}\right)^{3/2} \exp\left(-\frac{3x^2}{2N^2}\right)$$

Conditioning the random walk on the event that $w(N) = w(0)$ we get

$$\begin{aligned}
f(0, x, 0; 0, t/N, N) &= \frac{1}{\sqrt{(2\pi)^2 t(N - t/N)/N}} \exp\left(-\frac{x^2}{2t/N} - \frac{x^2}{2(N - t/N)}\right) \\
&= \frac{N}{2\pi\sqrt{t(N - t)}} \exp\left(-\frac{x^2}{2t(N - t)/N^2}\right)
\end{aligned}$$

and in 3D

$$f(0, x, 0; 0, \frac{t}{N}, N) = \left(\frac{N}{2\pi\sqrt{t(N - t)}}\right)^3 \exp\left(-\frac{xx^T}{2t(N - t)/N^2}\right)$$

1.9.1 Encounter probability in the Rouse ring

The vector between bead 1 and bead m of the chain has the probability density $f(0, x, 0; 0, \frac{m}{N}, 0)$. Since in the ring we cannot distinguish between beads, we

see that the encounter probability at equilibrium between beads m and n is

$$f(0, 0, 0; 0, \frac{|m-n|}{N}, 0) = \left(\frac{N}{2\pi\sqrt{|m-n|(N-|m-n|)}} \right)^3$$

To normalized the quantity above we write

$$f(0, x, 0; 0, \frac{m}{N}, 0) = \left(\frac{N}{2\pi\sqrt{m(N-m)}} \right)^3 / \sum_{t=1}^{N-1} \left(\frac{N}{2\pi\sqrt{t(N-t)}} \right)^3$$

which is the encounter probability at equilibrium between two beads with a distance m along the ring between them (note the symmetry between m and $N - m$).

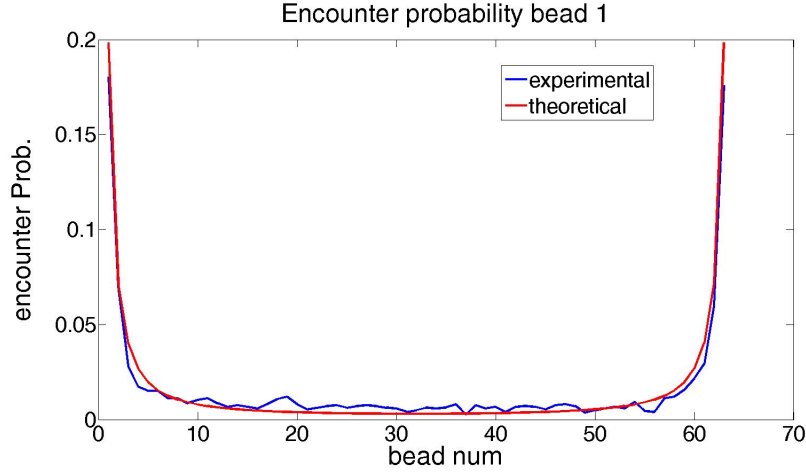


Figure 1.1: Encounter Probability of bead 1 in a ring of 64 beads (blue) from 10,000 simulation compared to the theoretical result (red)

The normalization is made in accordance to the encounter data, in which we divide all encounter frequency by the total number of encounter for each bead, to give an area under the curve of 1.

1.9.2 The relation between a ring and a chain

We note that the pdf of the ring is just the conditional probability of the end to end vector of a chain of length $N - t$ and a chain of length t are equal. This can easily be verified by multiplying the pdfs of the mentioned chains. [Needs elaboration]

We further note that by adding the encounter probabilities of bead 1 and $t = 1..N$ and bead N with $t = N - 1, N - 2, \dots, 1$ we get something similar to the Rouse ring, although a weighting must be applied

$$\left(\frac{3}{2\pi b^2 t} \right)^{1.5} + \left(\frac{3}{2\pi b^2 (N-t)} \right)^{1.5} = \left(\frac{3N}{2\pi b^2 t(N-t)} \right)^{1.5} \left(\left(1 - \frac{t}{N} \right)^{1.5} + \left(\frac{t}{N} \right)^{1.5} \right)$$

which is a scaled version of the Rouse ring's encounter probability. effectively, we can now try to replace each ring with a sum of two chains.

