

MAHARASHTRA STATE BOARD OF TECHNICAL EDUCATION

SUMMER-13 EXAMINATION

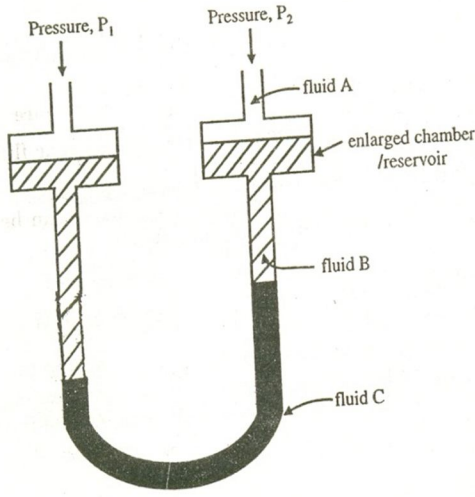
Model Answer

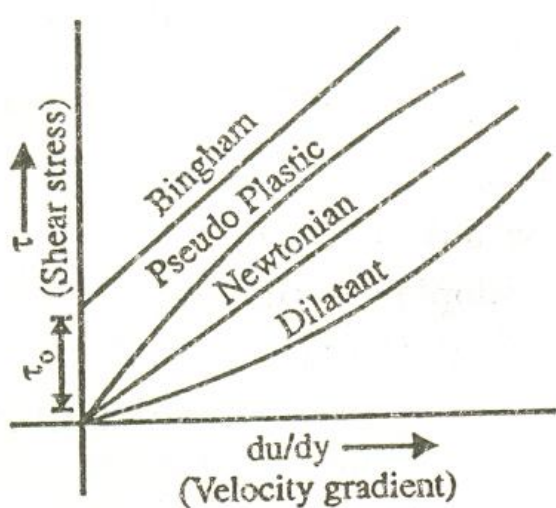
Subject & code : FFO(12128)

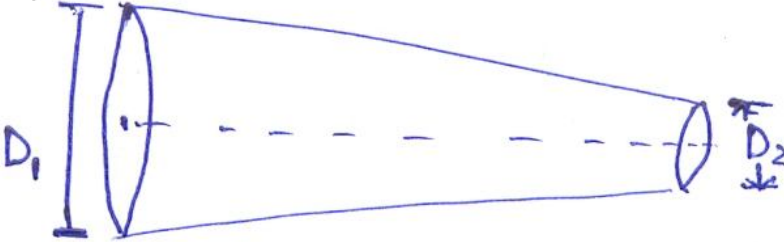
Important instructions to examiners :

1. The answers should be examined by keywords and not as word to word as given in the model answer scheme.
2. The model answer and the answer written by candidate may vary, but the examiner may try to assess the understanding level of the candidate.
3. The language errors such as grammatical, spelling errors should not given more importance.
4. While assessing figures, examiner may give credit for principal components indicated in a figure. The figures drawn by candidate and model answer may vary. The examiner may give credit for any equivalent figure drawn.
5. Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answer and model answer.
6. In case of some questions credit may be given by judgment of relevant answer based on candidates understanding.

