

# Supplementary Information

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## 1 Asteroseismic Model

In order to extract signatures of stellar rotation from the asteroseismic p mode frequencies, we built a model that simultaneously treats the convective background ( $B(\nu)$ ), the oscillations ( $O(\nu)$ ), and the white noise ( $W$ ), where  $\nu$  is frequency [1]. Our data, observed with *Kepler*, are also subject to the apodization (attenuation) of signals in the frequency-domain, where we fit our model [2]. The apodization in power is given by

$$\eta^2(\nu) = \text{sinc}^2\left(\frac{\pi}{2} \frac{\nu}{\nu_{\text{nyq}}}\right), \quad (1)$$

where  $\nu_{\text{nyq}}$  is the Nyquist frequency for the *Kepler* short cadence, which was treated as a free parameter in our model to account for gaps in the data. Apodization only affects signals with characteristic timescales, meaning that it does not affect the white noise level, only the oscillations and convective background components. Given the above, our comprehensive model for the power spectrum is

$$M(\nu) = W + \eta^2(\nu)[O(\nu) + B(\nu)]. \quad (2)$$

### 1.1 Convective Background ( $B(\nu)$ )

To model the convective background we used three Harvey components [3], which express the background in power as Lorentzian-like functions centered on zero frequency. The Harvey components take the form

$$H(\nu, a, b, x) = \frac{4a^2/b}{1 + (2\pi b\nu)^x}, \quad (3)$$

where  $a$  and  $b$  are the free parameters in our model, and  $x$  is fixed. The three Harvey components together form our background function as

$$B(\nu) = H(\nu, a, b, x = 4) + H(\nu, c, d, x = 4) + H(\nu, j, k, x = 2), \quad (4)$$

where we have labeled parameters for the separate components. The  $x = 2$  term here contributes to the background at high frequencies, whereas the  $x = 4$  terms contribute the background at low frequencies.

## 1.2 Modes of Oscillation ( $O(\nu)$ )

Modes of oscillation appear in the power spectrum as Lorentzian peaks [4]. These peaks can be described by three values: the radial order ( $n$ , the overtone number of the oscillation), the angular degree ( $\ell$ ) and the azimuthal order ( $m$ ). Due to stellar rotation, each mode with an angular degree of  $\ell > 0$  is split into its  $(2\ell + 1)$  Lorentzian components, labeled by  $m$ . For all  $\ell = (0, 1, 2)$  modes identified for our targets in the ‘Kages’ and LEGACY studies [5, 6] we add a (set of) Lorentzian(s) to our model, building a composite model representing all visible modes. The construction of our oscillation model takes the form

$$O(\nu) = \sum_n \sum_\ell \sum_{m=-\ell}^{\ell} \frac{H_{n,\ell,m}}{1 + \frac{4}{\Gamma_{n,\ell}^2}(\nu - \nu_{n,\ell,m})^2}, \quad (5)$$

where  $H_{n,\ell,m}$  is the height of the mode,  $\Gamma_{n,\ell}$  is the linewidth of the mode (approximated to be equal for all split azimuthal orders at a single  $n$  and  $\ell$ ) and  $\nu_{n,\ell,m}$  is the frequency of the mode. The range of  $n$  differs per star depending on how many radial orders were reported in LEGACY or Kages, and the range of  $\ell$  depends on how many angular degrees were reported for the corresponding radial order.

### 1.2.1 Mode Frequencies and Rotational Splitting ( $\nu_{n,\ell,m}$ )

The mode frequencies of main sequence stars are described by the asymptotic expression [7, 8]. The asymptotic expression defines the locations of the modes as regularly spaced, with structured deviation around  $\nu_{\max}$ , the frequency of maximum oscillation amplitude. The expression takes the form

$$\nu_{n,\ell,m} = \Delta\nu \left( n + \epsilon + \delta\nu_{0\ell} + \frac{\alpha}{2} \left( n - \frac{\nu_{\max}}{\Delta\nu} + \epsilon \right)^2 \right) + m\nu_s, \quad (6)$$

where  $\Delta\nu$  is the large frequency separation between two consecutive radial orders  $n$ ,  $\epsilon$  is a phase offset,  $\delta\nu_{0\ell}$  is the small frequency separation between two oscillation modes of different  $\ell$  at the same radial order,  $\alpha$  describes the curvature of the spacing around  $\nu_{\max}$ , and  $\nu_s$  is the rotational splitting. Note that here we have expressed the small separation  $\delta\nu_{0\ell}$  as a fraction of  $\Delta\nu$ . In order to improve the computational efficiency of this analysis, we fixed  $\Delta\nu$  to the values reported in LEGACY and Kages.

Instead of calculating mode frequencies directly from Equation 6 for the model, we treated the individual mode frequencies as parameters as well, drawn from Equation 6. This is called a ‘latent parameter’ implementation [9, 10], as it forms a step between the parameters we

want to draw inference on (also called hyperparameters) and our data. The parameters  $\nu_{n,\ell,m}$  were allowed to vary within an uncertainty  $\sigma_\ell$ , which has a single value for each angular degree and also varied as a free parameter. This allowed us to account for small shifts in frequency due to sudden changes in the stellar structure [11].

The mode frequency latent parameters were drawn from a normal distribution using Equation 6 as its mean function, as

$$\nu_{n,\ell,m} \sim \mathcal{N}(\nu_{n,\ell,m}, \sigma_\ell), \quad (7)$$

where the expression  $\nu_{n,\ell,m}$  on the right hand side represents the contents of Equation 6, and  $\mathcal{N}$  represents a normal distribution with a mean equal to  $\nu_{n,\ell,m}$  and a standard deviation equal to  $\sigma_\ell$ . The symbol ‘ $\sim$ ’ indicates that the parameters on the left hand side of the equation are drawn from the probability distribution on the right hand side. This notation will be used throughout this work.

### 1.2.2 Mode Linewidth ( $\Gamma_{n,\ell}$ )

The linewidths of asteroseismic p modes vary roughly as a function of mode frequency, and do so slowly relative to  $\Delta\nu$ . This can be expressed as an empirical relation [6, 12, 13]. However, this relation has six free parameters, none of which are directly relevant to this work. Instead of fitting this relation, we chose to employ a more flexible Gaussian Process [14, GP] to act as a prior on the linewidths. This can be considered as us modelling the linewidths as correlated measurements, effectively loosely constraining how linewidth varies with frequency.

A GP is defined by a covariance kernel (describing the degree of correlation between linewidths) and a mean function (describing a global trend with frequency). As this approach describes the mode linewidths relative to one another in frequency, the radial orders of each target  $n$  were rescaled to be between 0 (for the lowest  $n$ ) and 1 (for the highest  $n$ ). The radial orders of  $\ell = 2$  modes were increased by 1 to ensure this approximation applied to all modes. This approximation was used to describe the change in linewidth as a function of frequency without depending on the exact frequencies of the modes, which themselves were free parameters (see above). Given this, we defined our GP covariance kernel as a Squared Exponential Kernel to capture the slight periodicity of linewidth with frequency, as

$$K_{i,j} = \rho^2 \exp \left[ -\frac{(n_{f,i} - n_{f,j})^2}{2L^2} \right], \quad (8)$$

where  $n_f$  is the fractional radial order of a given mode and  $K_{i,j}$  represents an element of the covariance matrix  $\underline{K}$ , describing the covariance between two values of linewidth at different fractional radial orders. The GP kernel has two hyperparameters:  $\rho$ , which determines the spread of the kernel in linewidth, and  $L$ , which determines the length scale in terms of  $n_f$ . The length scale  $L$  was significantly larger than the large frequency separation ( $\Delta\nu$ ) in all cases, and so we considered the use of fractional radial orders a valid approximation in this model.

A linear function was used for the mean of the GP, as

$$\mu = m \times n_f + c, \quad (9)$$

where  $m$  and  $c$  are the slope and intercept of the line. The linewidth latent parameters were then drawn from the multivariate probability distribution

$$\Gamma \sim \mathcal{N}(\mu, \underline{K}), \quad (10)$$

where  $\Gamma$  represents the linewidths of all the modes in the model. The parameters  $m$ ,  $c$  and  $\rho$  were marginalised over, whereas  $L$  was fixed to a pre-determined value.

