

Masterthesis Medientechnologie

RHOT

A real time hand and object tracking system with
low cost consumer grade hardware

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1 Introduction

The standard interface between human and computer has for long years been mouse and keyboard. But with the advance of technology, new interfacing methods were developed in the last few years.

Touch technology for interfacing with mobile devices and desktop computers has become a reliable technology and has been integrated into our everyday lives. Advances in capabilities of CPU as well as GPU hardware has build a foundation for the use of advanced AR and VR technology. 3D and stereoscopic rendering can now be accomplished even by mobile hardware (with some limitations) without on-board hardware. For an intensely immersive experience VR goggles are used to explore digitally created worlds.

With this level of immersiveness, a touch device or just a mouse and keyboard setup is rather hindering the user experience and the logical and more natural way of interfacing with our digital technology would be by utilizing the build in human control elements that we carry around with us every day. The human hands offer a build-in control element that provides a large number of "*Degrees-of-Freedom*" (DOF's) and furthermore adds the possibility of combining these with a tactile component.

The first more humble attempts of solving this problem already began in the early 1980's where a lack of computational power and low-res imaging hardware made more complex systems impossible. These systems were mostly aimed at registering simple hand gestures like pointing as an interface method and were not able to reconstruct full hand positions in realtime[4]. Modern day elaborate system for hand tracking use infrared or stereoscopic Cameras to achieve a performant tracking result, utilizing the calculation capability of standard consumer computers. These systems are rather specialized for the task they are doing and are therefore rather expensive to attain.

This thesis assesses if it is possible to create a real-time hand and object tracking system based on easily accessible consumer grade hardware and open source Programs as well as displaying the tracking result on a head mounted display. The system should provide an experience for the user that is as natural as possible in terms of grabbing precision and the components should not hinder the motion capability of the hand. Furthermore the system should aim at being comfortable in terms of design as a cumbersome system would not be used in everyday life. Before evaluating a prototype system, an overview of existing technologies in terms of tracking and display of the human hand will be given. A small overview over the anatomical properties of the human hand will be given as the understanding of these plays a major role in the setup for the hand simulation.

2 Description of hand in digital space

Tracking of the human hand has always been a challenging problem. In comparison to other larger body parts like the arm or the head, the human hand itself contains a large variety of smaller parts, namely bones and muscles. These components have to be taken into account when trying to replicate the natural motion of the hand in digital space.

2.1 Physiological structure of the human hand

Lee and Kuni [25] describe the human hand as "an articulated structure with about 30 degrees of freedom [which] changes shape in various ways by its joint movements."

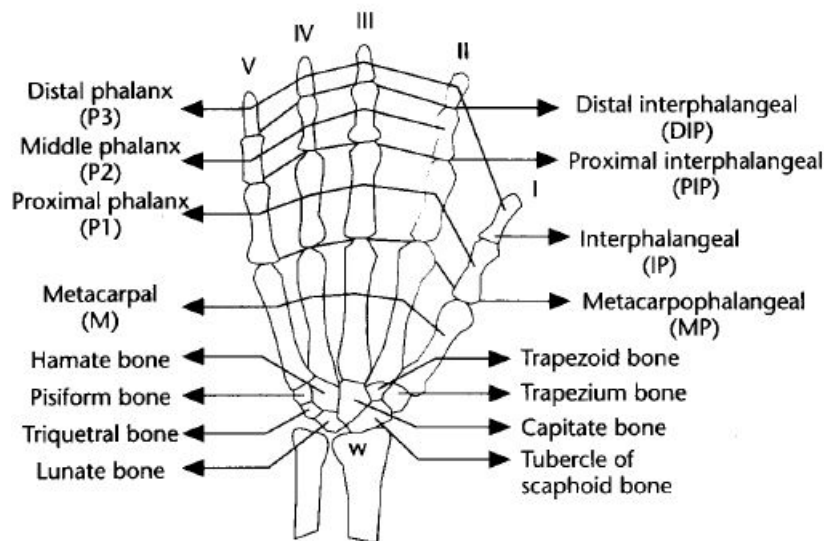


Figure 2.1: Bone structure of the human left hand ([25])

All of the hand components are connected to at least one neighboring component via a joint. The joints affect the position of the connected components. To describe the movement of the hand components, we can use the rotation angles of the joints to correlate to a specific position.

To do so, we define a local coordinate system for each of the existing hand joints. By doing so, we achieve a sequence of rotations in the local coordinate systems of the joints. Such a sequence can then be used to describe a specific movement and/or position of

a component. Not all of the joints in the human hand have equal degrees of freedom. Their functionality can be classified in the amount of DOFs (Degrees of freedom)[20]

- 1 DOF
 - A joint movement that can perform a **flexion** or **twist** in one direction
- 2 DOF
 - A joint movement that can perform **flexion** in more than one direction (**directive**)
- 3 DOF
 - A joint movement that permits simultaneous **directive** and **twist** movements. (**spherical**)

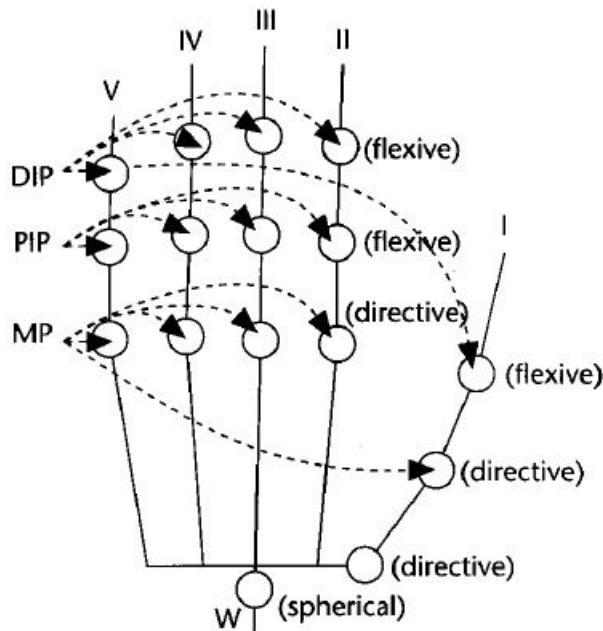


Figure 2.2: Representation of the DOFs of the human hand

When looking at the DOF's displayed in Figure 2.2, each finger (II-V) sums up to 4 DOF's and the thumb to 5 DOF's. Also considering 6 DOFs for the rotation and position of the whole and itself, the result gets us to 27 DOF's for the human hand.

2.1.1 Constraints in Hand Motion

A full usage of all the declared DOFs would lead to a large amount of possible combination. Since the hand is not only made up of bones but also Muscles and the skin, we can impose some constraints [3, 34] to the movement of the joints. Ling, Wu and Huang([26]) proposed following classification for the constraints:

- **Type I constraints**

- A constraint that limits the range of finger motions based on hand anatomy

- **Type II constraints**

- A constraint that the position of the joints during finger movement

- **Type III constraints**

- A constraint that limits position based on natural hand motions

The **Type I** and **Type II** constraints rely on the physiological and mechanical properties of the human hand. **Type III** constraints are results of common and natural movements and can be differing from person to person. As these movements are to some degree similar for everyone, a broad grouping can be applied. The curling of the fingers at the same time when forming a fist is way more natural than curling each finger by itself. Here the motion of the hand is quite similar between different persons, but the constraints cannot be described in a mathematical form.

A **Type I** constraint example would be that the position of the fingertip is limited by the length of the other finger segments and thereby can only reach as far as the combined length.

An example for **Type II** constraints would be that, for your fingertip to touch your hand palm, all joints in the finger have to be bend to achieve this position. The following inequalities can be used to describe these constraints:

Type I:

$$\begin{aligned} 0^\circ &\leq \Theta_{MP_flex} \leq 90^\circ \\ 0^\circ &\leq \Theta_{PIP_flex} \leq 110^\circ \\ 0^\circ &\leq \Theta_{DIP_flex} \leq 90^\circ \\ -15^\circ &\leq \Theta_{MP_abduct/adduct} \leq 15^\circ \end{aligned} \tag{2.1}$$

A further constraint that is specific to the middle finger is, that this fingers MP normally does not abduct and adduct much. Therefore we can infer an approximation and thereby remove 1 DOF from the model:

$$\Theta_{MP_abduct/adduct} = 0^\circ \tag{2.2}$$

The same behavior can be seen in the combination of hand parts labeled W(the connection point between hand and lower arm). This approximation also eliminates one DOF on the connected thumb:

$$\Theta_{W_abduct/adduct} = 0^\circ \tag{2.3}$$

Since the DIP,PIP and MP joints of our index, middle, ring, and little fingers only have 1 DOF for flexion, we can further assume that their motion is limited to movement in one plane.

Type II:

The **Type II** constraints can be split into interfinger and intrafinger constraints. Regarding intrafinger constraints between the joints of the same finger, human hand anatomy implies that to bend the DIP joints on either the index, middle, ring or little fingers, the corresponding PIP joints of that finger must also be bent. The approximation for this relation[36] can be described as :

$$\Theta_{DIP} = \frac{2}{3}\Theta_{PIP} \quad (2.4)$$

Inter-finger constraints can be imposed between joints of adjacent fingers. Inter-finger constraints describe that the bending of an MP joint in the index finger forces the MP joint in the middle finger to bend as well.

When combining the constraints described in the above equations, the starting number 21 DOF's of the human hand can be reduced to 15. Inequalities for these cases, obtained through empiric studies, can be found in [25].

2.2 Kinematics

The preceding sections gave an overview of how we can describe a model of the human hand and introduced some limiting constraints. With the model and the constraints, we can now start to build a kinematic system for the animation of the model.

Kinematic systems contain so called *kinematic chains*, which consist of a *starting point* or *root*, kinematic elements like *joints*, *links* and an *endpoint*, also called *end effector*. Applied to the human hand, the whole hand model represents the kinematic system. This system contains several *kinematic chains*, namely the fingers of the hand with the fingertips being the *end effectors* of each of these chains.

Each of these components has its set of DOF's which can be described mathematically. The established convention for describing this kind of linked systems is the *Denavit-Hartenberg* convention (D-H)[9]. It was actually introduced for the order to standardize the coordinate frames for spatial linkages in the field of robotics, but has since then been applied in other fields as well.[38]

As we begin to move our hands, the states of the kinematic chains begin to change. Joint angles and end effector positions are modified until the end position is reached. To represent the new position and angle data set of our physical hand with our kinematic system, two major paths for achieving a solution can be taken.

