

Vector Calculus

• Study of vector (and scalar) fields.

• $\vec{a} = \langle a_1, a_2, a_3 \rangle$ → vector notation.

$$\vec{a} = i a_1 + j a_2 + k a_3$$

• Sum of Vectors

$$\vec{a} + \vec{b} = \langle a_1 + b_1, a_2 + b_2, a_3 + b_3 \rangle$$

• Multiplication by Constant.

$$c\vec{a} = \langle ca_1, ca_2, ca_3 \rangle$$

• Properties

$$\vec{a} + \vec{b} = \vec{b} + \vec{a}$$

$$\vec{a} + 0 = \vec{a}, \langle 0, 0, 0 \rangle$$

$$(cd)\vec{a} = c(d\vec{a})$$

• Multiplication of Vectors

- Dot Product → ~~$\vec{a} \cdot \vec{b} = a_1 b_1 + a_2 b_2 + a_3 b_3$~~

$$\vec{a} \cdot \vec{b} = |\vec{a}| |\vec{b}| \cos \theta$$

$$\vec{a} \cdot \vec{b} = 0 \Leftrightarrow \vec{a} \perp \vec{b}$$

Perpendicular (orthogonal)

- Vector Product → $\vec{a} \times \vec{b} = \langle a_2 b_3 - a_3 b_2, a_3 b_1 - a_1 b_3, a_1 b_2 - a_2 b_1 \rangle$

$$\vec{a} \times \vec{b} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \end{vmatrix}$$

$$|\vec{a} \times \vec{b}| = |\vec{a}| |\vec{b}| \sin \theta.$$

$$\Rightarrow \vec{a} \parallel \vec{b} \Rightarrow \vec{a} \times \vec{b} = 0.$$

→ $\vec{a} \times \vec{b}$ is perpendicular to \vec{a} & \vec{b}

$$\hat{i} \times \hat{j} = \hat{k}, \hat{j} \times \hat{k} = \hat{i}, \hat{k} \times \hat{i} = \hat{j}$$

$$\hat{j} \times \hat{i} = -\hat{k}, \hat{i} \times \hat{k} = -\hat{j}, \hat{k} \times \hat{j} = -\hat{i}$$

$$\vec{a} \times \vec{b} = -(\vec{b} \times \vec{a})$$



- Interesting Properties → $\vec{a} \cdot (\vec{b} \times \vec{c}) = (\vec{a} \times \vec{b}) \cdot \vec{c}$

$$\vec{a} \times \vec{b} \times \vec{c} = (\vec{a} \cdot \vec{c}) \vec{b} - (\vec{a} \cdot \vec{b}) \vec{c}$$

$$\vec{a} \cdot (\vec{b} \times \vec{c}) = \begin{vmatrix} a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \\ c_1 & c_2 & c_3 \end{vmatrix}$$

← triple vector product identity.

$$V = |\vec{a} \cdot (\vec{b} \times \vec{c})|$$

Fields

- Scalar field is a function, $f: \mathbb{R}^n \rightarrow \mathbb{R}$
 ↑
 vector
 argument
 ↑
 scalar
 value.
 Usually $n=2$ or 3
- Vector field is a function $\vec{F}: \mathbb{R}^n \rightarrow \mathbb{R}$
 ↑
 vector
 argument
 ↑
 vector
 value.

• Arguments of scalar and vector fields are interpreted as position in space

• Example: $f(x, y, z) = x^2y + y^2z$, Temperature = $T(x, y, z)$ → scalar field

$$\vec{F}(x, y, z) = z\hat{i} + (y^2 + y)\hat{j} + xyz\hat{k}, \text{ gravitational force} \rightarrow \text{Vector field}$$

• Vector field is a function that assigns a vector to each point in space.

$$\vec{F}(x, y) = -y\hat{i} + x\hat{j}$$

• Scalar field is a function that assigns a scalar to each point in space

$$f(x, y) = xy^2 + x^3$$

• Gradient field is a special type of field

$$\begin{aligned}\vec{F}(x, y, z) &= \nabla f(x, y, z) \Rightarrow \nabla = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle \\ &= \left\langle \frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right\rangle \\ &= f_x\hat{i} + f_y\hat{j} + f_z\hat{k}\end{aligned}$$

$$\begin{aligned}E_x \cdot \nabla f(x, y, z) \cdot \nabla (xy^2 + x^3) &= \langle y^2 + 2xy, xz + x^2, xy + x^2y \rangle \\ &= (yz + 2xy)\hat{i} + (xz + x^2)\hat{j} + (xy + x^2y)\hat{k}\end{aligned}$$

at (x, y, z) , ∇f indicates direction of most rapid increase off.

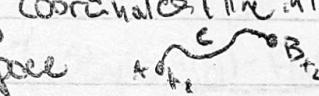
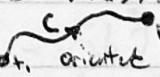
- Some vector fields are gradients of scalar fields
- If there exists scalar field f , such that $\vec{F} = \nabla f$, then \vec{F} is conservative.

Double
of
motion

Calculus of Vectors Fields

- Vector calc covers integration and differentiation.
- In that order as well

Line Integrals

- Two Types:
 - ① With respect to arc length (line integral of scalar field)
 - ② With respect to coordinates (line integral of vector field)
- Let C be a curve in 2D/3D space 
- Define \mathcal{L} with respect to arc length of scalar f over C . $\mathcal{L} = \text{Line Integral}$
- $$\int_C f(x, y, z) ds \stackrel{\text{def}}{=} \int_{t_1}^{t_2} f(x(t), y(t), z(t)) \sqrt{x'(t)^2 + y'(t)^2 + z'(t)^2} dt$$
 where $x(t), y(t), z(t)$ is parameterization of C .
- Ex find $\int_C xy ds$ where C is quarter of circle  \rightarrow parameterization of C : $x(t) = \cos t, y(t) = \sin t, t \in [0, \frac{\pi}{2}]$, $t_1 = 0, t_2 = \frac{\pi}{2}$.
- $$\int_C xy ds = \int_0^{\frac{\pi}{2}} \cos t \sin t \sqrt{\cos^2 t + \sin^2 t} dt = \int_0^{\frac{\pi}{2}} \cos t \sin t dt = \left[\frac{1}{2} \sin^2 t \right]_0^{\frac{\pi}{2}} = \frac{1}{2}$$
- If f represents density, $\int_C f ds$ represents mass.
- Let C be a curve in 2D/3D space 
- Define \mathcal{L} with respect to coordinates of vector field \vec{F} over C .
- ~~$\vec{F}(x, y, z) = P(x, y, z)\hat{i} + Q(x, y, z)\hat{j} + R(x, y, z)\hat{k}$~~
- $$\int_C \vec{F}(x, y, z) \cdot d\vec{r} = \int_C P(x, y, z) dx + Q(x, y, z) dy + R(x, y, z) dz$$
- $$= \int_{t_1}^{t_2} P(x(t), y(t), z(t)) x'(t) dt + Q(x(t), y(t), z(t)) y'(t) dt + R(x(t), y(t), z(t)) z'(t) dt$$
- $$= \int_{t_1}^{t_2} [P(x(t), y(t), z(t)) x'(t) + Q(x(t), y(t), z(t)) y'(t) + R(x(t), y(t), z(t)) z'(t)] dt$$
- Ex $\vec{F}(x, y) = y\hat{i} + x\hat{j}$  $A = (1, 2), B = (9, 8)$.

Parameterization: $x(t) = 1 + 8t, y(t) = 2 + 6t, t \in [0, 1]$

$$\int_C \vec{F} \cdot d\vec{r} \Rightarrow \int_0^1 P(x(t), y(t)) x'(t) dt + Q(x(t), y(t)) y'(t) dt = \int_0^1 y(t) x'(t) dt + x(t) y'(t) dt$$

$$= \int_0^1 (2 + 6t)(8) dt + (1 + 8t)(6) dt = \int_0^1 (16 + 48t) dt + (6 + 48t) dt = \dots = 70$$

$\int_C \vec{F} \cdot d\vec{r}$ represents work done by force field, \vec{F} , along curve C .

$$d\vec{r} = \langle dx, dy, dz \rangle$$

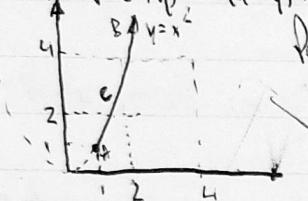
$$\vec{F} = \langle P, Q, R \rangle$$

$$\vec{F} \cdot d\vec{r} = P dx + Q dy + R dz$$

$$\frac{dx}{dt} = x'(t) \Rightarrow dx = x'(t) dt$$

Properties of Line Integrals

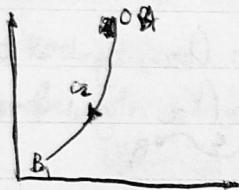
Ex. $\vec{F}(x,y) = (x-y)\vec{i} + (x+y)\vec{j}$. Compute $\int_C \vec{F} d\vec{r}$ for all



Parameterization: $x(t) = t$ $t_1 = 0$ $t_2 = 2$

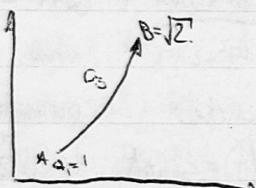
$$\begin{aligned}y(t) &= t^2 \\y'(t) &= 1 \\y''(t) &= 2\end{aligned}$$

$$\int_C \vec{F} d\vec{r} = \dots \frac{32}{3}$$



Parameterization: $x(t) = 2-t$ $t_1 = 0$ $t_2 = 2$ $\int_C \vec{F} d\vec{r} = \frac{32}{3}$

$$\begin{aligned}y(t) &= 2-t \\y'(t) &= -1 \\y''(t) &= 1\end{aligned}$$



Parameterization: $x(t) = t^2$ $t_1 = 0$ $t_2 = \sqrt{2}$ $\int_C \vec{F} d\vec{r} = 32$.

$$\begin{aligned}y(t) &= t^4 \\y'(t) &= 4t^3 \\y''(t) &= 12t^2\end{aligned}$$

- $\int_C \vec{F} d\vec{r}$ depends on orientation of C , but not on details of parameterization.

- Let $-C$ be C but in the opposite direction

$$-\int_C \vec{F} d\vec{r} = -\int_{-C} \vec{F} d\vec{r}.$$

- Remark: $\int_C f(x,y,z) ds = \int_{-C} f(x,y,z) ds$.

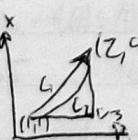
- If C is closed $A=B$, we use notation $\oint_C \vec{F} d\vec{r}$.

- Sometimes orientation is indicated $\oint_C \vec{F} d\vec{r}$ or $\oint_{C'} \vec{F} d\vec{r}$.

clockwise counter-clockwise.

Path Dependence and Independence

Ex: $\vec{F}(x,y) = y\vec{i} + 2x\vec{j}$ $\int_C \vec{F} d\vec{r} = \frac{23}{2}$



$$\begin{aligned}C: \quad x(t) &= t & t \in [0,1] \\y(t) &= t^2\end{aligned}$$

$$\int_C \vec{F} d\vec{r} = \frac{23}{2}$$

C₂: $x(t) = t$ $t \in [1,2]$ $\int_{C_2} \vec{F} d\vec{r} = \frac{35}{3}$

$$y(t) = t^2$$

C₃: $x(t) = t$ $t \in [1,2]$ $\int_{C_3} \vec{F} d\vec{r} = 13$.

$$\begin{aligned}y(t) &= 1 \\y'(t) &= 0\end{aligned}$$

$$\begin{aligned}x(t) &= 2 \\x'(t) &= 1\end{aligned}$$

- Q: When is $\int_C \vec{F} \cdot d\vec{r}$ independent of path joining A & B?
- A: (Yes for conservative forces) Fundamental theorem of calculus for line integrals

Let $\vec{f}: \mathbb{R}^3 \rightarrow \mathbb{R}$ (scalar field) have continuous partial derivatives at each point of curve C . Let C be parameterized by $\vec{r}(t) = (x(t), y(t), z(t))$ for $a \leq t \leq b$, then $\int_C \nabla f \cdot d\vec{r} = f(\vec{r}(b)) - f(\vec{r}(a))$

- Recall Fundamental theorem of calculus.

$$\int_a^b g(t) dt = [G(t)]_a^b = G(b) - G(a).$$

Implications: Let $\vec{F} = \nabla f$, $\int_C \vec{F} \cdot d\vec{r} = f(\vec{r}(b)) - f(\vec{r}(a))$
 $= f(x(b), y(b), z(b)) - f(x(a), y(a), z(a))$.

No dependence on shape of C , only on position of end points of C .

- If C is closed and \vec{F} is conservative, then $\oint_C \vec{F} \cdot d\vec{r} = 0$.
- If \vec{F} is conservative, $\vec{F} = \nabla f$, then f is called potential of \vec{F} .
- Given \vec{F} , how do we know if \vec{F} is conservative?
- If it is, how do we find potential \vec{F} ?

Fundamental Theorem of Line Integrals.

- If C is parameterized by $\vec{r}(t) = (x(t), y(t), z(t))$
 $\int_C \nabla f \cdot d\vec{r} = f(\vec{r}(b)) - f(\vec{r}(a))$, where $f(x, y, z)$ is a scalar field.
- Proof: $\nabla f = \left(\frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right)$, $d\vec{r} = (dx, dy, dz)$
 $\nabla f \cdot d\vec{r} = \int_a^b \left[\frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy + \frac{\partial f}{\partial z} dz \right] dt$
 $= \int_a^b \left[\frac{\partial f}{\partial x} x'(t) dt + \frac{\partial f}{\partial y} y'(t) dt + \frac{\partial f}{\partial z} z'(t) dt \right]$
 $= \int_a^b \left[\frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt} + \frac{\partial f}{\partial z} \frac{dz}{dt} \right] dt$

Define $G(t) = f(x(t), y(t), z(t))$

$G'(t) = \text{expression in square brackets}$

$$\int_a^b \left[\frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt} + \frac{\partial f}{\partial z} \frac{dz}{dt} \right] dt = \int_a^b G'(t) dt$$

- By fundamental theorem of calculus.

$$\int_a^b G'(t) dt = G(b) - G(a) \text{ so } f(\vec{r}(b)) - f(\vec{r}(a))$$

- This implies independence of paths for line integrals of \vec{F}
- Theorem: Let \vec{F} be conservative, i.e. $\vec{F} = \nabla f$ for some f . If the above is true in a region D , then $\int_C \vec{F} d\vec{r}$ is path independent for any curve C in region D .

* Existence of potential \Rightarrow path independence.

* One can also show ~~it~~ holds

* The Practice: Existence of potential is equivalent to path independence.

* Terminology: $\vec{F} = \nabla f$

\vec{F} conservative } The same meaning.
 \vec{F} admits potential

* If $\vec{F} = \nabla f$, f is called potential of \vec{F}

① How to determine if \vec{F} is conservative? How to find potential?