### 1.2.3 Mode Heights and Angle of Inclination ( $H_{n,\ell,m}$ )

The height in power of each mode,  $H_{n,\ell,m}$ , varies not only as a function of distance in frequency from  $\nu_{\max}$ , but also due to observation conditions, such as inclination angle and passband. In our model, we treated  $H_{n,\ell,m}$  as a deterministic parameter, as

$$H_{n,\ell,m} = \varepsilon_{\ell,m}(i) \frac{2(A_{n,\ell})^2}{\pi \Gamma_{n,\ell}}, \quad (11)$$

where  $\varepsilon_{\ell,m}(i)$  modulates the height as a function of inclination angle  $i$  (see below), and  $A_{n,\ell}$  and  $\Gamma_{n,\ell}$  are the mode amplitude and linewidth respectively for a given radial order and angular degree. Instead of modeling and modulating height directly, we instead sampled in amplitude and linewidth. This approach mitigates the correlations between height and linewidth in the sampling process [15].

As done above for the mode frequencies and linewidths, the mode amplitudes  $A_{n,\ell}$  were also treated as latent parameters drawn from a probability distribution governed by hyperparameters. For this, we used a Gaussian function  $G(\nu)$ , centered on  $\nu_{\max}$ , as

$$G(\nu) = A \times \exp \left[ -\frac{(\nu - \nu_{\max})^2}{2w^2} \right], \quad (12)$$

where  $A$  is the modes' amplitude at  $\nu_{\max}$ , and  $w$  is the width of the Gaussian, both free parameters in our model. The mode amplitude latent parameters were then drawn from the probability distribution

$$A_{n,\ell} \sim \mathcal{N}(G(\nu_{n,\ell}) \times V_\ell, \sigma_A), \quad (13)$$

where  $V_\ell$  is a free parameter for the mode visibility of different angular degrees, which should be consistent for all *Kepler* observations. These parameters describe the difference in relative height between modes of different radial order. The mode visibility for  $V_0$  is fixed at 1, and  $V_{1,2}$  are treated as free parameters. The parameter  $\sigma_A$ , the uncertainty on the distribution, is also a free parameter, and takes the same value for all amplitudes regardless of angular degree.

The angle of inclination of a star with respect to Earth changes the net perturbation by a given mode when integrated across the stellar disc, changing the amplitudes of modes of different azimuthal orders. This is a geometric problem, and is expressed by  $\varepsilon_{\ell,m}(i)$ , which takes the form [16]

$$\varepsilon_{\ell,m}(i) = \frac{(\ell - |m|)!}{(\ell + |m|)!} \left[ P_\ell^{|m|}(\cos(i)) \right]^2, \quad (14)$$

where  $P_\ell^{[m]}$  are associated Legendre functions. For the first three angular degrees, Equation 14 takes the form [17]

$$\begin{aligned}
\varepsilon_{0,0}(i) &= 1, \\
\varepsilon_{1,0}(i) &= \cos^2(i), \\
\varepsilon_{1,\pm 1}(i) &= \frac{1}{2} \sin^2(i), \\
\varepsilon_{2,0}(i) &= \frac{1}{4} (3 \cos^2(i) - 1)^2, \\
\varepsilon_{2,\pm 1}(i) &= \frac{3}{8} \sin^2(2i), \\
\varepsilon_{2,\pm 2}(i) &= \frac{3}{8} \sin^4(i),
\end{aligned} \tag{15}$$

where the sum of available components for a single  $\ell$  are normalized to one.

### 1.3 Likelihood Function for $M(\nu)$

If data have Gaussian noise in the time domain, they will appear in the frequency domain with noise following a  $\chi^2$  distribution with two degrees of freedom [18,  $\chi_2^2$  hereafter]. The noise properties of  $\chi_2^2$  distributed data are multiplicative, and require a specific treatment when fitting a model. As our frequency bins can be approximated to be independent, we used the likelihood function [19],

$$\ln p(\mathcal{P}|M(\nu)) = \sum_{j=0}^{N-1} \left[ \ln[M_j(\nu)] + \frac{\mathcal{P}_j}{M_j(\nu)} \right], \tag{16}$$

where  $\mathcal{P}$  is the power spectral density (and thus our data), and  $M(\nu)$  represents our model. The subscript  $j$  denotes an individual datum, for a total of  $N$  data. We have omitted the dependence of the model  $M(\nu)$  on its parameters, for clarity. This equation is functionally equivalent to the evaluation of a gamma distribution of the form  $\gamma(\mathcal{P}|1, \beta)$ , where  $\beta = 1/M(\nu)$ , which is the implementation we used in the sampling process.

## 1.4 Model preparation and hyperparameter priors

### 1.4.1 Fitting the convective background

Fitting the convective background, apodization and white noise component must be done for the full range of the power spectrum in order to be accurately constrained. However, fitting a single model to the full range of frequencies is computationally inefficient when we are interested in the modes of oscillation, as these occupy a relatively small range of frequencies.

In order to speed up this process, the background was first fit independently to a subset of our data for each star. This subset was created by removing all frequencies within a range  $0.1 \times \Delta\nu$  below and above the minimum and maximum mode frequencies reported in LEGACY and Kages. For KIC 3427720 we also removed frequencies in the range  $90 \mu\text{Hz} < \nu < 400 \mu\text{Hz}$ , where there were large peaks not of asteroseismic origin, skewing the background fit.

For each star the model function (see Eq. 2) was fit, as

$$M_B(\nu) = W + \eta^2(\nu)B(\nu), \quad (17)$$

where  $B(\nu)$  is the background model described in Equation 4. The parameter components of our background fit are then  $\phi_B = \{\log(a), \log(b), \log(c), \log(d), \log(j), \log(k), W, \nu_{\text{nyq}}\}$ , where the parameters of the Harvey components were sampled in log space. The model was fit to the background data using PyStan [20], run for 10,000 iterations on each star.

### 1.4.2 Obtaining First Guesses and Prior Values

In order to utilise some of the prior measurements of our targets without using them as hard constraints on our parameters, some of our model equations were fit to LEGACY and ‘Kages’ data to obtain first guesses and mean values on hyperparameter priors.

For first guesses for parameters in the asymptotic expression, we fit Equation 6, *not* including the rotational component  $m\nu_s$ , to the  $\ell = (0, 1, 2)$  mode frequencies reported in LEGACY and ‘Kages’ for each star, using their reported uncertainties. This yielded estimates of  $\hat{\epsilon}$ ,  $\hat{\delta\nu}_{01}$ ,  $\hat{\delta\nu}_{02}$  and  $\hat{\alpha}$ , where the hat symbol ‘ $\hat{\phantom{x}}$ ’ indicates a prior value (e.g.  $\hat{\nu}_{\text{max}}$  is taken from LEGACY or ‘Kages’). While not precise, as we did not mitigate any perturbations due to acoustic glitches, these rough results act as functional first guesses and prior mean values. The relation was fit to each star using PyMC3 [21] using 5000 iterations on 4 chains.

To obtain first guesses for the parameters used to set the GP prior on linewidth, we fit a GP constructed as in Equation 10 to the linewidths of the  $\ell = 0$  modes reported in LEGACY. Linewidths were not reported for the other angular degrees in LEGACY, but the estimates may be generalised to other  $\ell$ , as linewidth is a strong function of frequency. The relation was fit to each star using PyMC3 using 2500 iterations on 4 chains.

Fitting the LEGACY linewidths yielded rough estimates of  $\hat{m}$ ,  $\hat{c}$ ,  $\hat{\rho}$  and  $L$  for each star. As is noted in Equation 10,  $L$  was fixed to this fit value when fitting our full model to our data. For stars in ‘Kages’, for which no linewidths were reported, we instead fixed these prior values to  $\hat{m} = 1$ ,  $\hat{c} = 0.5$ ,  $\hat{\rho} = 0.1$ , and the length scale to  $L = 0.3$ . These values were chosen to reflect those found for the LEGACY stars.

Finally, we obtained prior values for the Gaussian function describing the distribution of mode amplitudes around  $\nu_{\text{max}}$  (Eq. 12). The mode amplitude of the highest peak in the spectrum was used for  $\hat{A}$ , which was typically at or near  $\nu_{\text{max}}$ . For the width of the Gaussian we used the empirical function [6]

$$\hat{w} = 0.25 \times \hat{\nu}_{\text{max}}, \quad (18)$$

For the mode visibilities, we used  $\hat{V}_1 = 1.2$  and  $\hat{V}_2 = 0.7$ , which reflect the results for these parameters reported in the LEGACY catalogue.