1.9.3 Configuration distribution of the Rouse ring

The increments of the Rouse ring are

$$\Delta B_t = B(t+1) - B(t) = w(t+1) - w(t) - (1/N)w(N)$$

which is a Gaussian process as the subtraction of two Gaussian processes, with the following properties

$$E[\Delta B_t] = E[w(t+1) - w(t) - (1/N)w(T)] = 0$$

and covariance

$$\begin{aligned} C_\Delta &= E[\Delta B_t \Delta B_s] \\ &= \min(s+1, t+1) - \min(t+1, s) - \min(t, s+1) \\ &\quad + \min(s, t) - (1/N^2)(2N-1) \end{aligned}$$

Setting $s = t$ we get the variance

$$\sigma_\Delta^2 = 1 - (1/N^2)(2N-1) = \frac{(N-1)^2}{N^2}$$

The joint pdf of the increments is therefore

$$f_\Delta(\vec{x}) = \left(\frac{1}{\sqrt{(2\pi)^N |C_\Delta|}} \right) \exp(-0.5 \vec{x}^T C_\Delta^{-1} \vec{x})$$

To fully express $f_\Delta(x)$ we need to estimate $|C_\Delta|$ and C^{-1} . The form of C_Δ is

$$C_\Delta = \begin{bmatrix} \sigma_\Delta^2 & \sigma_\Delta^2 - 1 & \sigma_\Delta^2 - 1 & \dots & \sigma_\Delta^2 - 1 \\ \sigma_\Delta^2 - 1 & \sigma_\Delta^2 & \sigma_\Delta^2 - 1 & \dots & \sigma_\Delta^2 - 1 \\ \sigma_\Delta^2 - 1 & \sigma_\Delta^2 - 1 & \sigma_\Delta^2 & \dots & \sigma_\Delta^2 - 1 \\ \cdot & \cdot & \cdot & \dots & \cdot \\ \cdot & \cdot & \sigma_\Delta^2 - 1 & \sigma_\Delta^2 & \sigma_\Delta^2 - 1 \\ \sigma_\Delta^2 - 1 & \dots & \dots & \sigma_\Delta^2 - 1 & \sigma_\Delta^2 \end{bmatrix}$$

or shortly

$$C_\Delta(s, t) = \begin{cases} \sigma_\Delta^2 & s = t \\ \sigma_\Delta^2 - 1 & s \neq t \end{cases}$$

The resulting C_Δ is a circulant matrix with normalized eigenvectors

$$\omega_j = (1/\sqrt{N})(1, \omega_j, \omega_j^2, \dots, \omega_j^{N-1})$$

with $\omega_j = \exp(\frac{2\pi ij}{N})$ $i = \sqrt{-1}$, $j = 0, \dots, N-1$. And eigenvalues

$$\lambda_j = c_0 + c_1\omega_j + c_2\omega_j^2 + \dots c_{N-1}\omega_j^{N-1} \quad j = 0, \dots, N-1$$

where, c_j is the first row of C_Δ , i.e $c_0 = \sigma_\Delta^2$, $c_{N-1} = \dots c_1 = \sigma_\Delta^2 - 1$. Therefore, the eigenvalues can be written as

$$\begin{aligned} \lambda_0 &= \sigma_\Delta^2 + (N-1)(\sigma_\Delta^2 - 1) = \frac{1-N}{N} \\ \lambda_j &= \sigma_\Delta^2 + (\sigma_\Delta^2 - 1) \sum_{n=1}^{N-1} \exp(\frac{2\pi n i j}{N}) \\ &= \sigma_\Delta^2 + (\sigma_\Delta^2 - 1) \left(\sum_{n=0}^{N-1} \exp(\frac{2\pi n i j}{N}) - 1 \right) \\ &= \sigma_\Delta^2 + (\sigma_\Delta^2 - 1) \left(\frac{1 - \exp(2\pi i j)}{1 - \exp(\frac{2\pi i j}{N})} - 1 \right) \\ &= \sigma_\Delta^2 - (\sigma_\Delta^2 - 1) = 1 \\ &\quad j = 1, \dots, N-1 \end{aligned}$$

Therefore, the determinant is

$$|C_\Delta| = \lambda_0 = \frac{1-N}{N}$$

The inverse, C_Δ^{-1} , is of the form

$$C_\Delta^{-1}(s, t) = \frac{1}{1-N} + \frac{1}{N} \sum_{n=1}^{N-1} (\omega_{s-1} \omega_{t-1})^n$$

$s = 1, \dots, N, t = 1, \dots, N$. Therefore,

$$C_\Delta^{-1}(s, t) = \begin{cases} \frac{N-(N-1)^2}{N(1-N)} & s = t \\ \frac{2N-1}{N(1-N)} & s \neq t \end{cases}$$

note, that $\frac{N-(N-1)^2}{N(1-N)} - 1 = \frac{2N-1}{N(1-N)}$, so we can write

$$\begin{aligned} C_\Delta^{-1}(s, t) &= \begin{cases} \alpha & s = t \\ \alpha - 1 & s \neq t \end{cases} \\ \alpha &= \frac{N - (N-1)^2}{N(1-N)} \end{aligned}$$

