

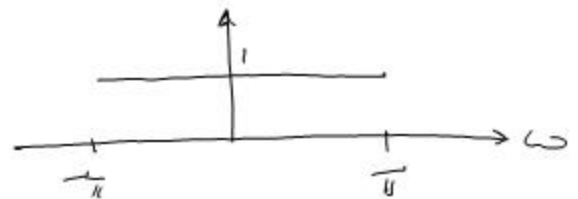
- Ideal LPF has real-valued frequency response.

$$H(e^{j\omega}) = |H(e^{j\omega})|, \quad \angle H(e^{j\omega}) = 0 \quad \text{"zero phase"}$$

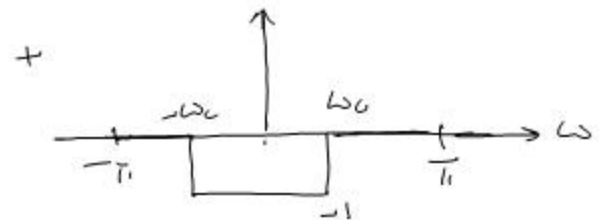
We can build piecewise-constant frequency responses by combining ideal responses.

Example: Highpass filter

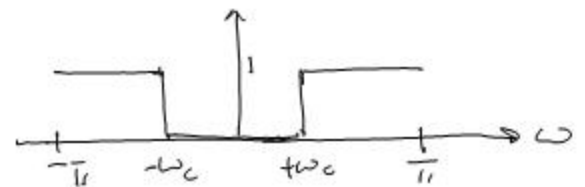
Allpass filter  $S[n] \Rightarrow$



lowpass filter  $-h_{lp}[n]$



highpass filter  $h_{hp}[n] =$



Therefore, 
$$h_{hp}[n] = S[n] - \frac{\sin(\omega_c n)}{\pi n}$$

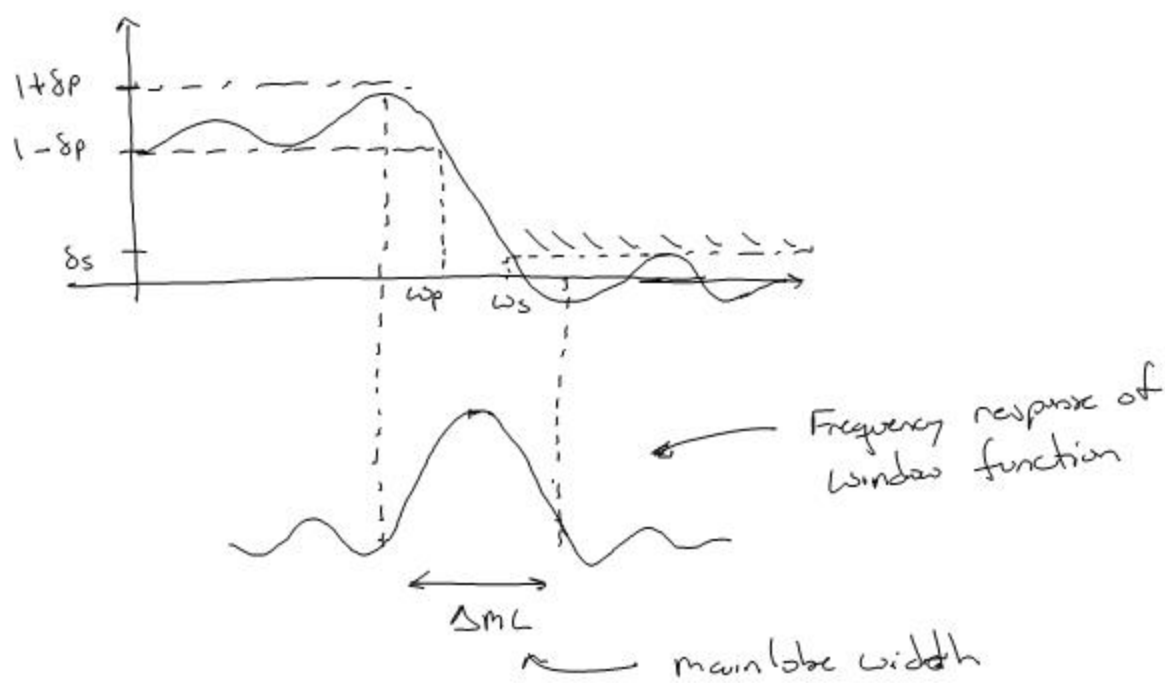
- FIR Filter order estimation (see 10.1.2)

