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Important Instructions to examiners:

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more Importance (Not applicable for subject English and Communication Skills).
- 4) While assessing figures, examiner may give credit for principal components indicated in the figure. The figures drawn by candidate and model answer may vary. The examiner may give credit for any equivalent figure drawn.
- 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and model answer.
- 6) In case of some questions credit may be given by judgement on part of examiner of relevant answer based on candidate's understanding.
- 7) For programming language papers, credit may be given to any other program based on equivalent concept.

Model Answer	Marks
Q. 1 (A) (a) Define Factor of Safety. What factors affect its selection?	4
Ans: Factor of Safety: Factor of safety is defined as the ratio of the maximum stress to the working stress or design stress.	2
Mathematically,	
Factor of Safety = Maximum Stress/ Working or design stress	
Following factors affects selection of factor of safety: (Any Four)	2
i) The reliability of applied load and nature of load;	2
ii) The reliability of the properties of material and change of these properties during service;	
iii) The reliability of test results and accuracy of application of these results to actual machine parts;	
iv) The certainty as to exact mode of failure;	
v) The extent of simplifying assumptions;	
vi) The extent of localized stresses;	
vii) The extent of initial stresses setup during manufacture;	
viii) The extent of loss of property if failure occurs;	
The extent of loss of life if failure occurs.	



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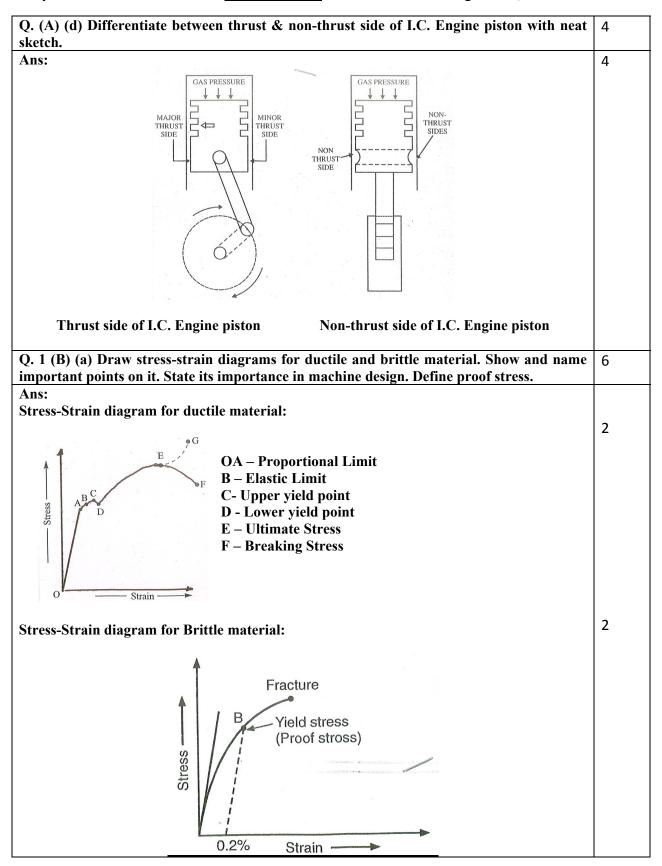
Q. 1 (A) (b) Define : i) Ergonomics, ii) Aesthetics	4
Ans:	2
i) Ergonomics:	ad
Ergonomics is defined as the relationship between man and machine the application of anatomical, physiological and psychological principles to so	
the problems arising from man-machine relationship.	
ii) Aesthetics:	2
Aesthetics is defined as it is a way of adding perceived value to a pro-	duct
and a pleasing design appearance. Or	
It is outward expression of quality of product.	
Q. 1 (A) (c) State the eight considerations in machine design.	4
Ans:	
Following are the general considerations in machine design (Any Eight of the Following)	4
i) Type of load and stresses caused by the load.	
ii) Motion of parts or kinetics of the machine.	
iii) Selection of materials	
iv) Form & size of parts	
v) Frictional resistance & lubrication	
vi) Convenient and economical features.	
vii) Use of standard parts	
viii) Safety of operation	
ix) Workshop facilities	
x) Number of machines to be manufactured	
xi) Cost of construction	
xii) Assembling	



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Importance of Stress strain diagram in machine design:

The proper and efficient use of material of construction requires considerable knowledge of their mechanical properties. Properties describe the behavior of the material under mechanical usage. The most important properties are strength, elasticity, stiffness, ductility etc. From stress-strain diagram, properties like ultimate strength, elastic limit, ductility etc. of material can be found out. Hence, these values can be used for designing and selection of proper material for machine design.

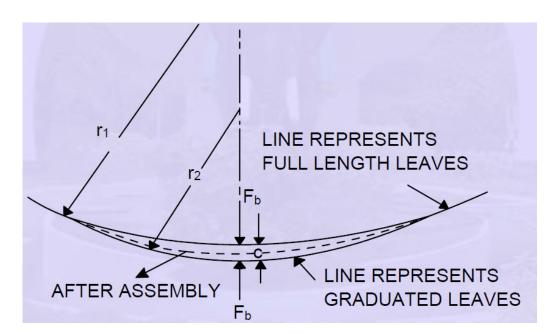
Definition of Proof Stress:

It is defined as the maximum stress a material can withstand without taking more than 0.01% permanent deformation.

Q. 1 (B) (b) What is Nipping of leaf springs? Why it is done? Write formula for final stress and deflection of leaf spring after nipping.

Ans:

The initial gap 'C' between the extra full length leaf and graduated length leaf before the assembly is called as 'Nip'. Such pre-stressing, achieved by a difference in radii of curvature I known as 'Nipping'.



It is seen that, stress in full length leaves is 50% greater than the stress in graduated leaves. In order to make best use of material, it is necessary that all the leaves must be equally stressed.

