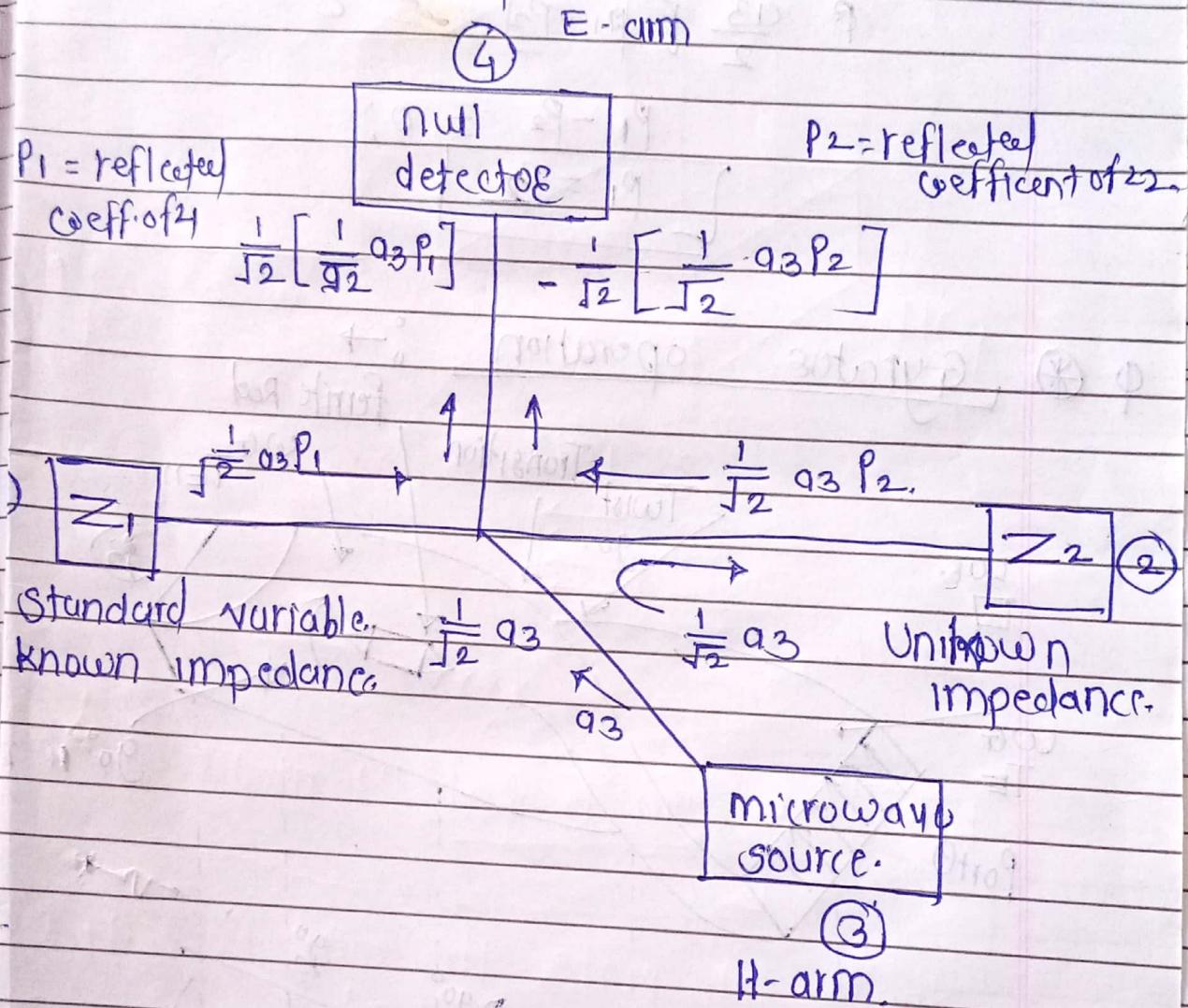


Unit - 3, Passive microwave component

with the help of suitable diagram explain how magic Tee is used for measurement of unknown impedance.