Kaiser's Formula

Bellanger's Formula

Hermann's Formula

- Window function and filter magnitude response



note: Smaller  $\Delta ML$  results in faster transition from  $\omega_p$  to  $\omega_s$ .

Reducing passband and stopband ripple requires area under window sidelobes to be smaller.

- Designing FIR filters by windowing method

1- determine  $\omega_c = (\omega_p + \omega_s) / 2$

2- Estimate  $M$  (e.g.  $N = 2M + 1$ )

$$\Delta\omega = (\omega_s - \omega_p) \propto \frac{C}{M} \quad \text{from 10.2 table in book.}$$

Example:  $\omega_p = 0.3\pi$   $\omega_s = 0.5\pi$   
 stopband attenuation needs to be at least 40dB  
 $\Rightarrow \alpha_s = 40\text{dB}$ .

$$1. \omega_c = (\omega_p + \omega_s) / 2 = 0.4$$

$$2. \Delta\omega = \omega_s - \omega_p = 0.2\pi$$

Using Table 10.2 we see  $\alpha_s$  can be achieved by the three windows: Hann, Hamming, Blackman.

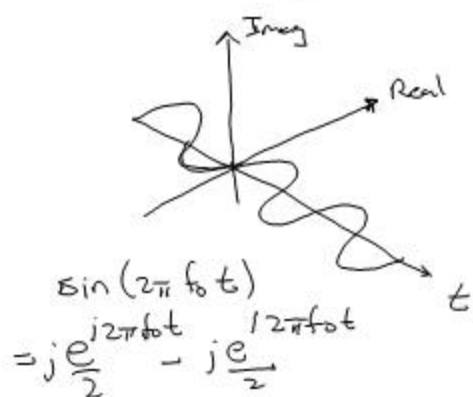
Lets use a Hann Window function.

$$M = \frac{3.11\pi}{0.2\pi} = 15.55 \approx 16$$

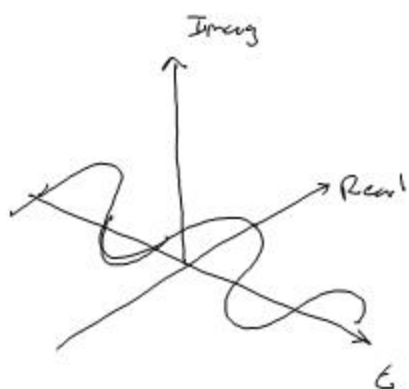
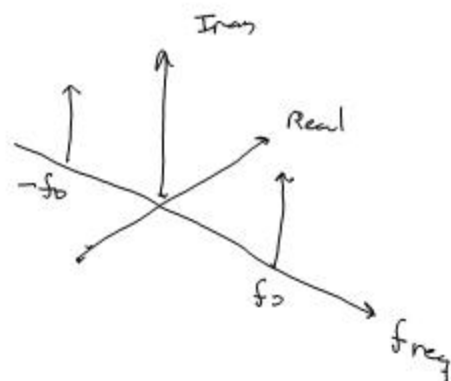
$$s.o., \quad N = 2M + 1 = 32$$