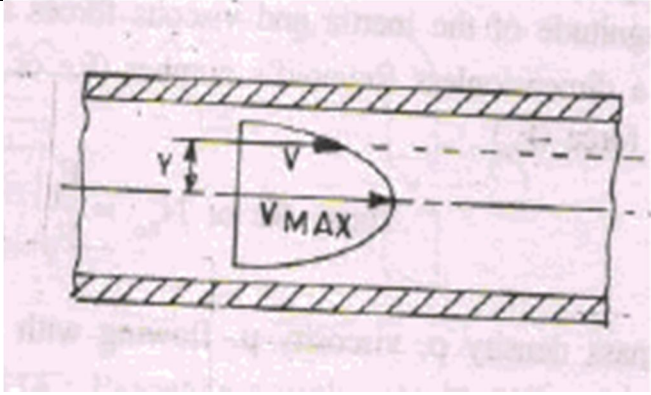
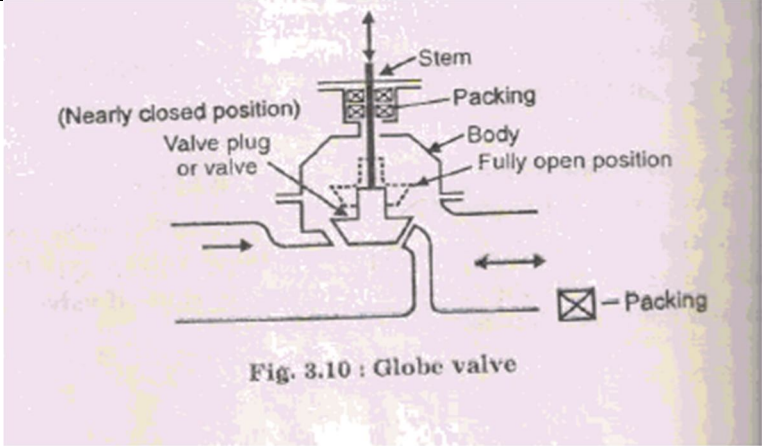
Q No:	Answer	Mark	Total marks
1.a.i	Water vapour is compressible. Its density is sensitive to changes in temperature and pressure.	1 1	2
1.a.ii	Flow is turbulent.	2	2
1.a.iii	Fanning's friction factor for turbulent flow: $f = 0.078/(N_{Re})^{0.25}$ or $1/\sqrt{f} = 4 \log(N_{Re}\sqrt{f}) - 0.4$	2 marks for any one formula	2
1.a.iv	Application of reducer and elbow i. Reducer: For connecting pipes of different diameter or for connecting a large diameter pipe with a small diameter pipe(any	1	2

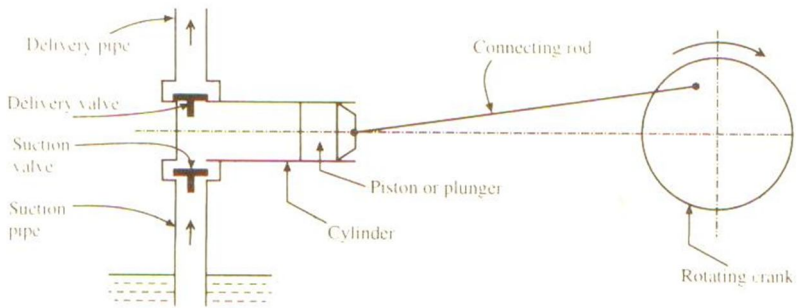
	one)		
	ii. Elbow: For changing the direction of flow through 90°	1	
1.a.v	M.S pipe: M.S. is mild steel pipe. It is a carbon alloy containing 0.3-0.6% carbon, iron and other elements like manganese, copper, silicon, cobalt, chromium, nickel etc. It is a cheaper alternative to steel, is corrosion resistant than iron and have high durability and strength	2	2
1.a.vi	Equipment for transporting slurry from a lower point to a higher point Centrifugal pump, diaphragm pump	2 marks for any one	2
1.a.vii	Pump for handling of viscous fluid: Gear pump	2	2
1.a.viii	Pressure inside the vessel = 600mm of Hg. Vacuum = atmospheric pressure- absolute pressure = 760 – 600 = 160 mm of Hg	2	2
1.b.i	Diagram of differential manometer 	4	4
1.b.ii	Expression to relate shear stress and shear rate: $F / A \propto du/dy$ ie $\tau \propto du/dy$ Unit of proportionality constant in MKS system: Kg/m.s	2 2	4

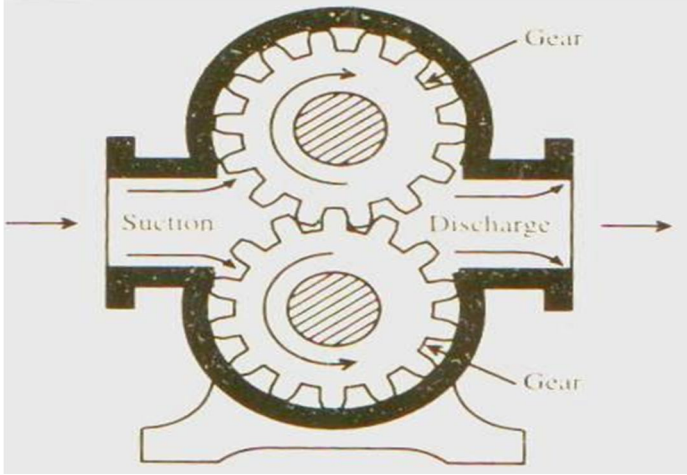
	$PA - (P + dP)A - \rho g h A = 0$ $dP + \rho g dh = 0 \dots (1)$ For incompressible fluids , density is constant Integrating equation (1) $\int_{P_1}^{P_2} dP + \rho g \int_0^{h_1} dh = 0$ $P_2 - P_1 + \rho g h_1 = 0$ $P_1 - P_2 = \rho g h_1$ P_1 is the pressure at the base of the column where $h = 0$ $P_2 - P_1 + \rho g h_1 = 0$ $P_1 - P_2 = \rho g h_1$	1	
2.b	 <p>Or shear rate</p>	4	4
2.c	Mass flow rate = 1000kg/ hr Diameter of the pipe = 5cm = 0.05m Density of liquid = 1000kg/m ³ Area of the pipe = $\pi d^2 / 4 = 1.9625 \cdot 10^{-3} \text{ m}^2$ i) Average velocity = <u>Mass flow rate</u>	2	4