This can be achieved by in following two ways:

- i) By making full length leaves of smaller thickness than graduated leaves. In this way the full length leaves will induce a smaller bending stress due to small distance from neutral axis to edge of the leaf.
- ii) By giving a greater radius of curvature to the full length leaves than graduated leaves

2

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before leaves are assembled to form a spring.

By doing so, gap or clearance will be left between the leaves.

Formula for final stress and deflection of leaf spring after nipping:

2

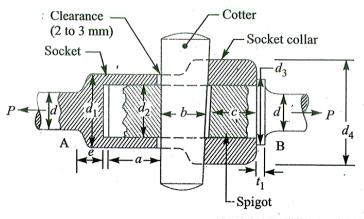
Final stress =
$$\sigma = \frac{6.W.L}{n.b.t^2}$$

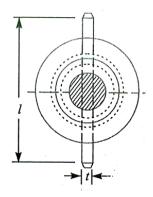
Deflection of leaf spring after nipping = $\delta = \frac{12.W.L^3}{E.b.t^3(2nG+3nf)}$

Q. 2 (a) Draw neat sketch of socket & spigot type cotter joint. Design a rod diameter for joint that has to withstand a load of 30kN, permissible stresses are 55 N/mm2 & 40 N/mm2 in tension & shear respectively.

3

Ans:





Socket and spigot cotter joint.

$$P=30kN=30x10^{3} N$$

 $\sigma_{t}=55 N/mm^{2}$

 $\tau = 40 \ N/mm^2$

Let, Diameter of rods 'd',

Considering the failure of rod in tension,

1

Load,
$$P = \frac{\pi}{4} x d^2 x \sigma_t$$

$$30x10^3 = \frac{\pi}{4}xd^2x \ 55$$

d=26.35mm

d=27mm ... say



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Q.2. (b) Draw neat sketch showing Through bolt, Tap bolt & stud. Write how screw threads are designated.	4
Sketch of Through bolt:	1
Sketch of Tap bolt:	1
Sketch of Stud:	
	1
Designation of Screw threads: According to Indian standards, IS:4218 (Part IV) 1976, (Reaffirmed 1990); the complete designation of screw thread shall include: i) Size Designation: The size of the screw thread is designated by the letter 'M' followed	1

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by the diameter and pitch, the two being separated by the sign 'X'. When there is no indication of the pitch, it shall mean that a coarse is implied.

- ii) Tolerance designation: This shall include
- a) A figure designating tolerance grade as indicated below, '7' for fine grade, '8' for normal (medium) grade and '9' for coarse grade.
- b) A letter designating the tolerance position as indicated below: 'H' for unit thread, 'd' for bolt thread with allowance, and 'h' for bolt thread without allowance.

For Example: M6-8d: A bolt thread of 6mm size of coarse pitch and with allowance on the threads and normal tolerance grade.

Q.2. (c) Design a knuckle joint to transmit a pull of 150kN. The ultimate strength of material used is 300MPa in tension, 240MPa in shear and 600 MPa in crushing. Take factor of safety = 4.

Ans:

Given Data:

 $\begin{aligned} P &= 150 kN = 150 x 10^3 \ N \\ \sigma_{tu} &= 300 MPa = 300 \ N/mm^2 \end{aligned}$

 $\tau_{\rm u} = 240 \text{ MPa} = 240 \text{ N/mm}^2$

 $\sigma_{cu} = 600 MPa = 600 N/mm^2$

Factor of Safety = 4

We know that, permissible tensile stress for rod material,

$$\begin{split} &\sigma_t = \frac{\sigma t u}{\textit{factor of safety}} = \frac{300}{4} = 75 \text{ N/mm}^2 \\ &\tau = \frac{\tau u}{\textit{factor of safety}} = \frac{240}{4} = 60 \text{ N/mm}^2 \\ &\sigma_c = \frac{\sigma c u}{\textit{factor of safety}} = \frac{600}{4} = 150 \text{ N/mm}^2 \end{split}$$

1) Failure of solid rod in tension:

$$d = Diameter of rod,$$

$$P = \frac{\pi}{4} x d^2 x \ \sigma_t$$

$$150x10^3 = \frac{76}{4}xd^2x \ 75$$

1

d= 50.4 mm

d=52mm



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Now various dimensions are fixed as follows:

i) Diameter of knuckle pin, $d_1 = d = 52$ mm

1

1

- ii) outer diameter of eye, $d_2 = 2d = 2x52=104$ mm
- iii) Diameter of knuckle pin head and collar, $d_3 = 1.5d=1.5x52 = 78mm$
- iv) Thickness of single eye or rod end, t = 1.25d = 1.25x52 = 65mm
- v) Thickness of fork, $t_1 = 0.75d = 0.75x52 = 39mm \sim 40mm$
- vi) Thickness of pin head, $t_2 = 0.5d = 0.5x52 = 26mm$
- 2) Failure of knuckle pin in shear:

Since the knuckle pin is in double shear,

Load,
$$P = 2x \frac{\pi}{4} x (d_1)^2 x \tau$$

$$150 \times 10^3 = 2 \times \frac{\pi}{4} \times (52)^2 \times \tau \quad \tau = 35.3 \text{ N/mm}^2$$

Note: Check with any one of the following Failure method .for single and Double eye

1) Failure of Single eye or rod end in tension:

The Single eye or rod end may fail in tension due to the load,

Load,
$$P = (d_2-d_1) \times t \times \sigma_t$$

$$150 \times 10^3 = (104-52) \times 65 \times \sigma_t$$

$$\sigma_{\rm t} = 44.4 \text{ N/mm}^2$$

2) Failure of Single eye or rod end in Shearing:

The Single eye or rod end may fail in shear due to the load,

Load,
$$P = (d_2 - d_1) \times t \times \tau$$

$$150 \times 10^3 = (104-52) \times 65 \times \tau$$

$$\tau = 44.4 \text{ N/mm}^2$$

3) Failure of Single eye or rod end in crushing:

