

b. Adapt the Control based on Computed Torque Method

$$\text{Robot Model: } \ddot{\tau} = m(\theta) \ddot{\theta} + v(\theta, \dot{\theta}) + g(\theta) = Y(\theta, \dot{\theta}, \ddot{\theta}) \cdot \varphi$$

$$\text{Computed Torque Method: } \ddot{\tau} = \alpha \ddot{\tau}' + \beta$$

$$\Rightarrow \ddot{\tau} = m(\theta) \ddot{\theta}^* + v(\theta, \dot{\theta}) + g(\theta) \quad (\text{C.T.M.})$$

where the servo control part is

$$\ddot{\tau}' = \ddot{\theta}^* = \ddot{\theta}_d + K_v \dot{E} + K_p E \quad \text{where } E = \theta_d - \theta$$

If the robot dynamic model is NOT precisely known, then the computed torque method gives the control law:

$$\ddot{\tau} = \hat{m}(\theta) \ddot{\theta}^* + \hat{v}(\theta, \dot{\theta}) + \hat{g}(\theta) = Y(\theta, \dot{\theta}, \ddot{\theta}) \hat{\varphi}$$

$$\text{where } \ddot{\theta}^* = \ddot{\theta}_d + K_v \dot{E} + K_p E \text{ with } E = \theta_d - \theta$$

and $(\hat{\cdot})$ is an estimate (model) of (\cdot) .

Now we can write the above control law as:

$$\begin{aligned} \ddot{\tau} &= \hat{m}(\theta) [\ddot{\theta}_d + K_v \dot{E} + K_p E] + \hat{v}(\theta, \dot{\theta}) + \hat{g}(\theta) \\ &= \hat{m}(\theta) [\ddot{\theta} + K_v \dot{E} + K_p E] + \hat{m}(\theta) \ddot{\theta}^* + \hat{v}(\theta, \dot{\theta}) + \hat{g}(\theta) \\ &= \hat{m}(\theta) [\ddot{\theta} + K_v \dot{E} + K_p E] + Y(\theta, \dot{\theta}, \ddot{\theta}) \hat{\varphi} \end{aligned}$$

Then the error dynamics is

$$Y(\theta, \dot{\theta}, \ddot{\theta}) \varphi = \hat{m}(\theta) [\ddot{\theta} + K_v \dot{E} + K_p E] + Y(\theta, \dot{\theta}, \ddot{\theta}) \hat{\varphi}$$

Model + Control = Error Dynamics

$$\Rightarrow \hat{m}(\theta) [\ddot{\theta} + K_v \dot{E} + K_p E] = Y(\theta, \dot{\theta}, \ddot{\theta}) (\varphi - \hat{\varphi})$$

$$= Y(\theta, \dot{\theta}, \ddot{\theta}) \hat{\varphi} \quad \hat{\varphi} = \hat{\varphi}$$

Multiply $\hat{m}^{-1}(\theta)$ from left side on both sides of above eqn.

$$\ddot{\theta} + K_v \dot{E} + K_p E = \hat{m}^{-1}(\theta) \cdot Y(\theta, \dot{\theta}, \ddot{\theta}) \hat{\varphi} \quad (*)$$

If $\hat{\varphi} = \varphi$ (dynamic model is precisely known), $\hat{\varphi} = 0$, then eqn. (*) becomes

$$\ddot{\theta} + K_v \dot{E} + K_p E = 0 \quad (\text{computed torque method})$$

Now since $\hat{\varphi} \neq \varphi$, since dynamic model is NOT precisely known, then we have to find a new approach.

$$\text{Define } \tilde{\theta} = \begin{bmatrix} \theta \\ \dot{\theta} \\ \ddot{\theta} \end{bmatrix}_{2n \times 1} \text{ and } \mathbf{B} = \begin{bmatrix} 0_n \\ I_n \\ 0_n \end{bmatrix}_{2n \times n} \quad \begin{cases} \text{State} \\ \text{Space} \\ \text{Approach} \end{cases}$$

$$\text{and } \mathbf{A} = \begin{bmatrix} 0_n & I_n \\ -K_p & -K_v \end{bmatrix}_{n \times n}$$

Then we can rewrite (*) in state space as follows:

$$\tilde{\theta} = \mathbf{A} \tilde{\theta} + \mathbf{B} \hat{m}^{-1}(\theta) \cdot Y(\theta, \dot{\theta}, \ddot{\theta}) \hat{\varphi}$$

Error dynamic equation in state space

Apply Lyapunov stability analysis to show that this error vector \bar{E} is asymptotically stable.

Select the Lyapunov function candidate as:

$$\dot{V}(x) = \underbrace{\bar{E}^T P \bar{E}}_{\substack{2n \times 2n \\ 2n \times 2n \\ 2n \times 1}} + \underbrace{\dot{\varphi}^T \Pi \dot{\varphi}}_{\substack{n \times n \\ r \times r \\ r \times 1}} > 0 \text{ except } V(0)=0.$$

where P is a $2n \times 2n$ positive definite, constant, symmetric matrix and Π is a diagonal, positive definite $r \times r$ matrix (constant). That is Π can be written as

$$\Pi = \begin{bmatrix} \gamma_1 & & & \\ & \gamma_2 & & \\ & & \ddots & \\ & & & \gamma_r \end{bmatrix}_{r \times r} = \text{diag}(\gamma_1, \gamma_2, \dots, \gamma_r)$$

where γ_i 's are positive scalar constants.