### 1.4.3 Priors on our Hyperparameters

Given our first guesses and measured prior values, we can define the prior probabilities of the hyperparameters on which our model depends. For the mode frequency hyperparameters (Eq. 6), these are

$$\begin{aligned}
\nu_{\max} &\sim \mathcal{N}(\hat{\nu}_{\max}, 10), \\
\epsilon &\sim \mathcal{N}(\hat{\epsilon}, 1), \\
\alpha &\sim \ln \mathcal{N}(\ln(\hat{\alpha}), 0.01), \\
\delta\nu_{01} &\sim \ln \mathcal{N}(\ln(\widehat{\delta\nu_{01}}), 0.1), \\
\delta\nu_{02} &\sim \ln \mathcal{N}(\ln(\widehat{\delta\nu_{02}}), 0.1), \\
\sigma_{0,1,2} &\sim \mathcal{C}_{1/2}(\beta = 2),
\end{aligned} \tag{19}$$

where  $\ln \mathcal{N}$  represents a log-Normal distribution and  $\mathcal{C}_{1/2}$  represents a half-Cauchy distribution. The half-Cauchy distribution ensures the standard deviations do not inflate to large numbers, and is generally well-behaved close to zero in the case of stars with little deviation from Eq. 6 [22]. Other symbols are as described above. All three hyperparameters  $\sigma_{0,1,2}$  describing the uncertainty on the latent parameters of different angular degree were subject to the same prior.

For the mode linewidths (Eq. 8 and 9), our hyperparameter priors took the form

$$\begin{aligned}
m &\sim \mathcal{N}(\hat{m}, 1), \\
c &\sim \mathcal{N}(\hat{c}, 1), \\
\rho &\sim \ln \mathcal{N}(\ln(\hat{\rho}), 0.1),
\end{aligned} \tag{20}$$

where the conventions are the same as above. For our mode amplitudes (Eq. 12 and 13), they took the form

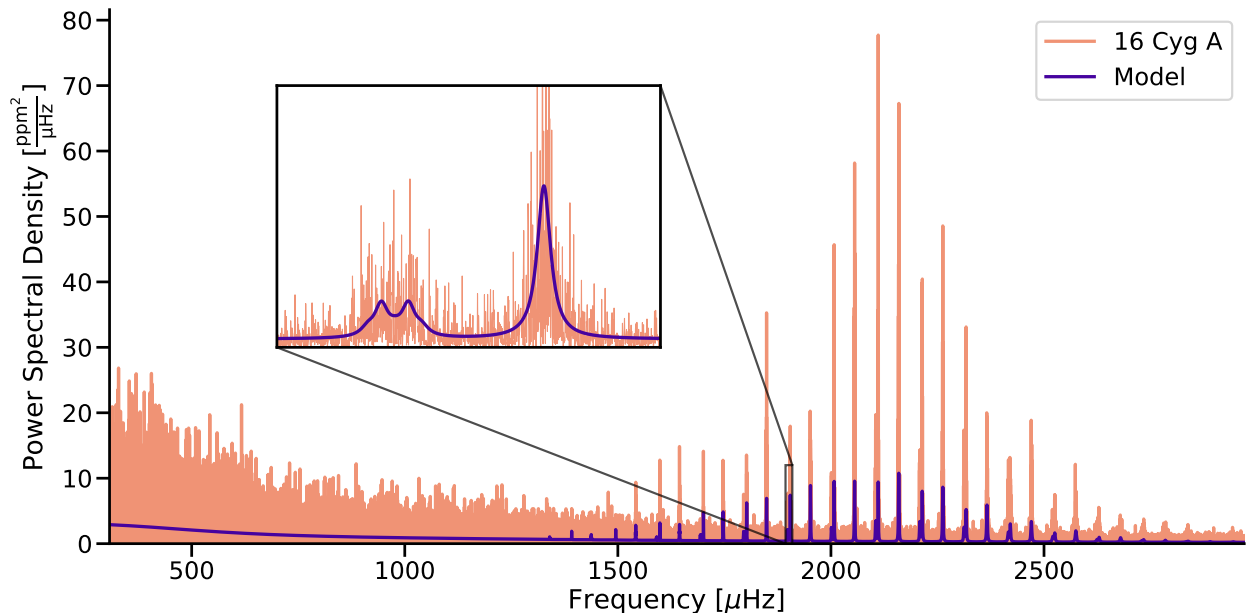
$$\begin{aligned}
w &\sim \ln \mathcal{N}(\ln(\hat{w}), 10), \\
A &\sim \ln \mathcal{N}(\ln(\hat{A}), 1), \\
V_1 &\sim \ln \mathcal{N}(\ln(\hat{V}_1), 0.1), \\
V_2 &\sim \ln \mathcal{N}(\ln(\hat{V}_2), 0.1), \\
\sigma_A &\sim \mathcal{C}_{1/2}(\beta = 1).
\end{aligned} \tag{21}$$

As the convective background had already been fit to our data excluding the region where the modes are present, the results from that fit could be used as extremely informative priors on our fit to the region containing the modes, where there is little information present to constrain the background. To do so, we modeled the background parameters  $\phi_B$  in our full model as being drawn from a multivariate normal distribution as

$$\phi_B \sim \mathcal{N}(\hat{\phi}_B, \underline{\Sigma}_{\hat{\phi}_B}), \tag{22}$$

where  $\hat{\phi}_B$  are the median values of our posterior distributions from our prior background fit, and  $\underline{\Sigma}_{\hat{\phi}_B}$  is the full covariance matrix of all the posterior distributions from our prior background fit, taking into account the correlations between the different Harvey components.

Finally, we defined the priors on the rotational parameters: the mode splitting ( $\nu_s$ ), and the inclination angle ( $i$ ). In order to give these an appropriate treatment, we made two



Supplementary Figure 1: A power spectrum constructed from four years of *Kepler* observations of 16 Cyg A (KIC 12069424). Plotted over the top is the model resulting from the fit to the data described in this work. The model implements both the mode frequencies, seen on the right hand side of the plot, and the convective background, the effects of which are seen on the left. Low frequencies have been cropped out for clarity. *Inset*: A zoom in on a radial (right) and quadrupole (left) ( $\ell = 0, 2$ ) pair of modes. The quadrupole mode is split into five components by the star’s rotation. Due to the star’s inclination angle with respect to us, two out of five peaks are more distinct. The height and spacing of the mode components is a function of the star’s rotational splitting ( $0.56 \mu\text{Hz}$ , equivalent to  $P = 20.5$  days) and angle of inclination ( $45^\circ$ ).

reparameterizations. First, we sampled the projected rotational splitting,  $\nu_s \sin(i)$ , which is more efficiently sampled due to the strong correlations between  $i$  and  $\nu_s$  [23, 24]. A prior was applied over this as

$$\nu_s \sin(i) \sim \ln \mathcal{N}(\ln(0.75), 0.75), \quad (23)$$

where conventions are as above. This subjective prior was chosen to reflect that most stars will have a solar-like rotation, with a long tail to allow for the fastest rotators. Second, we sampled in  $\cos(i)$ , and gave this a prior of

$$\cos(i) \sim \mathcal{U}(0, 1), \quad (24)$$

which is equivalent to stating that probability to observe an inclination angle  $i$  is equal to  $\sin(i)$ . Here, the  $\mathcal{U}(0, 1)$  indicates a uniform prior between 0 and 1. Using a uniform prior on  $\cos(i)$  allowed us to account for the geometric effect that stars with a large inclination angle with respect to us are more common [4].



## 1.5 Fitting procedure

Using our prior information and model described above, we fit Equation 2 to our data  $\mathcal{P}$ , using the likelihood function described in Section 1.3.

In order to speed up the fitting process, we only applied our model to the region of the power spectrum that contains visible modes of oscillation. We created this subset by removing all frequencies outside a range  $0.25 \times \Delta\nu$  below and above the minimum and maximum mode frequencies reported in LEGACY and Kages. This region overlaps minimally with the data used to fit for our prior information of the convective background (see Section 1.4.1), so that both model fits are independent.

To improve computational efficiency, we reduced the number of oscillation modes being fit in five targets. For 16 Cyg A & B, KIC 7970740 and KIC 8478994, we excluded any modes with a Bayes Factor ( $\ln(K)$ ) of less than 6, as reported in LEGACY [5, 6, 25]. For KIC 8478994, which is reported without a value for  $\ln(K)$  in Kages, we only included modes of an overtone number that contained a detection for all of  $\ell = (0, 1, 2)$ , retaining 5 sets of higher signal-to-noise overtones. We do not expect this reduced scope to bias our results, although they may reduce the precision on our measured rotation rates.