	<p style="text-align: center;">area of pipe * density of liquid</p> 1000 $= \frac{\text{area of pipe} * \text{density of liquid}}{1000 * 1.9625 \cdot 10^{-3}}$ $= 509.5 \text{ m/hr}$ <p>ii) Mass velocity = Mass flow rate / area of pipe</p> $= \frac{1000}{1.9625 \cdot 10^{-3}} = 509554 \text{ kg/m}^2\text{hr}$	2	
2.d	<p>Relation between velocity and diameter of pipe in tapering form.</p>  <p> $A_1 = \pi D_1^2 / 4$ $A_2 = \pi D_2^2 / 4$ From equation of continuity , $\rho_1 u_1 A_1 = \rho_2 u_2 A_2$ Same fluid is flowing through the pipe, $\rho_1 = \rho_2$ $u_1 A_1 = u_2 A_2$ $u_1 * \pi D_1^2 / 4 = u_2 * \pi D_2^2 / 4$ $u_1 * D_1^2 = u_2 * D_2^2$ </p>	2 2	4
2.e		Any one	4

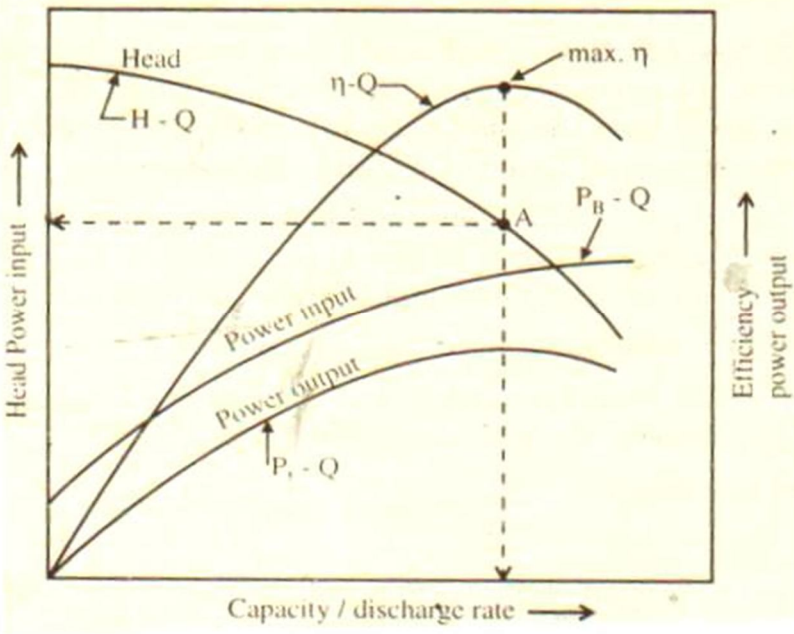
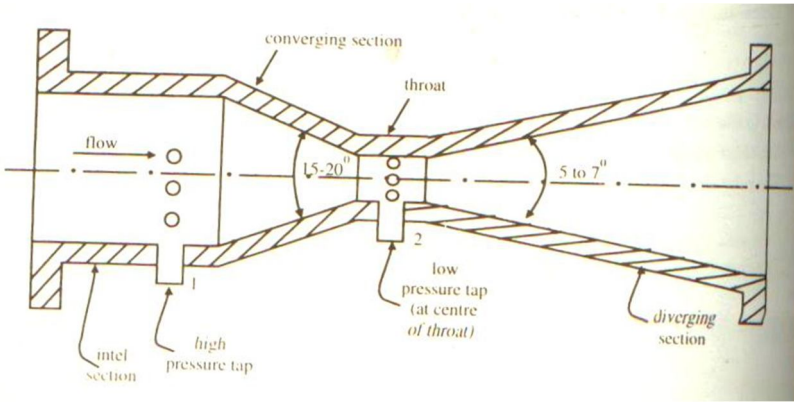
	<div data-bbox="349 241 1006 682" data-label="Image"> </div> <p>Close position</p> <p>Swing check valve.</p> <div data-bbox="349 861 641 1165" data-label="Image"> </div> <p>Open position</p> <p>Lift check valve.</p> <div data-bbox="389 1312 803 1648" data-label="Image"> </div> <p>Open position</p> <p>Foot valve.</p>	<p>diagram 4 marks</p>	
2.f	$N_{Re} = DV \rho / \mu$ <p>Where D is the diameter of the pipe in cm or m v is the velocity of fluid in cm/s or m/s</p>	<p>1 2</p>	4