# Hilbert Transform

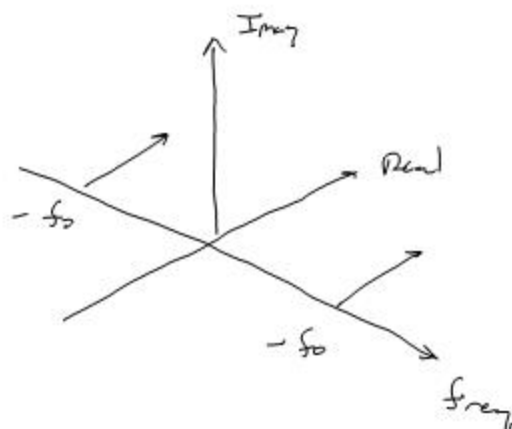
Complex Signals -



FT  
⇒

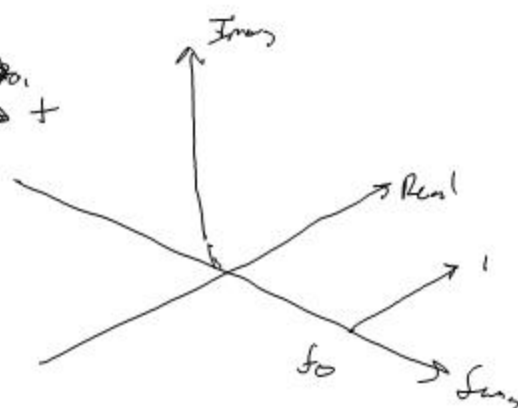
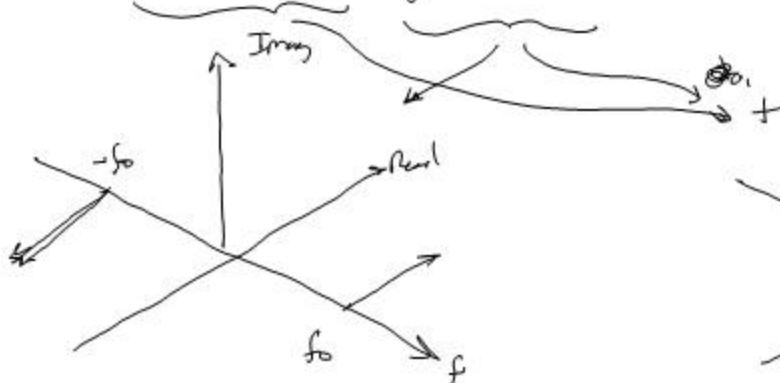


FT  
⇒



$$\cos(2\pi f_0 t) = \frac{e^{j2\pi f_0 t}}{2} + \frac{e^{-j2\pi f_0 t}}{2}$$

$$z(t) = \cos(2\pi f_0 t) + j \sin(2\pi f_0 t)$$

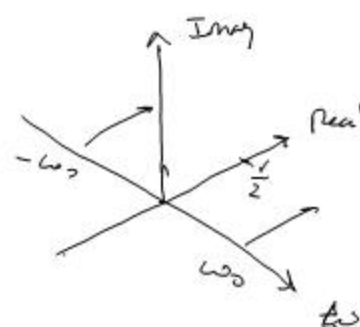


HT is process of changing real signals  $x_r(t)$  into a new real signal  $x_{HT}(t)$  where positive freq components are shifted in phase by  $+90^\circ$  and negative components are shifted in phase by  $-90^\circ$ .

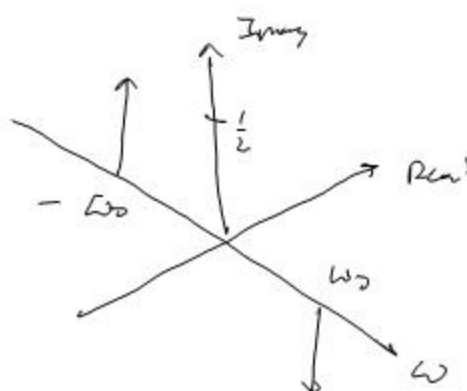
$$H_{HT}(e^{j\omega}) = \begin{cases} +j & -\pi < \omega < 0 \\ -j & 0 < \omega < \pi \end{cases}$$

$$X_{HT}(e^{j\omega}) = H_{HT}(e^{j\omega}) X_r(e^{j\omega})$$

Example  $X_r(t) = \cos(\omega_0 t)$



$$X_{HT}(t) = \sin(\omega_0 t)$$



Q: Why do we care?