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2.2.1 Forward Kinematics

Forward kinematics (FK) uses the knowledge of the new angles and positions after the application of known transformations to the kinematic chain. The data of the *joints* and *links* between the *root* and the *end effector* is then used to solve the problem of finding the *end effector's* position.

We can denote the existing end effectors relative position to an origin as s_1, \dots, s_k . The s_i position is the result of the combination of all the joint angles in the corresponding kinematic chain. Respectively, we define the target position of the end effectors as t_1, \dots, t_i , with t_i being the target position for the end effector s_i . The required positional change for the end effector can now be described as $e_i = t_i - s_i$. In systems with more than one end effector, like our hand system, the components can be written as vectors.

$$\begin{aligned}\vec{s} &= (s_1, \dots, s_n)^T \\ \vec{t} &= (t_1, \dots, t_n)^T \\ \vec{e} &= \vec{t} - \vec{s}\end{aligned}\tag{2.5}$$

As the vector components of \vec{s} are results of the chain joint angles $\theta_1, \dots, \theta_n$ and therefore are effected by them, we define

$$\begin{aligned}\vec{s}_i &= f_i(\theta) \\ \vec{s} &= f(\theta)\end{aligned}\tag{2.6}$$

With θ being the column vector $\theta = (\theta_1, \dots, \theta_n)^T$. The second vector equation displayed in (2.6) is also called the *Forward Kinematics*(FK) solution.

The advantage of an FK solution is that there is always an unique solution to the problem. In consequence, this approach is commonly used in the field of robotics, where the information on the chain elements is easily available.

The tracking of the human hand and all if its chain components is rather complicated. Therefore a solution which takes a known position of the *end effector* and calculates the parameters for the rest of the chain would be more desirable.

2.2.2 Inverse Kinematics

"Inverse Kinematics (IK) is a method for computing the posture via estimating each individual degree of freedom in order to satisfy a given task"
[1]

The concept of *Inverse Kinematics* (IK) already describes it's principle in it's name. It takes the reversed approach in comparison to the FK principle in chapter 2.2.1. Instead

of knowing the states of the chain elements and calculating the resulting position of the *end effector*, we take the position of the *end effector* and try to retrieve the possible states of the other chain elements.

$$\theta = f^{-1}(\vec{s}_d) \quad (2.7)$$

The result of this equation is the vector θ for which the values of \vec{s} coincide to the desired configuration \vec{s}_d . In the case of an optimal result, this configuration would have the same position values as the target positions.

The main problem with this method occurs in the calculation of the f^{-1} function, due to it being a highly non linear operator which is not easily invertible. The approaches that [1] describes to counter this problem will be displayed later on in this chapter.

In contrary to having a unique solution with the FK approach, the IK approach can end at the point of not finding a suitable solution. Figure 2.3 displays three possible outcomes for the IK approach.

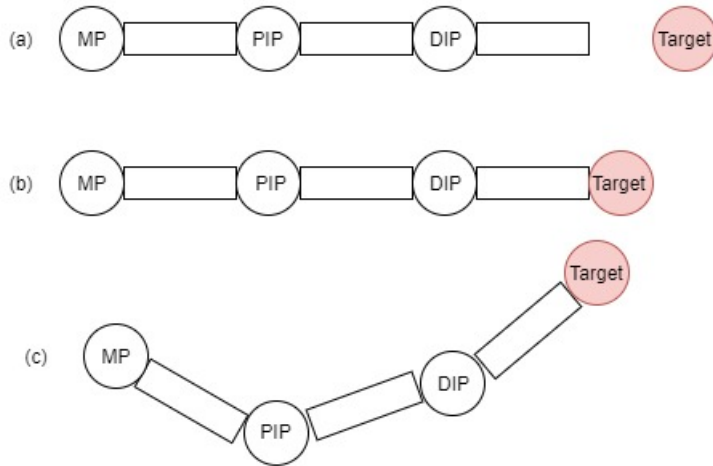


Figure 2.3: Possible solution for an IK problem of a human finger:

- (a) The given target position of the end effector can not be reached. (b) The given target can only be reached by one solution. (c) The target position can be reached with multiple different solutions.

2.2.3 Jacobian Inverse

One common approach to solve the IK problem is the utilization of a Jacobian Matrix and an iterative calculation process. This matrix contains the partial derivatives of the chain systems relative to the end effector \mathbf{s} . When using the Jacobian, a linear approximation of the IK problem will be applied for solving. The approximation's components model the end effector's relative movement to changes in transitions of the systems link translations and joint angles. Therefore, the resulting function is dependent on the joint angles θ values and can be defined as

$$J(\theta)_{ij} = \left(\frac{\partial \mathbf{s}_i}{\partial \theta_j} \right)_{ij} \quad (2.8)$$

with $i=1,\dots,k$ and $j=1,\dots,n$. Further readings on methods for the calculation of Jacobian matrices can be found in [33]. Based on definition (2.8), an entry for the j -th rotational joint would be calculated as follows:

$$\frac{\partial \mathbf{s}_i}{\partial \theta_j} = \mathbf{v}_j \times (\mathbf{s}_i - \mathbf{p}_j) \quad (2.9)$$

where \mathbf{p}_j is the position of the joint, and \mathbf{v}_j is the unit vector pointing along the current axis of rotation for the joint. Taking the derivative of definition (2.6) with respect to time gives the basic equation for forward kinematics that describes the velocities of the end effectors:

$$\dot{\mathbf{s}} = \mathbf{J}(\boldsymbol{\theta})\dot{\boldsymbol{\theta}} \quad (2.10)$$

Now having all the values for the angles, the *end effector* position and the target positions, we can compute the resulting Jacobian matrix. Thereafter we seek an update value $\Delta\boldsymbol{\theta}$ for incrementing the current joint values:

$$\boldsymbol{\theta}_{new} = \boldsymbol{\theta}_{curr} + \Delta\boldsymbol{\theta} \quad (2.11)$$

The idea here is that the chosen value for $\Delta\boldsymbol{\theta}$ should lead to the resulting $\Delta\vec{\mathbf{s}}$ being approximately equal to $\vec{\mathbf{e}}$ from (2.5). The $\vec{\mathbf{e}}$ can be approximated by:

$$\Delta\vec{\mathbf{s}} \approx \mathbf{J}(\boldsymbol{\theta}_{curr})\Delta\boldsymbol{\theta} \quad (2.12)$$

Using this approximation we can reformulate the FK problem as $\vec{\mathbf{e}} = \mathbf{J}\Delta\boldsymbol{\theta}$ and therefore our inverse kinematics problem from 2.7 can be expressed as $\Delta\boldsymbol{\theta} = \mathbf{J}^{-1}\vec{\mathbf{e}}$.

The problem we run into with this solution is the construction of the inverse Jacobian matrix. The Jacobian \mathbf{J} may not be square or invertible. In the case of it being invertible, the result may only work inferiorly because of it being nearly singular. Being singular means that no change in joint angle values may achieve the desired end effector position as an outcome.

Jacobian Transpose

One approach to calculating the value of $\Delta\boldsymbol{\theta}$ without having to calculate the inverse of \mathbf{J} is done by replacing the inverse with the transpose of \mathbf{J} .

$$\Delta\boldsymbol{\theta} = \alpha \mathbf{J}^T \vec{\mathbf{e}} \quad (2.13)$$

Of course the transpose and the inverse of \mathbf{J} are not the same thing. When using the theorems displayed in [7, 45] we can show that:

$$\langle \mathbf{J}\mathbf{J}^T \vec{\mathbf{e}}, \vec{\mathbf{e}} \rangle = \langle \mathbf{J}^T \vec{\mathbf{e}}, \mathbf{J}^T \vec{\mathbf{e}} \rangle = \|\mathbf{J}^T \vec{\mathbf{e}}\|^2 \geq 0 \quad (2.14)$$

Under a sufficiently small $\alpha > 0$ the updated angles from 2.11 will change the end effector positions by approximately $\alpha J J^T \vec{e}$. They also state that the value of α can be calculated by minimizing the new value of the error vector \vec{e} after each update.

$$\alpha = \frac{\langle \vec{e}, J J^T \vec{e} \rangle}{\langle J J^T \vec{e}, J J^T \vec{e} \rangle} \quad (2.15)$$

Jacobian Pseudo Inverse

Instead of calculating the normal inverse of the Jacoboian, which can lead to the problems described before, we can use the so called *pseudo-inverse*[6] for the calculation. The *pseudo inverse* is defined for all matrices J , even ones which are not square or not of full row rank.

$$\Delta \theta = J^\dagger \vec{e} \quad (2.16)$$

The *pseudo inverse* represents the best possible solution for $J \Delta \theta = \vec{e}$ in respect to least squares, but does suffer from instability near singularities. It has the property that the matrix $(I - J^\dagger J)$ performs a projection onto the null space of J . Therefore, for all vectors φ , $J(I - J^\dagger J)\varphi = 0$. Therefore $\Delta \theta$ can be set by

$$\Delta \theta = J^\dagger \vec{e} + (I - J^\dagger J)\varphi \quad (2.17)$$

for any vector φ and still obtain a value for $\Delta \theta$ which minimizes the value $J \Delta \theta - \vec{e}$.

The pseudo inverse of J can be derived as follows:

$$\begin{aligned} J^\dagger &= (J^T J)^{-1} J^T \\ \Delta \theta &= (J^T J)^{-1} J^T \vec{e} \\ (J^T J) \Delta \theta &= J^T \vec{e} \end{aligned} \quad (2.18)$$

Using $\vec{y} = J^T \vec{e}$, we can now solve the equation $(J^T J) \Delta \theta = \vec{y}$

Singular Value Decomposition

The usage of a *singular value decomposition* is another method of calculating the *pseudo inverse* of a jacobian matrix. A singular value decomposition of J consists of expressing J in the form

$$J = U D V^T \quad (2.19)$$

For an $m \times n$ Jacobian matrix, U is $m \times m$ and the columns are the eigenvectors of $J J^T$. D is $m \times n$, and the entries are zero except along the diagonal where $d_{ii} = \sigma_i$ with σ_i beeing the singular value and $\sigma_1 \geq \sigma_2 \geq \dots \geq \sigma_m \geq 0$. Singular values are the non-negative square roots of the eigenvalues of $J J^T$ and $J^T J$. V is $n \times n$ and the columns are the eigenvectors of $J^T J$. The construction of the pseudo inverse is done as follows:

$$J^\dagger = V D^\dagger U^T \quad (2.20)$$

The pseudo-inverse of the diagonal matrix \mathbf{D} is obtained by replacing each positive diagonal entry with it's reciprocal [15].