The Single eye or rod end may fail in crushing due to the load,

Load,
$$P = d_1 x t x \sigma_c$$

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1

$$150 \times 10^3 = 52 \times 65 \times \sigma_c$$

$$\sigma_{\rm c} = 44.4 \text{ N/mm}^2$$

1)Failure of double eye or forked end in tension:

The double eye or forked end may fail in tension due to the load,

Load,
$$P = (d_2-d_1) \times 2 \times t_1 \times \sigma_t$$

$$150 \times 10^3 = (104-52) \times 2 \times 40 \times \sigma_t$$

$$\sigma_t = 36 \text{ N/mm}^2$$

2) Failure of double eye or forked end in Shear:

The double eye or forked end may fail in Shear due to the load,

Load,
$$P = (d_2-d_1) \times 2 \times t_1 \times \tau$$

$$150 \times 10^3 = (104-52) \times 2 \times 40 \times \tau$$

$$\tau = 36 \text{ N/mm}^2$$

3) Failure of double eye or forked end in Crushing:

The double eye or forked end may fail in Crushing due to the load,

Load,
$$P = d_1 \times 2 \times t_1 \times \sigma_c$$

$$150 \times 10^3 = 52 \times 2 \times 40 \times \sigma_c$$

$$\sigma_c = 36 \text{ N/mm}^2$$

From above, we see that, the induced stresses are less than the given design stresses,

therefore the joint is safe.

Q.2. (d) A single plate with both sides effective, has outer and inner diameter 300 mm and 200 mm respectively. the maximum intensity of pressure at any point of contact is not to exceed 0.2 N/mm2. If the coefficient of friction is 0.3. Determine the power transmitted by clutch at shaft speed 2500 rpm.

Ans:

Given data:

Outer diameter = $d_1 = 300 \text{ mm}$ or $r_1 = d_1/2 = 300/2 = 150 \text{mm}$

Inner diameter = d_2 = 200 mm or r_2 = $d_2/2$ = 200/2 = 100mm

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Maximum intensity of pressure = $P_{max.} = 0.1 \text{ N/mm}^2$

Coefficient of Friction = 0.3

Shaft Speed = N = 2500 rpm

Since, the intensity of pressure is maximum at inner radius, therefore, for uniform wear,

 $P_{\text{max.}} \times r_2 = C$

 $C = 0.1 \times 100$

C = 10 N/mm

1

We know that, axial thrust,

 $W = 2\pi C (r_1 - r_2)$

 $= 2 \times \pi \times 10 \times (150-100)$

1

W = 3141.5 N

and mean radius of friction,

 $r = (r_1 + r_2)/2$

=(150+100)/2

r = 125 mm.

We know that, torque transmitted,

 $T = \eta.\mu.W.r$

 $= 2 \times 0.3 \times 3141.5 \times 125$

= 235612.5 N-mm

1

T = 235.6 Nm

Power transmitted by clutch,

$$P = \frac{2.\pi . N.7}{60}$$

$$P = \frac{2x \pi x 2500 x 235.6}{60}$$

1

 $P = 61.68 \, kW$



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Q.2. (e) Define stress concentration. Explain its causes and suggest with proper sketches	4
for following:	
i) Stepped shaft	
ii) Cylindrical member with threads	
Ans:	
Stress Concentration:	
Whenever a machine component changes the shape of its cross section, the	
Whenever a machine component changes the shape of its cross section, the simple stress distribution no longer holds good and neighborhood of the discontinuity is	
different.	
This irregularity in the stress distribution caused by abrupt changes of form is called stress	1
concentration.	
OR	
Whenever there is a change in cross section of machine components, it causes high localized	
stresses. This effect is called as stress concentration.	
Causes of stress concentration and their remedies:	
i) Stepped Shaft:	
Causes:	
Abrupt changes of shape and cross section.	
Concentrated loads applied at points or small areas of machine elements.	
Remedies:	
Avoid abrupt changes in cross section	
Provide fillet when change in cross section if necessary.	
Make gradual changes in cross section.	. 4 -
	1.5
(a) Poor (b) Good	
(c) Preferred (d) Preferred	
ii) Cylindrical members with threads	
Causes:	
Force flow line is bent as it passes from the shank portion to threaded portion of	
component due to changes in cross section.	
This results in stress concentration in transition plane. Remedies:	1.5
Small under cut is taken between shank and the threaded portion of the component	1.5
Shank diameter is reduced and made equal to the core diameter of the thicat.	
(a) Poor (b) Good (c) Preferred	
and a fillet radius is provided for this under cut. Shank diameter is reduced and made equal to the core diameter of the thread. (a) Poor (b) Good (c) Preferred	



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Q3a) list and draw sketches of any four types of keys and write their applications	04
Ans: Types of keys 1. Sunk Keys 2. Saddle Keys 3. Tangent Keys 4. Round Keys 5. Splines	1
Use: Key is used to connect shaft and hub of pulley or coupling.	
Saddle key-for low load	1
Sunk key – for medium load	
Splines – heavy load.	
(ANY 4 FIGURES, ONLY KEY CAN ALSO BE CONSIDERED)	
(a) Hollow saddle key, (b) flat saddle key, (c) round key	2
(a) Woodruff key, (b) splined shaft, (a) Feather key, (b) rectangular key, and (c) square key	0.4
Q3b) Define lever. Describe three basic types of levers	04
Ans:	1
Definition: A lever is a rigid rod or a bar capable of turning about a fixed point called fulcrum.	
In lever load 'W 'and Effort 'P' can be applied in three different ways depending on that levers are called First Type, Second Type and Third Type.	
In first type Fulcrum is in between load and effort. Eg handle of pump, hand wheel punching press, beam of balance, foot lever etc	
In second type the load is in between the fulcrum and effort. Eg. Levers of loaded safety valve	