The configuration distribution in 3D can be written as

$$f_{\Delta}(\vec{x}) = \left(\frac{N}{(2\pi)^N(N-1)} \right)^{1.5} \exp(-1.5\vec{x} \cdot \delta S(\vec{x}; \alpha))$$

where

$$\delta S(\vec{x}; \alpha) = \begin{bmatrix} \alpha \sum_{n=1}^N x_n - \sum_{n \neq 1} x_n \\ \alpha \sum_{n=1}^N x_n - \sum_{n \neq 2} x_n \\ \vdots \\ \alpha \sum_{n=1}^N x_n - \sum_{n \neq N} x_n \end{bmatrix}$$

Note, that when $\alpha = 1$ the system becomes decoupled. This happens at the limit $N \rightarrow \infty$, which makes the increments of the bridge

$$\lim_{N \rightarrow \infty} \Delta B_t = \lim_{N \rightarrow \infty} w(t+1) - w(t) - (1/N)w(N) = w(t+1) - w(t)$$

From $f_{\Delta}(\vec{x})$ we see that whenever $\sum_{n=1}^N x_n = 0$ we get $\delta S(\vec{x}; \alpha) = [x_1, x_2, \dots, x_N]$

and we retrieve the pdf of the ring.

The term $\vec{x} \delta S(\vec{x}, \alpha)$ in the exponent of the pdf, can be written in the following form

$$\vec{x} \delta S(\vec{x}; \alpha) = (\alpha - 1) \left(\sum_{n=1}^N x_n \right)^2 + \sum_{n=1}^N x_n^2$$

1.9.4 Eigenvalues of the Rouse Ring

Connecting bead 1 and N to form a ring, we now search for the eigenvalues of the new *Rouse ring* matrix, R , harboring such a connection. For this end, we have to calculate the determinant of the matrix

$$D_N = |R - \lambda I| = \begin{vmatrix} x & -1 & 0 & 0 & \dots & -1 \\ -1 & x & -1 & 0 & \dots & 0 \\ 0 & -1 & x & -1 & \dots & 0 \\ \cdot & & & \cdot & & \cdot \\ \cdot & \cdot & & & \cdot & \\ \cdot & & & -1 & x & -1 & 0 \\ 0 & & & & -1 & x & -1 \\ -1 & \cdot & \cdot & \cdot & 0 & -1 & x \end{vmatrix}_{N \times N}$$

with $x = 2 - \lambda$. We can apply to the matrix of size $(N-1) \times (N-1)$ the same procedure as before and try to solve it recursively. The boundary conditions now read

$$D_1 = x; D_2 = x^2 - 1$$

According to the solution in section 1.6.5 and in [5], we have

$$D_{N-1} = \frac{\sin(N\theta)}{\sin(\theta)}$$

The relationship between D_N and D_{N-1} is found by developing the determinant of D_N according to the last column

$$D_N = x(-1)^{2N}D_{N-1} + (-1)(-1)^{2N-1}D^* + (-1)(-1)^{N+1}D^{**} = xD_{N-1} + D^* + (-1)^{N+2}D^{**}$$

with the determinant D^* and D^{**} defined as the minors

$$D^* = \begin{vmatrix} x & -1 & 0 & 0 & \dots & 0 \\ -1 & x & -1 & 0 & \dots & 0 \\ 0 & -1 & x & -1 & \dots & \\ \cdot & & & \cdot & & \\ \cdot & & & \cdot & & \\ \cdot & & & -1 & x & -1 \\ -1 & & & 0 & -1 & \end{vmatrix}_{(N-1) \times (N-1)} \quad D^{**} = \begin{vmatrix} -1 & x & -1 & 0 & \dots & 0 \\ 0 & -1 & x & -1 & \dots & 0 \\ \cdot & & & \cdot & & \cdot \\ \cdot & & & \cdot & & \cdot \\ \cdot & & & -1 & x & -1 \\ 0 & & & & -1 & x \\ -1 & & & & 0 & -1 \end{vmatrix}_{(N-1) \times (N-1)}$$