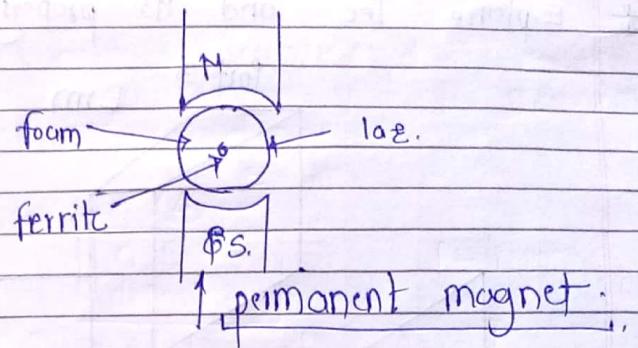
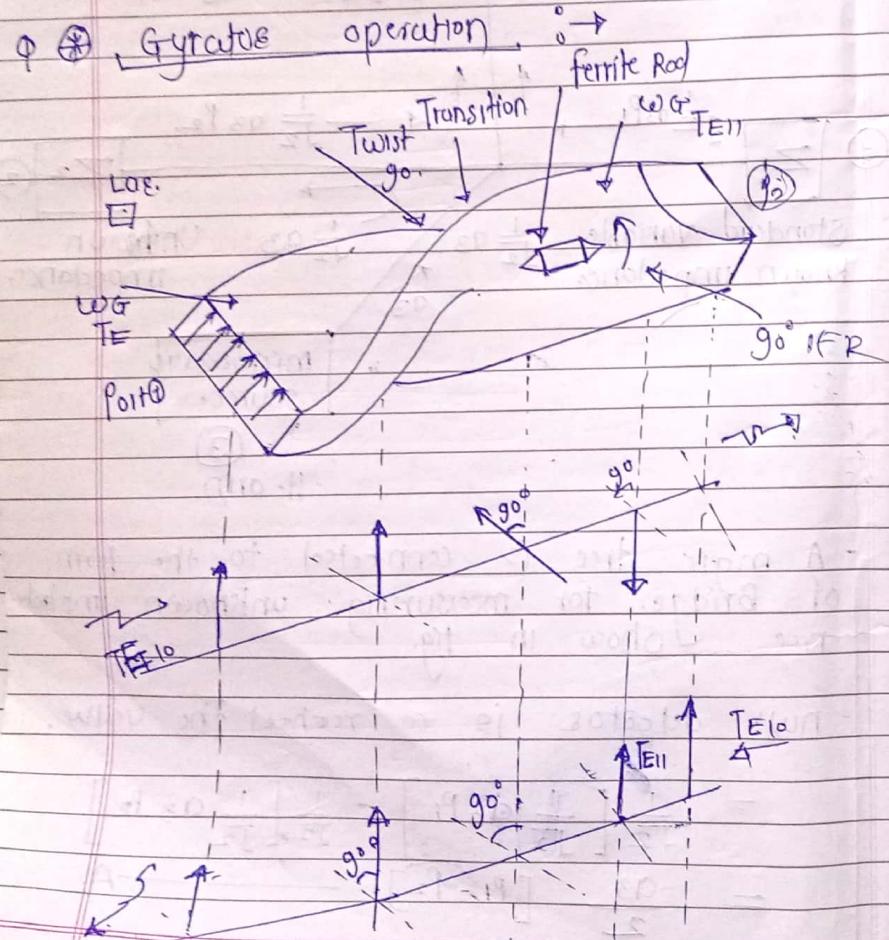
- A magic tee is connected to the form of Bridge for measuring unknown impedance. Show in fig.
- null detector is reached the value.

$$\begin{aligned}
 &= \frac{1}{\sqrt{2}} \left[\frac{1}{\sqrt{2}} \alpha_3 P_1 \right] - \frac{1}{\sqrt{2}} \left[\frac{1}{\sqrt{2}} \alpha_3 P_2 \right] \\
 &= \frac{\alpha_3}{2} - [P_1 - P_2] = A
 \end{aligned}$$