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	~ .	is in between fulcrum a	and load. Such levers are not cal advantage less than one.	2
	first type lever	Second type lever	Third type lever	1
	Compare foot lever and ication iii) cross section used		effort required to operate ii)	04
Sr.	Basis	Hand lever	Foot lever	
No				
1	effort required to operate	About 400 N	About 800 N	1
2	Application	Hand pump (or similar)	Brake pedal (or similar)	1
3	cross section used	Retangular:	Retangular:	
		Thickness is constant but taper in width	Thickness is constant but taper in width	1
4	Material	Wrought iron or mild steel	Wrought iron or mild steel	1
of 75 Find negle	mm. if the permissible sheather the axial load which the cting the effect of curvature	or stress is 350Mpa and m spring can carry and t e. Take shear stress factor		04
Ans:	Given: d=6mm, D _o =75mm, τ	=350Mpa, G= 84 Kn/mm ² =	84 x 103 N/mm ² .	
	Outside diameter of sprin	$\log D = D_o - d = 75-6 = 69 \text{m}$	n.	
	Therefore Spring Index C	=D/d = 69/6 = 11.5		
	Let W = Axial load and			1
	δ/n = Deflection per active	turn.		



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			1
	Neglecting the effect of curvature		
	$K_s = 1 + 1/2C = 1.$		
	And maximum shear stress induced in v	vire (τ)	1
	$\tau = K_s \times 8 \text{ W.D/} \pi d^3$		
	Therefore W= 412.7 N		
	Deflection of spring $\delta = 8W.D^3.n / G.d^4$		1
	Therefore deflection per active turn		
	$\delta/n = 8W.D^3 / G.d^4$		1
	= 9.96 mm.		
Q3e) C	Compare clutch with gear box		04
Ans:			4
	Clutch	Gear box	
	1)Clutch is a device used in	1)Gear box is used to provide	
	automobile to engage or disengage	different torque ratios at varied	
	the engine to transmission system	speed and road requirement	
	2)It transmits the same torque	2)It increases or decreases the	
		torque produced by the engine	
	3)The clutch is located between	3)It is located between clutch and	
	engine and gear box.	propeller shaft	
	4) The clutch is disengaged while	4)Gear is changed to obtain	
	shifting gears.	required torque.	
Q4.a) Determine the smallest size of the pu	nch that can be made to punch 10 mm thick	04
_	<i>′</i>	kN/mm ² and permissible crushing stress for	
harder	ned punch is 1.3 kN/mm ² .		
Ans:	Given: $\sigma_p = 1.3$ KN/mm2, $\tau_{ult. m} = 0.3$ I	KN/mm ² , thickness of plate t=10mm	
	Let'd '= smallest size of hole that can b	e punched	
	For punching the hole.		
	Permissible crushing strength of punch	≥ ultimate shear strength of material	
			1

1 = length of cotter

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$\Pi/4 \ .d^2 . \ \sigma_p \geq \ \Pi \ d \ t . \ \tau_{ult}$	2
Putting values we get $d \ge 9.2 \text{ mm}$	1
Therefore smallest size of hole that can be punched = 9.2 mm.	1
Q4.b) With neat sketch of socket and spigot cotter joint, write procedure to design cotter	04
only.	
Clearance (2 to 3 mm) Socket A Socket collar Spigot Spigot Socket and spigot cotter joint. In Fig:	02
P = load carried by the rods	
d = Diameter of the rods	
d_1 = outside diameter of socket	
d ₂ = Daimeter of Spigot or inside diameter of socket	
d ₃ = outside diameter of spigot collar	
t_1 = thickness of spigot collar	
d_4 = diameter of socket collar	
c = thickness of socket collar	
b = mean width of cotter	
t = thickness of cotter	



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a = distance from end of the slot to the end of rod	
Failure of cotter in shear: Since cotter fails in double shear Therefore shearing area of cotter = $2 b x t$ And shearing strength of cotter = $2b x t x \tau$ Equating this to load 'P' we get $P = 2b x t x \tau$ from this width of cotter is determined.	2
Q 4. c) State material and application of turn buckle. Design only rod diameter for a	4
turnbuckle to withstand a load of 50kN. The permissible stresses in rod material are 75 N/mm ² and 60 N/mm ² in tension and shear respectively.	l l
Ans: Material for turn buckle: The tie rod and coupler may be of same material. Generally it is made up of steel or Cast iron.	1
Applications: it is used in aeroplanes, tie bar of jib crane, to connect compartment of locomotives, tie string of electric poles.	1
Example:	
Given P=50 KN, $\sigma_t = 75 \text{ N/mm2}$, $\tau = 60 \text{ N/mm}^2$	
1. Design load $P_d = 1.3 P = 1.3 x 50 = 65 N$	1
2. Let Core diameter of rod = dc Now, Pd = $\Pi/4$. dc ² . σ_t	
dc = 33.2 mm	
3. Rod diameter $d = dc/0.84 = 39.5 \text{ mm} \approx 40 \text{mm}$	1
d) How are the solid shafts subjected to combined twisting moment and bending moment designed?	04