We fit our model to our power spectrum data with PyMC3, using 2500 iterations each on 4 chains. An example of our model fit to an asteroseismic power spectrum of 16 Cyg A is shown in Supplementary Figure 1.

## 2 Supplementary Table

Table 1: Parameters for the 94 stars for which seismic rotation rates were obtained in this work. Temperature ( $T_{\text{eff}}$ ), age, mass, metallicity ( $[\text{Fe}/\text{H}]$ ) and surface gravity ( $\log(g)$ ) are adopted from the LEGACY [6, 26, L] and ‘Kages’ [27, 5, K] catalogues, as listed in the Source column. Projected splitting ( $\nu_s \sin(i)$ ), inclination angle ( $i$ ) and asteroseismic rotation ( $P$ ) are from this work. Uncertainties were taken using the 15.9<sup>th</sup> and 84.1<sup>st</sup> percentiles of posterior distributions on the parameters, which are frequently asymmetrical in linear space. Reported values are the median of the posteriors. For parameters with no direct posterior samples (e.g. rotation) the full posterior samples were transformed before taking the summary statistics. The stellar type denotes whether a star is roughly classified as belonging to the main sequence (MS), Sub-Giants (SG) or ‘hot’ stars (H) (see text). The flags indicate the following: 0; no issues, used in the gyrochronology analysis. 1; has either a number of effective samples  $n_{\text{eff}} < 1000$  for the asteroseismic splitting, or Gelman-Rubin convergence metric of  $\hat{R} > 1.1$  [?], indicating that rotation measurements for these stars are less robust than those with a flag of 0. 2; was found to strongly disagree with multiple literature values, excluded from the gyrochronology analysis. 3; fell outside the model range of the stellar models, and were therefore not used in the gyrochronology analysis. Table is continued on the next page.

KIC	$T_{\text{eff}}$ [K]	Age [Gyr]	Mass [ $M_{\odot}$ ]	$[\text{Fe}/\text{H}]$ [dex]	$\log(g)$ [dex]	$\nu_s \sin(i)$ [ $\mu\text{Hz}$ ]	$i$ [ $^{\circ}$ ]	$P$ [days]	Flag	Type	Source
1435467	6326 $\pm$ 77	3.02 $^{+0.50}_{-0.35}$	1.32 $^{+0.03}_{-0.05}$	0.01 $\pm$ 0.10	4.100 $^{+0.009}_{-0.009}$	1.58 $^{+0.10}_{-0.09}$	63.4 $^{+10.2}_{-6.6}$	6.5 $^{+0.8}_{-0.6}$	0	H	L
2837475	6614 $\pm$ 77	1.63 $^{+0.11}_{-0.18}$	1.43 $^{+0.02}_{-0.02}$	0.01 $\pm$ 0.10	4.163 $^{+0.007}_{-0.007}$	3.12 $^{+0.08}_{-0.08}$	70.7 $^{+6.0}_{-4.4}$	3.5 $^{+0.2}_{-0.2}$	0	H	L
3425851	6343 $\pm$ 85	3.32 $^{+0.85}_{-0.64}$	1.18 $^{+0.05}_{-0.05}$	-0.04 $\pm$ 0.10	4.243 $^{+0.008}_{-0.008}$	1.17 $^{+0.48}_{-0.62}$	60.9 $^{+20.1}_{-22.7}$	8.1 $^{+8.6}_{-2.7}$	0	H	K
3427720	6045 $\pm$ 77	2.23 $^{+0.24}_{-0.24}$	1.11 $^{+0.02}_{-0.01}$	-0.06 $\pm$ 0.10	4.387 $^{+0.005}_{-0.004}$	0.30 $^{+0.06}_{-0.06}$	56.4 $^{+10.2}_{-11.8}$	31.6 $^{+10.2}_{-11.8}$	0	MS	L
3456181	6384 $\pm$ 77	2.09 $^{+0.13}_{-0.13}$	1.50 $^{+0.03}_{-0.02}$	-0.15 $\pm$ 0.10	3.949 $^{+0.008}_{-0.009}$	0.92 $^{+0.08}_{-0.08}$	58.2 $^{+20.4}_{-17.6}$	10.7 $^{+2.0}_{-2.8}$	0	H	L
3544595	5669 $\pm$ 75	6.63 $^{+0.62}_{-0.57}$	0.90 $^{+0.01}_{-0.01}$	-0.18 $\pm$ 0.10	4.468 $^{+0.003}_{-0.003}$	0.40 $^{+0.04}_{-0.04}$	66.0 $^{+13.9}_{-13.9}$	26.1 $^{+3.9}_{-4.7}$	0	MS	K
3632418	6193 $\pm$ 77	2.63 $^{+0.18}_{-0.17}$	1.41 $^{+0.02}_{-0.02}$	-0.12 $\pm$ 0.10	4.024 $^{+0.008}_{-0.008}$	0.98 $^{+0.03}_{-0.03}$	72.3 $^{+7.4}_{-7.4}$	11.2 $^{+0.6}_{-0.7}$	0	MS	L
3656476	5668 $\pm$ 77	8.37 $^{+1.72}_{-1.57}$	1.04 $^{+0.05}_{-0.04}$	0.25 $\pm$ 0.10	4.225 $^{+0.008}_{-0.010}$	0.21 $^{+0.02}_{-0.02}$	62.4 $^{+18.9}_{-20.5}$	48.0 $^{+8.1}_{-12.7}$	0	MS	L
3735871	6107 $\pm$ 77	2.35 $^{+1.04}_{-0.85}$	1.09 $^{+0.04}_{-0.04}$	-0.04 $\pm$ 0.10	4.396 $^{+0.007}_{-0.007}$	0.69 $^{+0.05}_{-0.05}$	70.4 $^{+13.4}_{-15.1}$	15.8 $^{+1.8}_{-2.5}$	0	MS	L
4141376	6134 $\pm$ 91	3.27 $^{+0.59}_{-0.64}$	1.02 $^{+0.02}_{-0.02}$	-0.24 $\pm$ 0.10	4.412 $^{+0.004}_{-0.003}$	0.76 $^{+0.13}_{-0.13}$	64.0 $^{+17.5}_{-16.7}$	13.4 $^{+3.4}_{-3.0}$	0	MS	K
4143755	5622 $\pm$ 106	11.27 $^{+1.35}_{-1.35}$	0.92 $^{+0.02}_{-0.03}$	-0.40 $\pm$ 0.11	4.102 $^{+0.002}_{-0.001}$	0.18 $^{+0.08}_{-0.09}$	45.8 $^{+30.6}_{-27.3}$	48.1 $^{+27.4}_{-32.7}$	1	MS	K
4349452	6270 $\pm$ 79	3.45 $^{+0.81}_{-0.72}$	1.16 $^{+0.04}_{-0.02}$	-0.04 $\pm$ 0.10	4.275 $^{+0.008}_{-0.007}$	1.50 $^{+0.09}_{-0.15}$	79.7 $^{+7.1}_{-10.8}$	7.5 $^{+0.5}_{-0.6}$	0	H	K
4914423	5845 $\pm$ 88	6.67 $^{+0.69}_{-0.62}$	1.10 $^{+0.02}_{-0.03}$	0.07 $\pm$ 0.11	4.155 $^{+0.004}_{-0.004}$	0.42 $^{+0.14}_{-0.14}$	61.3 $^{+19.8}_{-30.5}$	23.1 $^{+11.7}_{-9.6}$	0	MS	K
4914923	5805 $\pm$ 77	7.57 $^{+1.79}_{-1.05}$	1.06 $^{+0.06}_{-0.05}$	0.08 $\pm$ 0.10	4.197 $^{+0.008}_{-0.007}$	0.39 $^{+0.03}_{-0.03}$	46.6 $^{+8.1}_{-13.3}$	21.4 $^{+5.4}_{-3.5}$	0	MS	L
5094751	5952 $\pm$ 75	6.35 $^{+1.05}_{-1.57}$	1.07 $^{+0.04}_{-0.04}$	-0.08 $\pm$ 0.10	4.213 $^{+0.008}_{-0.010}$	0.39 $^{+0.16}_{-0.16}$	51.5 $^{+31.1}_{-36.7}$	22.9 $^{+19.3}_{-15.8}$	0	MS	K
5184732	5846 $\pm$ 77	4.85 $^{+0.88}_{-0.88}$	1.15 $^{+0.04}_{-0.04}$	0.36 $\pm$ 0.10	4.255 $^{+0.008}_{-0.008}$	0.55 $^{+0.02}_{-0.02}$	71.3 $^{+11.2}_{-10.8}$	19.9 $^{+1.9}_{-1.9}$	0	MS	L
5773345	6130 $\pm$ 84	2.55 $^{+0.26}_{-0.24}$	1.47 $^{+0.03}_{-0.03}$	0.21 $\pm$ 0.09	3.993 $^{+0.008}_{-0.007}$	1.08 $^{+0.08}_{-0.08}$	33.7 $^{+2.8}_{-2.3}$	5.9 $^{+0.7}_{-0.5}$	0	SG	L
5866724	6169 $\pm$ 50	3.89 $^{+0.59}_{-0.48}$	1.20 $^{+0.03}_{-0.03}$	0.09 $\pm$ 0.08	4.224 $^{+0.007}_{-0.005}$	1.34 $^{+0.07}_{-0.07}$	80.9 $^{+6.3}_{-9.4}$	8.4 $^{+0.5}_{-0.5}$	0	MS	K
5950854	5853 $\pm$ 77	8.93 $^{+1.12}_{-1.15}$	0.97 $^{+0.03}_{-0.03}$	-0.23 $\pm$ 0.10	4.238 $^{+0.007}_{-0.007}$	0.29 $^{+0.64}_{-0.12}$	27.6 $^{+34.2}_{-15.2}$	22.9 $^{+34.2}_{-19.7}$	1	MS	L