② Theorem: Let P & Q be continuous functions and continuously differentiable in the region $R = [a, b] \times [c, d]$

- Then $\vec{F} = P\hat{i} + Q\hat{j}$ is conservative in region R if and only if $\frac{\partial P}{\partial y} = \frac{\partial Q}{\partial x}$ for any $(x, y) \in R$

③ Explicit computation of

* Example: $\vec{F} = \underbrace{(6xy - y^3)}_P \hat{i} + \underbrace{(4y + 3x^2 - 3xy^2)}_Q \hat{j}$

$$-\frac{\partial P}{\partial y} = 6x - 3y^2 \quad \frac{\partial Q}{\partial x} = 6x - 3y^2$$

$\therefore \frac{\partial P}{\partial y} = \frac{\partial Q}{\partial x} \Rightarrow \vec{F}$ is conservative, there exists potential $f(x, y)$ such that $\vec{F} = \nabla f$

* Finding Potential: $-\nabla f = \left(\frac{\partial f}{\partial x}, \frac{\partial f}{\partial y} \right) \quad \vec{F} = (P, Q)$

$$\therefore \frac{\partial f}{\partial x} = P \quad \frac{\partial f}{\partial y} = Q$$

$$\begin{cases} \frac{\partial f}{\partial x} = 6xy - y^3 \\ \frac{\partial f}{\partial y} = 4y + 3x^2 - 3xy^2 \end{cases} \quad \leftarrow F(x, y) \text{ is not known.}$$

$$\begin{aligned} \therefore \int \frac{\partial f}{\partial x} dx &= \int (6xy - y^3) dx \Rightarrow f(x, y) = 3x^2y - xy^3 + C(y) \end{aligned}$$

- Substitute to 2nd equation.

$$\cancel{- \int \frac{\partial f}{\partial y} dy = \int (4y + 3x^2 - 3xy^2) dy}$$

$$\therefore \frac{\partial f}{\partial y} = 3x^2 - 3xy^2 + C'(y) \quad \text{this must equal}$$

$$- 3x^2 - 3xy^2 + C'(y) = 3x^2 - 3xy^2 + 4y \quad \text{constant} \#.$$

$$\therefore C'(y) = 4y \Rightarrow C(y) = \int 4y dy = 2y^2 + C$$

$$\therefore f(x, y) = 3x^2y - xy^3 + 2y^2 + C$$

- Note: Potential is not unique (unique up to a constant)

* Remark:- Why Conservative?

Potential Energy
↓

- In physics, potential V is usually $V = -F$

- Suppose \vec{F} be force field with potential F , $\vec{F} = \nabla F$ or
 $\vec{F} = -\nabla V$

- $\int_C \vec{F} \cdot d\vec{r} =$ work done by \vec{F} , denoted by W .

$$W = \int_C \vec{F} \cdot d\vec{r} = F(\vec{r}(b)) - F(\vec{r}(a)) = -V(\vec{r}(b)) + V(\vec{r}(a)) = V(\vec{r}(a)) - V(\vec{r}(b))$$

* Recall Newton's 2nd Law

- $\vec{F} = m\vec{a}$

$$- \vec{F}(\vec{r}(t)) = m \frac{d\vec{r}}{dt} = m\vec{v}(t) \text{ where } v(t) = \frac{d\vec{r}}{dt} \Rightarrow dv = v(t) dt.$$

$$- \int_a^b \vec{F} \cdot d\vec{r} = \int_a^b m\vec{v}(t) \cdot v(t) dt = \int_a^b m \frac{d(\frac{1}{2}\vec{v}(t) \cdot \vec{v}(t))}{dt} dt = m \left[\frac{1}{2}\vec{v}(t) \cdot \vec{v}(t) \right]_a^b$$

$$\left[\frac{1}{2}m\vec{v}^2 \right]_a^b = \frac{1}{2}m\vec{v}_b^2 - \frac{1}{2}m\vec{v}_a^2 = W = V(a) - V(b)$$

$$- \frac{1}{2}m\vec{v}_b^2 - \frac{1}{2}m\vec{v}_a^2 = V(a) - V(b) \Rightarrow \frac{1}{2}m\vec{v}_a^2 + V(a) = \frac{1}{2}m\vec{v}_b^2 + V(b)$$

- total energy is constant in conservative vector field.

Green's Theorem

* Fundamental Theorem of Line Integrals

$$- \int_C \vec{F} \cdot d\vec{r} = F(\vec{r}(b)) - F(\vec{r}(a))$$

$$- \oint_C \vec{F} \cdot d\vec{r} = 0 \quad (\text{because } \vec{r}(b) = \vec{r}(a) \text{ for closed curve})$$

* What if \vec{F} is not conservative?

$$- \oint_C \vec{F} \cdot d\vec{r} = ?$$

* Theorem - Let D be a closed region in \mathbb{R}^2 with sectionally smooth boundaries. $P(x, y), Q(x, y)$ - continuous functions with continuous partial derivatives. Let C be a boundary of D , counter-clockwise oriented. Then

$$\oint_C P dx + Q dy = \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dx dy.$$

- Note: If $\oint_C \vec{F} \cdot d\vec{r}$ is conservative, $\frac{\partial P}{\partial x} = \frac{\partial Q}{\partial y}$, $\oint_C \vec{F} \cdot d\vec{r} = 0$.

* Proof - Consider a special region D .



$$- \int_C P dx = \int_{C_1} P dx + \int_{C_2} P dx + \int_{C_3} P dx + \int_{C_4} P dx$$

- along C_2 , $x(t) = 1$, $y(t) = 0$, $dx = x'(t) dt = 0 \cdot dt$ so $C_2 \cdot dy = 0$.

$$- \int_{C_1} P dx = \int_a^b P(+, g_1(t)) dt.$$

$$- \int_{C_3} P dx = \int_b^a P(x_2 +, g_2(t)) dt$$

$$- \int_{C_4} P dx = \int_a^b P(t_1 g_1(t)) dt + \int_b^a P(t_1 g_2(t)) dt = - \int_a^b [P(t_2 g_2(t)) - P(t_1 g_1(t))] dt$$

Hilary

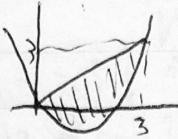


$$\bullet = - \int [P(x, g_2(x)) - P(x, g_1(x))] dx = - \int_a^b \int_{g_1(x)}^{g_2(x)} \frac{\partial P}{\partial y} dy dx$$

$$= - \int_a^b \frac{\partial P}{\partial y} dx$$

• And similarly for $\int \frac{\partial Q}{\partial x} dt$.

• Ex. find $\oint 3xy dx + 2x^2 dy$



$$\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} = 4x - 3y = x.$$

$$I = \iint_D x dA = \int_0^3 \int_{x^2}^x x dy dx = \int_0^3 [xy]_{x^2}^x dx = \int_0^3 [3x^2 - x^3] dx$$

$$= \left[x^3 - \frac{x^4}{4} \right]_0^3 = \frac{27}{4}$$

$$\bullet \text{Ex. } F = (0, x) = 0\hat{i} + x\hat{j} = x\hat{j}$$

$$\oint_D \vec{F} d\vec{r} = \oint_D 0 dy + x dy = \oint_D x dy = \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA$$

$$= \iint_D (1-0) dA = \iint_D dA = A \text{ (area of D)}$$

$$A = \oint_C x dy$$

$$\bullet \text{Consider ellipse } \frac{x^2}{a^2} + \frac{y^2}{b^2} = 1 \quad \text{Diagram of an ellipse}$$

$$A = \oint_C x dy$$

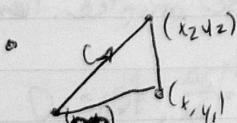
$$\text{Parameterization: } x(t) = a \cos t \quad t \in [0, 2\pi]$$

$$y(t) = b \sin t$$

$$A = \int_0^{2\pi} a \cos t \cdot y'(t) dt = \int_0^{2\pi} a \cos t \cdot b \cos t dt = \int_0^{2\pi} ab \cos^2 t dt$$

$$= \int_0^{2\pi} ab (1 + \cos 2t) dt = \int_0^{2\pi} ab dt + \int_0^{2\pi} \frac{1}{2} ab \cos 2t dt = \frac{1}{2} ab 2\pi = \pi ab$$

$$A = \pi ab$$



$$A = \oint_C x dy = - \int_{C_1} y dx$$

$$2A = \oint_C x dy - \int_{C_1} y dx$$

$$= \oint_C x dy - y dx$$

$$A = \frac{1}{2} \oint_C x dy - y dx$$

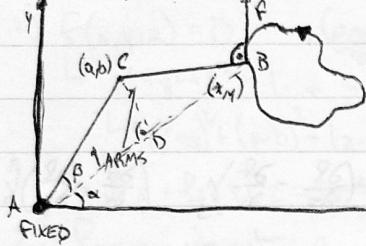
$$A = \frac{1}{2} \left[\int_{C_2} x dy - y dx + \int_{C_3} x dy - y dx + \int_{C_1} x dy - y dx \right]$$

$$A = \frac{1}{2} \int_{C_2} x dy - y dx = \frac{1}{2} (x_1 y_2 - y_1 x_2)$$

$$A = \frac{1}{2} [(a_2 - a_1)(b_3 - b_1) - (a_3 - a_1)(b_2 - b_1)]$$

- If \vec{F} has the property $\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} = 1$, then $\oint_C \vec{F} \cdot d\vec{r} = \iint_D dt = \text{Area enclosed by } C$.

Polar Parameters.



Distance travelled by wheel

$$\Rightarrow \int \vec{F} \cdot d\vec{r}$$

$$\vec{CB} = \langle x-a, y-b \rangle \quad \text{Note: } (a, b) \text{ depends on } (x, y)$$

$$\vec{F} = \langle -(y-b), x-a \rangle$$

$$(\vec{CB} \cdot \vec{F} = 0, \text{ so } \vec{CB} \perp \vec{F})$$

We need to express a, b in terms of x, y

$$\tan \alpha = \frac{y}{x} \quad \alpha = \arctan \left(\frac{y}{x} \right)$$

$$\cos \beta = \frac{|AC|}{|AC|} = \frac{1}{2}|AB| = \frac{1}{2}\sqrt{x^2+y^2} \Rightarrow \beta = \arccos \left(\frac{1}{2}\sqrt{x^2+y^2} \right)$$

$$\theta = \alpha + \beta = \arctan \left(\frac{y}{x} \right) + \arccos \left(\frac{1}{2}\sqrt{x^2+y^2} \right) \quad \begin{cases} a = \cos \theta \\ b = \sin \theta. \end{cases}$$

$$a(x, y) = \cos \left(\arctan \left(\frac{y}{x} \right) + \arccos \left(\frac{1}{2}\sqrt{x^2+y^2} \right) \right)$$

$$b(x, y) = \sin \left(\arctan \left(\frac{y}{x} \right) + \arccos \left(\frac{1}{2}\sqrt{x^2+y^2} \right) \right)$$

$$\vec{F} = \langle -y+b, x-a \rangle$$

$$P(x, y) = -y + b(x, y) \quad Q(x, y) = x - a(x, y).$$

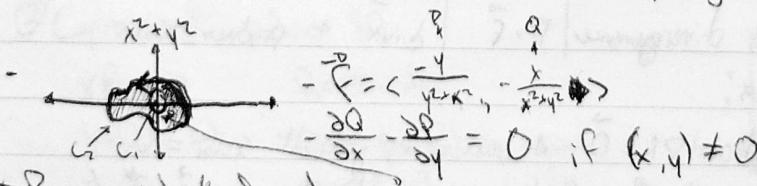
Exercise:

$$\text{Show } \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} = 1$$

Example & Application of Green's Theorem:

Compute line integral

$$\oint_C -y dx + x dy \quad \text{where } C \text{ is smooth enclosing } (0, 0).$$



- Remove disk of radius 0

$$\text{- Greens Theorem for } D: \oint_C \vec{F} \cdot d\vec{r} = \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA.$$

$$\oint_C \vec{F} \cdot d\vec{r} * \oint_C \vec{F} \cdot d\vec{r} = 0 \Rightarrow$$

$$\Rightarrow \oint_C \vec{F} \cdot d\vec{r} = - \oint_C \vec{F} \cdot d\vec{r}.$$

$$x = a \cos t, \quad x'(t) = -a \sin t$$

$$y = a \sin t, \quad y'(t) = a \cos t$$

$$\oint_C \vec{F} \cdot d\vec{r} = \int_0^{2\pi} \frac{(-a \sin t)(-a \sin t) dt + a \cos t(a \cos t) dt}{a^2 \cos^2 t + a^2 \sin^2 t} dt$$

$$= \int_0^{2\pi} dt$$

$$= 2\pi$$

$$\oint_C \frac{-y dx + x dy}{x^2+y^2} = 2\pi \quad \text{independent of } C.$$

Hilroy

Differential Operators (in \mathbb{R}^3)

• Recall $\nabla = \langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \rangle$

• ∇f = gradient of f (scalar field)

• If $\vec{F} = P\hat{i} + Q\hat{j} + R\hat{k}$

$$\bullet \nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ P & Q & R \end{vmatrix} = \left(\frac{\partial R}{\partial y} - \frac{\partial Q}{\partial z} \right) \hat{i} + \left(\frac{\partial P}{\partial z} - \frac{\partial R}{\partial x} \right) \hat{j} + \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) \hat{k}$$

• Line above can be denoted by $\text{curl } \vec{F} = \nabla \times \vec{F} =$ (sometimes $\text{rot } \vec{F}$)

$$\bullet \nabla \cdot \vec{F} = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z} \quad \text{Divergence of } \vec{F}$$

• Line above can be denoted by $\text{div } \vec{F} = \nabla \cdot \vec{F}$

• $\nabla \cdot \vec{F} = 0$ vector field.

• Ex. $\vec{F} = \langle xz, xy^2, -y^2 \rangle$

$$\text{curl } \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ xz & xy^2 & -y^2 \end{vmatrix} = (-2y - xy)\hat{i} - (0 - x)\hat{j} + (yz - 0)\hat{k} \\ = -y(2+x)\hat{i} + x\hat{j} + yz\hat{k} \quad \text{vector field.}$$

$$\text{div } \vec{F} = \frac{\partial(xz)}{\partial x} + \frac{\partial(xy^2)}{\partial y} + \frac{\partial(-y^2)}{\partial z}$$

$$= 2 + xz \quad \text{scalar}$$

• Notation: gradient ∇f produces scalar

curl $\nabla \times \vec{F}$ produces vector

divergence $\nabla \cdot \vec{F}$ produces scalar

• Identities:

- $\text{curl } \nabla f = \vec{0}$ (curl of a gradient scalar = $\vec{0}$).