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inder Allower	
If shaft is subjected to twisting moment 'T' and bending moment 'M'	
Then equivalent twisting moment 'T _e ' is calculated by using formula $Te = \sqrt{M2 + T2}$	1
also equivalent bending moment is calculated by using formula $Me = \frac{1}{2} [M + \sqrt{M2 + T2}]$	1
and shaft diameter is calculated by using equation	1
Te = $\sqrt{M2 + T2} = \Pi / 16 \tau d^3$	1
and Me = $\frac{1}{2}$ [M + $\sqrt{M2 + T2}$] = $\Pi/32 \sigma_b d^3$	1
Where τ = allowable shear stress in shaft material	
σ_b = allowable bending stress in shaft material	
The maximum value of above two is considered.	
Q4 B) a) The rear axle shaft connecting differential to side wheel is required to transmi	
30 kW at 1500 rpm. If maximum torque is two times average torque and allowable shear stress is 80 N/mm ² for axle shaft material, find out diameter of axle shaft if	
stress is 80 N/mm ² for axle shaft material, find out diameter of axle shaft if	
stress is 80 N/mm ² for axle shaft material, find out diameter of axle shaft if i)shaft is solid	
stress is 80 N/mm² for axle shaft material, find out diameter of axle shaft if i)shaft is solid ii) shaft is hollow with outside diameter 1.5 times inside diameter.	
stress is 80 N/mm² for axle shaft material, find out diameter of axle shaft if i)shaft is solid ii) shaft is hollow with outside diameter 1.5 times inside diameter. Given: $P=30 \text{ KW} = 30 \text{ x } 10^3 \text{ W}, \text{ n=1500 rpm}, \tau = 80 \text{ N/mm}^2$ 1. Let average torque transmitted by rear axle shaft = 'T'	1
stress is 80 N/mm² for axle shaft material, find out diameter of axle shaft if i)shaft is solid ii) shaft is hollow with outside diameter 1.5 times inside diameter. Given: $P = 30 \text{ KW} = 30 \text{ x } 10^3 \text{ W}$, $n = 1500 \text{ rpm}$, $\tau = 80 \text{ N/mm}^2$ 1. Let average torque transmitted by rear axle shaft = 'T' We know that, $P = 2 \Pi \text{nT/60}$	1
stress is 80 N/mm² for axle shaft material, find out diameter of axle shaft if i)shaft is solid ii) shaft is hollow with outside diameter 1.5 times inside diameter. Given: $P=30 \text{ KW} = 30 \text{ x } 10^3 \text{ W}, \text{ n=1500 rpm}, \tau = 80 \text{ N/mm}^2$ 1. Let average torque transmitted by rear axle shaft = 'T' We know that, $P=2 \text{ II nT/60}$ Therefore, $T=190.98 \text{ N-m} = 190.98 \text{ x } 10^3 \text{ N-mm}$	1 1
stress is 80 N/mm² for axle shaft material, find out diameter of axle shaft if i)shaft is solid ii) shaft is hollow with outside diameter 1.5 times inside diameter. Given: $P=30 \text{ KW} = 30 \text{ x } 10^3 \text{ W}, \text{ n=1500 rpm}, \tau=80 \text{ N/mm}^2$ 1. Let average torque transmitted by rear axle shaft = 'T' We know that, $P=2 \text{ II nT/60}$ Therefore, $T=190.98 \text{ N-m} = 190.98 \text{ x } 10^3 \text{ N-mm}$ Now maximum torque $T_{max}=T \text{ X } 2=190.98 \text{ x } 10^3 \text{ X } 2=381.97 \text{ x } 10^3 \text{ N-mm}$	
stress is 80 N/mm² for axle shaft material, find out diameter of axle shaft if i)shaft is solid ii) shaft is hollow with outside diameter 1.5 times inside diameter. Given: $P=30 \text{ KW} = 30 \text{ x } 10^3 \text{ W}, \text{ n=1500 rpm}, \tau = 80 \text{ N/mm}^2$ 1. Let average torque transmitted by rear axle shaft = 'T' We know that, $P=2 \text{ II nT/60}$ Therefore, $T=190.98 \text{ N-m} = 190.98 \text{ x } 10^3 \text{ N-mm}$ Now maximum torque $T_{max} = T \text{ X } 2 = 190.98 \text{ x } 10^3 \text{ X } 2 = 381.97 \text{ x } 10^3 \text{ N-mm}$ Case I: if shaft is solid	1
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We know that $T_{max} = \Pi / 16 \tau do^3 (1 - k^4)$

2

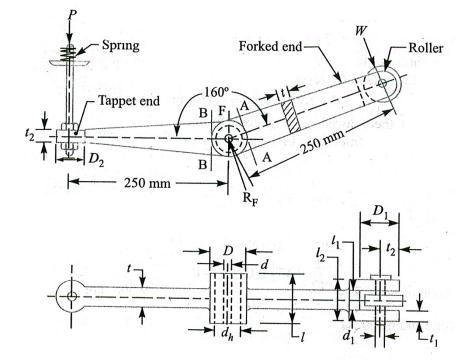
Putting values we get $do^3 = 30302.68$

Do = 31.176mm \approx 32mm, and di = 21.33 \approx 21 mm

Q4 B) b) With simple sketch explain procedure to design rocker arm for exhaust valve.

06

3



- a. Figure shows the rocker arm for operating the exhaust valve. In designing rocker arm following steps are followed
 - 1. Rocker arm is usually I-Section it is subjected to bending moment. To find bending moment it is assumed that the arm of the lever extends from point of application of load to centre of pivot.
 - 2. The ratio of length to the diameter of the fulcrum pin and roller pin is taken as 1.25. the permissible bearing pressure on this pin is taken from 3.5 to 6 N/mm².
 - 3. The outside diameter of boss at fulcrum is usually taken twice the diameter of the pin at fulcrum. The boss is provided with a 3mm thick phosphor bronze bush to take up the wear.

- 4. One end of rocker arm has a forked end to receive roller.
- 5. The outside diameter of the eye at the forked end is also taken as twice the diameter of pin. The diameter of roller is slightly larger (at least 3mm more) than the diameter of eye at the forked end. The radial thickness of each eye of the forked end is taken half the diameter of pin. Some clearance about 1.5mm must be provided between the roller and the eye at the forked end so that roller can move

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freely. The pin should, therefore be checked for bending.

- 6. The other end of rocker arm (i.e. tappet end) is made circular to receive the tappet which is a stud with a lock nut. The outside diameter of the circular arm is taken as twice the diameter of the stud. The depth of section is also taken twice the diameter of stud.
- Q-5 .a) Design and make a neat sketch of a rigid coupling for a shaft which transmits 250 N-m between two co-axial shafts. The shaft is made up of alloy steel. Flanges out of cast iron and bolts out of steel. Four bolts are used to couple flanges. The shafts are keyed to flange hub. The permissible stresses are given below:

Shear stress for shaft = 100 MPa, Crushing stress on shaft = 200 MPa,

Shear stress on key = 100 MPa, Bearing stress on key =250 MPa,

Shear stress on cast iron = 200 MPa, Shear stress on bolt = 100 MPa.