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Table 1: *Continued from previous page.*

KIC	$T_{\text{eff}}$ [K]	Age [Gyr]	Mass [ $M_{\odot}$ ]	[Fe/H] [dex]	$\log(g)$ [dex]	$\nu_s \sin(i)$ [ $\mu\text{Hz}$ ]	$i$ [ $^{\circ}$ ]	$P$ [days]	Flag	Type	Source
6106415	6037 $\pm$ 77	5.03 $^{+1.28}_{-1.12}$	1.07 $^{+0.05}_{-0.04}$	-0.04 $\pm$ 0.10	4.295 $^{+0.009}_{-0.009}$	0.69 $^{+0.02}_{-0.02}$	73.1 $^{+8.4}_{-6.3}$	16.0 $^{+0.7}_{-0.8}$	0	MS	L
6116048	6033 $\pm$ 77	9.58 $^{+2.16}_{-1.90}$	0.94 $^{+0.05}_{-0.05}$	-0.23 $\pm$ 0.10	4.254 $^{+0.009}_{-0.012}$	0.63 $^{+0.02}_{-0.02}$	76.3 $^{+9.0}_{-10.2}$	17.9 $^{+0.8}_{-1.2}$	0	MS	L
6196457	5871 $\pm$ 94	5.52 $^{+0.51}_{-0.48}$	1.21 $^{+0.02}_{-0.03}$	0.17 $\pm$ 0.11	4.049 $^{+0.005}_{-0.004}$	0.43 $^{+0.19}_{-0.19}$	52.5 $^{+26.0}_{-29.1}$	20.7 $^{+19.2}_{-13.7}$	0	MS	K
6225718	6313 $\pm$ 76	2.41 $^{+0.53}_{-0.43}$	1.16 $^{+0.03}_{-0.03}$	-0.07 $\pm$ 0.10	4.319 $^{+0.005}_{-0.007}$	0.81 $^{+0.03}_{-0.03}$	29.1 $^{+21.1}_{-1.8}$	6.9 $^{+0.6}_{-0.5}$	0	H	L
6278762	5046 $\pm$ 74	11.54 $^{+0.99}_{-0.94}$	0.74 $^{+0.01}_{-0.01}$	-0.37 $\pm$ 0.09	4.560 $^{+0.003}_{-0.003}$	0.30 $^{+0.09}_{-0.09}$	62.2 $^{+19.0}_{-29.5}$	33.0 $^{+13.6}_{-13.5}$	1, 3	MS	K
6508366	6331 $\pm$ 77	2.06 $^{+0.13}_{-0.14}$	1.53 $^{+0.03}_{-0.02}$	-0.05 $\pm$ 0.10	3.942 $^{+0.003}_{-0.004}$	2.28 $^{+0.04}_{-0.04}$	87.0 $^{+3.1}_{-3.2}$	5.1 $^{+0.1}_{-0.1}$	0	H	L
6521045	5825 $\pm$ 75	6.50 $^{+0.46}_{-0.56}$	1.11 $^{+0.02}_{-0.02}$	0.02 $\pm$ 0.10	4.125 $^{+0.004}_{-0.004}$	0.45 $^{+0.03}_{-0.02}$	75.7 $^{+9.7}_{-11.2}$	24.8 $^{+1.9}_{-2.0}$	0	MS	K
6603624	5674 $\pm$ 77	7.82 $^{+0.94}_{-0.86}$	1.01 $^{+0.03}_{-0.02}$	0.28 $\pm$ 0.10	4.320 $^{+0.004}_{-0.005}$	1.13 $^{+0.13}_{-0.13}$	6.9 $^{+0.8}_{-0.8}$	1.2 $^{+0.0}_{-0.0}$	2	MS	L
6679371	6479 $\pm$ 77	1.95 $^{+0.18}_{-0.16}$	1.53 $^{+0.04}_{-0.02}$	0.01 $\pm$ 0.10	3.934 $^{+0.007}_{-0.008}$	1.90 $^{+0.05}_{-0.06}$	82.1 $^{+3.5}_{-7.2}$	6.0 $^{+0.2}_{-0.2}$	0	H	L
6933899	5832 $\pm$ 77	6.34 $^{+0.72}_{-0.62}$	1.13 $^{+0.03}_{-0.03}$	-0.01 $\pm$ 0.10	4.087 $^{+0.008}_{-0.007}$	0.36 $^{+0.02}_{-0.02}$	64.3 $^{+16.1}_{-14.0}$	28.9 $^{+3.7}_{-4.8}$	0	MS	L
7103006	6344 $\pm$ 77	2.47 $^{+0.22}_{-0.24}$	1.42 $^{+0.04}_{-0.02}$	0.02 $\pm$ 0.10	4.015 $^{+0.007}_{-0.007}$	1.36 $^{+0.08}_{-0.09}$	56.8 $^{+14.8}_{-8.8}$	7.1 $^{+1.3}_{-1.0}$	0	H	L
7106245	6068 $\pm$ 102	6.27 $^{+1.06}_{-1.06}$	0.92 $^{+0.02}_{-0.04}$	-0.99 $\pm$ 0.19	4.325 $^{+0.007}_{-0.007}$	0.32 $^{+0.16}_{-0.12}$	33.4 $^{+38.4}_{-14.7}$	21.4 $^{+23.8}_{-13.2}$	1, 3	MS	L
7206837	6305 $\pm$ 77	2.90 $^{+0.42}_{-0.30}$	1.30 $^{+0.03}_{-0.03}$	0.10 $\pm$ 0.10	4.163 $^{+0.008}_{-0.007}$	1.53 $^{+0.12}_{-0.12}$	31.7 $^{+3.2}_{-2.8}$	4.0 $^{+0.6}_{-0.4}$	0	H	L
7296438	5775 $\pm$ 77	7.23 $^{+1.49}_{-1.77}$	1.08 $^{+0.06}_{-0.05}$	0.19 $\pm$ 0.10	4.201 $^{+0.009}_{-0.010}$	0.20 $^{+0.06}_{-0.06}$	50.5 $^{+28.2}_{-31.1}$	45.6 $^{+23.4}_{-29.0}$	1	MS	L
7510397	6171 $\pm$ 77	2.82 $^{+0.14}_{-0.16}$	1.37 $^{+0.02}_{-0.02}$	-0.21 $\pm$ 0.10	4.036 $^{+0.007}_{-0.004}$	0.64 $^{+0.06}_{-0.06}$	19.9 $^{+2.0}_{-2.0}$	6.1 $^{+0.7}_{-0.6}$	0	MS	L
7670943	6463 $\pm$ 110	2.78 $^{+0.62}_{-0.51}$	1.24 $^{+0.04}_{-0.05}$	0.09 $\pm$ 0.11	4.228 $^{+0.008}_{-0.008}$	1.83 $^{+0.14}_{-0.14}$	75.7 $^{+9.8}_{-11.5}$	6.0 $^{+0.6}_{-0.6}$	0	H	K