- If $\vec{F} = \vec{f}$ (conservative field) then $\text{curl } \vec{F} = \vec{0}$ (conservative

fields are curl-free). Converse is true (if P, Q, R have

continuous partial derivatives $(\nabla \times \vec{F} = \vec{0}$, then \vec{F} is conservative)

• Remark: $\vec{F} = P\hat{i} + Q\hat{j} + R\hat{k}$

$$\nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ P & Q & R \end{vmatrix} = 0\hat{i} + 0\hat{j} + \left(\frac{\partial R}{\partial x} - \frac{\partial Q}{\partial y} \right) \hat{k}$$

$$- \text{curl } \vec{F} \cdot \hat{k} = \frac{\partial R}{\partial x} - \frac{\partial Q}{\partial y}$$

- Green's Theorem: $\oint_C \vec{F} \cdot d\vec{r} = \iint_D \text{curl } \vec{F} \cdot \hat{k} dA$

Surfaces

• Surfaces can be represented by:

$$1) f(x, y, z) = 0 \quad (\text{equation of surfaces})$$

$$\Leftrightarrow x^2 + y^2 + z^2 = 1 \quad \leftarrow \text{sphere of radius 1 centred at } (0, 0, 0)$$

$$\Leftrightarrow (x-a)^2 + (y-b)^2 + (z-c)^2 = R^2 \quad \leftarrow \text{sphere of radius } R \text{ centred at } (a, b, c)$$

$$\Leftrightarrow Ax + By + Cz = D \quad \leftarrow \text{plane}$$

2) Parametrization

$$\begin{cases} x(u, v) = f(u, v) \\ y(u, v) = g(u, v) \\ z(u, v) = h(u, v) \end{cases} \quad \text{where } (u, v) \text{ belong to some set in } \mathbb{R}^2$$

- u, v parameters

- Parametrization of a surface in 3D

Note:

$$x(t) = f(t), \quad y(t) = g(t),$$

$$z(t) = h(t), \quad t \in [a, b]$$

parametrization
of curve in 3D.

• Examples: ① Sphere of radius R centred at $(0, 0, 0)$.

$$\begin{cases} x = R \sin \varphi \cos \theta \\ y = R \sin \varphi \sin \theta \end{cases} \quad \theta \in [0, \pi]$$

$$\begin{cases} x = R \sin \varphi \cos \theta \\ y = R \sin \varphi \sin \theta \end{cases} \quad \theta \in [0, \pi]$$

$$z = R \cos \varphi$$

$$x^2 + y^2 + z^2 = R^2 \sin^2 \varphi \cos^2 \theta + R^2 \sin^2 \varphi \sin^2 \theta + R^2 \cos^2 \varphi = R^2$$

- φ, θ parameters



② Cylinder of radius R .

$$x \neq 0$$

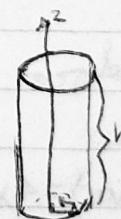
$$R = \text{constant}$$

$$y = R \sin \theta$$

θ + parameter constant

$$z = t$$

$$\theta \in [0, 2\pi], \quad t \in [0, h]$$



Note

$$x = a \cos t$$

$$y = b \sin t$$

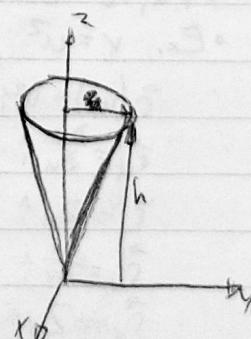
$$z = t \rightarrow \text{elliptical cylinder}$$

③ Elliptic Cone

$$\begin{cases} x = a \cos t \\ y = b \sin t \end{cases} \quad a, b = \text{constants}$$

$$\begin{cases} x = a \cos t \\ y = b \sin t \end{cases} \quad t \in [0, \pi]$$

$$z = n t \quad n = 1$$



④ Paraboloid of revolution

$$x = u \cos v \quad h - \text{constant}$$

$$y = u \sin v \quad u, v - \text{param}$$

$$z = hv^2 \quad v \in [0, 2\pi], \quad h - \text{as needed.}$$

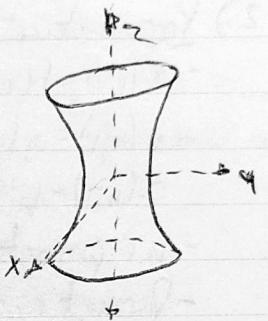


⑤ Hyperboloid of one sheet

$$x = a \sin u \cosh(v) \quad u \in [0, 2\pi]$$

$$y = b \sin u \sinh(v) \quad v - \text{as needed}$$

$$z = c \sinh(v) \quad a, b, c - \text{constants}$$



Memorize the parameterizations

Goals

- ① How to compute surface area?
- ② How to generalize line integrals into surface integrals?
- ③ Formulate Green's Theorem in 3D.

Surface area.

$$\bullet \vec{r}(uv) = \langle x(uv), y(uv), z(uv) \rangle$$

$\bullet \vec{r}_u, \vec{r}_v$ define a tangent plane.

\bullet Ex. $x = u^2, y = v^2, z = u + 2v$. Find Tangent Plane at $(1, 1, 3)$.

$$\vec{r}(uv) = u^2 \hat{i} + v^2 \hat{j} + (u + 2v) \hat{k}$$

$$\vec{r}_u = \frac{\partial \vec{r}}{\partial u} \hat{i} + \frac{\partial \vec{r}}{\partial u} \hat{j} + \frac{\partial \vec{r}}{\partial u} \hat{k}$$

$$\vec{r}_v = 2u \hat{i} + 0 \hat{j} + \hat{k} = 2u \hat{i} + \hat{k}$$

$$\vec{r}_v = \frac{\partial \vec{r}}{\partial v} \hat{i} + \frac{\partial \vec{r}}{\partial v} \hat{j} + \frac{\partial \vec{r}}{\partial v} \hat{k}$$

$$\vec{r}_v = 2v \hat{j} + 2 \hat{k}$$

$$\vec{r}_u \times \vec{r}_v = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 2u & 0 & 1 \\ 0 & 2v & 2 \end{vmatrix} = -2v \hat{i} - 4u \hat{j} + 4uv \hat{k}$$

at $(1, 1, 3), u=1, v=1$

$$-2 \hat{i} - 4 \hat{j} + 4 \hat{k} = \vec{n}$$

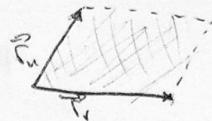
\vec{n} is the normal vector

at $(1, 1, 3)$.

$$-2(x-1) - 4(y-1) + 4(z-3) = 0$$

$$x + 2y - 2z + 3 = 0$$

tangent plane.

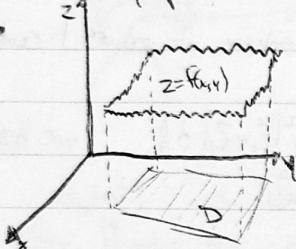


- Surface Area = $A(s) = \iint |\vec{r}_u \times \vec{r}_v| d\sigma$

Special Case:

- Surface area of $z = f(x, y)$ lying directly over region D

in $x-y$ plane



$$A = \iint_D |\vec{r}_u \times \vec{r}_v| d\sigma.$$

Natural Parameterization

$$x = u, y = v, z = f(u, v)$$

$$\vec{r} = \langle u, v, f(u, v) \rangle$$

$$\vec{r}_u = \left\langle 1, 0, \frac{\partial f}{\partial u} \right\rangle$$

$$\vec{r}_v = \begin{vmatrix} i & j & k \\ 1 & 0 & \frac{\partial f}{\partial u} \\ 0 & 1 & \frac{\partial f}{\partial v} \end{vmatrix} = i\left(-\frac{\partial f}{\partial u}\right) - j\left(\frac{\partial f}{\partial v}\right) + k = \frac{\partial f}{\partial u} i - \frac{\partial f}{\partial v} j + k.$$

$$|\vec{r}_u \times \vec{r}_v| = \sqrt{\left(\frac{\partial f}{\partial u}\right)^2 + \left(\frac{\partial f}{\partial v}\right)^2 + 1^2} = \sqrt{i + \left(\frac{\partial f}{\partial x}\right)^2 + \left(\frac{\partial f}{\partial y}\right)^2}$$

$$\vec{r}_u = \langle u, v, f_u, f_v \rangle$$

$$\vec{r}_v = \langle u, v, 0, 1 \rangle$$

Note: Arc

length \Rightarrow

$$L = \int_a^b \sqrt{1 + F'(u)^2} du$$

$$A = \iint_D \sqrt{1 + f_x^2 + f_y^2} dx dy$$

Example:

- Find surface area of a sphere of radius a , $x^2 + y^2 + z^2 = a^2$

Parameterization: $x = a \sin \varphi \cos \theta \quad D = \{(\varphi, \theta) : 0 \leq \varphi \leq \pi, 0 \leq \theta \leq 2\pi\}$

$$y = a \sin \varphi \sin \theta$$

$$z = a \cos \varphi$$

$$\vec{r}_\varphi \times \vec{r}_\theta = \begin{vmatrix} i & j & k \\ 1 & a \sin \varphi \cos \theta & a \cos \varphi \cos \theta \\ \frac{\partial x}{\partial \varphi} & \frac{\partial y}{\partial \varphi} & \frac{\partial z}{\partial \varphi} \\ \frac{\partial x}{\partial \theta} & \frac{\partial y}{\partial \theta} & \frac{\partial z}{\partial \theta} \end{vmatrix} = \begin{vmatrix} i & j & k \\ a \cos \varphi \cos \theta & a \cos \varphi \sin \theta & -a \sin \theta \\ -a \sin \varphi \sin \theta & a \sin \varphi \cos \theta & 0 \end{vmatrix}$$

$$= a^2 \sin^2 \varphi (\cos \theta i + \sin \theta j + \sin \varphi \cos \theta k)$$

$$|\vec{r}_\varphi \times \vec{r}_\theta| = \sqrt{a^4 \sin^4 \varphi \cos^2 \theta + a^4 \sin^4 \varphi \sin^2 \theta + a^4 \sin^2 \varphi \cos^2 \theta} = a^2 \sin \varphi \sqrt{\sin^2 \theta + \sin^2 \varphi \cos^2 \theta} \quad \text{since } \sin \theta \text{ is positive}$$

$$A = \iint_D a^2 \sin \varphi d\varphi d\theta = \int_0^\pi \int_0^{2\pi} a^2 \sin \varphi d\varphi d\theta = 4\pi a^2.$$

Hilroy

Surface Integral of function $f(x_{u,v})$ over the surface S .

• Surface Integral - $\iint_S f(x_{u,v}) dS \stackrel{\text{def}}{=} \iint_D f(\vec{r}(u,v)) |\vec{r}_u \times \vec{r}_v| dA$.

where $\vec{r}(u,v)$ is parametrization of S , $(u,v) \in D$.

• $\iint_S f(\vec{r}(u,v)) |\vec{r}_u \times \vec{r}_v| dA = \iint_D f(x(u,v), y(u,v), z(u,v)) |\vec{r}_u \times \vec{r}_v| dA$.

• Example: Compute $\iint_S x^2 dS$, where S is a sphere of radius 1 centered at $(0,0,0)$

$$f(x,y,z) = x^2 \quad \iint_S x^2 dS = \iint_D (\sin\varphi \cos\theta)^2 |\vec{r}_u \times \vec{r}_v| dA. \quad \text{we know } |\vec{r}_u \times \vec{r}_v| \sin\varphi$$
$$x = \sin\varphi \cos\theta \quad = \iint_D (\sin\varphi \cos\theta)^2 \sin\varphi d\varphi d\theta.$$

$$y = \sin\varphi \sin\theta \\ z = \cos\varphi$$

$$0 \leq \varphi \leq \pi \\ 0 \leq \theta \leq 2\pi$$

$$= \frac{4\pi}{3}$$

Recall Line Integrals

• $\int_C f(x,y) ds = \int_0^b f(x(t), y(t)) \sqrt{x'(t)^2 + y'(t)^2} dt$

Special Case: \mathbb{R}^2

• If S is a graph of $z = g(x,y)$ then we use x, y as parameters

$$x = x$$

$$y = y \\ z = g(x,y) \Rightarrow \vec{r} = \hat{x}\hat{i} + \hat{y}\hat{j} + g(x,y)\hat{k}$$

$$\frac{\partial \vec{r}}{\partial x} = \hat{i} + \frac{\partial g}{\partial x} \hat{k}$$

$$\frac{\partial \vec{r}}{\partial y} = \hat{j} + \frac{\partial g}{\partial y} \hat{k}$$

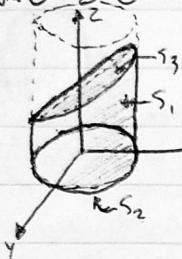
$$\vec{r}_x \times \vec{r}_y = \frac{-\partial g}{\partial x} \hat{i} - \frac{\partial g}{\partial y} \hat{j} + \hat{k}$$

$$|\vec{r}_x \times \vec{r}_y| = \sqrt{1 + g_x^2 + g_y^2}$$

$$\iint_S f(x,y,z) dA = \iint_D f(x,y, g(x,y)) \sqrt{g_x^2 + g_y^2 + 1} dx dy$$

Example:

- Compute $\iint_S z dS$, when S consists of surface of cylinder $x^2 + y^2 = 1$ above $z=0$ and below $z=1+x$.



$$\iint_S z dS = \iint_{S_1} z dS + \iint_{S_2} z dS + \iint_{S_3} z dS$$

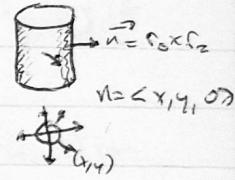
$$S_1: \begin{cases} x = \cos\theta & 0 \leq \theta \leq 2\pi \\ y = \sin\theta & \\ z = z & 0 \leq z \leq 1+\cos\theta \end{cases}$$

lower surface $z=0$
higher surface $z=1+x$

$$\vec{r}_\theta \times \vec{r}_z = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0 & 1 \\ -\sin\theta & \cos\theta & 0 \end{vmatrix} = \cos\theta \hat{i} + \sin\theta \hat{j}, \quad |\vec{r}_\theta \times \vec{r}_z| = 1$$

$$\iint_{S_1} z dS = \iint_D z |\vec{r}_\theta \times \vec{r}_z| dA = \iint_D z \cdot 1 \cdot d\theta dA = \dots = \frac{3\pi}{2}.$$

- $S_2: \iint_S z dS$ but since $\frac{x=0}{y=0} \Rightarrow z=0$ $\iint_S z dS = 0$.



