

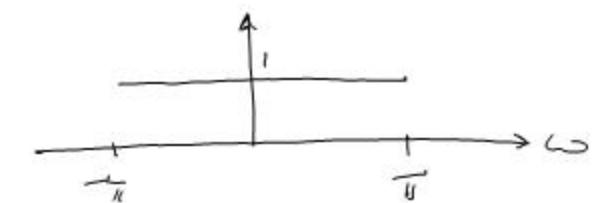
- Ideal LPF has real-valued frequency response.

$$H(e^{j\omega}) = |H(e^{j\omega})|, \quad \theta(\omega) = 0 \quad \text{"zero phase"}$$

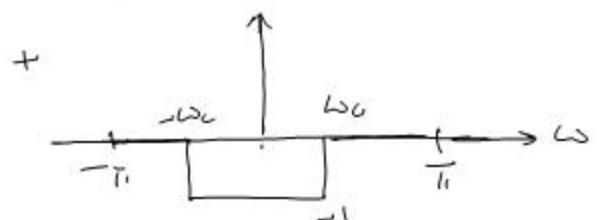
We can build piecewise-constant frequency responses by combining ideal responses.

Example: Highpass filter

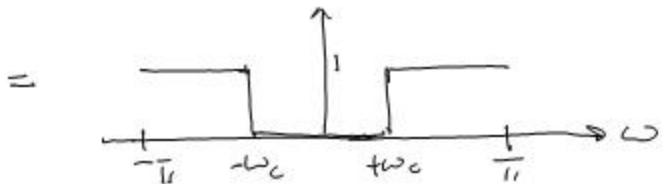
Allpass filter $\delta[n] \Rightarrow$



Lowpass filter $-h_{LP}[n]$



Highpass filter $h_{HP}[n]$



$$\text{Therefore, } h_{HP}[n] = \delta[n] - \frac{\sin(\omega_0 n)}{\pi n}$$

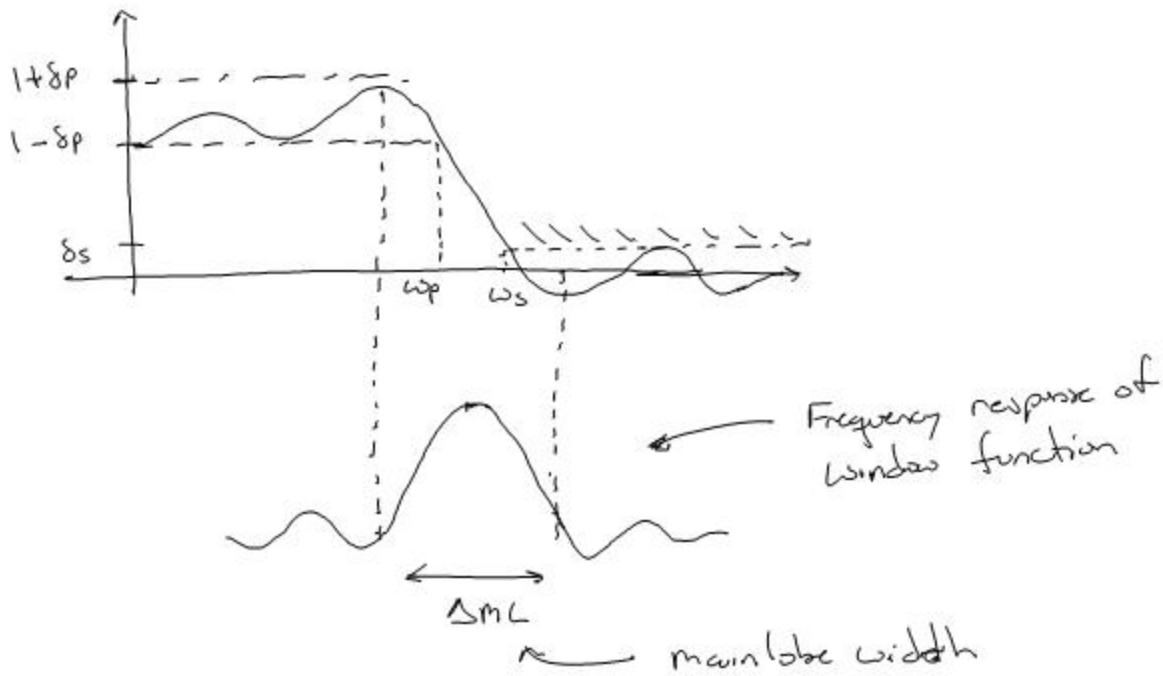
- FIR Filter order estimation (see 10-1.2)