7680114	5811 $\pm$ 77	7.68 $^{+1.45}_{-1.28}$	1.06 $^{+0.05}_{-0.05}$	0.05 $\pm$ 0.10	4.172 $^{+0.008}_{-0.010}$	0.26 $^{+0.05}_{-0.04}$	37.0 $^{+34.3}_{-16.3}$	27.3 $^{+19.6}_{-13.5}$	0	MS	L
7771282	6248 $\pm$ 77	3.24 $^{+0.35}_{-0.32}$	1.29 $^{+0.03}_{-0.03}$	-0.02 $\pm$ 0.10	4.112 $^{+0.007}_{-0.007}$	1.01 $^{+0.14}_{-0.18}$	69.5 $^{+14.6}_{-17.8}$	10.4 $^{+2.3}_{-1.7}$	0	MS	L
7871531	5501 $\pm$ 77	9.96 $^{+1.93}_{-1.77}$	0.83 $^{+0.03}_{-0.02}$	-0.26 $\pm$ 0.10	4.478 $^{+0.007}_{-0.005}$	0.33 $^{+0.03}_{-0.03}$	71.3 $^{+12.0}_{-13.2}$	33.1 $^{+4.1}_{-4.1}$	0	MS	L
7940546	6235 $\pm$ 77	2.33 $^{+0.08}_{-0.08}$	1.40 $^{+0.01}_{-0.01}$	-0.20 $\pm$ 0.10	4.007 $^{+0.003}_{-0.001}$	1.14 $^{+0.03}_{-0.03}$	78.9 $^{+7.4}_{-7.9}$	9.9 $^{+0.3}_{-0.4}$	0	MS	L
7970740	5309 $\pm$ 77	12.98 $^{+1.36}_{-2.00}$	0.73 $^{+0.03}_{-0.01}$	-0.54 $\pm$ 0.10	4.539 $^{+0.004}_{-0.005}$	0.26 $^{+0.03}_{-0.02}$	60.7 $^{+17.4}_{-15.3}$	39.2 $^{+6.7}_{-9.0}$	0	MS	L
8006161	5488 $\pm$ 77	3.59 $^{+1.53}_{-1.45}$	0.98 $^{+0.03}_{-0.03}$	0.34 $\pm$ 0.10	4.494 $^{+0.007}_{-0.007}$	0.34 $^{+0.02}_{-0.02}$	37.0 $^{+4.1}_{-3.4}$	20.6 $^{+2.2}_{-1.8}$	0	MS	L
8077137	6072 $\pm$ 75	6.23 $^{+1.23}_{-1.23}$	1.12 $^{+0.04}_{-0.04}$	-0.09 $\pm$ 0.10	4.056 $^{+0.010}_{-0.013}$	0.84 $^{+0.06}_{-0.07}$	72.8 $^{+11.3}_{-12.6}$	13.0 $^{+1.3}_{-1.5}$	0	MS	K
8150065	6173 $\pm$ 101	3.83 $^{+0.99}_{-1.07}$	1.19 $^{+0.04}_{-0.05}$	-0.13 $\pm$ 0.15	4.220 $^{+0.008}_{-0.008}$	0.54 $^{+0.11}_{-0.13}$	64.0 $^{+21.1}_{-18.0}$	18.6 $^{+4.9}_{-6.4}$	0	MS	L
8179536	6343 $\pm$ 77	3.54 $^{+0.81}_{-0.81}$	1.16 $^{+0.05}_{-0.05}$	-0.03 $\pm$ 0.10	4.255 $^{+0.010}_{-0.010}$	1.46 $^{+0.10}_{-0.09}$	55.7 $^{+13.3}_{-7.4}$	6.5 $^{+1.2}_{-0.8}$	0	H	L
8228742	6122 $\pm$ 77	2.89 $^{+0.16}_{-0.18}$	1.38 $^{+0.06}_{-0.02}$	-0.08 $\pm$ 0.10	4.035 $^{+0.007}_{-0.005}$	0.64 $^{+0.04}_{-0.04}$	37.9 $^{+6.2}_{-4.0}$	11.0 $^{+2.0}_{-1.3}$	0	MS	L
8292840	6239 $\pm$ 94	3.85 $^{+0.81}_{-0.75}$	1.15 $^{+0.02}_{-0.05}$	-0.14 $\pm$ 0.10	4.240 $^{+0.008}_{-0.008}$	1.45 $^{+0.07}_{-0.07}$	76.2 $^{+8.9}_{-9.1}$	7.7 $^{+0.5}_{-0.5}$	0	MS	K
8349582	5699 $\pm$ 74	8.03 $^{+0.80}_{-0.70}$	1.07 $^{+0.02}_{-0.02}$	0.30 $\pm$ 0.10	4.163 $^{+0.004}_{-0.003}$	0.23 $^{+0.07}_{-0.06}$	59.6 $^{+20.7}_{-24.1}$	41.7 $^{+19.6}_{-14.9}$	1	MS	K
8379927	6067 $\pm$ 120	1.99 $^{+0.85}_{-0.75}$	1.12 $^{+0.04}_{-0.04}$	-0.10 $\pm$ 0.15	4.388 $^{+0.008}_{-0.007}$	1.12 $^{+0.02}_{-0.02}$	63.3 $^{+2.5}_{-2.3}$	9.2 $^{+0.3}_{-0.2}$	0	MS	L
8394589	6143 $\pm$ 77	4.45 $^{+0.94}_{-0.83}$	1.04 $^{+0.03}_{-0.03}$	-0.29 $\pm$ 0.10	4.322 $^{+0.008}_{-0.008}$	1.01 $^{+0.03}_{-0.03}$	71.1 $^{+7.9}_{-5.9}$	10.9 $^{+0.6}_{-0.6}$	0	MS	L
8424992	5719 $\pm$ 77	9.61 $^{+1.74}_{-1.92}$	0.92 $^{+0.04}_{-0.04}$	-0.12 $\pm$ 0.10	4.359 $^{+0.007}_{-0.007}$	0.22 $^{+0.06}_{-0.06}$	59.1 $^{+21.3}_{-30.3}$	42.3 $^{+19.4}_{-17.7}$	1	MS	L
8494142	6144 $\pm$ 106	2.62 $^{+0.26}_{-0.24}$	1.42 $^{+0.03}_{-0.02}$	0.13 $\pm$ 0.10	4.038 $^{+0.005}_{-0.005}$	0.67 $^{+0.22}_{-0.28}$	62.8 $^{+18.5}_{-23.8}$	14.5 $^{+9.9}_{-4.5}$	0	MS	K
8554498	5945 $\pm$ 60	5.60 $^{+0.45}_{-0.42}$	1.20 $^{+0.02}_{-0.03}$	0.17 $\pm$ 0.05	4.007 $^{+0.003}_{-0.003}$	0.25 $^{+0.21}_{-0.09}$	48.1 $^{+30.0}_{-36.6}$	35.7 $^{+25.6}_{-31.4}$	0	MS	K

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Table 1: *Continued from previous page.*