- $S_3: z=1+x$

$$f(x, y, z) = z = \sqrt{(1+x)^2 + 1 + 0} dt = \sqrt{2}(1+x) dt.$$

It is a projection of $\int_0^{z_3} (1+\cos\theta) \cdot d\theta d\theta = \dots = \sqrt{2}\pi$,

on (x, y) plane

so it is a dish-like surface opening outwards

at $(0, 0)$.

$$\iint_{S_3} z dS = \iint_D 1 + \sqrt{1 + (\frac{\partial z}{\partial x})^2 + (\frac{\partial z}{\partial y})^2} dA.$$

$$(1+x)\sqrt{1+1+0} dt = \iint_D \sqrt{2}(1+x) dA.$$

$$\iint_S z dS = \iint_{S_1} z dS + \iint_{S_3} z dS = \frac{3\pi}{2} + \sqrt{2}\pi \cdot \left(\frac{3}{2} + \sqrt{2}\right)\pi$$

Orientation of Surfaces

- $\vec{r}_u \times \vec{r}_v$ is orthogonal to surface

The normal vector could face either way depending on your choosing.

- Choosing direction of normal vector is called orienting the surface

- Example: Surface $z = g(x, y)$ Define unit normal vector to $z=g(x, y)$

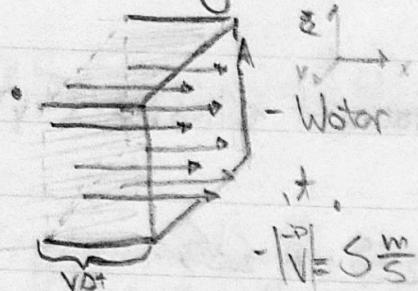
$$\vec{r} = \langle x, y, g(x, y) \rangle$$

oriented up

$$\vec{r}_x \times \vec{r}_y = -g_x \hat{i} - g_y \hat{j} + \hat{k}$$

$$\hat{n} = \frac{-g_x \hat{i} - g_y \hat{j} + \hat{k}}{\sqrt{g_x^2 + g_y^2 + 1}}, \text{ so that } |\hat{n}| = 1$$

Surface Integrals of Vector Fields



- Water flowing through zone cross-sectional area

$$\cdot \int v \, dA = S \frac{m}{s}$$

- Q: How much water (in kg) flows through A per unit time? ($\rho = 1000 \frac{\text{kg}}{\text{m}^3}$)

- Volume passing A in time $\Delta t = A v \Delta t$

- Mass passing A in time $\Delta t = \rho A v \Delta t$

- $\Delta m = \rho A v \Delta t \Rightarrow \frac{\Delta m}{\Delta t} = \rho A v \Rightarrow 1000 \cdot 5 \cdot 2 \left(\frac{\frac{kg}{m^3} \cdot \frac{m}{s} \cdot \frac{s}{s}}{\frac{kg}{s}} \right) = 10,000 \frac{\text{kg}}{\text{s}}$

- But what if A is not perpendicular to v?



In general, $\frac{\Delta m}{\Delta t} = \rho v \cdot \vec{n} \cdot A$ where \vec{n} is the normal unit vector to A
(if $\vec{v} \parallel \vec{n}$, $\vec{v} \cdot \vec{n} = |\vec{v}| = v$)

- If instead of flat A we have surface S

- 
- $\frac{\Delta m}{\Delta t} = \iint_S \rho v \cdot \vec{n} \, dS$

- In general, for vector fields $\vec{f}(x, y, z)$ the flux of \vec{F} across surface S is defined as $\iint_S \vec{f} \cdot \vec{n} \, dS$ (normal vector to S)

- Remark: If $\vec{f} = \rho \vec{v}$, then we have flux of the fluid

$$\begin{aligned} \vec{n} &= \frac{\vec{r}_n \times \vec{r}_t}{|\vec{r}_n \times \vec{r}_t|} \\ &= \frac{1}{2} \frac{\vec{r}_n \times \vec{r}_t}{|\vec{r}_n \times \vec{r}_t|} \end{aligned}$$

- Notation: $\iint_S \vec{f} \cdot d\vec{S} = \iint_S \vec{f} \cdot \vec{n} \, dS$ \leftarrow Surface Integral of Vectorfield (Type II)

- Before: $\iint_S f(x, y, z) \, dS$ \leftarrow Surface Integral of Scalar Field. (Type I)

- Note Analogy: $\int_C f(x, y, z) \, ds$ \leftarrow Line Integral of Scalarfield (Type I (1))

- $\int_C \vec{f} \cdot d\vec{r}$ \leftarrow Line Integral of Vectorfield (Type II (1))

Example:

• Find the flux of $\vec{F}(x,y,z) = z\hat{i} + y\hat{j} + x\hat{k}$ across the unit sphere

$x^2 + y^2 + z^2 = 1$

$\int \int_S \vec{F} \cdot d\vec{S} = \int \int_S \vec{F} \cdot \vec{n} dS = \int \int_D \vec{F} \cdot (\vec{r}_u \times \vec{r}_v) dA = \int \int_D \vec{F} \cdot (\vec{r}_u \times \vec{r}_v) \cdot (\vec{r}_u \times \vec{r}_v) dA$

$= \int_0^{2\pi} \int_0^\pi \vec{F} \cdot (\vec{r}_u \times \vec{r}_v) d\theta d\phi$, where $dA = dr d\theta$.

• $\vec{r}_u \times \vec{r}_v = \sin^2 \phi \cos \theta \hat{i} + \sin^2 \phi \sin \theta \hat{j} + \sin \phi \cos \theta \hat{k}$ # Parameterization
 $\vec{r}(u,v) = \sin u \cos v \hat{i} + \sin u \sin v \hat{j} + \cos u \hat{k}$

• $\vec{F}(\vec{r}(u,v)) = \cos u \hat{i} + \sin u \sin v \hat{j} + \sin u \cos v \hat{k}$

• $\int \int_S \vec{F} \cdot d\vec{S} = \int \int_D \vec{F}(\vec{r}(u,v)) \cdot (\vec{r}_u \times \vec{r}_v) dudv$

$= \int_0^{2\pi} \int_0^\pi (\cos u \hat{i} + \sin u \sin v \hat{j} + \sin u \cos v \hat{k}) \cdot (\sin^2 \phi \cos \theta \hat{i} + \sin^2 \phi \sin \theta \hat{j} + \sin \phi \cos \theta \hat{k}) dudv$

$= \int_0^{2\pi} \int_0^\pi \cos u \sin^2 \phi \cos \theta \hat{i} + \sin u \sin v \sin^2 \phi \cos \theta \hat{j} + \sin u \cos v \sin^2 \phi \cos \theta \hat{k} dudv$

$= \int_0^{2\pi} \int_0^\pi 2 \sin^2 \phi \cos^2 u \cos \theta \hat{i} + \sin^3 \phi \sin^2 v \cos \theta \hat{j} + \sin^3 \phi \cos v \cos \theta \hat{k} dudv$

$= 2 \int_0^\pi 2 \sin^2 \phi \cos^2 u \cos \theta \int_0^{2\pi} \cos u dudv + \int_0^\pi \sin^3 \phi \sin^2 v \int_0^{2\pi} \cos v dudv$

$= 2 \int_0^\pi \sin^2 \phi \cos^2 u \cos \theta \Big|_0^{2\pi} + \int_0^\pi \sin^3 \phi \sin^2 v \Big|_0^{2\pi}$

$= 4\pi$

Applications

1) Electric Field $\vec{E}(x,y,z)$

- Gauss Law

• Work Surface Q - Electric Charge in S.

$Q = \epsilon_0 \int_S \vec{E} \cdot d\vec{S}$, $\epsilon_0 = 8.85 \frac{C}{Nm^2}$

FLUX OF ELECTRICAL FIELD

2) Heat Flow

- $u(x,y,z)$ - temperature at (x,y,z)

- If u is constant heat will not flow from high to low

- Heat Flow - amount of heat (energy) flowing across surface

S per unit time

- Side: $\vec{F} = -k \nabla u$ thermal conductivity constant

- Heat Flow = $\int_S \vec{F} \cdot d\vec{S} = -k \int_S \nabla u \cdot d\vec{S}$

Example

- $U(x, y, z) = C \downarrow \text{constant.} (x^2 + y^2 + z^2)$
- $\vec{F} = -k \nabla U = -kC (2x\hat{i} + 2y\hat{j} + 2z\hat{k})$
- Let S - sphere & radius a , $x^2 + y^2 + z^2 = a^2$
- $\iint_S \vec{F} \cdot d\vec{S} = ?$
- Note: Recall that for sphere $\hat{n} = \frac{1}{a}(x\hat{i} + y\hat{j} + z\hat{k})$
- $\hat{n}^2 = |\hat{n}|^2 = 1$
- $\vec{F} \cdot \hat{n} = -\frac{2kC}{a} (x^2 + y^2 + z^2) = -\frac{2kC a^2}{a} = -2kC a$
- $\iint_S \vec{F} \cdot d\vec{S} = \iint_S \vec{F} \cdot \hat{n} dS = -2kC a \iint_S dS = -2kC a [4\pi a^2]$
 $= -8kC a^3 \pi$

Stokes Theorem

• We define $\iint_S \vec{F} \cdot d\vec{S} = \iint_S \vec{F} \cdot \vec{n} dS$ normal unit vector

• Stokes Theorem: Let S be oriented and piecewise-smooth, piece bounded by a closed piecewise-smooth curve, C piece with positive orientation. Let \vec{F} be a vector field with continuous partial derivatives on some region R^3 containing S . Then,

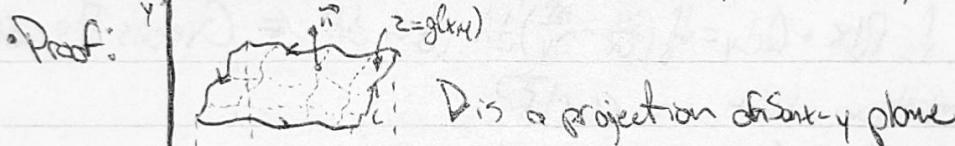
$$\oint_C \vec{F} \cdot d\vec{r} = \iint_S \operatorname{curl} \vec{F} \cdot \vec{n} dS$$

- Can use right hand rule to figure out orientation.

- Remark: C is boundary of $S \Rightarrow \iint_S \operatorname{curl} \vec{F} dS = \oint_C \vec{F} \cdot d\vec{r}$

∂S is a symbol for boundary of S .

• Proof:



D is a projection of S onto plane

$$\iint_S \operatorname{curl} \vec{F} dS = \iint_D \operatorname{curl} \vec{F} \cdot \vec{n} dA$$

$$\iint_D \left(\frac{\partial P}{\partial y} - \frac{\partial Q}{\partial x} \right) dx - \left(\frac{\partial P}{\partial z} - \frac{\partial R}{\partial x} \right) dy + \left(\frac{\partial Q}{\partial z} - \frac{\partial R}{\partial y} \right) dz$$

x component of curl of curl
y component of curl of curl

Remark:

$$\oint_C \vec{F} \cdot d\vec{r} = \iint_D \left(-P \frac{\partial g}{\partial x} - Q \frac{\partial g}{\partial y} + R \frac{\partial g}{\partial z} \right) dt$$

- Suppose C is parameterized by $x=x(t)$, $y=y(t)$. Then parameterization of C is $x=x(t)$, $y=y(t)$, $z=g(x(t), y(t))$.

For $t \in [a, b]$,

$$\oint_C \vec{F} \cdot d\vec{r} = \int_a^b P dx + Q dy + R dz = \int_a^b \left(P \frac{dx}{dt} + Q \frac{dy}{dt} + R \frac{dz}{dt} \right) dt$$

$$= \int_a^b \left(P \frac{dx}{dt} + Q \frac{dy}{dt} + R \left(\frac{\partial z}{\partial x} \frac{dx}{dt} + \frac{\partial z}{\partial y} \frac{dy}{dt} \right) \right) dt.$$

By chain rule

$$\int_a^b \left[\left(P + R \frac{\partial z}{\partial x} \right) \frac{dx}{dt} + \left(Q + R \frac{\partial z}{\partial y} \right) \frac{dy}{dt} \right] dt \Rightarrow \int_a^b \left(P + R \frac{\partial z}{\partial y} \right) dx + \left(Q + R \frac{\partial z}{\partial x} \right) dy$$

$$= \iint_D \left[\frac{\partial}{\partial x} \left(P + R \frac{\partial z}{\partial y} \right) - \frac{\partial}{\partial y} \left(P + R \frac{\partial z}{\partial x} \right) \right] dA = \iint_D \vec{F} \cdot d\vec{r}$$

$$= \iint_D \left[\left(\frac{\partial P}{\partial x} + \frac{\partial R}{\partial x} \frac{\partial z}{\partial y} + \frac{\partial R}{\partial y} \frac{\partial z}{\partial x} \right) - \left(\frac{\partial P}{\partial y} + \frac{\partial R}{\partial y} \frac{\partial z}{\partial x} + \frac{\partial R}{\partial x} \frac{\partial z}{\partial y} \right) \right] dA$$

- What is left is identical to

$$\iint_S \operatorname{curl} \vec{F} dS$$

By
Green's Theorem

Interpretation and Remarks

- Green's Theorem is a special case of Stokes

- Take $\vec{F} = P\hat{i} + Q\hat{j} + \hat{k}$, where $P = P(x, y)$ and $Q = Q(x, y)$

$$\text{curl } \vec{F} = \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ P & Q & 0 \end{vmatrix} = i\left(\frac{\partial Q}{\partial y} - \frac{\partial P}{\partial z}\right) - j\left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial z}\right) + k\left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y}\right)$$

- Let S be in (x, y) plane, $\vec{n} = \hat{k}$
- $\int_C \vec{F} \cdot d\vec{r} = \iint_S \text{curl } \vec{F} \cdot d\vec{s}$



becomes

$$\int_C P dx + Q dy = \iint_S \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) \hat{k} \cdot \hat{k} dS$$

$$\int_C P dx + Q dy = \iint_S \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA \quad (dS = dA). \Leftarrow \text{Green's Theorem}$$

- Interpretation - What is $\text{curl } \vec{F}$?

- Let $\vec{v} = \vec{v}$ (velocity of fluid)

- $\int_C \vec{v} \cdot d\vec{r} = \iint_S \text{curl } \vec{v} \cdot d\vec{s}$

$$\iint_S \text{curl } \vec{v}(P_0) \cdot \hat{n}(P_0) dS = \text{curl } \vec{v}(P_0) \cdot \hat{n}(P_0) \iint_S dS = \text{curl } \vec{v}(P_0) \cdot \hat{n}(P_0) \pi r^2$$

~~current~~

- Therefore $\text{curl } \vec{v}(P_0) \cdot \hat{n}(P_0) = \lim_{\Delta S \rightarrow 0} \frac{1}{\Delta S} \iint_S \vec{v} \cdot d\vec{r}$

- $\int_C \vec{v} \cdot d\vec{r} \geq 0$



$$\int_C \vec{v} \cdot d\vec{r} = 0$$

- curl - measure of rotation per unit area.