2.2.4 Damped Least Squares

The *Dampened Least Squares* method is applied for inverse kinematics as it avoids the singularity problems that can occur when using the pseudoinverse. It further provides a numerical stable method for selecting $\Delta\theta$. First occurrences for inverse kinematics can be found in [30, 42]. Instead of finding the minimum for $\Delta\theta$ as a best solution for the equation displayed in 2.5, the goal of this method is to find the value that minimizes the following quantity with $\lambda \in \mathbb{R}$ as a dampening factor.

$$\| J\Delta\theta - \vec{e} \|^2 + \lambda^2 \| \Delta\theta \|^2 \quad (2.21)$$

which can be rewritten to the corresponding

$$(\mathbf{J}^T \mathbf{J} + \lambda^2 \mathbf{I}) \Delta\theta = \mathbf{J}^T \vec{e} \quad (2.22)$$

and therefore

$$\Delta\theta = (\mathbf{J}^T \mathbf{J} + \lambda^2 \mathbf{I})^{-1} \mathbf{J}^T \vec{e} \quad (2.23)$$

The selection of a correct λ value is essential for this method, small values of λ give accurate solutions but low robustness to the occurrence of singular and near-singular configurations, while large values of λ result in low tracking accuracy even when a feasible and accurate solution would be possible[1, 5].

2.2.5 Newton Methods

The Newton family of methods is based on a second order Taylor series expansion of the object function $f(x)$:

$$f(x + \sigma) = f(x) + [\nabla f(x)]^T \sigma + \frac{1}{2} \sigma^T H_f(x) \sigma \quad (2.24)$$

where $H_f(x)$ is the Hessian matrix. The downside of this approach is that the calculation of the Hessian matrix bares high computational cost for each iteration as a result of its complexity. Like the approximation of the Jacobian inverse, several attempts to lower the computational cost have benn made by utilizing an approximation of the Hessian matrix based on a function gradient value.

Since the Newton methods are posed as a minimization problem, they return smooth motion without erratic discontinuities. The Newton methods also have the advantage that they do not suffer from singularity problems, such as that which occurs when finding the Jacobian Inverse.

2.2.6 FABRIK Algorithm

A more recent approach in the kinematics field is the **FABRIK** algorithm proposed by Aristidou and Lasenby[2]. As shown in section 2.2.2, these approaches all depend on computational intensive matrix operation like calculating an inverse and may have problems with matrix singularity.

The **FABRIK** algorithm does not depend on these matrix operations as it solves for the position of a point on a line to retrieve the new joint positions. This is done in a forward and also inverse solving approach, iterating these steps until the calculated position converges towards the target position from the tracking data.

Figure 2.4 illustrates the steps that are contained in one iteration step. The chain joints are denoted as \mathbf{p}_i with the distance \mathbf{d}_i being $|\mathbf{p}_{i+1} - \mathbf{p}_i|$. The target point for the end effector is denoted as \mathbf{t} . Step (a) displays the starting point of the iteration. The joint positions are taken from either a previous iteration or from an initial calibration.

But before calculations can begin, the algorithm has to check whether the intended target point \mathbf{t} is reachable for the end effector. This is done by measuring the distance between the root of the kinematic chain and the target point \mathbf{t} . This value is then compared with the sum of the distances \mathbf{d}_i .

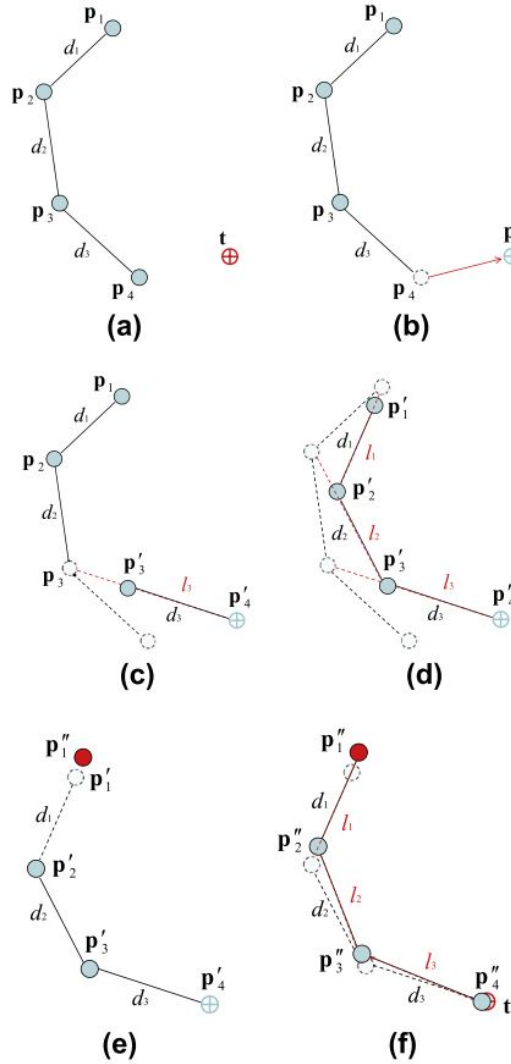


Figure 2.4: Forward and backward calculation steps for one iteration of the **FABRIK** algorithm. (a) initial position of the system. (b) End effector is moved to target position. (c) Determine position of next joint on constructed line. (d) repeat until root is reached. (e) move root joint to initial position. (f) repeat calculation in reverse direction [2]

$$dist_{t,d_1} < \sum_{k=1}^i d_i \quad (2.25)$$

The inverse calculation step is the first step, which is displayed in **(b)** and **(c)**. The calculation is started at the end effector, moving to the root of the chain. If the summed distance is greater, then the **t** is within the reach of the system and the calculation can continue, otherwise the calculation has to be aborted and the error has to be managed otherwise. Assuming this requirement to be met, we can now begin with the first calculation. Therefore we assume that the new position \mathbf{p}'_n with $n=4,\dots,1$ is equal to **t**.

$$\mathbf{p}'_n = \mathbf{t} \quad (2.26)$$

From this new point, we can construct a line that goes through \mathbf{p}'_n and \mathbf{p}_{n-1} .

$$\begin{aligned} A &= \mathbf{p}'_n \\ B &= \mathbf{p}_{n-1} \\ l_{n-1} &= \overline{AB} \end{aligned} \quad (2.27)$$

The resulting position of the new \mathbf{p}'_{n-1} point is located in this line with the distance of d_{n-1} from \mathbf{p}'_n (see **(c)**).

$$\mathbf{p}'_{n-1} = \mathbf{p}'_n + \left(\frac{\overline{AB}}{|\overline{AB}|} \cdot d_{n-1} \right) \quad (2.28)$$

Consecutively, this is done with the remaining joints until the root joint is reached (see **(d)**). This finishes the first halve of the iteration step. With the calculated positions, we now perform a forward calculation, starting from the root until we reach the end effector. Since the root of the system normally does not move from its initial position, we have to reset the root joint to this value before starting to calculate the new positions of the subsequent joints (see **(e)**).

Analogous to the procedure in the inverse step, we construct the lines between the points and determine the new position values of the joints. The end result of this step is shown in **(f)**. At this point, we can decide if the result position of the end effector is appropriate in comparison to the value of **t**. A simple threshold value for this case could be the position difference between these two points.

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3 Tracking in real space

The previous sections provided information on the structure of the human hand and how to represent it in the digital space. To apply the algorithms presented in Section 2.2 to our digital hand model, we need input data from our real world representative.

3.1 General tracking technologies

The methods for gaining positional data can be roughly categorized into two major groups, glove based methods and vision based methods. Glove based methods have already been in development since the 1980's [4] and have since then resulted in several solution attempts. Sturman and Zeltzer gave a survey on the existing tracking methods in their paper [40].

They distinguish between two areas of tracking, first the 3D positional tracking of the hand (and also other bodyparts) without regard to the hands shape and secondly the tracking of the hand shape with glove technologies.

These tracking technologies presented are still applied today in modern tracking solutions [37, 44]. They account for solutions based in optical tracking based on marker detection, magnetic detection via measurements of an artificial magnetic field[35] and acoustic measurements via triangulation of ultrasonic pings.

3.1.1 *Optical tracking*

The components for an optical tracking systems are several cameras for object detection and some kind of tracking characteristic of the object to be tracked. These characteristics can be either artificially applied ones like active flashing infrared LED on key tracking positions of the body or infrared reflective markers.

A series of cameras positioned around the tracking subject will then track these markers inside their visual fields. The second method uses a single camera to capture the silhouette image of the subject, which is analyzed to determine positions of the various parts of the body and user gestures.

The image data is supplied to special software which correlates the marker positions in the multiple viewpoints and uses the different lens perspectives to calculate a 3D coordinate for each marker. These image interpretation and correlation tasks require computationally costly operations. The marker tracking is also prone to errors through variation in lighting of the scene, material reflection properties and also marker occlusion as the trackers are moved. Also most of the systems rely on several tracking cameras for

3 Tracking in real space

a complete coverage of the tracking space. This leads to a higher system complexity in terms of setup and calibration.

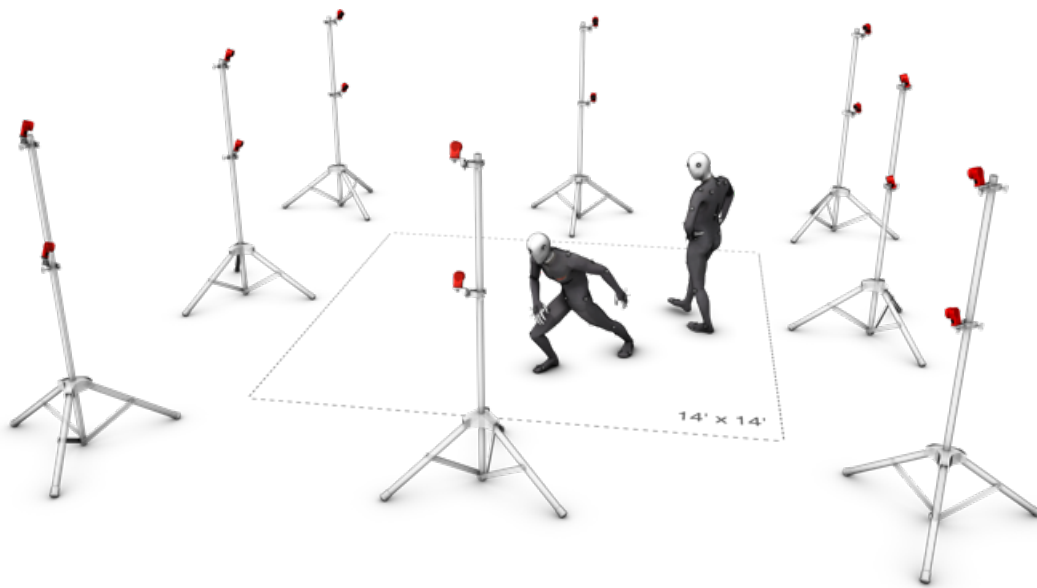


Figure 3.1: Example for an optical tracking system with passive infrared reflector markers [32]

3.1.2 Magnetic tracking

The usage of a magnetic field for position tracking is a relatively uncomplicated technique. The earth already provides us with a magnetic field to orient on. Similar to the optical trackers, magnet field sensors can be placed at key tracking positions. These sensors measure field strength in 3 orthogonal oriented axes to produce a 3D vector of the units orientation with respect to the excitation. As the earths magnetic field prone to changes based on geographical location, data corrections have to be applied to the measurements. Another solution is to generate an local magnetic field via a multi-coil source unit. The source unit coils are energized in sequence and the corresponding magnetic field vector is measured in the sensor unit. With three such excitation's, you can estimate the position and orientation of the sensor unit with respect to the source unit.

the downside of this technology is that ferromagnetic and conductive material in the surrounding environment will have an effect on the generated magnetic field. These distortion effects will form small unwanted secondary source units through the induction of small Foucault currents by the main sources magnetic field. Magnetic fields have the property of having an inverse cubic falloff as a function of distance from the source, which limits the range of operation for the system. Position resolution in the radial direction from source to sensor depends on the gradient of the magnetic field strength, and thus the positional jitter grows as the fourth power of the separation distance.