3.d	 <p>When liquid is flowing through a pipeline, velocity at center is maximum and it is zero at the surface of pipe. There is very small region near surface where velocity is very small and hence flow is laminar. This layer is called viscous sub layer.</p>	1	4
3.e	<p>Equivalent length of pipe fitting is straight length of pipe of same diameter which will give the same pressure drop as is given by the fitting.</p> <p>$L_e/D = \text{Number}$</p> <p>Therefore $L_e = \text{equivalent length of straight pipe} = D * \text{Number}$</p> <p>For a fitting L_e can be determined by using the pressure drop across the fitting and should be same as pressure drop across straight length found experimentally.</p> <p>Equivalent length is necessary to find out pressure drop in a pipe line without actual experiment.</p>	1 1 1 1	4
3.f	 <p>Fig. 3.10 : Globe valve</p>	2	4

	<p>Diameter of pipe : $d = 0.055 \text{ m}$</p> <p>Discharge : $Q = 4 \text{ lit/min} = 4000/60 \text{ cm}^3/\text{s}$</p> <p>$Q = 66.67 \text{ cm}^3/\text{s} = 66.67 \times 10^{-6} \text{ m}^3/\text{s}$</p> <p>Viscosity = $1.5 \text{ poise} = 0.15 \text{ kg/m.s}$</p> <p>Density = $1.04 \text{ gm/cm}^3 = 1040 \text{ kg/m}^3$</p> <p>Area of pipe = $\pi / 4 \times d^2$</p> <p>Area of pipe = $\pi / 4 \times (0.055)^2$</p> <p>Area of pipe = $2.376 \times 10^{-3} \text{ m}^2$</p> <p>As discharge $Q = \text{area} \times \text{velocity}$</p> <p>$u = Q/A$</p> <p>$u = 66.67 \times 10^{-6} / 2.376 \times 10^{-3}$</p> <p>$u = \mathbf{0.028 \text{ m/s}}$</p> <p>Reynolds no. = $NRe = d u \rho / \mu$</p> <p>$NRe = 0.055 \times 0.028 \times 1040 / 0.15$</p> <p>$NRe = \mathbf{10.67}$</p> <p>As $NRe < 2100$, the flow is laminar.</p> <p>Friction factor: $f = 16 / NRe$</p> <p>$f = 16 / 10.67 = \mathbf{1.5}$</p> <p>Frictional losses: $h_f = 4 f L u^2 / 2d$</p> <p>$h_f = 4 \times 0.15 \times 10 \times (0.028)^2 / 2 \times 0.55$</p> <p>$h_f = \mathbf{0.043 \text{ N.m/kg} = 0.043 \text{ J/kg}}$</p>	1	
5.c	<p><u>WORKING OF RECIPROCATING PUMP:</u></p>  <p>The diagram illustrates the internal components of a reciprocating pump. On the left, a vertical section shows the suction and delivery pipes with their respective valves. The suction pipe is at the bottom, and the delivery pipe is at the top. A horizontal cylinder contains a piston or plunger. This piston is connected to a rotating crank on the right via a connecting rod. The crank is shown in a circular path, indicating its rotation. Arrows indicate the flow direction: suction into the cylinder and delivery out of the cylinder.</p>	1	4