~~STOKES~~

Stokes' Theorem

If S is given by

$$z = g(x, y)$$

$$\iint_S \vec{F} \cdot d\vec{S}$$

$$= \iint_D \left(-P \frac{\partial z}{\partial x} - Q \frac{\partial z}{\partial y} + R \right) dA$$

for $\vec{F} = \langle P, Q, R \rangle$

$$\text{① } \iint_S \text{curl } \vec{F} \cdot d\vec{S} = \int_C \vec{F} \cdot d\vec{r} \quad \text{②}$$

• Applications: Either ① or ② is easier to complete.

• Example: Compute $\int_C \vec{F} \cdot d\vec{r}$, $\vec{F} = \langle -y^2, x, z^2 \rangle$ and C is the intersection

$$x^2 + y^2 = 1 \text{ and } y + z = 2,$$

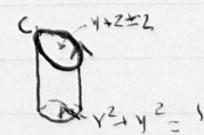
$$\iint_S \vec{F} \cdot d\vec{S} = \iint_S \text{curl } \vec{F} \cdot d\vec{S}$$

$$\text{curl } \vec{F} = \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -y^2 & x & z^2 \end{vmatrix} = 0\hat{i} + 0\hat{j} + \left(\frac{\partial x}{\partial y} - \frac{\partial (-y^2)}{\partial z} \right) \hat{k} = (1+2y)\hat{k}$$

$$g(x, y) = z = 2 - y, \vec{G} = \text{curl } \vec{F}$$

$$\iint_S \vec{G} \cdot d\vec{S} = \iint_D \left(-0 \cdot 0 - 0 \cdot (-1) + (1+2y) \right) dt$$

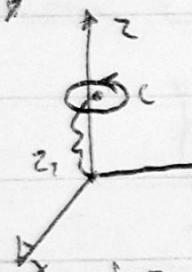
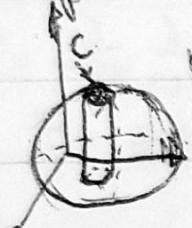
$$= \iint_D (1+2y) dt$$



$$x^2 + y^2 = 1$$

• Example. Compute $\iint_S \operatorname{curl} \vec{F} d\vec{s}$ for $\vec{F} = \langle xz, 2y, xy \rangle$, where S is

part of $x^2 + y^2 + z^2 = 4$ in the cylinder $l = x^2 + y^2$.



- Need parameterization of C (circle)

$$\rightarrow C \text{ satisfies } \begin{cases} x^2 + y^2 = 1 \\ x^2 + y^2 + z^2 = 4 \end{cases} \Rightarrow z^2 = 3, z = \pm\sqrt{3}.$$

$$\text{Parameterization of } C: \begin{array}{l} x(t) = \cos t \\ y(t) = \sin t \\ z(t) = \sqrt{3} \end{array} \quad \begin{array}{l} x'(t) = -\sin t \\ y'(t) = \cos t \\ z'(t) = 0 \end{array}$$

$$\int_C \vec{F} \cdot d\vec{s} = \int_0^{2\pi} P dx + Q dy + R dz = \int_0^{2\pi} xz dx + yz dy + xy dz =$$

$$= \int_0^{2\pi} x(t)z(t)x'(t)dt + y(t)z(t)y'(t)dt + \cancel{x(t)y(t)dz} =$$

$$= 0.$$

The Divergence Theorem

$$\cdot \nabla = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle, \vec{F} = \langle U, V, W \rangle$$

$$\cdot \operatorname{div} \vec{F} = \nabla \cdot \vec{F} = \frac{\partial U}{\partial x} + \frac{\partial V}{\partial y} + \frac{\partial W}{\partial z}$$

* Theorem: Let E be a solid with which is x -simple, y simple \hat{z} simple. Let S be the surface of E , with positive (outward) orientation. Let \vec{F} be a smooth vector field.

$$\text{Then } \iint_S \vec{F} \cdot d\vec{S} = \iiint_E \operatorname{div} \vec{F} dV$$

$$= \text{Remark: } \iint_S \operatorname{div} \vec{F} dV = \iint_S \vec{F} \cdot d\vec{S} \quad (\text{if } E \text{ is boundary of } E)$$

$$\textcircled{1} \quad \iint_S \operatorname{curl} \vec{F} \cdot d\vec{S} = \iint_E \vec{F} \cdot d\vec{r}$$

$$\textcircled{2} \quad \int_{a}^{b} \frac{\partial F}{\partial x} dx = F(b) - F(a) \quad (\text{FTC})$$

$$\int_a^b \frac{\partial f}{\partial x} dx = \int_a^b f' dx$$

$$\text{Left: } \int_a^b f' dx \quad \text{Right: } f(x)$$

Flux over S

* Interpretation: If \vec{F} such that $\operatorname{div} \vec{F} = 0$, then $\iint_S \vec{F} \cdot d\vec{S} = 0$

- Think of electric field E where $\iint_S E \cdot d\vec{S} = 0$ for closed surface (no charge in S) \Rightarrow no source of field inside.

- $\operatorname{div} \vec{F} = 0$ - source free vector field.

- If at (x_0, y_0, z_0) , we have $\operatorname{div} \vec{F}(x_0, y_0, z_0) \neq 0$ then $\begin{cases} \operatorname{div} > 0 \text{ source} \\ \operatorname{div} < 0 \text{ sink} \end{cases}$

- $\vec{F} = \langle P, Q, R \rangle$

Source



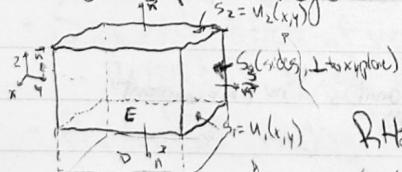
Sink



Source free



* Proof: Simplified Region E



$$\vec{F} = \langle P, Q, R \rangle$$

$$\text{RHS: } \iiint_E \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z} \right) dV = \underbrace{\iint_S \frac{\partial P}{\partial x} dV}_{\textcircled{1}} + \underbrace{\iint_S \frac{\partial Q}{\partial y} dV}_{\textcircled{2}} + \underbrace{\iint_S \frac{\partial R}{\partial z} dV}_{\textcircled{3}}$$

$$(\text{HS:}) = \iint_S \vec{F} \cdot d\vec{S} = \iint_S (P \hat{i} + Q \hat{j} + R \hat{k}) \cdot \vec{n} dS = \iint_S P \hat{i} \cdot \vec{n} dS + \iint_S Q \hat{j} \cdot \vec{n} dS + \iint_S R \hat{k} \cdot \vec{n} dS$$

$$\textcircled{1} = \textcircled{6} \quad \textcircled{2} = \textcircled{5} \quad \textcircled{3} = \textcircled{4}$$

$$\textcircled{3} = \iint_S \frac{\partial R}{\partial z} dS = \iint_S R \hat{k} \cdot \vec{n} dS = \iint_S R \hat{k} \cdot \vec{n} dS + \iint_{S_1} R \hat{k} \cdot \vec{n} dS + \iint_{S_2} R \hat{k} \cdot \vec{n} dS$$

use surface integral formula: $z = g(x, y)$

$$\iint_S G \cdot \vec{n} dS = \iint_D (-\frac{\partial g}{\partial x} \frac{\partial g}{\partial y} + R) dA \Rightarrow \textcircled{3} = \iint_S R(x, y, g(x, y)) dS + \iint_D R(x, y, g(x, y)) dA$$

$$G = R \hat{k} = \langle 0, 0, R \rangle$$

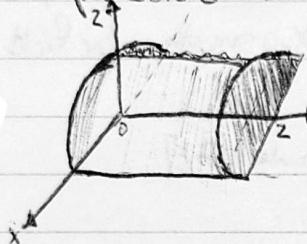
$$\textcircled{3} = \textcircled{8}$$

Hilroy

Example of Application

- $\vec{F} = \langle x + \cos y, y + \sin z, z + e^x \rangle$

- Compute flux over our surface S , bounded by $z=0, y=0, y=2$, planes and paraboloid $z=1-x^2$



$$\iint_S \vec{F} \cdot d\vec{s} =$$

$$\text{div } \vec{F} = 1+1+1=3$$

$$\iint_S \vec{F} \cdot d\vec{s} = \iint_E 3 dV = \int_{-1}^1 \int_{0}^{1-x^2} 3 dz dy dx = 8$$

If \vec{F} is "simpler" than \vec{F} , then $\iint_S \vec{F} \cdot d\vec{s}$

More Complex Applications



S_1 is inside of S_2

S_1 is empty, inside.

$$\iint_E \text{div } \vec{F} = \iint_S \vec{F} \cdot d\vec{s} = \iint_S \vec{F} \cdot \vec{n} dS = \iint_S \vec{F} \cdot (\vec{n}_1) dS + \iint_{S_2} \vec{F} \cdot \vec{n}_2 dS$$

$$S = S_1 \cup S_2$$

$$= - \iint_{S_1} \vec{F} \cdot \vec{n}_1 dS + \iint_{S_2} \vec{F} \cdot \vec{n}_2 dS$$

$$\text{If } \text{div } \vec{F} = 0, \text{ then } \iint_S \vec{F} \cdot \vec{n} dS = \iint_{S_2} \vec{F} \cdot \vec{n}_2 dS$$

We can replace complicated S by simple S_2 (sphere).

Electric Field

$$\text{We know } \vec{E} = \frac{kq}{r^3} \vec{r}, \text{ where } \vec{r} = \langle x, y, z \rangle$$

$$\vec{E} = \frac{kq}{r^3} \vec{r} \quad \leftarrow \text{Coulomb's law (k=constant)}$$

$$\vec{E} = \frac{kq}{(x^2+y^2+z^2)^{\frac{3}{2}}} \cdot \langle x, y, z \rangle$$

Compute flux of \vec{E} over S enclosing q .

$$\text{div } \vec{E} = kq \left[\frac{1}{r^3} (\nabla \cdot \vec{r}) + \left(\frac{1}{r} \right) \cdot \vec{r} \right] = kq \left[\frac{3}{r^3} - \frac{3}{2} (x^2+y^2+z^2)^{-\frac{5}{2}} (2x^2y^2z^2 + x^2+y^2+z^2) \right]$$

$$= kq \left[\frac{3}{r^3} - 3 \cdot \frac{1}{r^5} (x^2+y^2+z^2) \right] = kq \left[\frac{3}{r^3} - 3 \cdot \frac{1}{r^5} r^2 \right] = kq \left[\frac{3}{r^3} - 3 \cdot \frac{1}{r^3} \right] = 0$$

If $r \neq 0$, $\text{div } \vec{E} = 0$

$$\vec{E} \cdot \vec{n} = \frac{kq}{r^3} \vec{r} \cdot \vec{n} = \frac{kq}{r^3} \vec{r} \cdot \vec{r} = \frac{kq}{r^3} r^2 = \frac{kq}{r^2}$$

$$\iint_S \vec{E} \cdot \vec{n} dS = \iint_S kq dS = kq \cdot 4\pi r^2 = 4\pi kq$$

$$\iint_S \vec{E} \cdot d\vec{s} = \iint_S \vec{E} \cdot \vec{n} dS$$

only surface
square, s
enclosing (p, q)
of size 1

View identity for scalar field f , and vector field G

$$\nabla \cdot (fG) =$$

$$f(\nabla \cdot G) + \nabla f \cdot G \text{ or}$$

$$f \text{div } G + g \text{ grad } f \cdot G$$

$$\nabla \cdot \vec{r} = \langle x, y, z \rangle = 3$$

$$\nabla \cdot \vec{r} = \langle x^2+y^2+z^2 \rangle^{-\frac{3}{2}}$$

$$= -\frac{3}{2} (x^2+y^2+z^2)^{-\frac{5}{2}}$$

Flux of \vec{E} produced by single charge q , is

$$\iint_S \vec{E} \cdot d\vec{s} = 4\pi kq$$

(from 1st Law)

Remarks about Divergence.

- $S_r \rightarrow$ Sphere of radius, r
- $B_r \rightarrow$ Solid ball bounded by S_r .
- What is the meaning of $\operatorname{div} \vec{F}$ at P ?
- $\int \vec{F} \cdot d\vec{s} \stackrel{\text{def}}{=} \iiint_{B_r} \operatorname{div} \vec{F} dV \approx \iint_{S_r} \operatorname{div} \vec{F}(p) dV = \operatorname{div} \vec{F}(p) \iint_{S_r} dV = \operatorname{div} \vec{F}(p) V_r$
- $\Rightarrow \operatorname{div} \vec{F}(p) = \frac{1}{V_r} \iint \vec{F} \cdot d\vec{s} \Rightarrow \operatorname{div} \vec{F}(p) = \lim_{r \rightarrow 0} \iint \vec{F} \cdot d\vec{s}$
- $\operatorname{div} \vec{F}(p) > 0$, P is a source of \vec{F}
- $\operatorname{div} \vec{F}(p) < 0$, P is a sink of \vec{F}

Physical Applications:

- $\vec{E} = \text{electric field}$ ①
- $\operatorname{div} \vec{E} = 0$ at any point where there is no charge difference
- $\operatorname{div} \vec{E} = \frac{q}{\epsilon_0}$ otherwise ($q = \text{charge}$, $\epsilon_0 = \text{constant}$)
- $\vec{B} = \text{Magnetic Field}$ ②
- $\nabla \cdot \vec{B} = 0$ everywhere (no single magnetic charge or monopole)
- By divergence theorem, ①, ② can be written in integral form
 - $\iint \vec{E} \cdot d\vec{s} = \frac{q}{\epsilon_0} \iiint \vec{E} dV$ (Gauss' Law)
 - $\iint \vec{B} \cdot d\vec{s} = 0$ (Gauss' Law for magnetism)

Some identities of vector field theory Laplacian

$$\nabla \cdot (\nabla f) = \nabla \cdot \left(\frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right) = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} = \nabla^2 f$$

- Problem of finding f such that $\nabla^2 f = 0$ \leftrightarrow Laplace Equation is equivalent to finding potential of vector field with zero divergence

- Greens Identities $\frac{\partial F}{\partial n} \stackrel{\text{def}}{=} \nabla F \cdot \vec{n}$ $\vec{n} = \text{directional derivative}$
- $\iint \frac{\partial F}{\partial n} dS = \iint \nabla F \cdot \vec{n} dS = \iint \nabla F \cdot \vec{dS} = \iiint \nabla \cdot \nabla F dV = \iiint \nabla^2 F dV$

- First Greens Identity $\iint F \frac{\partial F}{\partial n} dS = \iiint \operatorname{div} F dV$

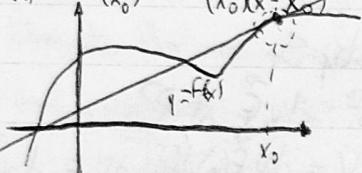
$$\begin{aligned} \rightarrow \text{Proof: } \iint F \nabla F \cdot \vec{n} dS &= \iint F \cdot \nabla F dS = \iint \nabla \cdot (F \nabla F) dV = \iint (\nabla F \cdot \nabla F + F \nabla \cdot \nabla F) dV \\ &= \iint (\nabla F)^2 + F \nabla^2 F dV = \iiint |\nabla F|^2 dV \end{aligned}$$