In comparison to other tracking technologies, the magnetic field tracking solution has the convenience of not suffering from line of sight problems from tracker occlusion. The magnetic fields are capable of passing through the human body. Also the sensor

size for measuring magnetic fields is rather small, giving the trackers a small volume. Furthermore, only one source unit is needed for the tracking of multiple sensor units.

3.1.3 Acoustic tracking

The principles of acoustic tracking are very similar to those of the optic tracking technologies. Instead of using lightwaves, the systems utilize acoustic pulses of ultrasonic wavelengths to time the time of flight between emitter and sensor for range measurement. To get a good measuring result from the systems, the used acoustic transducers have to be as omnidirectional as possible, so that the signal can be detected no matter how the emitter is positioned or oriented in the tracking volume. For the speakers to achieve a wide beam width, their size has to be small.

To be able to build the microphones into the tracker, they can only have active surfaces a few millimeters in diameter. This leads to a reduction in range as the efficiency of acoustic transducers is proportional to the active surface area. Also acoustic systems can have problems with ambient noises occluding the signal. This becomes even more critical when using such a system outdoors.

Sound waves travel at a much slower speed than light waves which brings benefits and downsides with it. Sound waves can be reflected from objects, producing so echos which arrive at the receiving sensor at a later point in time. Here the slower speed can be beneficial as we can await the first sound occurrence to arrive at the sensor and filter out all later reflections from the data. The reflections of the previous pulse also have to be subsided before a new measurement can be made, lowering the update rates of the system. The air the sound waves travel through is also a limiting factor as humidity, air pressure and air currents can influence the traveling sound waves. In comparison to the optical systems, the acoustic systems are not as prone to occlusion errors since sound waves have a better ability to bend around obstacles than light waves.

Most of these downside can be adressed with a combination of these systems with another form of tracking like in [13].

3.2 Hand tracking Systems

In comparison to the tracking of the whole human body, the tracking of the human hands with their maximum of 27 DoF's each in a small space is rather difficult to handle.

The systems that try to achieve this have to encounter several difficulties. Self occlusion also plays a great role in the system design, especially when working with only one tracking optical system for reduced complexity. Also these systems need to maintain a certain amount of processing speed for achieving a fluent reproduction of the captured motion. This demands the capability of processing large amounts of data in very short intervals. Most prototype testing for the described systems will be done in an controlled environment where the background is known. For a more widespread use, these systems

need to be capable of registering the hand on an unrestricted background, which may have a wide range of patterns, color and lighting differences. Also human hand motion itself is quite fast, resulting in a higher frame rate demand for the tracking cameras. The following section will describe different approaches to solve the aforementioned difficulties.

3.2.1 Sensor based

Tracking systems that make use of sensors mounted to the hand via straps or a glove have already been in use since the 1970's. First prototype glove systems included the Sayre Glove[41] and the Digital Entry Data Glove[16].

The Sayre glove is based off an idea of Richard Sayre. The system utilizes a light source and a photocell which are connected via a flexible tube. These components are mounted along each finger of the hand. The light that passes through the tube is influenced by the bending angle of the tube which corresponds to the finger bending. A large bending angle of the finger induces a larger bending angle of the tube, reducing the intensity of the light that reaches the photo diode. The resulting voltage in the photocell can then be mapped to a specific bending angle of the finger.

The Digital Entry Data Glove was patented by Gary Grimes in 1983. Instead of using only one type of sensors for measurement, this glove based systems used several sensor types for different measurements. Touch or proximity sensors were used for determining whether the user's thumb was touching another part of the hand or fingers. To measure the flexion of the joints in the thumb, index, and little finger four "knuckle-bend sensors" were used. To get measurements for the tilting of the hand in respect to the horizontal plane two tilt sensors were mounted. Finally two inertial sensors for measuring the twisting of the forearm and the flexing of the wrist were utilized. This glove was intended for creating "alphanumeric characters" from hand positions. Recognition of hand signs was performed via a hard-wired circuitry, which mapped 80 unique combinations of sensor readings to a subset of the 96 printable ASCII characters.

These early systems only provided a limited amount of sensors and were rather impractical in use. As they were developed to serve very specific applications, they were used only briefly, and never commercialized.

Newer developments in this sector include [18, 22, 27]. The *AcceleGlove* presented by [18] consists of six dual-axis accelerometers, mounted on the fingers and the back of the palm, reporting position with respect to the gravitational vector. Sensors are placed on the back of the middle phalanges, on the back of the distal phalange of the thumb, and



Figure 3.2: AcceleGlove system with the described sensor positions [18]

on the back of the palm.

Kuroda et al [22] introduced the *StrinGlov*, which obtains full degrees of freedom of human hand using 24 Inductocoders and 9 contact sensors, and encodes hand postures into posture codes on its own DSP. The bending angles of the fingers are measured with the inductocoders. These sensors relate the finger movement to a change in magnetic flux induced by the movement of the sensor parts that are attached to the finger. The sensor functionality is similar to the functionality of the light sensors from [41]. The 9 contact sensors, also based on magnetic fields, are put on the fingertips and on the inside of the hand to be able to measure contact between two fingertips or the fingertips and the hand. The system furthermore benefits from simple structure, which leads to low production cost. Majeau et al [27] proposed a system that uses optical flexion sensors to determine the bending angles of the fingers. The optical flexion sensors consist of a LED, a Photodetector and an optical fibre. The LED emits light which travels through the optical fibres and the intensity that results as the output from the fibre end is measured by the Photosensor. This measuring principle also corresponds to the principle of [41]. Furthermore the system is also capable of measuring the abduction of two fingers. Here the LED is mounted to one finger and the detector on the other. The optical fiber is run from the LED down the finger to the knuckle base and then up to the detector. When abducting the two fingers, the angle at the knuckle base changes, resulting in an intensity change at the detector through the loss of intensity at the curvature of the optic fiber. The change in intensity of both measuring techniques can be mapped to corresponding hand movements.

Further readings on sensor based hand tracking systems can be found in [10, 40]

Find 1-2 newer systems for comparison

3.2.2 Appearance Based - Optical marker

Optical approaches use properties of the human hand to estimate the current position. The evaluation of the hand pose is usually split up into two steps. The first one is the registration of the "real" hand.

This is mostly done by at least one camera which is aimed at the hand, supplying a "continuous" data stream to the evaluation Software. In the second step, the evaluation software then tries to find key spots in the provided images. This data is then used for the search of the match-



Figure 3.3: Color glove setup used by Wang and Popovic [43]

ing digital pose. The definition of these key spots can be achieved by several techniques. An example is the usage of some kind of marking for finger segments as displayed in [11, 14, 43]. In the method described by Wang and Popovic [43], a specially colored

glove is used. The glove is segmented into ten segments, colored randomly from a pool of ten distinct colors (see Figure 3.3).

The pattern is created by selecting twenty seed triangles on a 3-D hand model that are maximally distant from each other. The remaining triangles are assigned into patches based on their distance to each of these seeds. Each patch is assigned one of the ten colors at random. The jagged boundaries between the patches are artifacts from the low triangle count of the used hand model. Algorithms that use other characteristics for tracking like texture or shading [23] rely on an accurate pose from a previous frame to constrain the posture search in the current frame. When using bare hand pose estimation two different hand poses can map to similar images. This can lead to an inaccurate pose estimation and the breakdown of the algorithm if the wrong estimation is made. The benefit of the color glove is that the unique patch pattern, hand poses always map to distinguishable images, simplifying the search process. Therefore it can effectively recover itself at each frame without the need of a previous frame. With the colored glove as a tracking feature, the images from the camera are prepared for a database sampling step. The database that was used consisted of 18,000 finger configurations. A distance metric between two configurations was defined as the root mean square (RMS) error between the vertex positions of the corresponding skinned hand models. With this distance metric, a low dispersion low-dispersion sampling was used to draw a uniform set of samples from the over complete collection of finger configurations. The selected configurations are rendered at various 3-D orientations using a (synthetic) hand model at a fixed position from the (virtual) camera. The camera image was compared then compared to the database iamges. The comaprison is done via a nearest neighbor lookup using a Hausdorff-like distance [19] and penalizing the distance to the closest pixel of the same color in the other image. The resulting pose from the database can then be applied to the digital hand model. The method presented by Fredriksson and Ryen [14] also uses a color coded glove. In contrast to the fully colored glove described before, the used glove only has colored fingertips, color markers for the palm and a colored band for the wrist.