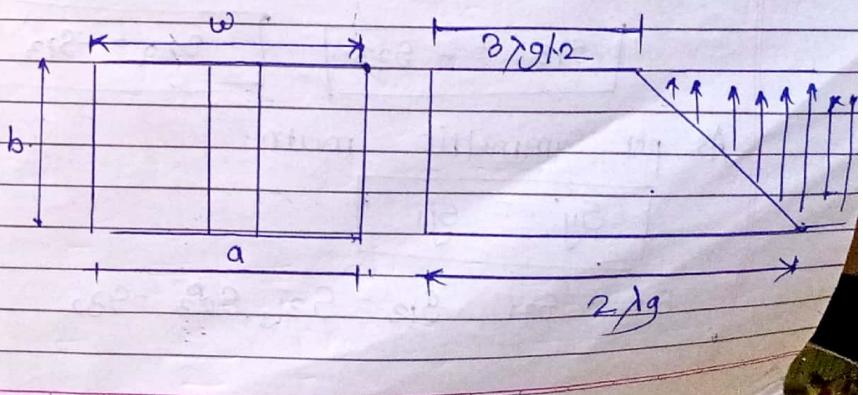
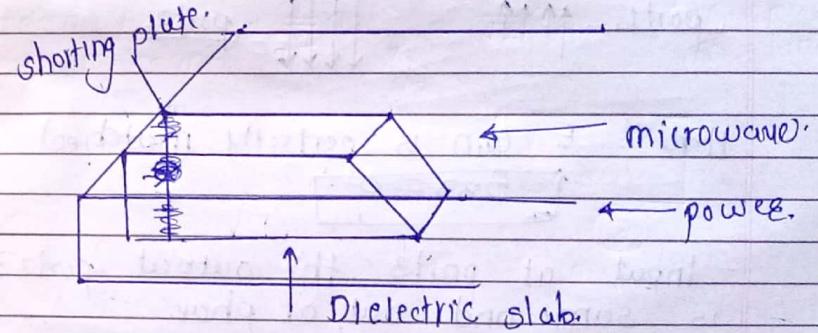
perfect balancing of bridge. After two current with zero or equal,

$$\beta \frac{a_3}{2} [P_1 - P_2] = 0$$

$$\begin{cases} P_1 - P_2 = 0; \\ P_1 = P_2 \end{cases}$$

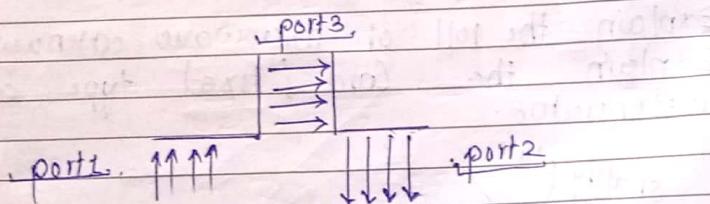
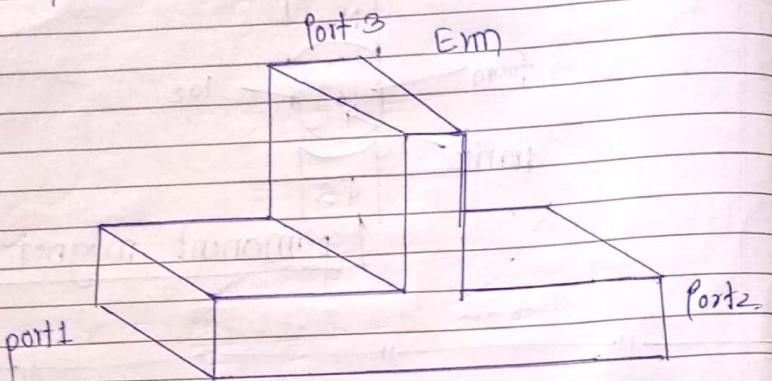


* Explain the roll of microwave attenuator.
Explain the card / fixed type of attenuators.



(b) $a_1 = a_2 = 0$, $a_3 = 0$
 (c) $a_1 \neq 0$, $a_3 = 0$

* Eplane Tee and its property.



Here - E arm is perfectly matched

$$S_{33} = 0$$

- Input at port 3, the output port 2's port is same and out of phase.

$$S_{13} = -S_{23}$$

$$S_{23} = -S_{13}$$

As per Symmetric matn:

$$S_{ij} = S_{ji}$$

$$S_{12} = S_{21}, S_{13} = S_{31}, S_{23} = S_{32}$$

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$$[S] = \begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{21} & S_{22} & S_{23} \\ S_{31} & S_{32} & S_{33} \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{12} & S_{22} & S_{13} \\ S_{13} & S_{23} & 0 \end{bmatrix}$$

- Let's unitarity property -

$$[S][S^*] = I$$

$$\begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{12} & S_{22} & S_{13} \\ S_{13} & S_{23} & 0 \end{bmatrix} \begin{bmatrix} S_{11}^* & S_{12}^* & S_{13}^* \\ S_{12}^* & S_{22}^* & -S_{13}^* \\ S_{13}^* & -S_{23}^* & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\Rightarrow R_1 C_1 = S_{11}^2 + S_{12}^2 + S_{13}^2 = 1.$$