$$\text{Then } \dot{V} = \dot{\bar{E}}^T P \bar{E} + \bar{E}^T P \dot{\bar{E}} + \dot{\varphi}^T \Pi^{-1} \dot{\varphi} + \dot{\varphi}^T \Pi^{-1} \dot{\varphi}$$

$$\Rightarrow \dot{V} = [A\bar{E} + B\hat{m}^{-1}y\hat{\varphi}]^T P \bar{E} + \bar{E}^T P [A\bar{E} + B\hat{m}^{-1}y\hat{\varphi}] + 2\dot{\varphi}^T \Pi^{-1} \dot{\varphi}$$

$$\Rightarrow \dot{V} = -\bar{E}^T Q \bar{E} + 2\dot{\varphi}^T \Pi^{-1} \dot{\varphi} + \dot{\varphi}^T \Pi^{-1} B^T P \bar{E} \quad (*)$$

where Q is a positive definite, symmetric matrix that satisfies the Lyapunov equation:

$$A^T P + P A = -Q \quad 2n \times 2n$$

If we want $\dot{V} = -\bar{E}^T Q \bar{E} < 0, V(0) = 0$

$$\text{then } 2\dot{\varphi}^T [\Pi^{-1} \dot{\varphi} + \dot{\varphi}^T \hat{m}^{-1} B^T P \bar{E}] = 0$$

$$\Rightarrow \Pi^{-1} \dot{\varphi} + \dot{\varphi}^T \hat{m}^{-1} B^T P \bar{E} = 0 \quad \checkmark$$

$$\Rightarrow \dot{\varphi} = -\Pi \cdot \dot{\varphi}^T \hat{m}^{-1} B^T P \bar{E}$$

$$\text{Let } \dot{\varphi} \underset{t \rightarrow \infty}{\approx} \frac{\hat{\varphi}(t+\Delta t) - \hat{\varphi}(t)}{\Delta t} = -\Pi \cdot \dot{\varphi}^T \hat{m}^{-1} B^T P \bar{E}$$

$$\Rightarrow \dot{\varphi}(t+\Delta t) = \dot{\varphi}(t) - \Pi \cdot \dot{\varphi}^T \hat{m}^{-1} B^T P \bar{E} \cdot \Delta t$$

If we update (identify) $\dot{\varphi}$ using

$$\dot{\varphi}_{\text{new}} = \dot{\varphi}_{\text{old}} - \Pi \cdot \dot{\varphi}^T \hat{m}^{-1} B^T P \bar{E} \cdot \Delta t$$

as the adaptation law, then

$$\dot{V} = -\bar{E}^T Q \bar{E} < 0, V(0) = 0$$

$$\Rightarrow \bar{E} \xrightarrow{t \rightarrow \infty} 0 \Rightarrow \dot{\bar{E}} \xrightarrow{t \rightarrow \infty} 0$$

The system is asymptotically stable, if we use the

following adaptive control law:

$$\ddot{\tau} = \hat{m}(\theta) \cdot \ddot{\theta}^* + \hat{v}(\theta, \dot{\theta}) + \hat{g}(\theta) = Y(\theta, \dot{\theta}, \ddot{\theta}) \hat{\psi}$$

+ and the following dynamic parameter adaptation law:

$$\dot{\hat{\psi}} = -\Gamma Y^T(\theta, \dot{\theta}, \ddot{\theta}) \hat{m}'(\theta) B^T P \bar{E}$$

which we can use to update/identify $\hat{\psi}$, the dynamic parameter vector \Rightarrow true parameters.

Conclusion: This makes it possible that we can use adaptive control based on the Computed Torque Method to stabilize the robot system and at the same time to estimate/update/identify the robot dynamic parameters simultaneously.

J. Dynamic Simulation/Animation

Problem: Given control τ , how the robot moves?

The model: $m(\theta) \ddot{\theta} + v(\theta, \dot{\theta}) + g(\theta) = \tau$ (***)

For simulation/animation, we need to know that under the control τ , what are θ , $\dot{\theta}$, $\ddot{\theta}$?

Let's rewrite eqn. (***)

$$\ddot{\theta} = \hat{m}'(\theta) [\tau - v(\theta, \dot{\theta}) - g(\theta)] \quad (*)-1$$

This is the acceleration caused by the control τ . We may use the acceleration to calculate the velocity and position as follows:

Given the initial conditions on the motion of the robot:

$\theta(0) = \theta_0$, $\dot{\theta}(0) = \dot{\theta}_0$. (let $\ddot{\theta}_0 = \ddot{\theta}_0 = 0$, we then numerically integrate (*)-1 forward in time by steps of size Δt using Euler integration, start with $t=0$, iteratively compute as follows:

$$\dot{\theta}(t+\Delta t) = \dot{\theta}(t) + \ddot{\theta}(t) \cdot \Delta t \quad (*)-2$$

$$\theta(t+\Delta t) = \theta(t) + \dot{\theta}(t) \cdot \Delta t + \frac{1}{2} \ddot{\theta}(t) \cdot \Delta t \quad (*)-3$$

Eqsns (*)-1 to (*)-3 numerically compute the acceleration $\ddot{\theta}$, velocity $\dot{\theta}$ and position θ of the robot dynamic motion caused by a control input vector τ .

Review:

- 1° Introduction & basic concepts.
- 2° Space description and transformation
Kinematics, inverse kinematics (two special approaches)
- 3° Jacobians: Singularities and workspace
- 4° Dynamics:
 - Lagrangian dynamics formulation
 - Different representations of dynamic formula
 - Regressor formulation
- 5° Linear & Feedback Control: Linear 2nd-order System
- 6° Nonlinear & Adaptive Control:
 - Computed Torque Method,
 - Lyapunov stability theory, adaptive control