We calculate the determinants D^* and D^{**} by minors according to the last row to get

$$D^* = (-1)(-1)^{2N-2}D_{N-2} + (-1)(-1)^{N-1+1}(-1)^{N-2} = (-1)^{2N-1}[D_{N-2} + 1]$$

$$D^{**} = (-1)(-1)^{2N-2}(-1)^{N-2} + (-1)(-1)^{1+N-1}D_{N-2} = (-1)^{3N-3} + (-1)^{N+1}D_{N-2}$$

Therefore,

$$\begin{aligned} D_N &= xD_{N-1} + (-1)^{2N-1}[D_{N-2} + 1] + (-1)^{N+2}[(-1)^{3N-3} + (-1)^{N+1}D_{N-2}] \\ &= xD_{N-1} + (-1)^{2N-1}[D_{N-2} + 1] + (-1)^{4N-1} + (-1)^{2N+3}D_{N-2} \\ &= xD_{N-1} + D_{N-2}[(-1)^{2N-1} + (-1)^{2N+3}] + (-1)^{2N-1} + (-1)^{4N-1} \\ &= xD_{N-1} - 2D_{N-2} - 2 \end{aligned}$$

Substituting the solution for D_{N-1} and D_{N-2} , we get

$$D_N = \frac{x \sin(N\theta) - 2 \sin((N-1)\theta) - 2 \sin(\theta)}{\sin(\theta)} = 0$$

Further simplification of D_N leads to

$$\begin{aligned} D_N &= 2 \frac{\cos(\theta) \sin(N\theta) - [\sin((N-1)\theta) + \sin(\theta)]}{\sin(\theta)} \\ &= \frac{2}{\sin(\theta)} [\cos(\theta) \sin(N\theta) - 2 \sin(\frac{N\theta}{2}) \cos(\frac{(N-2)\theta}{2})] \\ &= \frac{4}{\sin(\theta)} [\cos(\theta) \sin(\frac{N\theta}{2}) \cos(\frac{N\theta}{2}) - \sin(\frac{N\theta}{2}) [\cos(\frac{N\theta}{2}) \cos(\theta) + \sin(\frac{N\theta}{2}) \sin(\theta)]] \\ &= -4 \sin^2(\frac{N\theta}{2}) \end{aligned}$$

Equating $D_N = 0$ we get the solutions

$$\theta_p = \frac{2\pi p}{N}$$

for $p = 0, 1, \dots, (N - 1)$

Therefore, the eigenvalues of the Rouse ring are

$$\lambda_p = 2(1 - \cos(\theta_p)) = 2(1 - \cos(2\pi p/N))$$

Since $\cos(\frac{2\pi\phi}{N}) = \cos(\frac{2\pi(N-\phi)}{N})$, we have eigenvalues multiplicities. In our case, setting $\phi = p$ we have $\cos(\frac{2\pi p}{N}) = \cos(\frac{2\pi(N-p)}{N})$ for $p = 1, 2, 3, \dots, (N - 2)$. For the end-values, $p = 0$ and $p = N - 1$ the eigenvalues are unique.

1.9.5 Mean First Encounter Time in the Rouse ring

[UNFINISHED]

Following the method in [1]. First we transform the Rouse ring system of equation into normal coordinates using the Rouse ring eigenvalues found in Section 1.9.4. We transform to normal coordinates by $u_p = \sum_{n=1}^N \alpha_p^n R_n$, where α_p are the eigenvectors. We then represent our boundary conditions that bead j and bead k are in the same position, using the normal coordinates representation. The probability density function in the normal coordinates should then satisfy the forward Fokker Planck equation. The solution to the probability density function should then be expanded as an infinite sum of the form

$$p(x, t) = \sum_{i=1}^{\infty} a_i w_{\lambda_i^\epsilon}(x) e^{-\lambda_i^\epsilon t D} e^{-\phi(x)}$$

where $w_{\lambda_i^\epsilon}(x)$ and λ_i^ϵ are the eigenvectors and eigenvalues of the forward Fokker Planck operator outside of the domain, and a_i are coefficients. Integrate the probability density according to x , over the domain without the absorbing boundary (the encounter sphere), to get a function of time. An integration of the resulting function from time $t = 0$ to ∞ is the first moment of the survival function, which is the mean first encounter time (i.e the first time the polymer's ends are at the absorbing sphere).

1.10 A ring and a chain

In this section we combine the result of the Rouse chain and the Rouse ring by attaching a linear chain with a ring, reordering the indexes and deriving the encounter probability between beads in the composite structure.

1.10.1 Construction

We start by attaching the a chain of $N_c - 1$ beads to a ring of N_r beads by connecting bead N_c to an arbitrary bead in the ring. The first bead in the chain will be numbered 1. Given the choice of the connecting bead, we index the first bead in the ring as N_c and the last as $N_r + N_c$.