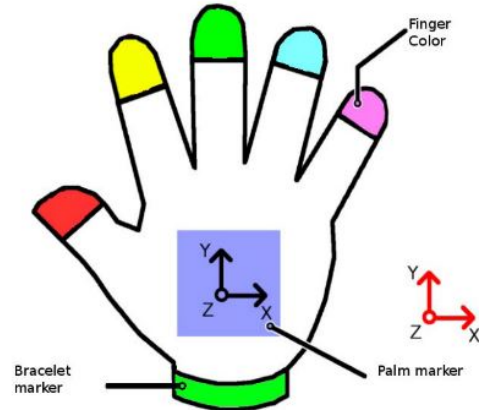


Figure 3.4: Color glove setup used by Fredriksson and Ryen [14]

The palm markers and the wrist band are used to retrieve the 3D position of the hand. The wrist marker is furthermore used to define the bounding box of the the tracking area in a calibration process. Defining a bounding greatly simplifies further image analysis operations by taking away a large amount of unneeded image data. After determining position and orientation of the hand in 3d by utilizing wrist band an palm marker position, the system tracks the grip angle and the lateral tilt angle for each finger. The grip angle

is defined as the curling of the finger towards the palm. The second angle is defined as the lateral tilt angle which measures the spread of the fingers. The grip angle is calculated by comparing the density of finger pixels around an estimated knuckle line. From the density, an estimation for the fingers Y position around an origin position at the knuckles base is made. This value is then transformed into an angle value using an inverse tangent operation.

One downside of this tracking method is that it does not yet incorporate the movement of the thumb. The thumb has other movement possibilities and therefore needs a different algorithmic approach. Also the approach only focuses on the tracking of the hand data and does not yet implement a digital counterpart like the previously described system.

3.2.3 Model Based - Image analysis

Hand tracking with image analysis of optical marker positions has the flaw that these markers have to be put onto the hand in some kind of fashion. Using a glove for this purpose imposes just a little bit of inconvenience, but has the drawback of not fitting every hand shape equally and also having to deal with hygiene when switching between users. The most natural way of tracking the human hand would be by simply using the properties of the human hand like skin color and shape for tracking. This would remove the need for any artificial added tracking features and have the greatest amount of comfort for the human user. A full overview of the technological advances in this area can be found in [28, 29]. This paper will only highlight some of the main topics displayed. As already explained before, the human hand motion leads to a large variety of shapes with many self-occlusions, which becomes even more critical when trying to reproduce the human hand pose via Computer vision. Also the separation between background image information and the relevant hand information is a major topic, which is usually also the first step in the algorithmic process. An established method for the extraction of background data was introduced by Stauffer and Grimson [39]. It uses the idea of representing each pixel value as a mixture of Gaussian functions (*MoG*) and updating these pixels during run time with new Gaussian functions. The algorithm stores mean, variance, and likelihood value, based on previous values, for each pixel location and distribution.

A new input is compared to the stored mean values for each distribution at this location. A result that is less than a constant times the variance declares that this pixel is part of that distribution and it is updated accordingly. For a higher result, a new distribution is created which replaces the least probable distribution. A new input belongs to the background if the distribution that it is part of is one of the most likely distributions. A foreground Pixel that keeps the same color over time will slowly be incorporated into the background. The decision rule, whether a new pixel belongs to an existing distribution

or not, can be written as [21]:

$$\text{if } (|P_{new} - P_{mean}^d| \leq K P_{std}^d) \text{ then } P_{new} \in \text{Distribution } d \quad (3.1)$$

where P_{new} is the new pixel value, P_{mean}^d and P_{std}^d are the stored mean value and standard deviation of distribution d , and K is a constant. The convenience of this method is that it is also able to subtract background information from uncontrolled environments, making it possible for systems to work outside of lab conditions. After the segmentation of foreground and background is achieved, the hand pose has to be retrieved from the left over image data. Solutions for retrieving a full set of DOF as hand pose estimation data can be split into two main categories [12], *Model-based tracking* and *Single frame pose estimation*.

Model-based tracking refers to a top-down tracking method based on parametric models of the 3D hand shape and its kinematic structure. The root idea here is to execute a search at each frame of an image sequence to find the pose of the shape model that best matches the features extracted from the image(s). A prediction based on previous motion and dynamics data from the object is set up as a base for the search. Optimization features can be incorporated, like employing a local search around the calculated prediction to produce a single best estimate at each frame. The downside of this method represents itself in the weakness of accumulating errors over longer run time periods due to occlusions and complexity of hand motion. These can be overcome by keeping track of multiple outcome hypotheses at each frame for error reduction.

Single frame pose estimation in contrast to the previous method, does not utilize assumptions on time coherence. At each iteration of the search algorithm the whole data set is searched for a match. This on one side introduces more computational work for achieving a match, on the other side lowers the amount of constraints that have to be put on the user when initializing the tracker system. Furthermore, the possibly rapid motion of the human hands and fingers acts as a factor for failure for time coherence dependent approaches, where a single frame approach is not as vulnerable.

4 Digital hand models

After retrieving all needed data from the real world counterpart and calculation for pose estimation is finished, the returned solution has to be displayed in the digital world. Therefore a digital hand model is needed to represent the calculated data. Modern day computer animation techniques make it possible to create nearly photo realistic digital replicas of human skin wrapped onto anatomically precisely modeled body parts. These highly complex models acquire a lot of calculation resources and are mostly not appropriate for a realtime rendering approach.

When adapting calculation data to digital hand models, those of lesser complexity are preferred, sacrificing the quality of the resulting output for speed and more fluent motion results.

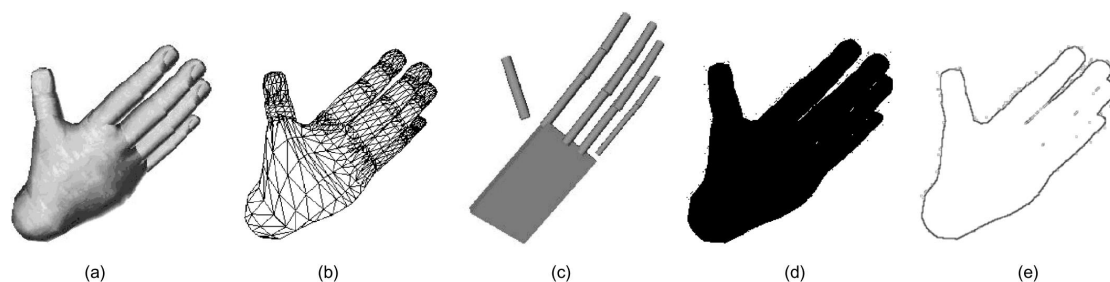


Figure 4.1: Pavlovic, Sharma et al: Hand models. Different hand models can be used to represent the same hand posture. (a) 3D Textured volumetric model. (b) 3D wire frame volumetric model. (c) 3D skeletal model. (d) Binary silhouette. (e) Contour.

[34, p. 682]

Figure 4.1 shows different model representations of the same hand posture. The models of **(a)** and **(b)** represent the aforementioned types of models that would be used in modern computer-graphics for displaying hand models realistically.

These models are based on complex 3D surfaces like *NURBS* (nonuniform rational B-splines) which are wrapped around an underlying skeleton. The wire frame model of **(b)** give a good overview of how many vertex calculation have to be made for the surface in each frame, causing these models to hardly run in real time if not supplying a large amount of computational power.

In applications where the 3D orientation of each individual finger is not necessary for processing and the general silhouette is sufficient (e.g general hand position tracking or sign language detection), even more reduced representation forms like **(d)** and **(e)** can be chosen. The model displayed in **(c)** is a simplification of the human hand structure with geometric primitives like cylinders and boxes. These geometric primitives have the

4 *Digital hand models*

virtue of being much easier to describe than a *NURBS* model. A cylinder for example is fully described by its height and its radius under the assumption that the position and orientation data is generally needed for all the described models. This type of model is also referred to as *skeletal models* as they mostly try to reproduce the structure of the human hand as described in Section 2.1

5 System prerequisites

Before elaborating a final system conception, some prerequisites have to be defined.

System components to be defined:

- Display hardware
- Tracking Technology
- Tracking Hardware
- Data cleaning
- Image analysis
- Inverse kinematics algorithm
- Hand model

5.1 Display

The first definition that has to be done is actually the last component of the processing chain. The final display hardware properties have to be defined initially as these are the determining factor for all other components. Since the goal of hand and object tracking is the most immersive when using a virtual reality headset rather than a normal display, these do not need to be taken into consideration.

Another device category which may be in the focus of interest are current mobile device platforms like *Google cardboard* or the *Samsung Gear* platform. In terms of creating a low cost consumer grade solution, these devices should be the first category to look at, as they are more widely available and do not need extra hardware except the smart-phone. Most modern devices have native support of WebGL in the browser, making it fairly easy to display VR content. They also come with the convenience of already having a set of integrated sensors for position and rotation integrated. The downside of this device class reveals when taking a look at the hardware specifications of these devices. Although the newest high tier consumer grade devices do have a good performance output for their size, but still no comparison for a desktop setup. Also these devices, as they are first of all mobile phones, lack in terms of connection ports, for wire connections, making it necessary to mostly communicate over wireless protocols. This leads to a growth in infrastructure (server, wi-fi-hotspot, etc.) and every further node in the processing chain

get device specs for current phones

leads to a physical signal delay.

After these first preliminary steps, only pure VR-Headsets like the *HTC Vive* or *Oculus Rift* should be the main focus. These headsets also provide the capabilities of motion tracking while utilizing the processing capabilities of a dedicated GPU and high-power CPU capabilities of modern desktop computers. Through these, they provide a variety of connection ports for wired connections, eliminating the need for wireless transmissions. In terms of cost, these devices do lie on the more costly side as you need the headset itself and a hardware setup which is capable of providing the output frame rate needed. But with the latest generations of GPU's and CPU's, this category was opened towards the normal consumer.

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The *HTC Vive* as well as the *Oculus Rift* are able to display 90 Images per second on their displays with each having a resolution of 2160x1200 pixels. The duration of one frame is therefore around 11 ms. This is the time frame in which the rest of the components can theoretically supply the image data, do the image analysis to retrieve the tracking data, recalculate the IK model, calculate the object position and render the whole scene.

Oculus
specs

5.2 Tracking technology

Physical sensor placed on the hand tend to give more precise tracking results compared to optical methods. The cost for the data precision is that the sensors have to be mounted to the hand in some kind of fashion. Cables or fibers, depending on sensor type, can hinder the hand movement. Utilizing a glove based system brings the downside of the "one size fits all" problem. Human hands can differ largely in size, therefore on glove will not be able to be used for a wide range of users. Furthermore cloth gloves tend to get dirty while usage and are therefore unsuitable in terms of hygiene.