			
6.b	<p><u>PRESSURE DEVELOPMENT IN CENTRIFUGAL PUMP:</u></p> <p>Once the trapped air in pump is removed (priming), the delivery valve is kept closed & power from electric motor is applied to the shaft. The delivery valve is kept closed to reduce the starting torque for motor.</p> <p>The impeller rotates within the casing, which produces the forced vortex & it imparts a centrifugal head to the liquid. The pressure throughout the liquid is increased.</p> <p>When delivery valve is opened, the liquid is made to flow in an outward radial direction thereby leaving the vanes of the impeller at the outer circumference of the impeller with high velocity & pressure.</p> <p>Due to centrifugal action, a partial vacuum is created at the eye of impeller.</p> <p>This causes the liquid from sump to rush through the suction pipe to the eye of impeller thereby replacing the liquid which is being discharged from the entire circumference of the impeller.</p> <p>The high pressure of the liquid leaving the impeller is utilized in lifting the liquid to the required height through the delivery pipe.</p>	<p>1</p> <p>1</p> <p>1</p> <p>1</p>	4
6.c	<p><u>1) NET POSITIVE SUCTION HEAD (NPSH)</u></p> <p>Def : "It is the amount by which the pressure at the suction point of pump expressed as a head of the liquid to be pumped (sum of</p>	2	4

	<p>velocity & pressure heads) is in excess of vapour pressure of the liquid.”</p> <p>For any installation of pump, NPSH must be calculated by taking into consideration the absolute pressure of the liquid, the level of pump, the velocity head in suction line & friction head in suction line.</p> <p>If the required value of NPSH is not obtained, then partial vaporisation takes place & both the suction & delivery heads get reduced.</p> <p>$NPSH = (\text{absolute pressure head at suction point}) - (\text{vapour pressure head})$</p> <p>$NPSH = P_1/\rho g - P_v/\rho g - h_{fs} + Z_1$</p> <p><u>2) CAVITATION:</u></p> <p>Def: “The vapour pressure of the liquid at pumping temperature sets the lower limit for the suction pressure. Hence pressure at any point in suction should not fall below the vapour pressure of the liquid to be pumped. If pressure in suction line is less than vapour pressure of the liquid, then some of the liquid flashes into vapour or if liquid contains gases, they may come out of the solution resulting into gas pockets that damage impeller. This phenomenon is called as cavitation.”</p> <p>Cavitation results in no pumping of liquid. It leads to mechanical damage to pump as bubbles collapse.</p> <p>Cavitation can be reduced by reducing the pumping rate or by slight modification in impeller design to give better streamlining & avoiding use of sharp bends in suction line to reduce loss of head.</p>	2	
6.d	<p><u>CHARACTERISTICS CURVES IN CENTRIFUGAL PUMP:</u></p> <p>Def: “The graphical relationship between head & discharge rate, efficiency & discharge rate & power input & discharge rate and discharge rate at a particular speed.”</p>	4	4

			
6.e	<p>Venturi meter:</p>  <p>Advantages of venturimeter over orifice plate:</p> <ol style="list-style-type: none"> 1) Pressure recovery in venturi meter is high than in orifice meter. 2) Venturi meter can be used where only a small head is available. ,orifice meter can not be used 3) Venturi meter consumes smaller power consumption than orifice meter. 4) There is no flow separation in venturimeter 	3	4
6.f	<p>GIVEN DATA:</p> <p>Diameter of orifice = $d_o = 20 \text{ mm} = 0.02 \text{ m}$</p>		4

	<p>Diameter of pipe =Dp= 80 mm = 0.08 m</p> <p>$\Delta H = 21.4 \text{ cm of water} = 0.214 \text{ m of water.}$</p> <p>Coefficient of discharge(C_o) = 0.64</p> <p>The Flow Equation of orificemeter:</p> $Q = \frac{C_o A_o \sqrt{2g\Delta H}}{\sqrt{(1 - \beta^4)}}$ <p>$A_o = \pi/4 * d_o^2$</p> <p>$A_o = 3.14 /4 * (0.02)^2$</p> <p>$A_o = 3.14 \times 10^{-4} \text{ m}^2$</p> <p>$\beta = 0.08/0.02 = 0.25$</p> $Q = \frac{0.64 * 3.14 * 10^{-4} (\sqrt{2 * 9.81 * 0.214})}{\sqrt{(1 - 0.25^4)}}$ $Q = \frac{2.009 * 10^{-4} * 2.04}{0.9979}$ <p>$Q = 4.1 * 10^{-4} \text{ m}^3/\text{s}$</p> <p>$Q = 0.41 \text{ lit/s} = 24.6 \text{ lit/min}$</p>	<p>2</p> <p>1</p> <p>1</p>	
--	--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	----------------------------	--