- Second Greens Identity $\iint F \frac{\partial g}{\partial n} dS = \iiint (f \nabla^2 g - g \nabla^2 f) dV$

Hilroy

Interpretation of Vector Field Operators (div, curl) in the Light of ~~Linear~~ Linear Algebra

for smooth functions

- We know that $f(x) = f(x_0) + f'(x_0)(x - x_0) + \frac{1}{2} f''(x_0)(x - x_0)^2 + \dots$
- $f(x) = f(x_0) + f'(x_0)(x - x_0)$ for $x \in (x_0 - \epsilon, x_0 + \epsilon)$ for small ϵ
- 
- $y = f(x_0) + f'(x_0)(x - x_0)$ a linear function

- Above is local linear approximation
- Vector field is a function $\mathbb{R}^2 \rightarrow \mathbb{R}^2$ (in 2D) or $\mathbb{R}^3 \rightarrow \mathbb{R}^3$ (in 3D)
- In 2D, $F(x, y) = P_i + Q_j = \langle P, Q \rangle$
- We can write F as "column vector function" $F(x, y) = \begin{bmatrix} P \\ Q \end{bmatrix}$
 - $F(x, y) = f(x_0, y_0) + DF(x_0, y_0) \left[\begin{bmatrix} x \\ y \end{bmatrix} - \begin{bmatrix} x_0 \\ y_0 \end{bmatrix} \right] + \dots$
 - where $DF(x, y) = \begin{vmatrix} \frac{\partial P}{\partial x} & \frac{\partial P}{\partial y} \\ \frac{\partial Q}{\partial x} & \frac{\partial Q}{\partial y} \end{vmatrix}$ → Jacobian matrix.
- If $\begin{bmatrix} x \\ y \end{bmatrix}$ is close to $\begin{bmatrix} x_0 \\ y_0 \end{bmatrix}$, then
 - $F(x, y) \approx F(x_0, y_0) + \begin{bmatrix} P_x & P_y \\ Q_x & Q_y \end{bmatrix} \left[\begin{bmatrix} x \\ y \end{bmatrix} - \begin{bmatrix} x_0 \\ y_0 \end{bmatrix} \right]$ a linear approximation of F

Theorem

- Let $A = \begin{bmatrix} a & b \\ c & d \end{bmatrix}$ then $A = A_{\text{SKew}} + A_{\text{Diag}} + A_{\text{Symm}}$
 - $A_{\text{SKew}} = \frac{1}{2}(A - A^T) = \begin{pmatrix} 0 & \frac{1}{2}(b-c) \\ \frac{1}{2}(c-b) & 0 \end{pmatrix}$ skewsymmetric matrix symmetric with trace 0.
 - $A_{\text{Diag}} = \text{trace}(A)I_2 = \begin{pmatrix} \frac{1}{2}(a+d) & 0 \\ 0 & \frac{1}{2}(a+d) \end{pmatrix}$
 - and $A_{\text{Symm}} = \frac{1}{2}(A + A^T) = \begin{pmatrix} \frac{a+b}{2} & \frac{b+c}{2} \\ \frac{b+c}{2} & \frac{c+a}{2} \end{pmatrix}$
- $DF(x, y) = \frac{1}{2} \begin{bmatrix} 0 & P_y - Q_x \\ Q_x - P_y & 0 \end{bmatrix} + \frac{1}{2} \begin{bmatrix} P_x & Q_y \\ Q_x & P_y \end{bmatrix} + A_{\text{skew}}$
- Note: In 2D, we could say ~~DF~~ ~~DF~~ ~~DF~~
- $\vec{F} = \langle P, Q, 0 \rangle$
- $\text{div } F = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} - \frac{\partial Q}{\partial z} = P_x + Q_y$
- $\text{curl } F = 0 \hat{i} + 0 \hat{j} + \frac{1}{2} \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) = (Q_x - P_y) \hat{k}$
- $DF(x, y) = \frac{1}{2} \begin{bmatrix} 0 & -\text{curl } F \\ \text{curl } F & 0 \end{bmatrix} + \frac{1}{2} \begin{bmatrix} P_x & Q_y \\ Q_x & P_y \end{bmatrix} + A_{\text{Symm}, 0}$

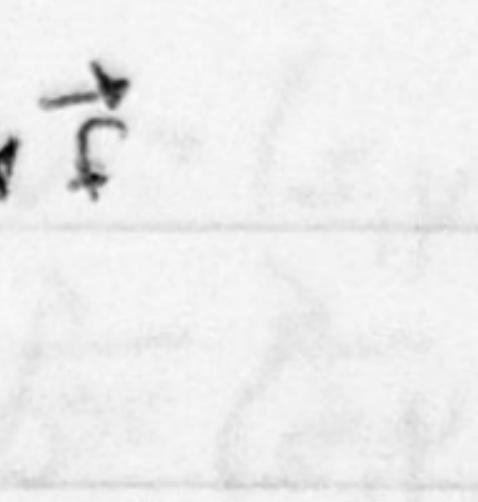
Part of linearization
responsible for local rotation

Part responsible
for contraction/expansion

Remaining part.

• Visualization - let P, Q be components of fluid velocity at (x, y)

$$\begin{cases} \frac{\partial x}{\partial t} = P(x, y) \\ \frac{\partial y}{\partial t} = Q(x, y) \end{cases}$$



Fluid Dynamics (Application of Vector Calculus)

- $\vec{v}(x, y, z)$ - velocity at (x, y, z)
- $\delta(x, y, z)$ - density of mass at (x, y, z) \rightarrow scalar function
 $\therefore \delta(x, y, z) = \frac{\text{mass}}{\Delta V} \rightarrow \frac{\Delta m}{\Delta V}$
-  $m = \iiint_D \delta(x, y, z) dV = \iiint_D \delta dV$
 rate of change of $m = \frac{\partial (\iiint_D \delta dV)}{\partial t} = \iiint_D \frac{\partial \delta}{\partial t} dV$. \leftarrow This is due to only flow
- flow across $D = \text{flux of } \vec{v} = \iint_D \vec{v} \cdot \hat{S}$ in/out of D
-  $V = A vAt$
 $m = \delta A vAt$
 flow per area = δvAt
 flow rate per area = δv not sign convention
- By conservation of mass $\Rightarrow \iiint_D \frac{\partial \delta}{\partial t} dV = - \iint_S \delta \vec{v} \cdot \hat{S}$ ↑ surface S

- $\iint_S \delta \cdot \hat{S} = \iint_D \text{div}(\delta \vec{v}) dV$ (Divergence theorem)
- $\iint_D \frac{\partial \delta}{\partial t} dV = - \iint_D \text{div}(\delta \vec{v}) dV$
- $\iint_D \frac{\partial \delta}{\partial t} + \text{div}(\delta \vec{v}) dV = 0$

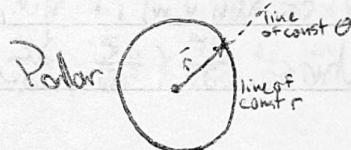
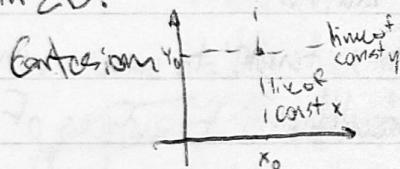
- True for any region, D . This can happen:
- $\iint_D \frac{\partial \delta}{\partial t} + \text{div}(\delta \vec{v}) = 0$ \leftarrow continuity equation
- Other eqn is Navier-Stokes eqn, which is derived starting from conservation of momentum
- $\delta \frac{\partial \vec{v}}{\partial t} + \delta(\vec{v} \cdot \nabla) \vec{v} = -\nabla p + \vec{F}$
 \uparrow pressure force

• If δ is constant in time and space, $\frac{\partial \delta}{\partial t} = 0, \frac{\partial \delta}{\partial x} = 0 = \frac{\partial \delta}{\partial y} = \frac{\partial \delta}{\partial z}$
 (incompressible fluid)

- $0 + \delta \text{div} \vec{v} = 0 \quad \delta > 0$
| $\text{div} \vec{v} = 0$ |

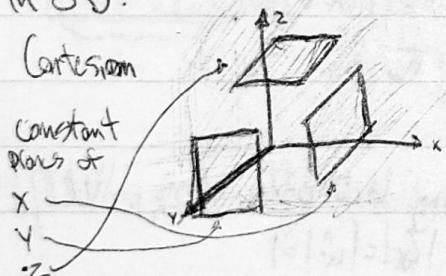
Differential Operators and Vector Calculus in Nonlinear Coordinates.

- $\vec{F}(x, y, z)$ in cartesian coordinates
- $\vec{\nabla} \times \vec{F}, \vec{\nabla} \cdot \vec{F}$ are computed using $\nabla = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle$
- If $\vec{F} = \vec{F}(r, \theta, \phi)$, is given in spherical coordinates, what is ∇ ?
- General Theory: Suppose we have (u, v, w) coordinate system
- In 2D:



Cylindrical - r, θ, z
Spherical - r, θ, ϕ

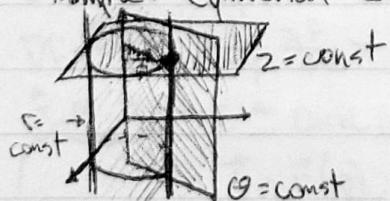
- In 3D:



- In general, $u = u_0$ represent surfaces (in 3D) of constant $w = w_0$
 $v = v_0$

coordinates, passing through (u_0, w_0, v_0) . If planes tangent to them are perpendicular then we call the system, orthogonal (u, v, w)

- Example: Cylindrical Coordinates



- For spherical coordinates, the same is true:

$$\left. \begin{array}{l} r = r_0 \\ \theta = \theta_0 \\ \phi = \phi_0 \end{array} \right\} \text{sphere}$$

$$\left. \begin{array}{l} r = r_0 \\ \theta = \theta_0 \\ \phi = \phi_0 \end{array} \right\} \text{cone}$$

$$\left. \begin{array}{l} r = r_0 \\ \theta = \theta_0 \\ \phi = \phi_0 \end{array} \right\} \text{semi-sphere}$$

are orthogonal

Curvilinear Coordinates



- $x = x(u, v, w)$ x, y, z - cartesian
 $y = y(u, v, w)$ u, v, w - curvilinear
 $z = z(u, v, w)$

$$\vec{r} = x(u, v, w)\hat{i} + y(u, v, w)\hat{j} + z(u, v, w)\hat{k}$$

- Consider vectors: $\frac{\partial \vec{r}}{\partial u}, \frac{\partial \vec{r}}{\partial v}, \frac{\partial \vec{r}}{\partial w}$ - Vectors tangent to curves which are intersections of surfaces of constant coordinates.

- Scale factors are: $h_u = |\frac{\partial \vec{r}}{\partial u}|, h_v = |\frac{\partial \vec{r}}{\partial v}|, h_w = |\frac{\partial \vec{r}}{\partial w}|$
 $\hat{u} = \frac{1}{h_u} \frac{\partial \vec{r}}{\partial u}, \hat{v} = \frac{1}{h_v} \frac{\partial \vec{r}}{\partial v}, \hat{w} = \frac{1}{h_w} \frac{\partial \vec{r}}{\partial w}$

Important:
 $\hat{u}, \hat{v}, \hat{w}$ are
 dependent on position
 (Except cartesian's
 constant vectors)

- Triad of unit vector forming local base, also called local base vectors $|\hat{u}| = |\hat{v}| = |\hat{w}| = 1$
- Any point in \mathbb{R}^3 can be expressed as linear combination of $\hat{u}, \hat{v}, \hat{w}$.
- If $\hat{u} \perp \hat{v}, \hat{v} \perp \hat{w}, \hat{u} \perp \hat{w}$ then $(\hat{u}, \hat{v}, \hat{w})$ is orthogonal
- $\hat{u} \cdot \hat{v} = 0, \hat{v} \cdot \hat{w} = 0, \hat{u} \cdot \hat{w} = 0$

• Ex. (spherical) unit

$$\vec{r} = r \sin \varphi \cos \theta \hat{i} + r \sin \varphi \sin \theta \hat{j} + r \cos \varphi \hat{k}$$

$$\frac{\partial \vec{r}}{\partial \theta} = \sin \varphi \cos \theta \hat{i} + \sin \varphi \sin \theta \hat{j} + \cos \varphi \hat{k}$$

$$\frac{\partial \vec{r}}{\partial \varphi} = r \cos \varphi \cos \theta \hat{i} + r \cos \varphi \sin \theta \hat{j} - r \sin \varphi \hat{k}$$

$$\frac{\partial \vec{r}}{\partial r} = \hat{i} + \hat{j} + \hat{k}$$

$$\text{Scale factor } h_r = \left| \frac{\partial \vec{r}}{\partial r} \right| = \sqrt{r^2(\cos^2 \varphi \cos^2 \theta + \cos^2 \varphi \sin^2 \theta) + \sin^2 \varphi} = 1.$$

$$h_\theta = \left| \frac{\partial \vec{r}}{\partial \theta} \right| = \sqrt{r^2(\cos^2 \varphi \cos^2 \theta + \cos^2 \varphi \sin^2 \theta + \sin^2 \varphi)} = r$$

$$h_\varphi = \left| \frac{\partial \vec{r}}{\partial \varphi} \right| = r \sin \varphi$$

Local unit vector

$$\hat{u} = \frac{1}{h_\theta} \frac{\partial \vec{r}}{\partial \theta} = \sin \varphi \cos \theta \hat{i} + \sin \varphi \sin \theta \hat{j} + \cos \varphi \hat{k}$$

$$\hat{v} = \frac{1}{h_\varphi} \frac{\partial \vec{r}}{\partial \varphi} = \cos \varphi \cos \theta \hat{i} + \cos \varphi \sin \theta \hat{j} - \sin \varphi \hat{k}$$

$$\hat{w} = \frac{1}{h_r} \frac{\partial \vec{r}}{\partial r} = -\sin \theta \hat{i} + \cos \theta \hat{j}$$

$$\hat{u} \times \hat{v} = \hat{w}$$



Alternative

Notation:

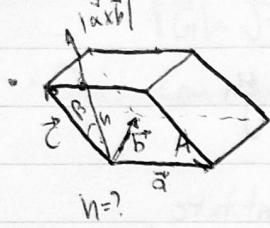
$$\hat{e}_\theta = \hat{i} \quad \hat{e}_r = \hat{1}$$

$$\hat{e}_\varphi = \hat{j} \quad \hat{e}_\theta = \hat{j}$$

$$\hat{e}_r = \hat{i} \quad \hat{e}_\varphi = \hat{k}$$

Spherical Cartesian

Applications of Triple Integrals



$$\text{Volume} = V = Ah \quad h = \sqrt{a^2 + b^2 + c^2}$$

$$A = |\vec{a}| \cdot |\vec{b}|$$

$$h = \sqrt{c^2 \sin^2 \alpha}$$

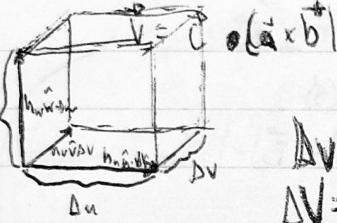
$$A = |\vec{a}| |\vec{b}| \sin \alpha$$

$$A = |\vec{a} \times \vec{b}|$$

$$V = hA$$

$$= |\vec{c}| \cdot |\vec{a} \times \vec{b}| \cdot \cos \beta$$

$$\beta = \gamma(\vec{c}, \vec{a} \times \vec{b})$$



$$dV = h_u h_v h_w dudvdw$$

$$dV = h_u h_v h_w dudvdw$$

Jacobian

$$\iiint f(x, y, z) dV = \iiint f(x(uvw), y(uvw), z(uvw)) h_u h_v h_w du dv dw$$

Change of coordinates in triple integrals

Transformation of Differential Operator

$$\nabla = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle$$

$$\nabla f = \left\langle \frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right\rangle = \frac{\partial f}{\partial x} \hat{i} + \frac{\partial f}{\partial y} \hat{j} + \frac{\partial f}{\partial z} \hat{k}$$

\hat{l} ~ curvilinear 3D.