Ans- Given: T=250 N-m = 250 x 10^3 N-mm; n = 4; τ_s =100 MPa = 100 N/ mm²;

$$\sigma_{cs}$$
=200 MPa =200 N/ mm²; τ_{k} =100 MPa= 100 N/ mm²; σ_{ck} =250 MPa =250 N/ mm²;

$$\tau_c = 200 \text{ MPa} = 200 \text{ N/ mm}^2$$
; $\tau_b = 100 \text{ MPa} = 100 \text{ N/ mm}^2$;

1. Design for hub

First of all, let us find the diameter of the shaft (d). Torques transmitted by the shaft(T),

$$250x10^{3} = \frac{\pi}{16} \times \tau_{s} \times d^{3} = \frac{\pi}{16} \times 100 \times d^{3} = 19.64d^{3}$$

$$\therefore d^3 = 250 \times 10^3 / 19.64 = 12729 \text{ ord} = 23.35 \text{ say } 25 \text{ mm}$$

Outer diameter of the hub, $D= 2d = 2 \times 25 = 50 \text{ mm}$

Length of the hub, L=1.5 d=1.5 x 25 = 37.5 mm

Check induced shear stress in the hub by considering it as a hollow shaft.

$$250 \times 10^{3} = \frac{\pi}{16} \times \tau_{c} \left(\frac{D^{4} - d^{4}}{D} \right) = \frac{\pi}{16} \times \tau_{c} \times \left(\frac{50^{4} - 25^{4}}{50} \right)$$

$$\tau_c = 10.86 \text{ N/mm}^2 = 10.86 \text{ MPa}$$

Since the induced shear stress for the hub material (i.e. cast iron) is less than 200 MPa, therefore the design for hub is safe.

2. Design for key

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Find that proportions of key for a 25 mm diameter shaft are:

Width of key w = 10 mm

Thickness of key t = 8 mm

The length of key (l) is taken equal to the length of hub,

$$1 = L = 37.5$$

Let us now check the induced shear and crushing stresses in the key.

Considering key in sharing

$$T = 1 \times w \times \tau_k \times \frac{d}{2}$$

$$250 \times 10^3 = 37.5 \times 10 \times \tau_{kx} \times \frac{25}{2}$$

$$\tau_{k} = 53.3 \text{ N/mm}^2 = 53.3 \text{ MPa}$$

Considering the key in crushing

$$T = 1 x \frac{t}{2} x \sigma_{ck} x \frac{d}{2}$$

$$250 \times 10^3 = 37.5 \times \frac{8}{2} \times \sigma_{\text{ck}} \times \frac{25}{2}$$

$$\sigma_{ck} = 133.3 \text{ N/mm}^2 = 133.3 \text{ MPa}$$

Since the induced share and crushing stresses in the key are less than the given stresses. Therefore the design of the key is safe.

3 Design for flange

The thickness of the flange (t_f) is taken at 0.5 d

$$t_f = 0.5 d = 0.5 \times 25 = 12.5$$

Now let us check the induced share stress in the flange by considering the flange at the junction of the hub in share.

Torque transmitted T =
$$\frac{\pi D^2}{2} \times \tau_c \times t_f$$

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 $250 \times 10^{3} = \frac{\pi 50^{2}}{2} \times \tau_{c} \times 12.5$

2

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$$\tau_c = 5.1 \text{ N/mm}^2$$

Since the induced share stress in the flange of cast iron is less than 200 MPa, therefore design of flange is safe.

4 Design for bolts

Let d_1 = Nominal diameter of the bolts

 D_1 = pitch circle diameter of bolts = 3d = 3 x 25 = 75

The bolts are subjected to share stress due to the torque transmitted.

We know that torque transmitted T

$$250 \times 10^{3} = \frac{\pi d_{1}^{2}}{4} \times \tau_{b} \times n \times \frac{D_{1}}{2} = \frac{\pi d_{1}^{2}}{4} \times 100 \times 4 \times \frac{75}{2} = 4.6 \text{ mm}$$

Assuming coarse threads .the nearest standard size of the bolt is M 6

Outer diameter of the flange

 D_2 = 4 d= 4 x 25 = 100 mm

Thickness of the protective circumferential flange,

$$t_p = 0.25 d = 0.25 x 25 = 6.25 mm$$

Q-5 .b) An automotive gear box gives three forward and a reverse speed with top gear of unity and bottom and reverse gear ratio's of 3.3:1, the centre distance between shafts is 110 mm approximately. Gear teeth of module 3.25 mm are to be employed. Sketch simple layout of constant mesh gear box for these conditions giving the number of teeth for various gear wheels and showing own closely the different gear ratios are obtained

8

2

Ans- Given data- Module=3.25 mm

centre distance between shafts =110 mm

Since the pitch is same for all wheels and the centre distance same for all the pairs meeting the wheels, the total no. of teeth must be same for each pair



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There fore $T_A + T_B = T_C + T_D = T_E + T_F = T$

$$T = (2 * C.D.) / M$$

$$T = (2 *110) / 3.25 = 67.8$$

1

T=68 teeth

In general practice for better results gear ratios are kept in geometric progression if G_1,G_2,G_3 are gear ratios in first, second and third gear ,then

$$\frac{G_1}{G_2} = \frac{G_2}{G_3}$$

$$G_2 = \sqrt{G_1 \times G_2}$$

$$=\sqrt{1\times3.3}$$

$$= 1.817$$

In general practice, while designing a gear box it is desired that the gear ratio should be minimum possible in all cases, so that the sizes of the gear box can be kept minimum.

To achieve this, the maximum reduction required in gear box (in first gear) is achieved in two equal steps.