Kaiser's Formula

Bellanger's Formula

Hermann's Formula

- Window function and filter magnitude response



Note: Smaller $\Delta\omega_L$ results in faster transition from ω_p to ω_s .

Reducing passband and stopband ripple requires area under window sidelobes to be smaller.

- Designing FIR filters by Windowing method

- 1- determine $\omega_c = (\omega_p + \omega_s) / 2$
- 2- Estimate M (e.g. $N=2m+1$)

$$\Delta\omega = (\omega_s - \omega_p) \times \frac{G}{M} \quad \text{from 10.2 table in book.}$$

Example: $\omega_p = 0.3\pi$ $\omega_s = 0.5\pi$

Stopband attenuation needs to be at least 40dB
 $\Rightarrow \alpha_s = 40 \text{ dB}$.

1. $\omega_c = (\omega_p + \omega_s)/2 = 0.4\pi$

2. $\Delta\omega = \omega_s - \omega_p = 0.2\pi$

Using Table 10.2 we see α_s can be achieved by
 the three windows: Hann, Hamming, Blackman.

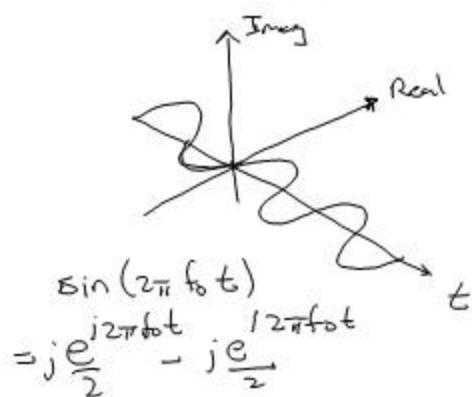
Let's use a Hann window function.

$$M = \frac{3.11\pi}{0.2\pi} = 15.55 \approx 16$$

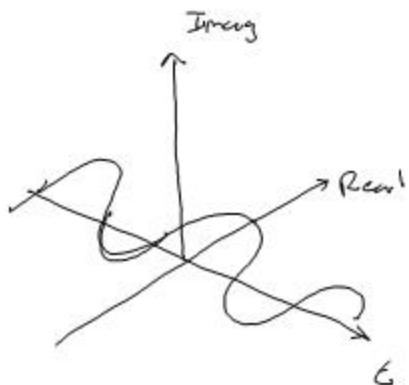
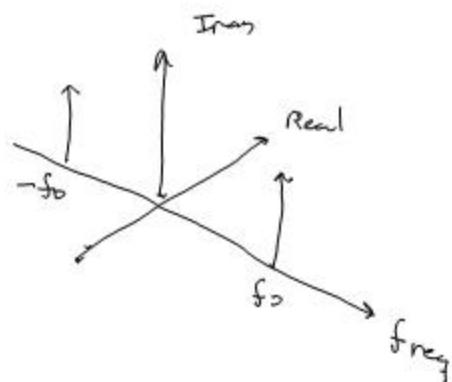
so, $n = 2M + 1 = 32$