$$R_2 C_2 = S_{12}^2 + S_{22}^2 + S_{13}^2 = 1$$

$$R_3 C_3 = S_{13}^2 + S_{23}^2 = 0 \quad \boxed{S_{13} = \frac{1}{\sqrt{2}}}$$

$$S_{11} = \frac{1}{2}, S_{22} = \frac{1}{2}$$

$$\boxed{S_{11} = S_{22}}$$

$$R_3 C_1 = S_{13} S_{11} + (-S_{13}) S_{12} = 0$$

$$\boxed{S_{11} = S_{12}}$$

$$\boxed{S_{11} = S_{12} = S_{22}}$$

$$R_1 C_1 = |S_{12}|^2 + |S_{12}|^2 + \left| \frac{1}{\sqrt{2}} \right|^2 = 1$$

$$\begin{bmatrix} \frac{1}{2} & \frac{1}{2} & \frac{1}{\sqrt{2}} \\ \frac{1}{2} & \frac{1}{2} & -\frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 0 \end{bmatrix}$$

$$\therefore [b] = [s] [a]$$

$$\begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix} = \begin{bmatrix} \frac{1}{2} & \frac{1}{2} & \frac{1}{\sqrt{2}} \\ \frac{1}{2} & \frac{1}{2} & -\frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 0 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}$$

$$b_1 = \frac{1}{2}a_1 + \frac{1}{2}a_2 + \frac{1}{\sqrt{2}}a_3$$

$$b_2 = \frac{1}{2}a_1 + \frac{1}{2}a_2 - \frac{1}{\sqrt{2}}a_3$$

$$b_3 = \frac{1}{\sqrt{2}}a_1 - \frac{1}{\sqrt{2}}a_2$$

(a) $a_1 = a_2 = 0, a_3 \neq 0$

$$b_1 = \frac{1}{\sqrt{2}}a_3$$

$$b_2 = -\frac{1}{\sqrt{2}}a_3$$

$$b_3 = 0$$

(b) $a_1 = a_2 = a, a \neq 0$

$$b_1 = \frac{a}{2} + \frac{a}{2}$$

$$b_2 = \frac{a}{2} + \frac{a}{2}$$

$$b_3 = \frac{a}{\sqrt{2}} - \frac{a}{\sqrt{2}} = 0$$

(c) $a_1 \neq 0, a_2 = 0, a_3 = 0$.

$$b_1 = \frac{1}{2}a_1, b_2 = \frac{1}{2}a_1, b_3 = \frac{1}{\sqrt{2}}a_1$$

Similarly, we have all combination of 11P and 01P.

Note - E

① $S_{13} = S_{23}$

② $S_{33} = 0$

③ $S_{ij} = S_{ji}$ symmetric property

④ $S_{12} = S_{21}, S_{13} = S_{31}, S_{23} = S_{32}$
Unitary prop.

$$[S][S^*] = I \cdot [R_3 G]$$

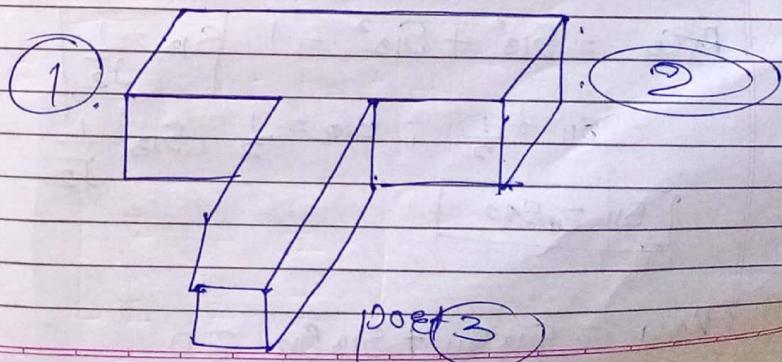
⑤ $[b] = [s][a]$

(a) $a_1 = a_2 = 0, a_3 \neq 0$

(b) $a_1 = a_2 = a, a_3 = 0$

(c) $a_1 \neq 0, a_2 = a_3 = 0$

H plane Tee and properties: →



(8)

$$\textcircled{1} \quad S_{13} = S_{23}$$

$$\textcircled{2} \quad S_{33} = 0$$

\textcircled{3} Symmetric property.

$$S_{ij} = S_{ji}$$

$$S_{12} = S_{21}, \quad S_{13} = S_{31}, \quad S_{23} = S_{32}$$

$$[S] = \begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{21} & S_{22} & S_{23} \\ S_{31} & S_{32} & S_{33} \end{bmatrix} \quad [S^*] = \begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{12} & S_{22} & S_{13} \\ S_{13} & S_{23} & 0 \end{bmatrix}$$