Many applications in DSP are easier to implement for analytic signals.



$$x_c(t) = x_r(t) + j x_{\text{imag}}(t)$$

AM modulation -  $x_r(t)$  is amplitude modulated - envelope contains information.

$$E(t) = |x_c(t)| = \sqrt{x_r^2(t) + x_i^2(t)}$$

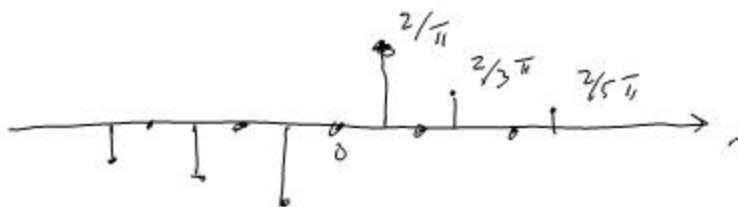
Instantaneous Phase -  $\phi(t) = \tan^{-1} \left( \frac{x_i(t)}{x_r(t)} \right)$

FM Demodulation.  $F(t) = \frac{d}{dt} \left\{ \tan^{-1} \left( \frac{x_i(t)}{x_r(t)} \right) \right\}$

HT filtering can make filtering easier.

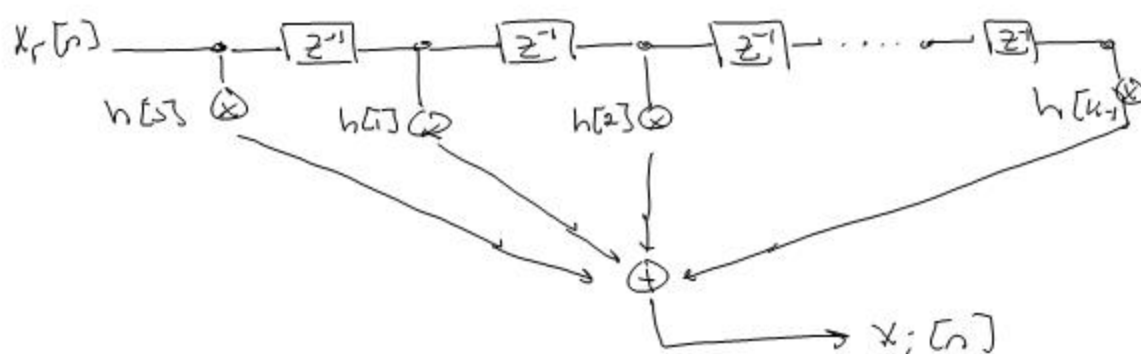
- HT impulse response

$$h[n] = \frac{1}{\pi n} (1 - \cos(\pi n)) = \frac{2 \sin^2(\pi n/2)}{\pi n} = \begin{cases} 0, & \text{even} \\ \frac{2}{\pi n}, & \text{odd} \end{cases}$$



- HT FIR Filter structure.

$$x_i[n] = \sum_{k=-\infty}^{\infty} h[k] x_r[n-k]$$



$h_{HT}[n]$ length $\rightarrow$	<u>odd (Type II)</u>	<u>Even (Type IV)</u>
	$ H(e^{j0})  = 0$	$ H(e^{j0})  = 0$
	$ H(e^{j\pi})  = 0$	no restriction

Note. Hard to design HT filter for low frequencies.

- Frequency Domain HT

1. Take  $N$ -point DFT of real, even length -  $N$  signal  $x_r[n]$  to get  $X_r[k]$  spectrum.
2. Set negative freqs. components to zero and scale positive freqs components by 2.
3. Inverse DFT to get  $x_c[n]$

Note: only works for block processing applications.