- Hilbert Transform

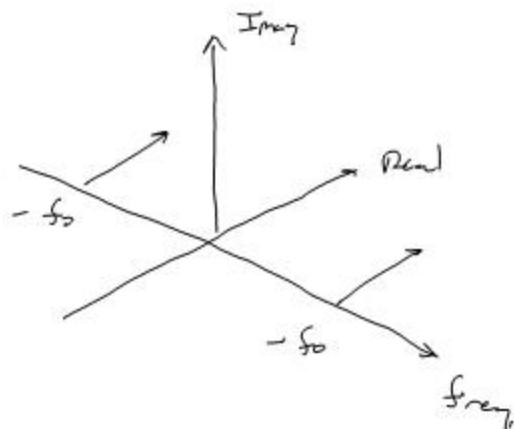
Complex Signals -



\Rightarrow
FT

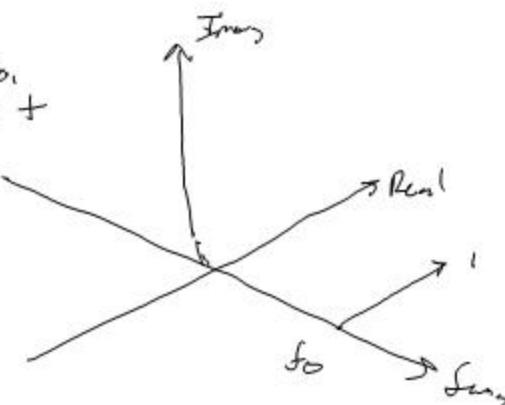
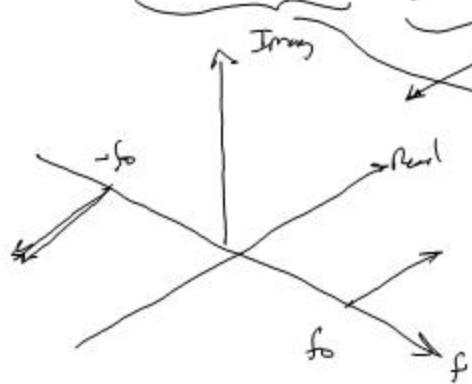


\Rightarrow
FT



$$\cos(2\pi f_0 t) = \frac{e^{j2\pi f_0 t}}{2} + \frac{e^{-j2\pi f_0 t}}{2}$$

$$z(t) = \underbrace{\cos(2\pi f_0 t)}_{-f_0} + j \underbrace{\sin(2\pi f_0 t)}_{f_0}$$

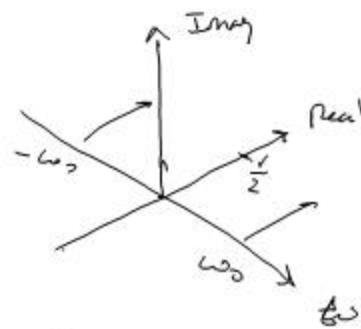


HT is process of changing real signals $x_r(t)$ into a new real signal $x_{HT}(t)$ where positive freq components are shifted in phase by +90° and negative components are shifted in phase by -90°.

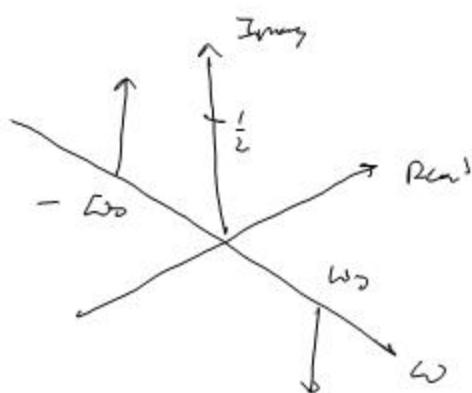
$$H_{HT}(e^{j\omega}) \begin{cases} +j & -\pi < \omega < 0 \\ -j & 0 < \omega < \pi \end{cases}$$

$$X_{HT}(e^{j\omega}) = H_{HT}(e^{j\omega}) X_r(e^{j\omega})$$

Example $x_r(t) = \cos(\omega t)$



$$x_{HT}(t) = \sin(\omega t)$$



Q: Why do we care?

Many applications in DSP are easier to implement for analytic signals.



$$x_c(t) = x_r(t) + j x_{\text{imag}}(t)$$

AM Modulation - $x_r(t)$ is amplitude modulated - envelope contains information.