$\vec{r} = \vec{r}(s)$ are length-parametrization

$$\frac{\partial \vec{r}}{\partial s} = \frac{\partial \vec{r}}{\partial u} \frac{\partial u}{\partial s} + \frac{\partial \vec{r}}{\partial v} \frac{\partial v}{\partial s} + \frac{\partial \vec{r}}{\partial w} \frac{\partial w}{\partial s}$$

$\frac{\partial \vec{r}}{\partial s} = \text{rate of change in direction of tangent unit vector } \hat{T} = \nabla f \cdot \hat{T}$

$$\cdot \hat{T} = \frac{\partial \vec{r}}{\partial s} = \frac{\partial \vec{r}}{\partial u} \frac{\partial u}{\partial s} + \frac{\partial \vec{r}}{\partial v} \frac{\partial v}{\partial s} + \frac{\partial \vec{r}}{\partial w} \frac{\partial w}{\partial s}$$

$$= h_u \hat{u} \frac{\partial u}{\partial s} + h_v \hat{v} \frac{\partial v}{\partial s} + h_w \hat{w} \frac{\partial w}{\partial s}$$

$$\cdot \frac{\partial \vec{r}}{\partial s} = \nabla f \cdot \hat{T} = f_u h_u \hat{u} + f_v h_v \hat{v} + f_w h_w \hat{w}$$

$$\nabla f = f_u \hat{u} + f_v \hat{v} + f_w \hat{w}$$

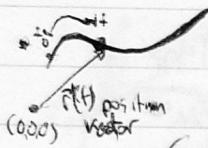
$$\cdot \frac{\partial \vec{r}}{\partial u} = f_u h_u \frac{\partial u}{\partial s} = f_u h_u, \quad \frac{\partial \vec{r}}{\partial v} = f_v h_v \frac{\partial v}{\partial s}, \quad \frac{\partial \vec{r}}{\partial w} = f_w h_w \frac{\partial w}{\partial s}$$

$$\cdot f_u = \frac{1}{h_u} \frac{\partial f}{\partial u}, \quad f_v = \frac{1}{h_v} \frac{\partial f}{\partial v}, \quad f_w = \frac{1}{h_w} \frac{\partial f}{\partial w}$$

$$\nabla f = \frac{1}{h_u} \frac{\partial f}{\partial u} \hat{u} + \frac{1}{h_v} \frac{\partial f}{\partial v} \hat{v} + \frac{1}{h_w} \frac{\partial f}{\partial w} \hat{w} \quad \text{Gradient in Curvilinear Coordinates.}$$

Hilroy

Front frame



$\vec{r}(t) \rightarrow$ reparametrize to arc length
 $S(t) \rightarrow$ $\vec{r}'(u)$ ch

Solve for t in terms of s and substitute,
obtain $\vec{r}(s)$

$$\vec{T}(s) = \vec{r}'(s) = \frac{d}{ds}(\vec{r}(s)) \text{ tangent vector}, |\vec{T}(s)| = 1$$

$$\vec{N}(s) = \frac{\vec{T}'(s)}{|\vec{T}'(s)|} \text{ normal vector}, \vec{T} \perp \vec{N}$$

Binormal vector = $\vec{B}(s) = \vec{T}(s) \times \vec{N}(s)$

We have triad $\vec{T}, \vec{N}, \vec{B}$, $|\vec{T}| = |\vec{N}| = |\vec{B}| = 1$

$$- \vec{T} \cdot \vec{N} = \vec{N} \cdot \vec{B} = \vec{T} \cdot \vec{B} = 0$$

- They form base in \mathbb{R}^3

Front frame - Orthogonal coordinate system with unit vectors $\vec{T}, \vec{N}, \vec{B}$

Front changes with s (and also t), moving frame

How $\vec{T}, \vec{N}, \vec{B}$ change with s ? Compute Derivatives

$$\text{Any vector } \vec{A} = a\vec{T} + b\vec{B} + c\vec{N}$$

$$\vec{A} \cdot \vec{T} = a\vec{T} \cdot \vec{T} + b\vec{B} \cdot \vec{T} + c\vec{N} \cdot \vec{T}$$

$$- a = \vec{A} \cdot \vec{T}, b = \vec{A} \cdot \vec{B}, c = \vec{A} \cdot \vec{N}$$

$$- \text{Now: } \vec{T}' = a\vec{T} + b\vec{B} + c\vec{N} \quad \Rightarrow \quad \vec{T}' = |\vec{T}'(s)| \vec{N}$$

$$\vec{T}'(s) = K(s) \vec{N}(s) \quad K = |\vec{T}'(s)| = \text{curvature}$$

$$- \vec{N}' \cdot \vec{T} = 0 \Rightarrow \vec{N}' \cdot \vec{T} \cdot \vec{N} \cdot \vec{T}' = 0.$$

$$\vec{N}' \cdot \vec{T} = -\vec{N} \cdot \vec{T}' = -\vec{N} \cdot b\vec{N} = b \Rightarrow \vec{N}' \cdot \vec{T} = b$$

$$- \vec{N}'(s) \cdot \vec{B}(s) = ? \quad \text{Def'n } \tau(s) = \vec{N}'(s) \cdot \vec{B}(s) = \text{torsion}$$

$$- \vec{N}' \cdot \vec{B} = \tau \Rightarrow \vec{N}' = 0 \cdot \vec{N} - K \vec{T} + \tau \vec{B}$$

• Frenet's First Formula - $\vec{T}'(s) = K(s) \vec{N}(s)$

• Frenet's Second Formula - $\vec{N}'(s) = -K \vec{T}(s) + \tau \vec{B}(s)$

• Frenet's Third Formula - $\vec{B}'(s) = -\tau \vec{N}$

$$\begin{bmatrix} \vec{T}' \\ \vec{N}' \\ \vec{B}' \end{bmatrix} = \begin{bmatrix} 0 & K & 0 \\ -K & 0 & \tau \\ 0 & -\tau & 0 \end{bmatrix} \begin{bmatrix} \vec{T} \\ \vec{N} \\ \vec{B} \end{bmatrix} \quad \text{Matrix form.}$$

is skew symmetric

of the
curve
being shown

Defn: $\vec{G} = \alpha \vec{T} + \kappa \vec{B}$ + Darboux Vector
 $|\vec{G}| = \sqrt{\alpha^2 + \kappa^2}$

One can show $\vec{T}' = \vec{G} \times \vec{T}$
 $\vec{N}' = \vec{G} \times \vec{N}$
 $\vec{B}' = \vec{G} \times \vec{B}$

Defn: $\text{span}[\vec{T}, \vec{N}]$ - Oscillating plane
 $\text{span}[\vec{T}, \vec{B}]$ - Rectifying plane
 $\text{span}[\vec{N}, \vec{B}]$ = Normal plane.

Darboux form of Frenet's equations,

Frenet Trihedron

Frenet Frame Cont.

- In other parameterizations (non-arc length)
- $\lambda(t)$ parameterization
- Aftw re-parameterization to s , $\vec{\beta}(s)$
- $\vec{\beta}(s) = \vec{\beta}(s(t)) = \vec{\alpha}(t)$
- $\vec{\alpha}'(t) = \frac{d}{dt}(\vec{\beta}(s(t))) = \vec{\beta}'(s(t)) s'(t) = \vec{T}(s(t)) v(t) \quad s'(t) = v(t)$
- $\frac{d\vec{T}}{dt} = \frac{dt}{ds} \frac{ds}{dt} = \kappa \vec{N} \quad v = \sqrt{\kappa}$
- $\vec{\alpha}''(t) = \frac{d}{dt} \vec{\alpha}'(t) = \frac{d}{dt} (\vec{T}(s(t)) v(t)) = \vec{T}(s(t)) v'(t) + \frac{d\vec{T}(s(t))}{dt} v(t)$
 $= v(t) \vec{T}'(s(t)) + v'(t) \vec{T}'(s(t)) s'(t) = v(t) \vec{T}'(s(t)) + v(t)^2 \kappa(s(t)) \vec{N}(s(t))$

$\vec{\alpha}''' = v \vec{T} + \kappa v^2 \vec{N}$ ← acceleration vector

$\vec{\alpha}' = \vec{T} v$ ← ~~velocity~~ velocity vector

$\vec{\alpha}$ ← position vector.

κ -curvature \odot_{κ} largest circle on K

One can show that

- for any parameterization $K = \frac{|\vec{\alpha}' \times \vec{\alpha}''|}{|\vec{\alpha}'|^3}$

- Proof:* $\vec{\alpha}' \times \vec{\alpha}'' = (\vec{T}) \times (v\vec{T} + Kv^2\vec{N}) = v^2 \vec{T} \times \vec{T} + v^2 K v^2 \vec{N} \vec{T}$
 $= v^3 K \vec{N} \vec{T} = Kv^3 \vec{B}$

$$|\vec{\alpha}' \times \vec{\alpha}''| = Kv^3 |\vec{B}| = Kv^3$$

$$K = \frac{|\vec{\alpha}' \times \vec{\alpha}''|}{|\vec{\alpha}'|^3} = \frac{|\vec{\alpha}' \times \vec{\alpha}''|}{v^3}, \text{ but } v = |\vec{\alpha}'|.$$

Note: $\vec{\alpha}(t) =$

- We can perform similar calculations for $\vec{T}, \vec{T}, \vec{N}, \vec{B}$

- Results: $\vec{T} = \frac{(\vec{\alpha}' \times \vec{\alpha}'') \times \vec{\alpha}'''}{|\vec{\alpha}' \times \vec{\alpha}''|^2}$ $K = \frac{|\vec{\alpha}' \times \vec{\alpha}''|}{|\vec{\alpha}'|^2}$
 $\vec{T} = \frac{\vec{\alpha}'}{|\vec{\alpha}'|}$ $\vec{B} = \frac{\vec{\alpha}' \times \vec{\alpha}''}{|\vec{\alpha}' \times \vec{\alpha}''|}$
 $\vec{N} = \vec{B} \times \vec{T} = \frac{(\vec{\alpha}' \times \vec{\alpha}'') \times \vec{\alpha}''}{|\vec{\alpha}' \times \vec{\alpha}''|^2}$

- Ex $\vec{\alpha}(t) = \langle a \cos t, a \sin t, 0 \rangle$

$$K = \frac{1}{a}, T = 0$$

- Ex $\vec{\alpha}(s) = \langle a \cos(\frac{s}{c}), a \sin(\frac{s}{c}), b(\frac{s}{c}) \rangle$ where $a > 0$, $c = \sqrt{a^2 + b^2}$

$$\vec{T}(s) = \vec{\alpha}'(s) = \frac{1}{c} \langle -a \sin(\frac{s}{c}), a \cos(\frac{s}{c}), b \rangle$$

$$\vec{T}'(s) = \frac{a}{c^2} \langle -a \cos(\frac{s}{c}), -a \sin(\frac{s}{c}), 0 \rangle$$

K must be \vec{N} by 1st front

$$\vec{N}(s) = \langle -\frac{b}{c} \cos(\frac{s}{c}), -\frac{b}{c} \sin(\frac{s}{c}), 0 \rangle; |\vec{N}| = |\vec{T}'| = 1$$

~~$$\vec{B}(s) = \frac{1}{c^2} \langle b \sin(\frac{s}{c}), b \cos(\frac{s}{c}), a \rangle; \vec{T} \times \vec{N} = \frac{1}{c} \langle b \sin(\frac{s}{c}), b \cos(\frac{s}{c}), a \rangle$$~~

~~$$\vec{B}'(s) = \frac{1}{c^2} \langle b \cos(\frac{s}{c}), -b \sin(\frac{s}{c}), 0 \rangle = \frac{b}{c} \vec{N}$$~~

$$T = \frac{b}{c^2} = \frac{b}{a^2 + b^2}$$

~~$$K = \frac{a}{c^2} = \frac{a}{a^2 + b^2}$$~~

If $b = 0$, $\vec{\alpha}(s) = \langle a \cos s, a \sin s, 0 \rangle$ is a circle and $T = 0$, and $K = \frac{1}{a}$.

~~Proposition~~ Proposition

curvature

- A space curve is a straight line if and only if $K=0$ everywhere

$$\Leftrightarrow \vec{r}(s) = s\vec{T} + \vec{C} \quad \text{where } \vec{T} \in \mathbb{C}^3 \text{ are constant vectors}$$

$$\vec{T}'(s) = \vec{\tau}'(s) = \vec{v} \quad \text{constant} \Rightarrow K=0$$

- \Leftrightarrow Assume $K=0$, $\vec{T}'(s) = \vec{T}_0$. $\vec{\tau}'(s) = \vec{\tau}_0$ constant.

$$\vec{\tau}'(s) = \vec{T}'(s) \quad \vec{r}'(s) = \vec{T}_0 s + \vec{C}$$

straightline torsion

- Remark: A space curve is planar if and only if $\tau=0$ everywhere.

The only planar curve with $K=\text{constant} \neq 0$ is a circle.

The Fundamental Theorem of Space Curves

- Let C_1 & C_2 be two curves, both of which have the same nonvanishing curvature function $K(s)$ and the same torsion function $\tau(s)$. Then the curves are congruent.

That is, one can be moved rigidly (translated & rotated) so as to coincide exactly with the other.