KIC	$T_{\text{eff}}$ [K]	Age [Gyr]	Mass [ $M_{\odot}$ ]	[Fe/H] [dex]	$\log(g)$ [dex]	$\nu_s \sin(i)$ [ $\mu\text{Hz}$ ]	$i$ [ $^{\circ}$ ]	$P$ [days]	Flag	Type	Source
8694723	6246 $\pm$ 77	4.69 $^{+0.48}_{-0.51}$	1.14 $^{+0.02}_{-0.02}$	-0.42 $\pm$ 0.10	4.113 $^{+0.007}_{-0.009}$	0.92 $^{+0.05}_{-0.05}$	34.7 $^{+3.4}_{-2.7}$	7.2 $^{+0.8}_{-0.6}$	0	MS	L
8760414	5873 $\pm$ 77	11.66 $^{+1.28}_{-1.61}$	0.81 $^{+0.03}_{-0.03}$	-0.92 $\pm$ 0.10	4.329 $^{+0.006}_{-0.006}$	0.69 $^{+0.26}_{-0.42}$	7.6 $^{+2.3}_{-1.7}$	2.0 $^{+4.5}_{-0.4}$	2, 3	MS	L
8866102	6325 $\pm$ 75	2.60 $^{+0.56}_{-0.53}$	1.23 $^{+0.04}_{-0.04}$	0.01 $\pm$ 0.10	4.262 $^{+0.008}_{-0.007}$	2.15 $^{+0.04}_{-0.04}$	78.2 $^{+6.6}_{-4.7}$	5.3 $^{+0.2}_{-0.2}$	0	H	K
8938364	5677 $\pm$ 77	10.25 $^{+0.65}_{-0.65}$	0.99 $^{+0.01}_{-0.01}$	-0.13 $\pm$ 0.10	4.173 $^{+0.007}_{-0.007}$	0.61 $^{+0.27}_{-0.50}$	8.7 $^{+5.5}_{-2.3}$	2.0 $^{+8.7}_{-0.2}$	2	MS	L
9025370	5270 $\pm$ 180	6.55 $^{+1.13}_{-1.26}$	0.97 $^{+0.03}_{-0.03}$	-0.12 $\pm$ 0.18	4.423 $^{+0.004}_{-0.004}$	0.43 $^{+0.04}_{-0.04}$	67.5 $^{+15.2}_{-19.1}$	24.7 $^{+3.7}_{-4.7}$	0	MS	L
9098294	5852 $\pm$ 77	8.08 $^{+0.99}_{-0.73}$	0.97 $^{+0.03}_{-0.03}$	-0.18 $\pm$ 0.10	4.308 $^{+0.007}_{-0.007}$	0.36 $^{+0.04}_{-0.04}$	58.2 $^{+21.0}_{-16.3}$	27.2 $^{+5.7}_{-7.0}$	0	MS	L
9139151	6302 $\pm$ 77	1.32 $^{+0.94}_{-0.75}$	1.18 $^{+0.04}_{-0.05}$	0.10 $\pm$ 0.10	4.382 $^{+0.008}_{-0.008}$	0.95 $^{+0.04}_{-0.04}$	73.5 $^{+11.0}_{-11.0}$	11.6 $^{+1.1}_{-1.1}$	0	H	L
9139163	6400 $\pm$ 84	1.60 $^{+0.22}_{-0.22}$	1.40 $^{+0.03}_{-0.02}$	0.15 $\pm$ 0.09	4.200 $^{+0.009}_{-0.008}$	1.59 $^{+0.07}_{-0.08}$	33.5 $^{+3.0}_{-3.0}$	4.0 $^{+0.3}_{-0.3}$	1	H	L
9206432	6538 $\pm$ 77	1.53 $^{+0.21}_{-0.30}$	1.38 $^{+0.04}_{-0.02}$	0.16 $\pm$ 0.10	4.220 $^{+0.005}_{-0.007}$	1.55 $^{+0.17}_{-0.20}$	34.3 $^{+3.7}_{-4.2}$	4.1 $^{+1.0}_{-0.5}$	0	H	L
9353712	6278 $\pm$ 77	2.15 $^{+0.11}_{-0.13}$	1.51 $^{+0.03}_{-0.02}$	-0.05 $\pm$ 0.10	3.943 $^{+0.007}_{-0.005}$	0.75 $^{+0.16}_{-0.17}$	37.6 $^{+29.1}_{-12.6}$	9.5 $^{+7.3}_{-3.9}$	0	H	L
9410862	6047 $\pm$ 77	6.93 $^{+1.49}_{-1.33}$	0.97 $^{+0.05}_{-0.04}$	-0.31 $\pm$ 0.10	4.300 $^{+0.009}_{-0.008}$	0.41 $^{+0.09}_{-0.08}$	46.4 $^{+9.8}_{-16.7}$	20.6 $^{+9.8}_{-8.1}$	1	MS	L
9414417	6253 $\pm$ 75	2.65 $^{+0.16}_{-0.18}$	1.40 $^{+0.02}_{-0.03}$	-0.13 $\pm$ 0.10	4.016 $^{+0.005}_{-0.005}$	1.09 $^{+0.05}_{-0.05}$	58.1 $^{+9.7}_{-6.9}$	9.0 $^{+1.1}_{-0.9}$	0	H	L
9592705	6174 $\pm$ 92	2.33 $^{+0.18}_{-0.16}$	1.51 $^{+0.03}_{-0.02}$	0.22 $\pm$ 0.10	3.961 $^{+0.003}_{-0.004}$	0.93 $^{+0.09}_{-0.09}$	59.3 $^{+17.8}_{-12.1}$	10.7 $^{+2.1}_{-1.9}$	0	SG	K
9812850	6321 $\pm$ 77	2.71 $^{+0.46}_{-0.35}$	1.37 $^{+0.04}_{-0.05}$	-0.07 $\pm$ 0.10	4.053 $^{+0.008}_{-0.009}$	1.54 $^{+0.09}_{-0.08}$	81.0 $^{+6.4}_{-10.0}$	7.4 $^{+0.4}_{-0.5}$	0	H	L
9955598	5457 $\pm$ 77	6.29 $^{+1.95}_{-1.84}$	0.90 $^{+0.05}_{-0.03}$	0.05 $\pm$ 0.10	4.497 $^{+0.007}_{-0.005}$	0.29 $^{+0.04}_{-0.04}$	53.4 $^{+20.8}_{-11.9}$	31.4 $^{+9.1}_{-6.4}$	0	MS	L
9965715	5860 $\pm$ 180	2.92 $^{+0.86}_{-0.75}$	1.21 $^{+0.04}_{-0.05}$	-0.44 $\pm$ 0.18	4.272 $^{+0.008}_{-0.009}$	1.75 $^{+0.05}_{-0.05}$	58.3 $^{+3.5}_{-3.2}$	5.6 $^{+0.3}_{-0.3}$	0	MS	L
10068307	6132 $\pm$ 77	2.36 $^{+0.10}_{-0.10}$	1.47 $^{+0.01}_{-0.02}$	-0.23 $\pm$ 0.10	3.967 $^{+0.004}_{-0.004}$	0.71 $^{+0.03}_{-0.03}$	41.7 $^{+6.0}_{-4.1}$	10.9 $^{+1.5}_{-1.1}$	0	SG	L
10079226	5949 $\pm$ 77	3.06 $^{+0.70}_{-0.65}$	1.12 $^{+0.02}_{-0.03}$	0.11 $\pm$ 0.10	4.366 $^{+0.005}_{-0.005}$	0.65 $^{+0.07}_{-0.08}$	75.1 $^{+10.6}_{-23.4}$	16.8 $^{+2.2}_{-3.0}$	1	MS	L
10162436	6146 $\pm$ 77	2.46 $^{+0.11}_{-0.11}$	1.45 $^{+0.02}_{-0.01}$	-0.16 $\pm$ 0.10	3.981 $^{+0.005}_{-0.005}$	0.84 $^{+0.05}_{-0.05}$	25.5 $^{+2.1}_{-1.8}$	5.9 $^{+0.6}_{-0.4}$	0	SG	L
10454113	6177 $\pm$ 77	2.89 $^{+0.56}_{-0.53}$	1.17 $^{+0.02}_{-0.03}$	-0.07 $\pm$ 0.10	4.314 $^{+0.005}_{-0.005}$	0.76 $^{+0.07}_{-0.07}$	40.9 $^{+26.9}_{-9.6}$	10.0 $^{+4.8}_{-2.5}$	0	MS	L
10514430	5784 $\pm$ 98	7.84 $^{+0.91}_{-1.33}$	1.06 $^{+0.04}_{-0.05}$	-0.11 $\pm$ 0.11	4.061 $^{+0.004}_{-0.004}$	0.18 $^{+0.05}_{-0.03}$	57.2 $^{+32.5}_{-12.0}$	53.6 $^{+23.6}_{-27.2}$	1	MS	K
10516096	5964 $\pm$ 77	7.01 $^{+1.45}_{-1.61}$	1.06 $^{+0.05}_{-0.05}$	-0.11 $\pm$ 0.10	4.169 $^{+0.010}_{-0.011}$	0.48 $^{+0.03}_{-0.16}$	71.8 $^{+12.5}_{-16.2}$	22.6 $^{+1.9}_{-3.1}$	0	MS	L
10586004	5770 $\pm$ 83	6.43 $^{+0.61}_{-1.12}$	1.18 $^{+0.02}_{-0.04}$	0.29 $\pm$ 0.10	4.071 $^{+0.003}_{-0.007}$	0.48 $^{+0.17}_{-0.08}$	59.3 $^{+22.4}_{-21.0}$	19.6 $^{+11.1}_{-6.5}$	1	MS	K
10644253	6045 $\pm$ 77	2.39 $^{+0.96}_{-0.29}$	1.10 $^{+0.04}_{-0.04}$	0.06 $\pm$ 0.10	4.396 $^{+0.007}_{-0.008}$	0.24 $^{+0.08}_{-0.11}$	55.6 $^{+41.0}_{-39.2}$	38.0 $^{+24.1}_{-19.1}$	0	MS	L
10666592	6350 $\pm$ 80	2.11 $^{+0.29}_{-0.24}$	1.50 $^{+0.04}_{-0.04}$	0.26 $\pm$ 0.08	4.017 $^{+0.009}_{-0.007}$	0.91 $^{+0.11}_{-0.23}$	47.2 $^{+27.2}_{-34.8}$	9.5 $^{+3.6}_{-3.2}$	0	H	K
10730618	6150 $\pm$ 180	3.05 $^{+0.46}_{-0.29}$	1.34 $^{+0.05}_{-0.05}$	-0.11 $\pm$ 0.18	4.062 $^{+0.008}_{-0.007}$	0.56 $^{+0.23}_{-0.25}$	55.6 $^{+23.7}_{-26.2}$	16.1 $^{+13.9}_{-7.2}$	0	MS	L
10963065	6140 $\pm$ 77	7.15 $^{+1.92}_{-1.61}$	0.99 $^{+0.06}_{-0.06}$	-0.19 $\pm$ 0.10	4.277 $^{+0.011}_{-0.011}$	0.67 $^{+0.03}_{-0.03}$	41.8 $^{+4.7}_{-3.6}$	11.5 $^{+1.3}_{-1.0}$	0	MS	L
11081729	6548 $\pm$ 82	1.88 $^{+0.59}_{-0.42}$	1.30 $^{+0.04}_{-0.05}$	0.11 $\pm$ 0.10	4.245 $^{+0.010}_{-0.009}$	3.35 $^{+0.10}_{-0.10}$	82.9 $^{+4.9}_{-5.9}$	3.4 $^{+0.1}_{-0.1}$	0	H	L
11133306	5982 $\pm$ 82	5.14 $^{+0.86}_{-0.88}$	1.06 $^{+0.03}_{-0.03}$	-0.02 $\pm$ 0.10	4.314 $^{+0.007}_{-0.004}$	0.39 $^{+0.14}_{-0.13}$	58.0 $^{+21.9}_{-24.1}$	24.6 $^{+14.3}_{-10.0}$	0	MS	K
11253226	6642 $\pm$ 77	1.60 $^{+0.06}_{-0.13}$	1.41 $^{+0.02}_{-0.01}$	-0.08 $\pm$ 0.10	4.173 $^{+0.005}_{-0.004}$	2.55 $^{+0.11}_{-0.12}$	49.3 $^{+6.3}_{-4.4}$	3.4 $^{+0.4}_{-0.3}$	0	H	L
11295426	5793 $\pm$ 74	6.31 $^{+0.32}_{-0.34}$	1.07 $^{+0.01}_{-0.02}$	0.12 $\pm$ 0.07	4.280 $^{+0.003}_{-0.003}$	0.22 $^{+0.03}_{-0.03}$	55.6 $^{+22.9}_{-20.9}$	42.6 $^{+11.5}_{-14.5}$	0	MS	K
11401755	5911 $\pm$ 66	7.10 $^{+0.61}_{-0.59}$	1.06 $^{+0.03}_{-0.02}$	-0.20 $\pm$ 0.06	4.039 $^{+0.004}_{-0.004}$	0.55 $^{+0.09}_{-0.10}$	64.6 $^{+17.4}_{-19.5}$	18.5 $^{+4.7}_{-4.3}$	0	MS	K
11772920	5180 $\pm$ 180	10.67 $^{+2.73}_{-2.97}$	0.83 $^{+0.04}_{-0.04}$	-0.09 $\pm$ 0.18	4.500 $^{+0.005}_{-0.008}$	0.31 $^{+0.03}_{-0.04}$	70.8 $^{+12.6}_{-14.3}$	35.1 $^{+5.3}_{-4.7}$	1	MS	L