\textcircled{4} Unitarity property: $[S][S^*] = I$

$$\begin{bmatrix} S_{11}^* & S_{12}^* & S_{13}^* \\ S_{12}^* & S_{22}^* & S_{13}^* \\ S_{13}^* & S_{23}^* & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_1 C_1 = |S_{11}|^2 + |S_{12}|^2 + |S_{13}|^2 = 1$$

$$R_2 C_2 = |S_{12}|^2 + |S_{22}|^2 + |S_{13}|^2 = 1$$

$$R_3 C_3 = |S_{13}|^2 + |S_{23}|^2 = 1 \quad S_{13} = \frac{1}{\sqrt{2}}$$

$$S_{11} = \frac{1}{2}, \quad S_{12} = \frac{1}{2}, \quad S_{13} = \frac{1}{\sqrt{2}}$$

$$S_{11} = S_{22}$$

$$R_3 C_1 = S_{13} S_{11} + S_{23} S_{12} = 0$$

$$TS_{11} = -S_{12}$$

$$S_{11} = S_{22} = -S_{12}$$

$$\begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix} = \begin{bmatrix} \frac{1}{2} & -\frac{1}{2} & \frac{1}{\sqrt{2}} \\ -\frac{1}{2} & \frac{1}{2} & \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 0 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix}$$

$$b_1 = \frac{1}{2} q_1 - \frac{1}{2} q_2 + \frac{1}{\sqrt{2}} q_3$$

$$b_2 = -\frac{1}{2} q_1 + \frac{1}{2} q_2 + \frac{1}{\sqrt{2}} q_3$$

$$b_3 = \frac{1}{\sqrt{2}} q_1 + \frac{1}{\sqrt{2}} q_2$$

$$\textcircled{5} \quad q_1 = q_2 = 0, \quad q_3 \neq 0$$

$$b_1 = \frac{1}{\sqrt{2}} q_3, \quad b_3 = 0$$

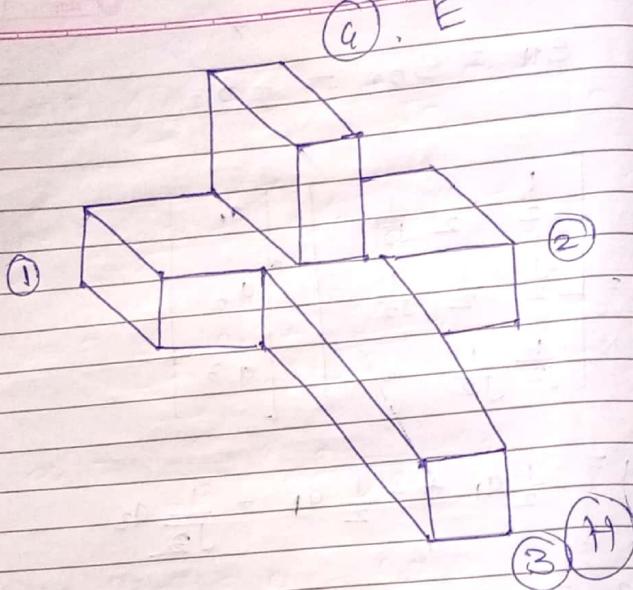
$$b_2 = \frac{1}{\sqrt{2}} q_3$$

$$\textcircled{6} \quad q_1 = q_2 = q, \quad q_3 = 0$$

$$b_1 = \frac{q}{2} - \frac{q}{2} \boxed{b_1 = 0}, \quad b_2 = 0,$$

$$\boxed{b_3 = \frac{q}{\sqrt{2}} + \frac{q}{\sqrt{2}}}$$

$$\textcircled{7} \quad q \neq 0 \quad (q_1 \neq q_2 \neq q_3 \neq 0)$$



$$\textcircled{1} H = S_{13} = S_{23}, S_{33} = 0$$

$$\textcircled{2} E = S_{14} = -S_{24}, S_{24} = -S_{14}, S_{44} = 0$$

$$S_{34} = S_{43} = 0$$

③ Symmetric.

$$S_{ij} = S_{ji}$$

S

$$S = \begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{21} & S_{22} & S_{23} & S_{24} \\ S_{31} & S_{32} & S_{33} & S_{34} \\ S_{41} & S_{42} & S_{43} & S_{44} \end{bmatrix}$$

$$\begin{aligned} S_{11}^2 &= \frac{1}{2} & S_{11} &= \pm \frac{1}{2} \\ S_{12}^2 &= \frac{1}{2} & S_{12} &= \pm \frac{1}{2} \\ S_{11} &= S_{12} = \frac{1}{2} \end{aligned}$$

$$S_{12} = S_{21}, S_{13} = S_{31}, S_{14} = S_{41},$$

$$S_{23} = S_{32}, S_{24} = S_{42}$$

\rightarrow Unitary property $[S][S^*] = I$.