In equilibrium, the link vectors are independent and we can treat the two structure, the ring and the chain, separately. The first bead in the loop will

be our reference point for the calculation of the encounter probability at equilibrium, by calculating the probability that both the vector $R_m - R_{N_c}$ and $R_n - R_{N_c}$ is equal to some s , over all possible vectors s .

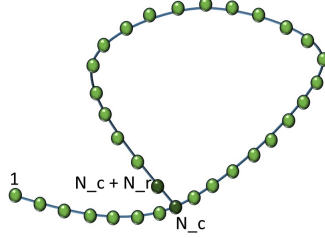


Figure 1.2: A sketch of the composite structure of a chain and a ring connected

1.10.2 The encounter probability

We note that distribution of the vectors between bead m and n at equilibrium is given by

$$f_c(R_m - R_n, n - m) = \left(\frac{3}{2\pi|m - n|b^2} \right)^{3/2} \exp\left(-\frac{3(R_m - R_n)^2}{2|m - n|b^2}\right)$$

The Rouse ring requires a change of variables such that the steps of the Brownian bridge will be at the same scale as that of the chain. Therefore, we define our ring as the process

$$B(t) = \sqrt{\frac{N_r}{3}} b [\omega(t) - \frac{t}{N_r} \omega(N_r)]$$

which has the pdf

$$f_r(R_t, N_r) = \left(\frac{3}{2\pi b^2 t(N_r - t)} \right)^{3/2} \exp\left(-\frac{3R_t^2}{2tb^2(N_r - t)}\right)$$

for the Rouse ring, with R_t the vector from the connecting bead between the chain and the ring and the t^{th} bead of the ring.

Due to the independence between the structures in equilibrium, the encounter probability between bead m of the chain ($1 \leq m \leq N_c$) and bead t ($N_c \leq t \leq N_l$) of the ring is the joint probability that $R_t - R_{N_c} = R_m - R_{N_c} = \vec{s}$. That is

$$P(R_m - R_{N_c} = \vec{s}, R_t - R_{N_c} = \vec{s}) = f_r(s, N_r) f_c(s, |m - N_c|)$$

or, $P(R_m + R_t - 2R_c = 2s)$. Since the sum of these random variables is the convolution of their respective pdfs, we can perform the integration, stated in

the general form for each dimension.

$$f_{rc}(x) = (f_r * f_c)(x) = \left(\frac{1}{(2\pi)^2 \sigma_r \sigma_c} \right)^{1/2} \int_{-\infty}^{\infty} \exp \left(- \left(\frac{(x-y)^2}{\sigma_c} + \frac{y^2}{\sigma_r} \right) \right) dy$$

which can be written as

$$(f_r * f_c)(x) = k \int_{-\infty}^{\infty} \exp(-fy^2 + gy + h) dy$$

with

$$\begin{aligned} k &= \left(\frac{1}{(2\pi)^2 \sigma_c \sigma_r} \right)^{1/2} \\ f &= \frac{\sigma_c + \sigma_r}{2\sigma_r \sigma_c} \\ g &= \frac{x}{\sigma_c} \\ h &= -\frac{x^2}{2\sigma_c} \end{aligned}$$

Using the identity for Gaussian integral, we get for 3D

$$f_{rc}(x) = k \sqrt{\frac{\pi}{f}} \exp\left(\frac{g^2}{4f} + h\right) = \left(\frac{1}{2\pi(\sigma_c^2 + \sigma_r^2)} \right)^{3/2} \exp\left(-\frac{xx^T}{2(\sigma_c^2 + \sigma_r^2)}\right)$$

as in the classical result. with

$$\begin{aligned} \sigma_c &= (N_c - m) \frac{b^2}{3} \\ \sigma_r &= t(N_r - t) \frac{b^2}{3} \end{aligned}$$

and $0 \leq t \leq N_r, 1 \leq m \leq N_c$

The encounter probability between bead m of the chain and bead t of the ring is then given by

$$f_{rc}(\vec{0}, m, t; N_c, N_r) = \left(\frac{3}{2\pi b^2 (N_c - m + t(N_r - t))} \right)^{3/2} / S$$

with S , the normalization constant, given by

$$S = \left(\frac{3}{2\pi b^2} \right)^{3/2} \left(\sum_{n=1}^{N_c} \left(\frac{1}{n} \right)^{3/2} + \sum_{t=1}^{N_r-1} \left(\frac{N_r}{t(N_r - t)} \right)^{3/2} \right)$$

$0 \leq t \leq N_r$. We therefore see that b is singled out in the calculation.