Color markers can be utilized very easily. The simplest form could be colored electrical tape wrapped around the fingertips. These markers can be made disposable after usage. The size of the marker can be adapted to be large enough to realize a robust tracking while being small enough to not constrain hand movement. They also provide the possibility to perform a person specific calibration of the hand model in an initialization step. The easiest way to detect color markers is to use an optical tracking system. The downside of optical tracking methods is that depth information can only be retrieved with shadow analysis or by the use of at least 2 cameras to obtain a stereoscopic image set.

shadow
analysis
ref

5.3 Tracking Hardware

As explained in the previous chapters, the motion of the human hand can be complex and in some cases really fast. Therefore, the optical tracking hardware should ideally be

able to record images with the same or higher frequency as the display medium that is to be used. Prosumer and professional grade cameras are theoretically able to produce these kind of Frame rates (60 fps and above), but most of the time store these high frame rate videos directly to a hard drive rather than broadcasting them somewhere as most of the current day devices are not able to display such high frame rates yet. Also the hardware that is needed to record such specific high frame rates is relatively expensive. Consumer grade cameras like the GoPro that are affordable, can record at a Frame rate of 120 fps but the live transmission of this material has a time lack of several frames.

When trying to utilize low cost hardware the limitation of recording and sending a video signal from a camera to a processing hardware will therefore be limited to 60fps. This process would also introduce further latency on the transport and would force a further reduction of frame rate to satisfy the time frame given by the display frame rate.

Another option that can be taken into consideration is to completely eliminate the need to transport the image data from camera to another device. This can be achieved when the camera and the computational hardware are located on the same hardware.

The *Raspberry Pi 3* microcomputer, which comes from the internet of things world provides this capability. It combines a for its size quite powerful computation capacity with an on-board hardware connector for a camera. The camera is able to record in a FullHD resolution at 60fps and at lower resolutions up to 90fps. The camera module is directly connected on the the chipboard, providing direct access for further processing.

For a complete 3 Dimension space tracking, a one camera setup is not sufficient as it lack the data for the depth position of the object. To get this data, further hardware is needed. One option would be the utilization of a time of light based depth sensing system, but these system do come at a rather high entry level price.

prices
and lit

Another option could be the tracking pods that HTC offers as an expansion to it's vive system. These trackers could provide 3D positional data but with the downside of being relatively bulky. This would hinder the movement space of the hand and the tracker would have to be positioned on the arm as near as possible to the wrist. This would result in the position of only the wrist and not providing data on each individual finger of the hand. But as hindering as these trackers are on the hand, they could be easily used to provide tracking data for used objects. the tracker could be positioned onto the object where it does not hinder the usage.

Since the hardware setup of the Raspberry Pi with the camera is relatively easy and cost efficient, the usage of a second Raspberry Pi with a camera is good leverage point. The two cameras can be setup to create a stereoscopic camera setup which provides information about depth position through the disparity of the two camera images. Furthermore the image operations that need to be independently applied to each of the cameras frames can be done on the two separate device, eliminating the need for sending data traffic with image information through the network for post processing.

Downside of this method is that with all stereoscopic camera setups, the two cameras need to have some kind of frame synchronization to get the right two frames for evaluation.

The setup is not only meant for tracking the hand, but also for tracking objects in the tracking space, the system needs to be capable to do this task as well. Since the computational power of the raspberry is limited at some point, it is to be evaluated if a separate hardware component is needed for the object tracking or if the tracking can be integrated into the tracking procedure of the hand markers.

Another question that has to be investigated would be, how important the depth position for the to be tracked object really is as they will not be floating in space while being tracked. Maybe a combination of hand position data and object orientation can already function as a suitable tracking method.

5.4 Data cleaning

Every system that deals with the computation of live data is suspect to data fluctuation in input and output values. It is also to be assumed that the system will not be able to achieve an ideal synchronization between the cameras. This will probably introduce a degradation of tracking performance which has to be handled. It has to be evaluated at which point a data cleaning will lead to the best end results.

5.5 Image analysis

The images recorded by the camera system need to be processed further down the line to get the positional data of selected hand features. The most common library to do such kinds of image processing is the *OpenCv* library which is originally written in C and was ported into several other programming languages. It has build in features for camera calibration, color and object detection as well as several image optimization features that might be helpful for the processing.

5.6 Inverse kinematics

The inverse kinematics model is the second essential part of the setup after the tracking hardware. It receives the position data from the image post-processing and calculates the resulting current hand model position. The applied algorithm for the IK solution should be able to keep up with the data-flow from the tracking algorithm and should produce a fluid optical result on the display. As the calculation of the IK solution and the rendering of the scene with the models should be done on the same machine, computation power and memory consumption should be critical criteria. As the system will rely on optical

tracking data, an algorithm that is capable of dealing with tracker occlusions and recovery from this data loss should be prioritized. [24]

5.7 Hand model

For evaluation purposes, a rather simple model form should be used for the representation of the tracked hand in the digital space. The outcome results for tracking accuracy, update speed and the resulting match of physical and digital position of the hand are of more relevance than a highly realistic hand model.

6 System conception

6.1 Technical conception

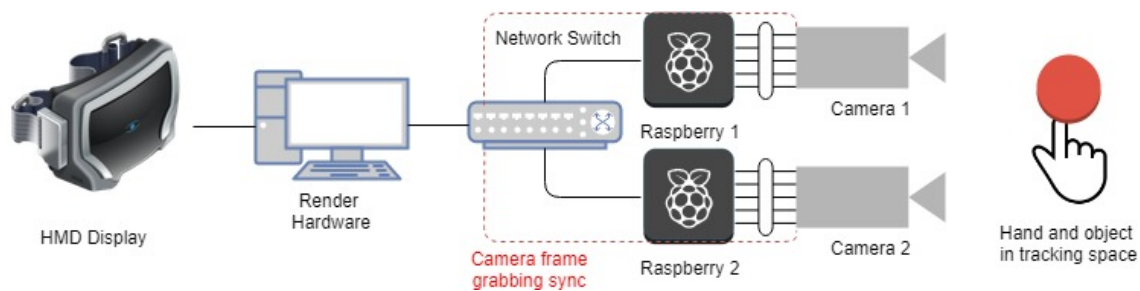


Figure 6.1: Technical conception of the single hardware parts

The technical setup of the whole system is relatively simple. Instead of using one large dimensioned unit which takes care of all calculations, the image processing steps that have to be done on both stereo images anyway, are outsourced onto the Raspberry Pi. As already mentioned in the conception phase, the image processing done directly on the Pi also reduces latency. This would occur when sending image data over network channels to the main unit.

rewrite

The two **Raspberry Pi 3 Model B**, which are used as the controllers for the **Raspberry Pi Camera** are connected via network cable to a network switch. A connection over wireless network would be possible with the on-board capabilities, but this might create latency problems and/or signal interference with other existing networks. Therefore a cable connection is the safer solution. The switch also connects to the "Master" PC to which the "Slave" Pi's communicate their data. The Master also takes care of the stereoscopic calculations, as it is dimensioned with far more computational power than the slaves. The 2D positional data from the slaves and the calculation results from the stereo image disparity is fed into the hand model running on the "Master". The model solution is then applied to the digital hand model and rendered to the HMD.

6.2 Image Analysis with OpenCV 3 and Python on the Raspberry

For the image analysis part, *OpenCV3* with its *Python 3* bindings is chosen. The *OpenCV* package needs to be downloaded and compiled onto each device before it can be used. Before the actual image analysis part can take place, the used cameras need to be calibrated. As they are basically pinhole cameras, they introduce amounts of radial

and tangential distortion to the images. These distortions need to be compensated for, especially when using them as source for the stereo images. Image distortion in these pictures would lead to incorrect calculations for image depth. *OpenCV* supplies the tools to calculate the distortion parameters as well as the camera matrix [31]. The camera matrix is basically a description for the transformation of points in 3D object space to the 2D image space of the camera. For the used Cameras, we can consider a central projection of points in space onto our image plane. The center of the camera is considered the center of an euclidean coordinate system and the projection plane z is located at distance f equal to the focal length of the camera.

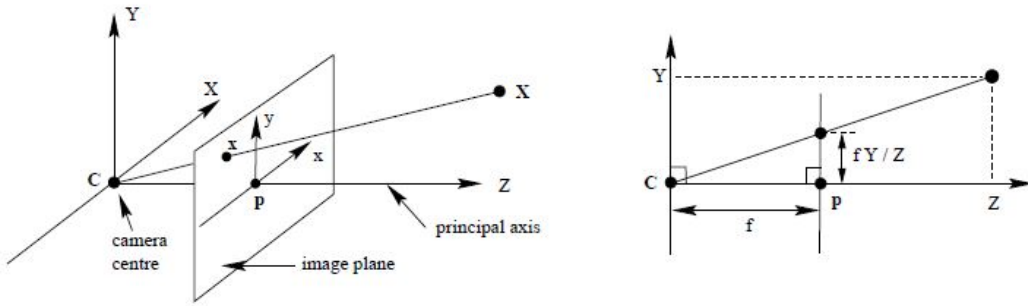


Figure 6.2: Image point projection for pinhole camera systems[17]

As shown in Figure 6.2, a point from the object space can be projected onto the image plane by drawing a ray from the object space point to the camera center. The intersection point of the ray with the image plane defines the projection point. With this knowledge the projection can be described as :

$$(X, Y, Z)^T \mapsto (fX/Z, fY/Z)^T \quad (6.1)$$

elaborate

For the calculation of the image distortion , *OpenCv* uses a chessboard image for calibration. The printed image is held in front of the camera at a constant distance and rotated and positioned differently. After every position/rotation change an image of the pattern should be taken. These images are then used to find the corners at the intersection of the black and white squares. With the previous knowledge of the square sizes, the projection errors in radial and tangential directions can be calculated:

add
Source
code

$$\begin{aligned} x_{tanDistorted} &= x(1 + k_1r^2 + k_2r^4 + k_3 + r^6) \\ y_{tanDistorted} &= y(1 + k_1r^2 + k_2r^4 + k_3 + r^6) \end{aligned} \quad (6.2)$$

$$\begin{aligned} x_{radDistorted} &= x + [2p_1xy + p_2(r^2 + 2x^2)] \\ y_{radDistorted} &= y + [p_1(r^2 + 2y^2) + 2p_2xy] \end{aligned}$$

As can be seen from the above equations, the parameters that need to be calculated are k_1, k_2, p_1, p_2, k_3 .

continue

The python program prototype that is used for tracking the specified color markers is comprised of the following components:

- Image acquisition from camera
- Image conversion to HSV colorspace
- Mask construction and Filtering
- Contour finding and position calculation
- Sending of positional data via Network as UDP Package

6.2.1 Image acquisition from camera

As the computation times for image filtering and mask generation may vary, it makes sense to separate the image acquisition from the computation part. Therefore the loading of the image data frame from the camera is outsourced into its own thread. Also this allows us to trigger the frame grabbing on both devices for synchronization. Frame grabbing synchronization can be done via triggering a PWM signal on one of the raspberry's and sending it to the other Pi. The synchronicity of the two frame reading threads is assumed for the first implementation and has to be tested on a finished setup.