Proof

- We require $K \neq 0$ because \hat{N} & \hat{B} are not defined where $K=0$. Move C_2 rigidly so their Frenet frames are the same. Let $\hat{T}_1, \hat{T}_2, \hat{N}_1, \hat{N}_2, \hat{B}_1, \hat{B}_2$ be unit tangent, normal, and binormal for the curves.

$$f(s) = \hat{T}_1(s) \cdot \hat{T}_2(s) + \hat{N}_1(s) \cdot \hat{N}_2(s) + \hat{B}_1(s) \cdot \hat{B}_2(s)$$

- We ~~differentiate~~ take the derivative of this

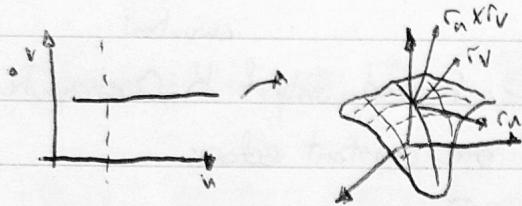
$$\begin{aligned} f'(s) &= \hat{T}_1'(s) \cdot \hat{T}_2(s) + \hat{T}_1(s) \cdot \hat{T}_2'(s) + \hat{N}_1'(s) \cdot \hat{N}_2(s) + \hat{N}_1(s) \cdot \hat{N}_2'(s) + \hat{B}_1'(s) \cdot \hat{B}_2(s) + \hat{B}_1(s) \cdot \hat{B}_2'(s) \\ &= KN(s) \cdot T_2(s) + K\hat{T}_1 \cdot \hat{N}_2 = KT_1 \cdot N_2 + \tau B_1 \cdot N_2 - KN \cdot T_2 + \tau B_1 \cdot B_2 - \tau N \cdot B_2 = 0 \end{aligned}$$

- $\therefore f(s)$ is constant since it's coincident at $s=0$. The constant part must be 0.

$$\hat{T}_1(s) \cdot \hat{T}_2(s) + \hat{N}_1(s) \cdot \hat{N}_2(s) + \hat{B}_1(s) \cdot \hat{B}_2(s) = 0$$

$$\frac{dx_1}{ds} = \hat{T}_1(s) = \hat{T}_2(s) = \frac{dx_2}{ds}$$

Parameterizable Surfaces



- Definition: A regular parametrization of a subset $M \subset \mathbb{R}^3$ is a (\mathbb{C}^3) one-to-one function

$r: U \rightarrow M \subset \mathbb{R}^3$ so that $r_u \times r_v \neq 0$

for some open set $U \subset \mathbb{R}^2$. A connected subset $M \subset \mathbb{R}^3$, \rightarrow called a surface if each point has a neighbourhood that is regularly parameterized.

- Torus - $r(u, v) = ((a + b \cos v) \cos u, (a + b \cos v) \sin u, b \sin v)$ $0 \leq u \leq 2\pi$



- Unit Sphere - $r(u, v) = (\cos u \cos v, \sin u \cos v, \cos u)$ $0 \leq u \leq \pi, 0 \leq v \leq 2\pi$

- Surface of Revolution - $r(u, v) = (f(u) \cos v, f(u) \sin v, g(u))$, $u \in I$, $0 \leq v \leq 2\pi$

- For a surface $\tilde{r}(u, v)$ with a regular parametrization, tangent plane at $P = \tilde{r}(u_0, v_0)$, is the plane $T_P = \text{span}\{\tilde{r}_u, \tilde{r}_v\}$

$$\hat{n} = \frac{\tilde{r}_u \times \tilde{r}_v}{\|\tilde{r}_u \times \tilde{r}_v\|} \quad \text{evaluated at } u_0, v_0$$

\hat{n} - normal unit vector

Define $E = \tilde{r}_u \cdot \tilde{r}_u$; $F = \tilde{r}_u \cdot \tilde{r}_v$; $G = \tilde{r}_v \cdot \tilde{r}_v$.

$I_p = \begin{bmatrix} E & F \\ F & G \end{bmatrix}$ dependent on u, v

Define $\tilde{U} = a\tilde{r}_u + b\tilde{r}_v$; $\tilde{V} = c\tilde{r}_u + d\tilde{r}_v \in T_P$

$\tilde{U} \cdot \tilde{V} = E(ac) + F(ad+bc) + G(bc) \leftarrow$ First normal form

$$\tilde{U} \cdot \tilde{V} \cong I_p(\tilde{U}, \tilde{V}) = [c \ c] \begin{bmatrix} E & F \\ F & G \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix}$$

$$|\tilde{U}|^2 = |\tilde{U}| \cdot \tilde{U} = \tilde{U} \cdot \tilde{U} = I_p(u, u) = Eu^2 + 2Fab + Gb^2$$

- **Formula:** Remember that surface area given by $\int_S |r_u \times r_v|^2 du dv$
One can show that $|r_u \times r_v| = \sqrt{E - F^2}$

Characterizations of Surfaces - Local Theory.

• $\vec{r}(u, v)$ - parameterization on a surface

$$\cdot S = \iint |\vec{r}_u \times \vec{r}_v| du dv \quad r_u = \frac{\partial \vec{r}}{\partial u}, \quad r_v = \frac{\partial \vec{r}}{\partial v}$$

$$\cdot \text{Laplace} \rightarrow (\vec{a} \times \vec{b}) \cdot (\vec{c} \times \vec{d}) = (\vec{a} \cdot \vec{c})(\vec{b} \cdot \vec{d}) - (\vec{a} \cdot \vec{d})(\vec{b} \cdot \vec{c})$$

$$(\vec{a} \times \vec{b}) \cdot (\vec{a} \times \vec{b}) = |\vec{a}|^2 |\vec{b}|^2 - (\vec{a} \cdot \vec{b})^2 \rightarrow (\text{special case})$$

$$\circ |\vec{r}_u \times \vec{r}_v|^2 = (\vec{r}_u \times \vec{r}_v) \cdot (\vec{r}_u \times \vec{r}_v) = |\vec{r}_u|^2 |\vec{r}_v|^2 - (r_u \cdot r_v)^2$$

• Recall first fundamental (quadratic):

$$\circ I_p = \langle \vec{r}_u \cdot \vec{r}_v \rangle, \text{ where } E = r_u \cdot r_u, \quad F = \vec{r}_u \cdot \vec{r}_v, \quad G = r_v \cdot r_v$$

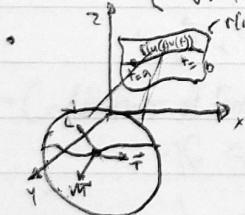
$$\circ |\vec{r}_u \times \vec{r}_v|^2 = EG - F^2, \quad |\vec{r}_u \times \vec{r}_v| = \sqrt{EG - F^2}$$

$$\cdot \text{Surface Area: } S = \iint \sqrt{EG - F^2} du dv = \iint \sqrt{\det I_p} du dv.$$

• Arc Length of a Curve lying on Surface $\vec{r}(u, v)$, let the curve be given by $u = u(t)$, $v = v(t)$. The curve has parameterization $\vec{r}(u(t), v(t))$

• Example $\vec{r}(u, v) = \langle u^2, u+v, v^3 \rangle$ - surface S

$$\left\{ \begin{array}{l} u = t+1 \\ v = t^2 \end{array} \right. \quad \vec{r}(t) = \langle (t+1)^2, t+1+t^2, t^6 \rangle \text{ - curve on surface } S.$$



Length of C for $t \in [a, b]$

$$L_{a-b} = \int_a^b \left| \frac{d}{dt} (\vec{r}(u(t), v(t))) \right| dt = \dots$$

$$= \int_0^b \left| \vec{r}_u u'(t) + \vec{r}_v v'(t) \right| dt$$

$$= \int_0^b \sqrt{(\vec{r}_{uu} u + \vec{r}_{uv} v) \cdot (\vec{r}_{uu} u + \vec{r}_{uv} v)} dt.$$

$$= \int_0^b \sqrt{r_u^2 u'^2 + 2r_u r_v u' v' + r_v^2 v'^2} dt.$$

$$L_{a-b} = \int_0^b \sqrt{E u'^2 + 2F u' v' + G v'^2} dt = \int_a^b \sqrt{[u' v'] \begin{bmatrix} E & F \\ F & G \end{bmatrix} \begin{bmatrix} u' \\ v' \end{bmatrix}} dt$$

• Recall for curves in 3D, we have Frenet frame $\vec{T}, \vec{N}, \vec{B}$

• For surface, use normal vector $\rightarrow \vec{M} = \vec{r}_u \times \vec{r}_v$. Let \vec{D} to be a

$$|\vec{r}_u \times \vec{r}_v|$$

normal vector to a curve C lying on a surface S , and \vec{T} the tangent vector of the curve

• Define $\vec{L} = \vec{M} \times \vec{T}$; T, M, L are unit orthogonal vectors at point P of $S \cap C$.

• Let $s(s)$ - arclength parameter of C .

$$\cdot \vec{T} = \frac{d\vec{r}}{ds}, \text{ recall } \frac{d\vec{r}}{ds} \perp \vec{T}$$

• Therefore $\frac{d\vec{r}}{ds}$ is a linear combination of \vec{M} & \vec{L}

$$\cdot \vec{r}'(s) = \dots \vec{M} + \dots \vec{L} \Rightarrow K_n \vec{M} + K_g \vec{L}$$

$$\cdot \vec{r}''(s) = \vec{T}' = K \vec{N}$$

$$\cdot K \vec{N} = K_n \vec{M} + K_g \vec{L}$$

$$\cdot \text{Therefore, } K = \sqrt{K_n^2 + K_g^2}$$

normal
curvature
 K
geodesic
curvature
 K_g

- K_n -curvature of "normal section", That is, curve obtained by intersecting S along the plane of \tilde{M} and \tilde{T}



- K_g - measure of deviation of C from geodesic line.
- for C_1 : $K = \frac{1}{R} \Rightarrow$ one can show $K_n = K = \frac{1}{R}$, $K_g = 0$
- for C_2 : $K = \frac{1}{r} \Rightarrow$ but $K_g > 0$, $K_n \neq K$



Second Fundamental Form.

Recall: $K^2 = K_n^2 + K_g^2$ \leftarrow geodesic curvature $\vec{\gamma} = \vec{\gamma}(u, v)$
normal curvature surface.

$\vec{\gamma} \rightarrow \vec{\gamma}(u(s), v(s)) \leftarrow$ Curve C

$$\vec{\gamma}' = \vec{\gamma}_u u' + \vec{\gamma}_v v'$$

$$\vec{\gamma}'' = \vec{\gamma}_{uu} u'^2 + 2\vec{\gamma}_{uv} u'v' + \vec{\gamma}_{vv} v'^2 + \vec{\gamma}_{uu} u'' + \vec{\gamma}_{vv} v''$$

- We want component of $\vec{\gamma}''(s)$ along \tilde{M} (normal to surface)
 $\vec{\gamma}'' \cdot \tilde{M} = ?$

$$\vec{\gamma}_u \cdot \tilde{M} = 0, \quad \vec{\gamma}_v \cdot \tilde{M} = 0$$

$$K_n = \vec{\gamma}'' \cdot \tilde{M} = \vec{\gamma}_{uu} \cdot \tilde{M} u'^2 + 2\vec{\gamma}_{uv} \cdot \tilde{M} u'v' + \vec{\gamma}_{vv} \cdot \tilde{M} v'^2$$

$$\text{Define: } L = \vec{\gamma}_{uu} \cdot \tilde{M}, \quad m = \vec{\gamma}_{uv} \cdot \tilde{M}, \quad n = \vec{\gamma}_{vv} \cdot \tilde{M}$$

$$K_n = L u'^2 + 2m u'v' + n v'^2$$

$$K_n = [u' \ v'] \begin{bmatrix} L & m \\ m & n \end{bmatrix} \begin{bmatrix} u' \\ v' \end{bmatrix}$$

$$I_{\rho} = \begin{bmatrix} L & m \\ m & n \end{bmatrix} \Rightarrow \text{second fundamental form.}$$

$$K_n = L du^2 + 2m dudv + ndv^2 = L \left(\frac{du}{ds}\right)^2 + 2m \left(\frac{du}{ds}\frac{dv}{ds}\right) + n \left(\frac{dv}{ds}\right)^2$$

- Recall from 1st form

$$K_n = \frac{L + 2M \frac{dv}{du} + N \left(\frac{dv}{du}\right)^2}{E + 2F \frac{dv}{du} + G \left(\frac{dv}{du}\right)^2}$$

$$K_n = \frac{L + 2M \mu + N \mu^2}{E + 2F \mu + G \mu^2}$$

$$E, F, G, L, M, N \text{ depend on surface along,}$$

μ depends on curve C_μ .

We want to find max & min of R as a function of μ .

$$\frac{\partial R_n}{\partial \mu} = 0 = \frac{(L+2M\mu+N\mu^2)}{E+2F\mu+G\mu^2} = \frac{(2\mu+2N\mu)(E+2F\mu+G\mu^2) - (L+2M\mu+N\mu^2)(2F+2G\mu)}{(E+2F\mu+G\mu^2)^2}$$

$$\text{numerator} = 0 \Rightarrow L+2M\mu+N\mu^2 = \frac{M+N\mu}{E+2F\mu+G\mu^2}$$

$$E+2F\mu+G\mu^2 \neq 0$$

at the critical point $R_n = \frac{M+N\mu}{E+2F\mu+G\mu^2}$ solve for μ . & substitute in to equation; numerator = 0.

$$\text{This yields: } (EG-F^2)K_n^2 - (EN-2FM+GL)K_n + (LN-M^2) = 0.$$

LN has solution K_1 & K_2

$$K = K_1 K_2 = \frac{LN - M^2}{EG - F^2} \rightarrow \text{Gaussian Curvature}$$

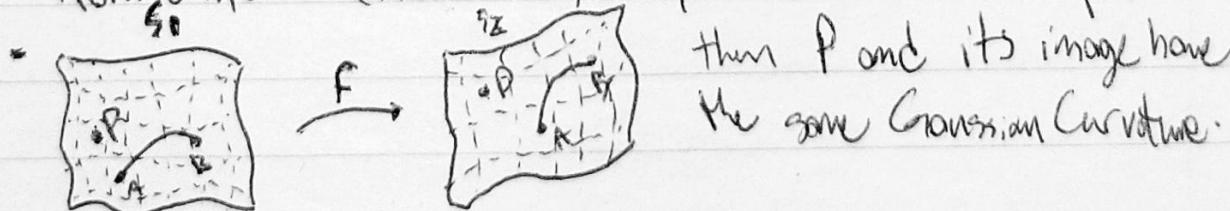
$$h = \frac{K_1 + K_2}{2} = \frac{EN - 2FM + GL}{2(EG - F^2)} \rightarrow \text{Average Curvature.}$$

Theorema Egregium: Curvature $k = K_1, K_2$ depends only on E, F, G and their partial derivatives of first & second order.

Corollary: E, F, G appear in distance formula

- If S_1, S_2 are related by distance-preserving

transformation (isometric), they have the same I_p (same EFG).



then P and its image have the same Gaussian Curvature.

Therefore, plane & sphere cannot be related by isometric transformation.