$$\begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{12} & S_{22} & S_{23} & -S_{14} \\ S_{13} & S_{23} & 0 & 0 \\ S_{14} & -S_{14} & 0 & 0 \end{bmatrix} \quad \begin{bmatrix} S_{11}^* & S_{12}^* & S_{13}^* & S_{14}^* \\ S_{12}^* & S_{22}^* & S_{23}^* & -S_{14}^* \\ S_{13}^* & S_{23}^* & 0 & 0 \\ S_{14}^* & -S_{14}^* & 0 & 0 \end{bmatrix}$$

$$R_1 C_1 = S_{11}^2 + S_{12}^2 + S_{13}^2 + S_{14}^2 = 1$$

$$R_2 C_2 = S_{12}^2 + S_{22}^2 + S_{23}^2 + S_{14}^2 = 1$$

$$R_3 C_3 = S_{13} = \frac{1}{\sqrt{2}}$$

$$R_4 C_4 = S_{14} = \frac{1}{\sqrt{2}}$$

$$S_{13} = S_{14} = \frac{1}{\sqrt{2}}, S_{11} = \frac{1}{2}, S_{22} = \frac{1}{2},$$

$$R_4 C_1 = S_{14} S_{11} + (-S_{14} S_{12})$$

$$S_{11} = S_{12}$$

$$S_{13} = \frac{1}{\sqrt{2}}, S_{14} = \frac{1}{\sqrt{2}}, S_{11} = \frac{1}{2}, S_{12} = -\frac{1}{2}.$$

$$S_{12} = \frac{1}{2}$$

$$\begin{bmatrix} b_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix} = \begin{bmatrix} \frac{1}{2} & \frac{1}{2} & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 0 & 0 \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 0 & 0 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ q_4 \end{bmatrix}$$

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$$a_1 = a_2 = a_3 = a_4 = 0$$

$$a_3 > a_4 = 0$$

$$b_1 = \frac{1}{\sqrt{2}} a_1 + \frac{1}{\sqrt{2}} a_2 + \frac{1}{\sqrt{2}} a_3 + \frac{1}{\sqrt{2}} a_4$$

$$b_2 = \frac{1}{\sqrt{2}} a_1 + \frac{1}{\sqrt{2}} a_2 + \frac{1}{\sqrt{2}} a_3 - \frac{1}{\sqrt{2}} a_4$$

$$b_3 = \frac{1}{\sqrt{2}} a_1 + \frac{1}{\sqrt{2}} a_2 \quad b_4 = 0$$

$$b_4 = \frac{1}{\sqrt{2}} a_1 + \frac{1}{\sqrt{2}} a_2 \quad b_4 = 0$$

(a) $a_1 = a_2 = a_3 = 0, a_4 \neq 0,$

$$b_1 = \frac{1}{\sqrt{2}} a_4, b_2 = -\frac{1}{\sqrt{2}} a_4, b_3 = b_4 = 0$$

(b) $a_1 = a_2 = a_4 = 0, a_3 \neq 0.$

$$b_1 = \frac{1}{\sqrt{2}} a_3, b_2 = \frac{1}{\sqrt{2}} a_3, b_3 = b_4 = 0$$

(c) $a_1 \neq 0, a_2 = a_3 = a_4 = 0.$

$$b_1 = 0, b_2 = \frac{1}{\sqrt{2}} a_1, b_3 = \frac{a_1}{\sqrt{2}}, b_4 = \frac{1}{\sqrt{2}} a_1$$

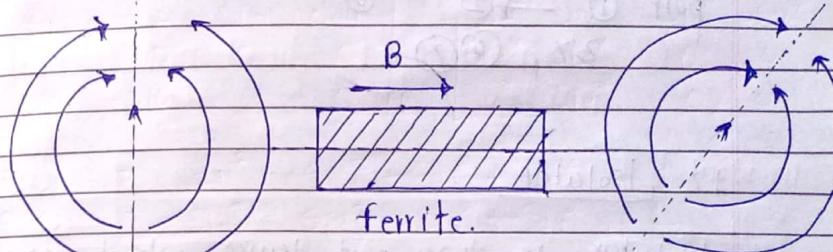
(d) $a_3 = a_4, a_1 = a_2 = 0.$

$$b_1 = \frac{a_1}{\sqrt{2}} (2a_3)$$

(e) $a_1 = a_2, a_3 = a_4 = 0.$

$$b_1 = 0, b_2 = 0, b_3 = \frac{1}{\sqrt{2}} (2a_1) \quad b_4 = 0$$

* Faraday's Rotation principle: →



(a)