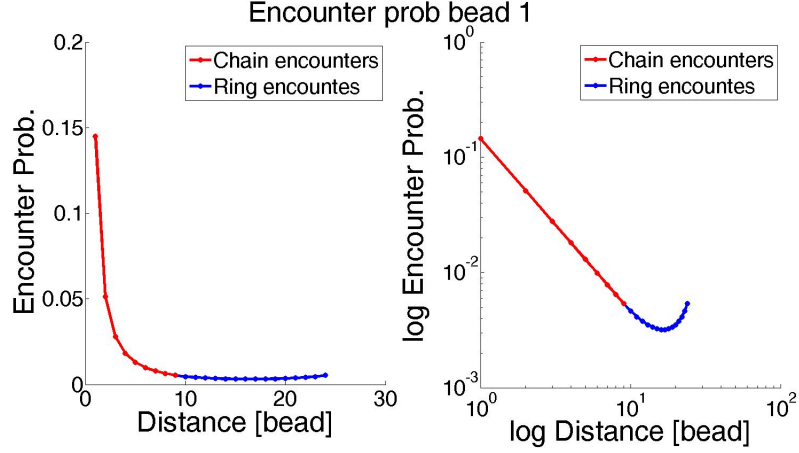


Figure 1.3: the encounter probability of bead 1 in a bead-ring structure in linear (left) and log (right) scales. A chain of 10 beads is connected to a ring of 15 beads. The encounter probability signal is shown to be equal between beads in equal distance along the chain. For the case of the ring, the distance is the shortest distance along the graph representing the polymer

1.11 Two Rings

We now turn to investigate the encounter probabilities between beads in a 2-ring connected structure.

1.11.1 Construction

We connect two Rouse rings in a single bead, i.e there exist a bead k which is shared by the two rings. The first ring is of size N_1 , the second N_2

1.12 Generalized Rouse Chain

A generalization of the Rouse model into a chain with arbitrary connectivity (springs) between its beads is given by the Generalized Gaussian chains. Assuming a chain with N beads, in which each bead is connected to its nearest neighbors and at most $N - 2$ beads with spring constants k_{ij} between bead i and j . We assume all beads are subjected to the same friction coefficient ζ . The configuration distribution of the chain is given by

$$\psi = \prod_{i=1}^{N-1} \prod_{j=1}^{N_i} \left(\frac{k_{ij}}{2\pi k_B T} \right)^{1.5} \exp \left(-\frac{k_{ij} r^2}{2k_B T} \right)$$

with N_i the number of connections of bead i , with multiplication over unique pairs.

If an external force $F_m^{(ext)}(t)$ operates on the m^{th} bead of the chain, then the Langevin equation of motion for the generalized structure is given by

$$\zeta \frac{dR_n(t)}{dt} = -\frac{3k_B T}{2b^2} \sum_{m=1}^N A_{nm} R_m(t) + f_m(t) + F_m^{(ext)}(t)$$

With A - the Kirchoff matrix and $R_m(t)$ the position vector of the m^{th} bead, and $f_m(t)$ is the thermal force (noise) acting on the bead. The information regarding the chain's connectivity is stored within the Kirchoff matrix A .

If the force is weak, then there is a linear relationship between the velocity field and the force

$$F_m^{(ext)}(t) = \zeta V_m(t)$$

with $V_m(t)$ the velocity of the solvent at the position of the m^{th} beads. If the chain undergoes deformation due to the force (strain) then

1.13 Simulations

1.13.1 Choosing Δt

The dynamics of beads is governed by the equation

$$\frac{dP}{dt} = -\frac{3D}{b^2} RP + \sqrt{2D} f_n$$

if we represent the Rouse matrix in its diagonal form

$$R = Q^{-1} \Lambda Q$$

where Q is an orthonormal matrix with the eigenvectors of R in its columns, and Λ is a diagonal matrix with the Rouse eigenvalues in the diagonal, we get

$$\frac{dP}{dt} = -\frac{3D}{b^2} Q^{-1} \Lambda Q + \sqrt{2D} f$$

multiplying from the left by Q and setting $S = QP$ we get

$$\frac{dS}{dt} = -\frac{3D}{b^2} \Lambda S + \sqrt{2D} Q f$$

The case with no noise

if we omit the noise term and solve for S the numerical scheme is

$$S(t + \Delta t) - S(t) = \left(-\frac{3D\Delta t}{b^2} \Lambda\right) S(t)$$

taking the norm of both sides and dividing

$$\frac{\|S(t + \Delta t) - S(t)\|}{\|S(t)\|} = \left\| \left(-\frac{3D\Delta t}{b^2} \Lambda \right) \right\| = \frac{3D\Delta t}{b^2} \lambda_{max} = \frac{12D\Delta t}{b^2}$$