Now
$$G_1 = \frac{T_B}{T_A} \times \frac{T_D}{T_C}$$

Let X be the reduction in one step

therefore $G_1 = X \times X$

$$3.3 = X^2$$

$$X = 1.817$$

$$\frac{T_B}{T_A} = \frac{T_D}{T_C} = 1.817$$

$$T_B$$
 = 1.817 T_A and T_D = 1.817 T_C

$$T_A + T_B = 68$$
, $T_A + 1.817$ $T_A = 68$, $T_A = 68/2.817$

$$T_A=24$$
 teeth

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 $T_B = 68-24$ $T_B = 44$ teeth

Similarly $T_C=24$ teeth and $T_D=44$ teeth

Actual gear ratio

$$G_1 = \frac{T_B}{T_A} \times \frac{T_D}{T_C}$$

$$G_1 = \frac{44}{24} \times \frac{44}{24}$$

$$G_1=3.36:1$$

Second gear ratio

$$G_2 = \frac{T_B}{T_A} \times \frac{T_F}{T_E}$$

$$1.817 = \frac{44}{24} \times \frac{T_F}{T_E}$$

$$T_F = 0.991 T_E$$

$$T_E + T_F = 68$$

$$T_E + 0.991 T_E = 68$$

$$T_E = 34$$
 teeth

$$T_F = 68 - 34 = 34 \text{ teeth}$$

Actual gear ratio in second gear = $G_2 = \frac{44}{24} \times \frac{34}{34} = 1.833$

Top gear ratio G_3 =1:1 is obtained by directly coupling the main shaft to engine shaft. Now reverse gear and idler is fitted due to presence of which the direction is reversed also it is required that $T_D + T_I < 68$ to avoid interference of gear C and D

Therefore $T_i < 68 - T_D$

$$T_i < 68 - 44$$

$$T_{i} < 22$$

Exact gear ratio
$$G_R = \frac{T_B}{T_A} \times \frac{T_D}{T_L}$$
 $G_R = \frac{44}{24} \times \frac{44}{20}$

$$G_R = 4.03:1$$

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Exact centre distance between shaft,

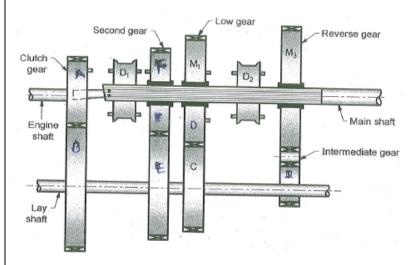
$$C.D. = \frac{M(TA + TB)}{2}$$

1

2

$$=\frac{3.25(68)}{2}$$

= 110.5 mm



Constant mesh gear box

Q-5 .c) Determine the thickness of plain cylinder head for 0.3 m cylinder diameter. The maximum gas pressure is 3.2 N/mm² .Design the studs and cylinder cover. Take allowable tensile stress for cylinder cover and bolt equal to 42 N/mm² and 63 N/mm² respectively.

3

Ans-Given Data:D = 0.3 m = 300 mm p = Maximum pressure = 3.2 N/mm², σ_c for cover = 42 N/mm², σ_t for bolts = 63 N/mm²

th- thickness of the cylinder head

$$t_h = D \sqrt{\frac{C \cdot p}{\sigma_c}}$$

D =Cylinder bore in mm

 $p = \text{Maximum pressure inside the cylinder in N/mm}^2$,

 σ_c = Allowable circumferential stress for cover in MPa or N/mm²

C =Constant whose value is taken as 0.1.

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 $th = 300 \sqrt{\frac{0.1 \times 3.2}{42}}$

2

 t_h = 26.2=26.5 mm

The pitch circle diameter (D_p) is usually taken as D + 3d.

d =Nominal diameter of the stud in mm,

 d_C = Core diameter of the stud in mm. It is usually taken as 0.84 d.

 σ_t = Tensile stress for the material of the stud which is usually nickel steel.

 n_b = Number of Bolts. It may be taken as 0.01 D + 4 to 0.02 D + 4=7 to 10

The load on bolts = $\pi/4D_p^2 * p$

$$\frac{\pi}{4}$$
 (300 + 3d)²*3.2

1

This load resisting by n_S No. of Bolts

$$\frac{\pi}{4} (300 + 3d)^2 * 3.2 = n_b \frac{\pi}{4} * dc^2 \sigma_t$$
 for bolts

 $d_{\mathcal{C}}$ = Core diameter of the bolts in mm. It is usually taken as 0.84 d.

Lets take $n_{b=8}$

$$\frac{\pi}{4}$$
 (300 + 3d)²*3.2= $n_{b_{4}}^{\pi} * dc^{2} \sigma_{t}$

d=40 mm

Now circular Pitch of Bolts =164.93 mm

Now minimum pitch should be 3d = 120 mm

3

Maximum pitch lies between 19 \sqrt{d} to 28.5 \sqrt{d}

=19
$$\sqrt{40}$$
 to 28.5 $\sqrt{40}$

2

Pitch circle of bolts = 164.93 mm is lies between 19 \sqrt{d} to 28.5 \sqrt{d}

Hence design is safe.

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Q 6.a) State and justify material used for piston. Draw a neat sketch showing allowance for piston expansion. Design crown thickness for following data,

O

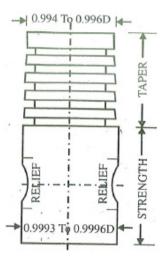
Maximum pressure inside the cylinder = 4.5N/mm²

Piston diameter = 70 mm, Stroke length = 80 mm, Allowing bending stress = 45 N/mm²

Ans:

Materials used for pistons of I.C. engines are cast iron, cast aluminum, forged aluminum, cast steel and forged steel. The cast iron pistons are used for moderately rated engines with piston speeds below 6 m/s and aluminum alloy pistons are used for highly rated engines running at higher piston speeds.