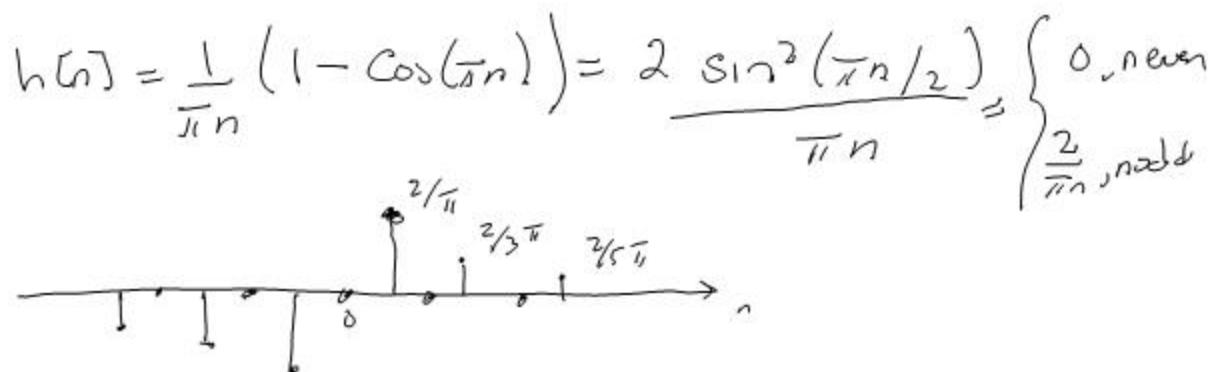
$$E(t) = |x_c(t)| = \sqrt{x_r^2(t) + x_i^2(t)}$$

Instantaneous Phase - $\theta(t) = \tan^{-1} \left(\frac{x_i(t)}{x_r(t)} \right)$

FM Demodulation . $F(t) = \frac{d}{dt} \left\{ \tan^{-1} \left(\frac{x_i(t)}{x_r(t)} \right) \right\}$

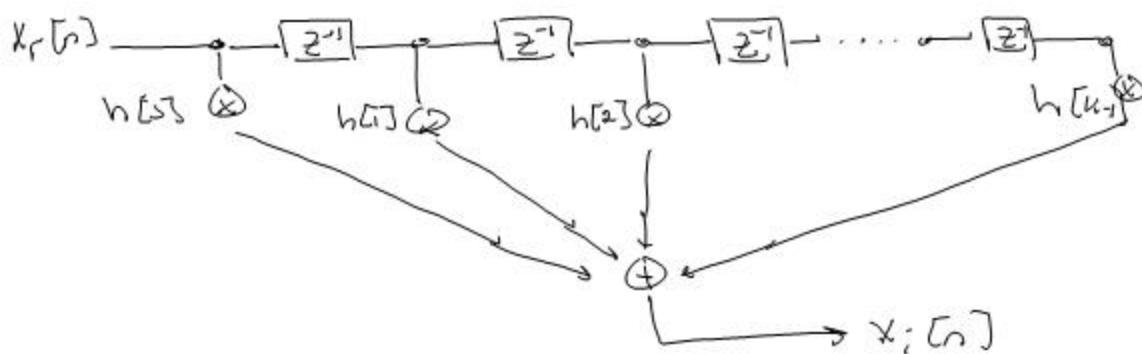
HT filtering can make filtering easier.

- HT impulse response



- HT FIR Filter structure.

$$x_i[n] = \sum_{k=-\infty}^{\infty} h[k] x_r[n-k]$$



$h_H[n]$ length	<u>odd (Type III)</u>	<u>Even (Type IV)</u>
	$ H(e^{j0}) = 0$	$ H(e^{j0}) = 0$
	$ H(e^{j\pi}) = 0$	no restriction

Note. Hard to design HT filter for low frequencies.

- Frequency Domain HT

- Take DFT of real, even length - n signal $x_r[n]$ to get $X_r[k]$ spectrum.
- Set negative freqs. components to zero and scale positive freqs components by 2.
- Inverse DFT to get $X_c[n]$

Note: only works for block processing applications.