where for the Rouse matrix $\lambda_{max} = 4$. Demanding that the quotient be smaller than 1 we have

$$\frac{12D}{b^2} \leq 1 \implies \Delta t \leq \frac{b^2}{12D}$$

The case with noise

using the same procedure as above,

$$\begin{aligned} \frac{\|S(t + \Delta t) - S(t)\|}{\|S(t)\|} &= \left\| \left(-\frac{3D}{b^2} \Lambda \right) S + \sqrt{2D} Q f \right\| / \|S\| \leq \left(\frac{3D}{b^2} \|\Lambda\| + \sqrt{2D} \|Q f\| / \|S\| \right) \\ &= \leq \frac{3D}{b^2} \lambda_{max} + \sqrt{2D} \frac{\|Q\| \|f\|}{\|S\|} = \frac{12D}{b^2} \leq \frac{3D}{b^2} \lambda_{max} \Delta t + \sqrt{2D} \Delta t \end{aligned}$$

Demanded that the quotient be smaller than 1 we have

$$\frac{12D}{b^2} \leq 1 \implies \Delta t \leq \frac{b^2}{12D + \sqrt{2D} b^2}$$

1.13.2 Relaxation time

The relaxation time is determined according to the formula

$$\tau_p = \frac{b^2 \Delta t}{12d^2 \sin^2\left(\frac{p\pi}{2N}\right)} \quad (1.4)$$

1.13.3 The dynamics of bond length

In simulations we would like to determine Δt such that no 'blow-ups' will occur. For this end, we constrain the mean of squared difference between bond length in consecutive steps to lay below some predefined small value.

The result show that

$$\gamma = \ll \|r_n(t + \Delta t) - r_n(t)\|^2 \gg = \left(\frac{3D\Delta t}{b} \right)^2 + 6D\Delta t$$

1.13.4 Encounter signal noise estimation

[UNFINISHED]

We now ask what is the expected probability to find bead n close to bead m given that bead 1 and N have met. This is given by the calculation in 1.10.

Chapter 2

2.1 Rubber elasticity

Polymer melt are different than rubber material in the sense that rubber is crossed-linked by chemical means. Therefore, the rubber can be regarded as a huge 3D network of cross-linked polymeric melt. Such a material, up to a maximal temperature, will recover its original shape after being released from deformation. In essence, the phenomena responsible for the restoring force of a rubber is the entropy change caused by applying deformation.

2.1.1 Entropy and rubber elasticity

The free energy of a strip of rubber is written as

$$A = U - TS$$

with U the internal energy and S is the entropy. This relation is the formulation of the first law of thermodynamics, which states that the internal energy is due to the work and heat transfer, $U = W + Q$. The work is force applied on the body times the distance it operates, whereas the heat transfer, Q , is the entropy times the temperature, namely $Q = ST$.

If we apply a stretching force f on the rubber strip, and as a result it elongate by a length of dl then the free energy is

$$dA = dU - d(TS) = dW + dQ - d(TS) = dW + dQ - dQ = dW = fdl$$

We can therefore write the force as

$$f = \left(\frac{dA}{dl} \right) = \left(\frac{d(U - TS)}{dl} \right) = \left(\frac{dU}{dl} \right) - T \left(\frac{dS}{dl} \right) = \left(\frac{dU}{dl} \right) + T \left(\frac{df}{dT} \right)$$

an ideal rubber is defined to have $dU/dl = 0$.

If a strand of polymer is fixed at the origin on one end, and on the other it is cross-linked to some moving boundary, then the end-to-end vector can be used to derive the free energy change of the polymer due to deformation. As a result, the force can also be characterized according to the relationship above.

The probability distribution function of the end-to-end vector, R , of this polymer is given by

$$\Phi(R, N) = \left(\frac{3}{2\pi b^2}\right)^{3/2} e^{-\frac{3R^2}{(2Nb^2)}} = \left(\frac{3}{2\pi b^2}\right)^{3/2} e^{-\frac{3(X^2+Y^2+Z^2)}{(2Nb^2)}} = W(X, Y, Z) \quad (2.1)$$

There is a large number of configurations, Ω , for a chain with a large N that lead to the same end to end vector. All of these configurations, in freely jointed chain, have the same energy. Therefore, the number of configurations Ω for a certain R is proportional to the probability density function. Thus $\Omega \propto W(X, Y, Z)$.