The thread takes the data of the current image frame and hands it over to the main thread, where the image processing is handled. For the first frames, the full image data is needed as the position of the markers is not yet known. Performance-wise, this introduces a lot of overhead, since each mask generation step for the specific colors has to go through the complete image data, meaning every pixel has to be read out at least 5 times to get the tracking for all different markers.

6 System conception

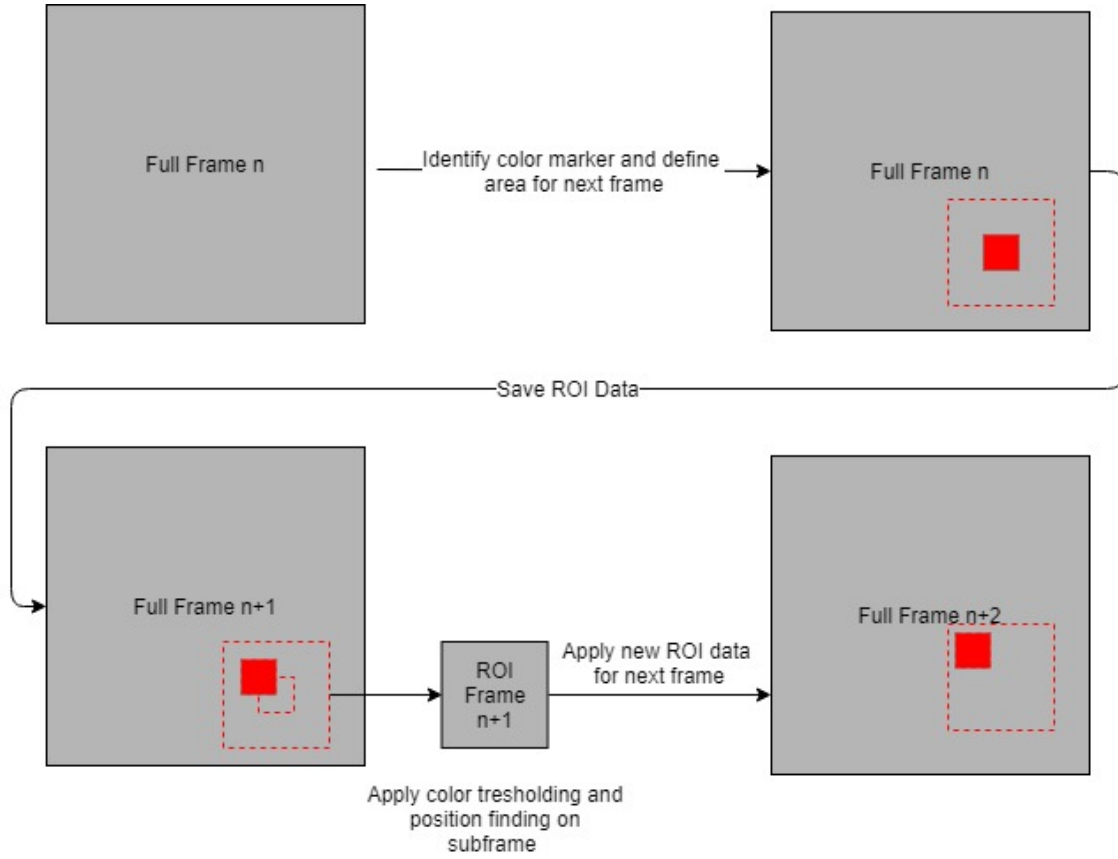


Figure 6.3: ROI calculation for consecutive frames

After a few frames, we get hold of the marker position and can define a reduced region of interest (ROI) on the image (Figure 6.3). The new ROI results from the positional data of the previous frame and has to be dimensioned correctly as to incorporate the possibility of large position differences between consecutive frames.

Furthermore the offset position, preferably the top left corner of the region, has to be kept track of. By taking a sub-region of the frame as input for further processing, the resulting coordinates relate to the top left corner of this sub-region as origin. Consequently only the first set of coordinates has the correct origin as reference point for the next frame. Consecutive frames need this information to retrieve the correct sub-region from the full frame by adding the offset to the calculated positional data. First frame ROI calculation is based on a minimum axis-aligned bounding box(AABB) fitted onto the marker. The offset value for the ROI is added to the bounding box values resulting in a rectangle data-set containing the position of the offset top-left corner \vec{tl} and the offset **width** and **height** of the ROI rectangle:

$$\begin{aligned}
 \vec{tl}_0 &= (AABB_{x_0} - \text{offset}_x, AABB_{y_0} - \text{offset}_y) \\
 \text{width} &= AABBw_0 + (2 \cdot \text{offset}_x) \\
 \text{height} &= AAB Bh_0 + (2 \cdot \text{offset}_y)
 \end{aligned} \tag{6.3}$$

These values are taken to extract the sub-region of the consecutive at \vec{tl} with size of width and height. The \vec{tl} value is also saved as offset value OffPos . The position

6 System conception

calculation for the proximate frame will utilize the offset value as follows:

$$\begin{aligned}
 \vec{tl}_{1x} &= x_1 + \vec{OffPos}_x - \text{offset}_x \\
 \vec{tl}_{1y} &= y_1 + \vec{OffPos}_y - \text{offset}_y \\
 \text{width} &= AAB B_{w_1} + (2 \cdot \text{offset}_x) \\
 \text{height} &= AAB B_{h_1} + (2 \cdot \text{offset}_y)
 \end{aligned} \tag{6.4}$$

This should result in the correct positional data for all frames following the initial frame. Finally, the resulting rectangle has to be fitted onto the size boundaries of the full image frame. When applying a fixed offset value, the resulting region that will be extracted from the following frame might reach outside the size boundaries of the full frame. This can happen when the markers are positioned near the edges of the frame. Trying to read out pixels outside the available size of the image will without doubt result into an error by reason of unavailable data at these points. Therefore the combination of position width, height and offset has to be clamped to fit into the available image data:

$$\begin{aligned}
 \text{width} &= (\max(0, \min(\text{width}, \text{image_width}))) \\
 \text{height} &= (\max(0, \min(\text{height}, \text{image_height})))
 \end{aligned} \tag{6.5}$$

Another option which could be evaluated instead of clamping the area would be shifting the offset point to a position where it does not violate the image boundaries and thereby preserving the size of the ROI.

Should no marker be found in the defined ROI or the certainty of the result is not high enough, the frame has to be dropped and the next frame should utilize the whole image data.

6.2.2 Image conversion to HSV colorspace

The image data that is supplied by the camera comes in an RGB data format, which we could already use for the further calculation. It does though make more sense to convert the input data into the HSV colorspace. Since we are not using high precision cameras, it is necessary to define a range of color values around the desired color which we want to track. The HSV colorspace is displayed as a cone, in comparison to the RGB colorspace, which is displayed as a cube. The color values for the HSV space are all located on a circle spanning from 0 to 360 degrees. The Hue value (H) corresponds to the angle on the circle, where 0° corresponds to a reddish color, 120° lies in the area of green and 240° and above correspond to blue. The saturation value (s) corresponds to the amount of white the color contains where 0 is pure white and 100 corresponds to the fully saturated color. For optimal results, only highly saturated colors should be used to ensure correct color detection. The last component is the value component (V) which describes the intensity of the color. Alike the value settings for the saturation, value ranges of at least 50 should be used for tracking precision.

For tracking the five fingers of the hand we need five distinguishable colors. Here the primary colors red, green and blue will be the choice for the first three colors. The other two selected colors are orange and yellow. To be able to clearly distinguish these colors in the video frame, a constant and homogeneous lighting is needed as well as a color temperature of the lighting that is in the neutral area to not change the color of the markers.

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results

the color conversion from the input RGB values to the desired HSV colorspace is done as follows:

$$\begin{aligned} hsv_{low} &= (hue_{targetcolor} - sensitivity, 100, 100) \\ hsv_{up} &= (hue_{targetcolor} + sensitivity, 100, 100) \end{aligned} \quad (6.6)$$

6.2.3 Mask construction and filtering

These values are the used as the parameters for a mask generation which generates a binary mask for the current frame where all pixels whose values lie outside of the specified range are set to zero (black) and the remaining are set to 255 (white). For these masks to work properly, any other larger objects that might contain similar colors should be removed from the scene to eliminate wrong tracking data. The used cameras run on an automated white balance and exposure mode. The variation of these values can cause shifts in the appearance of the colored markers and therefore alter the generated masks. To compensate for white balance shifting, a non-white ideally diffuse reflecting background should be used for the tracking space. Also the auto modes should be turned off and appropriate values for white balance and exposure have to be determined at the initialization step of the system.

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As all digital cameras tend to have signal noise in the sensor data, high frequency noise in the color channels will be present. This noise should be filtered out before any further computation on the image data can be done.

The first step in this progress is to use a Gaussian filter to blur the mask. The Gaussian filter acts as a low pass filter for the image. The application of the filter cuts out high frequency noise generated by the sensor electronic and other factors. The downside of applying a Blur onto the generated image is a loss of detail. As the markers will not be utilizing complex geometric forms or fine patterns, the loss of details is acceptable.