*Continued on next page*

Table 1: *Continued from previous page.*

KIC	$T_{\text{eff}}$ [K]	Age [Gyr]	Mass [ $M_{\odot}$ ]	[Fe/H] [dex]	$\log(g)$ [dex]	$\nu_s \sin(i)$ [ $\mu\text{Hz}$ ]	$i$ [ $^{\circ}$ ]	$P$ [days]	Flag	Type	Source
11807274	6225 $\pm$ 75	3.59 $^{+0.78}_{-0.45}$	1.24 $^{+0.04}_{-0.04}$	0.00 $\pm$ 0.08	4.135 $^{+0.009}_{-0.007}$	1.42 $^{+0.07}_{-0.07}$	76.8 $^{+8.8}_{-9.4}$	7.9 $^{+0.5}_{-0.5}$	0	MS	K
11853905	5781 $\pm$ 76	6.71 $^{+0.77}_{-0.67}$	1.12 $^{+0.02}_{-0.03}$	0.09 $\pm$ 0.10	4.102 $^{+0.004}_{-0.005}$	0.27 $^{+0.09}_{-0.09}$	54.7 $^{+24.5}_{-28.8}$	34.0 $^{+18.9}_{-17.2}$	1	MS	K
11904151	5647 $\pm$ 74	10.23 $^{+0.83}_{-0.67}$	0.92 $^{+0.01}_{-0.02}$	-0.15 $\pm$ 0.10	4.344 $^{+0.003}_{-0.003}$	0.24 $^{+0.06}_{-0.07}$	64.9 $^{+18.1}_{-28.4}$	40.9 $^{+16.5}_{-12.8}$	1	MS	K
12009504	6179 $\pm$ 77	3.97 $^{+0.57}_{-0.43}$	1.17 $^{+0.02}_{-0.04}$	-0.08 $\pm$ 0.10	4.211 $^{+0.007}_{-0.005}$	1.16 $^{+0.03}_{-0.04}$	71.3 $^{+8.0}_{-5.7}$	9.4 $^{+0.5}_{-0.5}$	0	MS	L
12069127	6276 $\pm$ 77	2.01 $^{+0.11}_{-0.13}$	1.57 $^{+0.03}_{-0.02}$	0.08 $\pm$ 0.10	3.912 $^{+0.005}_{-0.004}$	0.54 $^{+1.26}_{-0.33}$	16.6 $^{+54.2}_{-6.3}$	5.2 $^{+39.9}_{-3.9}$	1	H	L
12069424	5825 $\pm$ 50	6.67 $^{+0.81}_{-0.77}$	1.05 $^{+0.02}_{-0.02}$	0.10 $\pm$ 0.03	4.287 $^{+0.007}_{-0.007}$	0.40 $^{+0.01}_{-0.01}$	44.7 $^{+6.2}_{-2.9}$	20.5 $^{+2.0}_{-1.8}$	1	MS	L
12069449	5750 $\pm$ 50	7.39 $^{+0.89}_{-0.91}$	0.99 $^{+0.02}_{-0.02}$	0.05 $\pm$ 0.02	4.353 $^{+0.007}_{-0.005}$	0.31 $^{+0.01}_{-0.01}$	34.0 $^{+2.4}_{-2.4}$	21.2 $^{+1.8}_{-1.5}$	0	MS	L
12258514	5964 $\pm$ 77	4.05 $^{+0.18}_{-0.16}$	1.26 $^{+0.01}_{-0.01}$	0.00 $\pm$ 0.10	4.126 $^{+0.004}_{-0.003}$	0.39 $^{+0.04}_{-0.03}$	35.0 $^{+22.9}_{-6.6}$	16.7 $^{+10.0}_{-3.6}$	1	MS	L
12317678	6580 $\pm$ 77	2.46 $^{+0.22}_{-0.18}$	1.34 $^{+0.04}_{-0.01}$	-0.28 $\pm$ 0.10	4.048 $^{+0.008}_{-0.009}$	1.27 $^{+0.13}_{-0.14}$	35.3 $^{+10.1}_{-5.2}$	5.2 $^{+1.8}_{-0.9}$	0	H	L

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