3



Piston Clearance Diagram

Given Data - D = 8 mm, P = 4.5 N/mm²,
$$\sigma_b = 45 \text{ N/mm}^2$$

Let the thickness of piston head can be designed by assuming the head to be a flat plate uniform thickness and fixed at the edges and assuming the gas load to be uniform distributed

$$t_{\rm h} = \sqrt{\frac{3PD^2}{16\sigma_b}}$$

where $t_h = \text{thickness of piston crown}$

$$P = P_{max}$$

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$$t_{\rm h} = \sqrt{\frac{3 \times 4.5 \times 80^2}{16 \times 45}}$$

3

 $t_h = 10.95 \text{ mm}$

 $t_h = 11 \text{ mm}$

Q 6. b) Explain why I-section are used for connecting rod. What proportions of 8 dimensions are

used.Design the connecting rod cross section for following data for petrol engine:

Maximum pressure inside the cylinder = 4.5N/mm²

Piston diameter = 70 mm, Stroke length =80 mm,

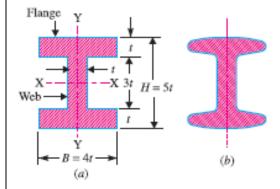
Effective length of connecting rod=140 mm

Ultimate crushing stress in rod material =300 N/mm²

Factor of safety =3 Take rankine constant for steel = 1/1600

Ans: I-sections are usually found to be most suitable for high speed engine connecting rod lightness is essential in order to keep inertia forces as small as possible .I-section also provides sufficient strength required to with stand momentary high gas pressure in the cylinder .Thus I-section fulfils most desirable conditions for connecting rod i.e. adequate strength and stiffness and minimum weight

2



The most suitable section for the connecting rod is *I*-section with the proportions as shown in Fig.

Let thickness of the flange and web of the section = t

Width of the section, B = 4 t

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2

2

and depth or height of the section, H = 5t

From Fig. find that area of the section,

 $A = 2 (4 t \times t) + 3 t \times t = 11 t^{2}$

Given Data- $P_{max} = 4.5 \text{ N/mm}^2$, D = 70 mm, l= 80 mm, L= 180 mm, $\sigma_{cu} = 330 \text{ N/mm}^2$,

$$\sigma_{\rm c} = \frac{\sigma_{cu}}{f.s} = \frac{300}{3} = 100 \text{ N/ mm}^2,$$

 $A = 11 t^2$ where t = thickness of rod

a = rankine contant = 1/1600

$$K = \sqrt{3.18 t^2}$$

w = maximum gas load= $P_{max} x \frac{\pi}{4} D^2 = 4.5 \times \frac{\pi}{4} 70^2$.

 $w = 17.32 \times 10^3 \text{ N}$

Assuming I-section

$$W = \frac{\sigma_c \times A}{1 + a[\frac{L^2}{k^2 r}]}$$

17.32 x 10³ N =
$$\frac{100 \times 11 t^2}{1 + 1/1600 \left[\frac{140^2}{2.18 t^2} \right]}$$

t = 4.08mm say t = 4.5 mm

Other dimensions of I-section at middle, small end and big end

- a) at the middle or centre dimension
- (i) depth or height of section

$$H=5 t=5 x 4.5$$

H = 22.5 mm

(ii) width of cross section B

 $B = 4 t = 4 \times 4.5 = 18 mm$



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1 uge 110. 23/ 3	
b)Dimension at small end	
(i) depth or height of section	
H ₁ =0.82H=0.82x22.5=18.45mm	
(ii) width of cross section B	
$B=B_1=18mm$	
c)Dimension at big end	
i)depth or height of section	
H ₂ =1.18H=26.55 mm	
ii) width of cross section B	
B ₂ =B=18mm	
Q 6. c) Draw a neat sketch of overhead valve mechanism .Mention the material used	1 8
For various components of mechanism .Design the port dimensions to li	
exhaust valve with following data: Diameter of piston = 70 mm, Stroke len	
80 mm,Exhaust velocity of gasses is 120 m/s with 5000 rpm gases enters at 45	_
	9
Δns Overhead valve mechanism	
Ans Overhead valve mechanism	
Valve Spring Valve Retainer Valve Clearance Tappet Adjusting Screw Tappet Guide Valve Filter Cam Shaft	2
Valve Retainer Valve Clearance Tappet Tappet Guide Valve Filter	2
Valve Retainer Valve Clearance Tappet Tappet Guide Valve Filter Cam Shaft	2



2

1

1

1

1

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Rocker arm: mild steel

Spring: Manganese steel

Valve seal : Alloy steel.

Tappet: Alloy steel

Inlet Valves: Alloy steel or nickel chromium steel

Exhaust valves: Austentic type chromium steel

Given Data-D=70 mm L=80 mm

$$V_1 = 120 \text{ m/s}, \alpha = 45^{\circ}, N = 5000 \text{ rpm} = 83.33 \text{ rev/sec}$$

In one revolution piston travells a distance = 2 x stroke length

hence in one sec ,piston travells a distance = $83.33 \times 160 \text{ mm/sec}$

Port Diameter d_p

Now $a_1V_1 = AV$ $a_1 = Area of the port, V = Mean velocity of the piston.$

$$\frac{\pi}{4}d_p^2 \times 120 = \frac{\pi}{4}70^2 \times 3.33$$

$$d_p^2 = 544.30$$

$$\therefore d_p = 23.33$$

Maximum lift of the valve L

$$L = d_p / 4\cos\alpha$$

L =Lift of the valve.

The lift of the valve may be obtained by equating the area across the valve seat to the area of the port. For a conical valve,

where

 α = Angle at which the valve seat is tapered = 45°.

 $L = 23.33/4\cos 45^{\circ}$.

L= 8.2484 mm

Valve stem diameter

The valve stem diameter (d_s) is given by

 $d_s = d_p/8 + 5 \text{ mm} = 7.911 = 8 \text{ mm}$



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