After this step an erosion and a dilation is applied to the image to further eliminate unwanted noise. A combination of these two morphological operation is used to further improve the data of the thresholded binary image [8, chapter 3.11-12]. Erosion and dilation operation on thresholded images perform the tasks of removing light spots on dark backgrounds as well as dark spots on light backgrounds. These spots are normally the result of the remaining image noise after the blurring or incorrect pixel values from the camera which cause the pixel to be incorrectly thresholded.

elaborate

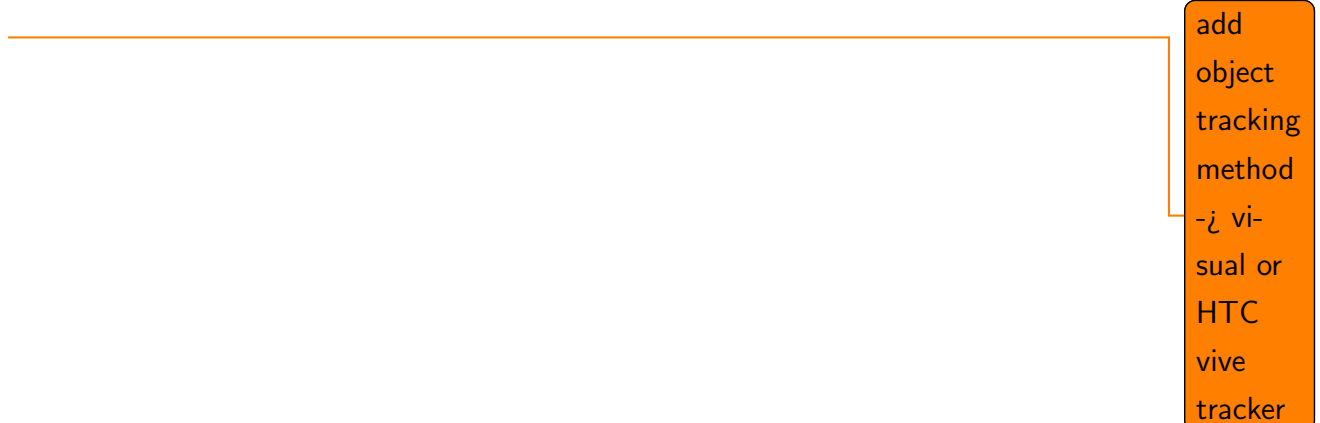
6.2.4 Contour finding and position calculation

With the cleaned mask we can continue and search for the white areas in the mask which might represent our target. Under the assumption that we have removed all other parasitic objects from the image, the marker should be the largest area of positive pixels in the mask frame. Therefore only the largest area found in the search is taken as the desired tracking marker. For the selected area, a fitting bounding box is calculated and the center of this box is used as the positional parameter of the tracking marker.

6.2.5 Sending of positional data via network as UDP package

The resulting data is then handed over to a UDP server which sends the positional data to the parent device where the stereoscopic calculations as well as the hand model and rendering is done

6.2.6 object tracking



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7 System Evaluation

7.1 Image processing performance

The image processing of the camera frames on the raspberry can be a significant bottleneck for the system. Real time evaluation demands the processing time of a frame to be in the range of the time of the camera FPS. With the current system setup running at 30fps, this means that the image processing time, containing frame readout and downstream processing of the images, has to be done in about $1/30s$ or 33 ms to achieve "real time" processing.

The first prototype implementation with *OpenCV* in *Python* showed, that this speed was reachable when only tracking one color. The implementation reached around 30-40 ms processing time when scanning whole images every time. An implementation of an "Region of interest" feature broke down the processing time to around 30 ms for a single color. The downside of the implementation was revealed when implementing the other 4 colors needed to do a full five finger tracking. This approach ramped-up up processing time to around 100 ms per frame, making this solution run at 10 FPS.

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The sequential algorithm also showed another design flaw. When not utilizing the ROI approach, the algorithm would scan the whole grabbed camera frame for each color to create the corresponding threshold map. The *OpenCV* color threshold methods are designed to only search for one color threshold at the time, therefore needing this procedure. One solution option is the already mentioned ROI usage. This solution would furthermore benefit from a multi threaded implementation, as we are not manipulating the original image. Parallel memory readout is not a problem and the generated mask can be saved separately.

Another approach which could help speed up the process is implementing an own method for thresholding the grabbed frame with the possibility to do all the needed color thresholds in one image loop. With this solution, the overhead would be reduced by 4 image iterations, thresholding operations would stay the same as these still have to be run on each pixel. The output of this method would then return the 5 needed threshold mask for further processing.

Another performance issue that arose from the first prototype was that the input camera frames came RGB coded. For better options of color separations, the image was initially converted into HSV colorspace. This operation turned out to be second longest operation after frame grabbing. Testing of the cameras showed that the color segmentation in the

original RGB images of the cameras are good enough for the used test colors, causing this step to be omitted and shaving off several milliseconds of processing time. The rest of the processing steps were lying in the sub millisecond range and are therefore not as valuable for performance optimization. The results from this prototype showed, that the *OpenCV-Python* combination is not suitable for reaching the 30 ms target time. *Python* is not a very performant language in this area. The OpenCV library used by python is actually just the ported version of the C code library with bindings for python. As C and C++ are more hardware near and therefore more performant, the second prototype implementation was done in C++. The usage of C++ as the programming language provides more control over memory management and therefore reduces unnecessary memory data copies as these can be handled by pointers to memory locations.

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time

The ported version of the Python code to C++ initially showed similar performance measurements when using the sequential approach. This was to be expected, as it is the same code the python bindings are using. Further investigation into code timings showed, that another bottleneck was the image optimization feature which applied an erosion and dilation to remove high frequency noise in the image. This operation brought the time up to 100 ms processing time when processing the whole frame area, making the algorithm not usable for "real time" application. Removing this feature brought a major speed up in processing time. Furthermore, the implementation of a thread pool, which handles all the color detection jobs, brought down the calculation time for 5 colors to around 120-140 ms. Although these times are still not usable for real time, it brought a significant performance boost.

test im-
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Test of using lower resolution than 640x480 showed that the calculation time reduced furthermore. This indicated that the ROI idea would be feasible for further performance optimizations. A test at a frame resolution of 320x240 pixels reduced the processing time for all five colors to below 10 ms.

Utilization of the knowledge from these tests led to the implementation of the aforementioned "region of interest" feature (see Figure 7.1). The first frame is analyzed as a whole frame, optimally resulting in the detection of a marker. As the marker detection creates a rectangle around the tracked area, we already have the coordinates for the ROI and only have to add an offset to this area. This value of the offset has to be set high enough to ensure that in the following frame, the tracking marker is still contained in the ROI. It also has to be ensured, that the generated ROI is clamped to the frame dimensions. If not doing so, parts of the readout are can be located outside of the image plane, causing readout errors when used for the subsequent frame. The following frames will then be processed with the input of the ROI, selecting only the defined section of the image and updating the ROI with the new data for that frame.

7 System Evaluation

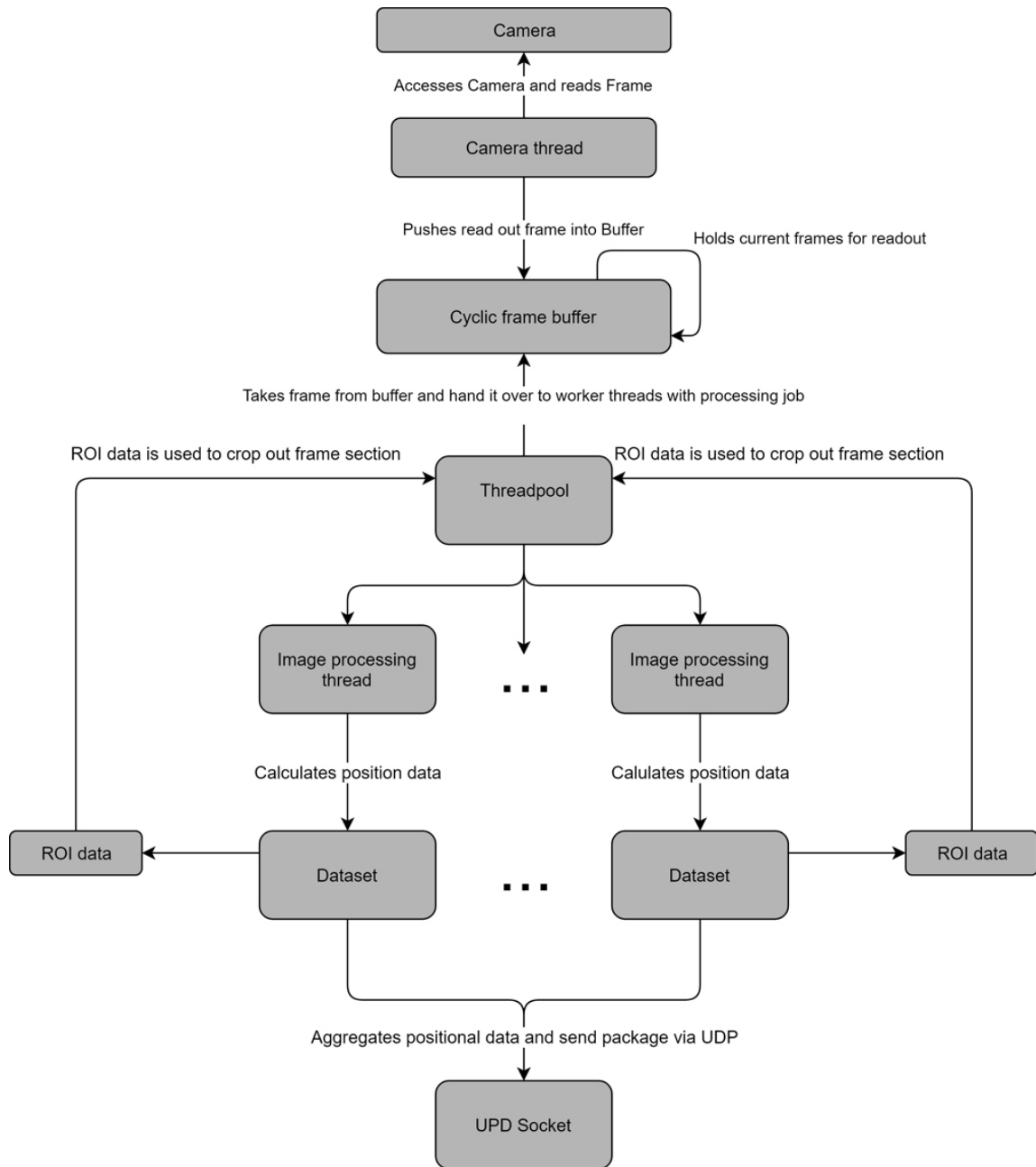


Figure 7.1: Work flow of the C++ implementation with thread pool solution and ROI

Table 7.1: My caption

Timings in ms	Python Single Thread without ROI	C++ Single Thread without ROI	C++ Single Threadpool Thread with ROI
Frame Reading			
HSV Conversion	50.852	41.125	omitted
Image Blur		147.239	varies with ROI size
Mask erode/dilate		165.663	varies with ROI size
Color Threshold		14.686	
Position Calculation			
ROI Readout			

8 Resume

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Eidesstattliche Erklärung

Ich versichere, die von mir vorgelegte Arbeit selbständig verfasst zu haben.

Alle Stellen, die wörtlich oder sinngemäß aus veröffentlichten oder nicht veröffentlichten Arbeiten anderer entnommen sind, habe ich als entnommen kenntlich gemacht. Sämtliche Quellen und Hilfsmittel, die ich für die Arbeit benutzt habe, sind angegeben.

Die Arbeit hat mit gleichem Inhalt bzw. in wesentlichen Teilen noch keiner anderen Prüfungsbehörde vorgelegen.

Köln, xx. August 2016

Oliver Kalbfleisch