The entropy of the chain, according to Boltzmann, is given by

$$s = k \ln(\Omega) = -\frac{3k}{2Nb^2}(X^2 + Y^2 + Z^2) + C$$

with C a constant from the proportionality. If the polymer is extended in one axes (say the x axis) and the polymer is contained within a rectangular rubber block with sides of length L_x^0, L_y^0, L_z^0 before deformation and L_x, L_y, L_z after deformation. The end-to-end vector $R_0 = (x_0, y_0, z_0)$ before deformation and $R = (x, y, z)$ after deformation.

If the deformation from R_0 to R is linearly proportional to the deformation of the whole piece of rubber (affine deformation) then $X/X_0 = L_x/L_x^0 = \lambda_x$, and similarly for λ_y, λ_z in the other dimensions. If the density of the rubber doesn't change, $\lambda_x \lambda_y \lambda_z = 1$. Due to the symmetry of deformation $\lambda_y = \lambda_z = 1/\sqrt{\lambda_x}$.

The difference between the entropy at rest and after deformation can be written in terms of λ_x

$$\Delta s = s - s_0 = -\frac{3k}{2Nb^2}[(\lambda_x^2 - 1)X_0^2 + (1/\lambda_x - 1)Y_0^2 + (1/\lambda_x - 1)Z_0^2]$$

When there are n chains we multiply the above quantity by n and the X_0^2, Y_0^2, Z_0^2 are replaced by their average equilibrium values

$$\langle X_0^2 \rangle = \langle Y_0^2 \rangle = \langle Z_0^2 \rangle = Nb^2/3$$

Now, using the relation $dA = du - Tds$ we find the free energy

$$\Delta A = -T\Delta S = nkT(\lambda_x^2 + 2/\lambda_x - 3)/2 = nkT(L_x^2/(L_x^0)^2 + 2L_x^0/L_x - 3)$$

And therefore the force

$$f = \partial(\Delta A)/\partial L_x = nkT(L_x/(L_x^0)^2 - L_x^0/L_x^2)$$

This relation allows us to retrieve the force acting on Gaussian chain, when the displacement in one axis is known.

2.1.2 The Maxwell equation

We start with an explanation of viscosity and elasticity of liquids. If a layer of liquid is trapped between two plates of area A at a distance h apart, and the upper plate is displaced in constant velocity v by with a constant force f relative to the lower plate in a direction parallel to the plate, then the *shear deformation rate* is

$$\dot{\lambda} = \frac{v}{h}$$

and the resulting *stress* is

$$\sigma = -\frac{f}{A}$$

The viscosity of the liquid is defined by

$$\eta = -\frac{\sigma}{\dot{\lambda}}$$

that is, the negative ratio of the stress and the shear deformation rate.

If the upper plate is displaced by a distance s due to the force, then the *shear strain* is defined by

$$\lambda = \frac{s}{h}$$

In a Hookian solid, the stress is linearly proportional to the strain

$$G = -\frac{\sigma}{\lambda} \quad (2.2)$$

the constant G is called the *modulus of the solid*.

In a simplified model, a dashpot and a spring are connected in series. The dashpot represents the viscous properties and the spring the elastic properties of the system. If the system is of length D , then we divide it into two parts of the spring and dashpot of length D_1 and D_2 respectively. Therefore, the modulus of the solid can be calculated if we apply force on the system which elongates it

$$G = -\frac{\sigma}{\lambda} = -\frac{-f/A}{s/h} = -\frac{F}{D_1 - D_0}$$

the force $-F$ operates in the direction of the spring elongation, and D_0 is the length of D_1 with minimal potential energy. The spring stores energy (elasticity), while the dashpot dissipates it (viscosity). The viscosity corresponds to

$$\eta = -\frac{\sigma}{\dot{\lambda}} = -\frac{F}{dD_2/dt}$$

extracting D_1 and differentiating it in time and adding to it the derivative of D_2 , we arrive at the differential equation for the length of the system

$$\frac{dD}{dt} = \frac{d}{dt}(D_1 + D_2) = -\left[\frac{1}{G} \frac{dF}{dt} + \frac{F}{\eta}\right]$$

For polymer systems the force F needs to be replaced by the stress σ and the rate of elongation by the shear deformation rate $\dot{\lambda}$ which gives the **Maxwell equation**

$$\frac{d\sigma}{dt} + \frac{\sigma}{\tau} = -\frac{\eta}{\tau}\dot{\lambda}, \quad \tau = \frac{\eta}{G} \quad (2.3)$$

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