Circularly polarized wave

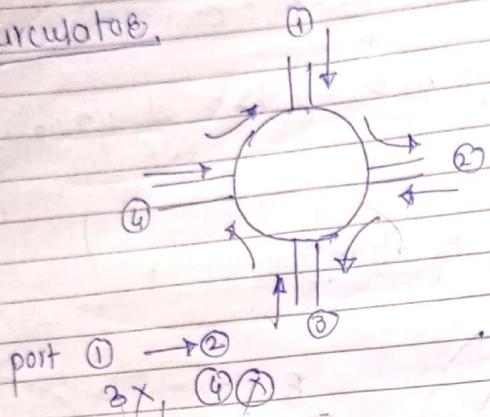
(b)

Tilted pt. polarized wave

fig. a 3.20 illustration of Faraday's rotation principle.

1) Faraday's Rotation principle state that circularly polarized wave (TE₁₁) in a waveguide made to pass through the ferrite rod. This circular polarized wave pass through B magnetic field through ferrite rod and get tilted in clockwise direction and the amount of tilted is dependent upon the strength of magnetic field and geometry ferrite rod shown in fig

Circulator:

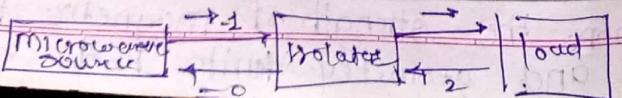
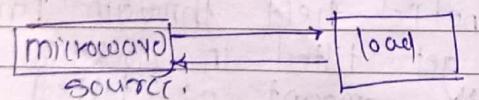


Isolator:

Isolator is two port device which provides small amount of attenuation for transmission from port ① and ②.

- But High amount of attenuation for transmission from port ② to port ①.

- Suppose the two port are not matched. transmission reflected from port ② to port ① with maximum amount of attenuation but isolator isolate this EM wave from port ② to port ①.



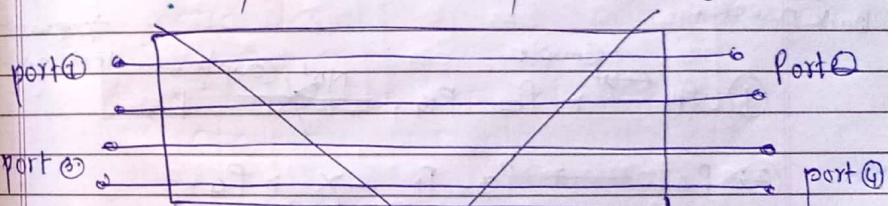
* Directional couplers: →

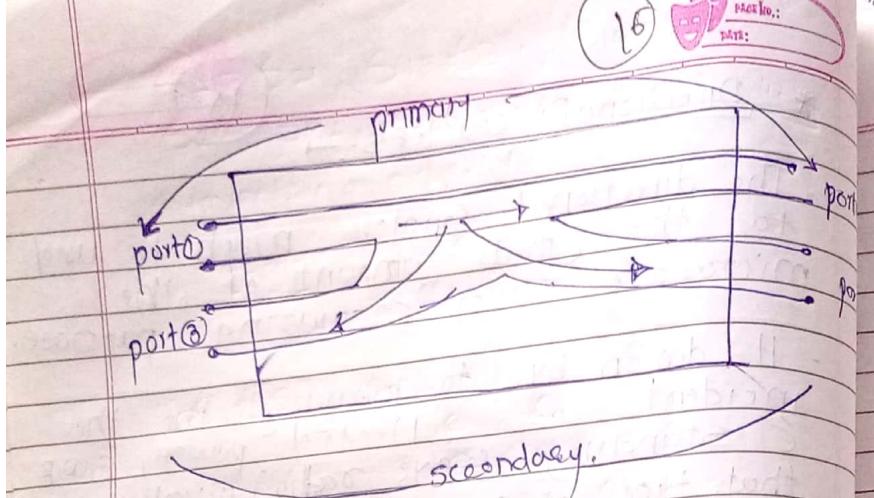
- The directional couplers much be used to the small amount of the microwave power measuring purpose.

- It design by to measured the the incident or reflected powers, SWR (standing wave ratio) value. that type of operation perform in which.

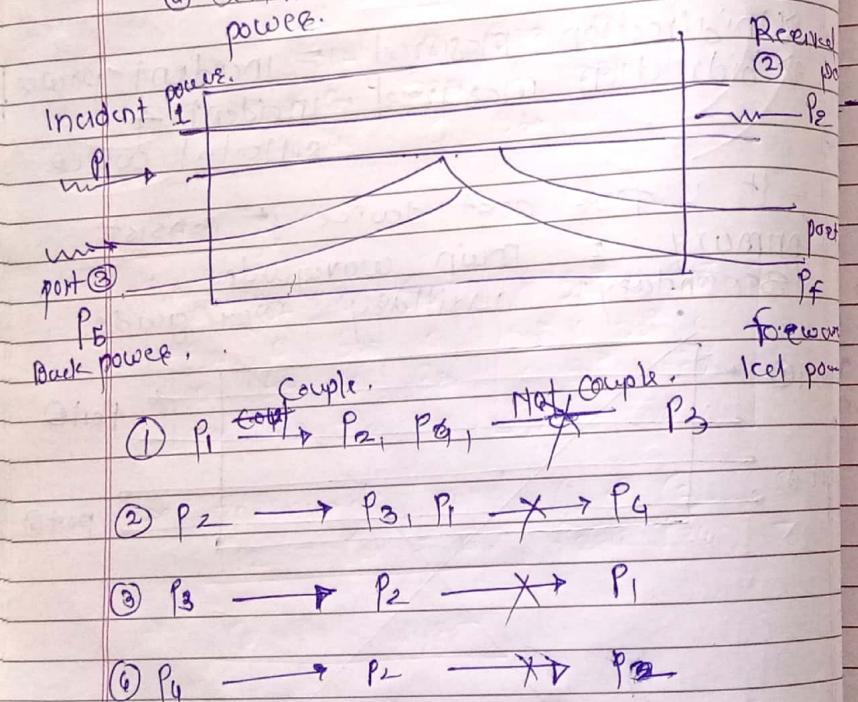
⇒ Unidirection measured = Incident power
⇒ bidirection measured = Incident + Reflected power.

- It is four port device it consist primary = main waveguide.
secondary = auxiliary waveguide.





① Schematic of directional coupler.

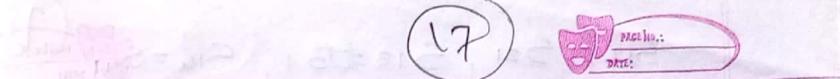


P_i = Incident power at port (1)

P_r = Received power at port (2)

P_f = Forward couple power at port (3)

P_b = Back power at port (3)



① Coupling factor (C)

$$C = 10 \log_{10} \frac{P_i}{P_f} \text{ dB.}$$

② Directivity (D)

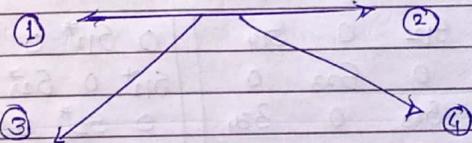
$$D = 10 \log_{10} \frac{P_f}{P_b} \text{ dB.}$$

③ Isolation (I)

$$I = 10 \log_{10} \frac{P_i}{P_b} \text{ dB.}$$

Isolation in dB = Coupling factor + Directivity

Scattering matrix of A. Bidirectional Coupler.



$$[S] = \begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{21} & S_{22} & S_{23} & S_{24} \\ S_{31} & S_{32} & S_{33} & S_{34} \\ S_{41} & S_{42} & S_{43} & S_{44} \end{bmatrix}$$

four port one match. \rightarrow

$$S_{11} = S_{22} = S_{33} = S_{44} = 0$$

Coupled ① & ③ and ② & ④

$$S_{13} = S_{31} = 0,$$

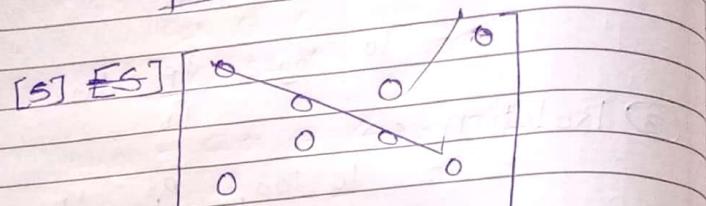
$$S_{24} = S_{42} = 0$$

$$S_{12} = S_{21}, S_{13} = S_{31}, S_{14} = S_{41}$$

$$S_{23} = S_{32}, S_{34} = S_{43}, S_{24} = S_{42}$$

Symmetry property

$$\text{EJE } S_j = S_j^t$$



$$\begin{bmatrix} 0 & S_{12} & 0 & S_{14} \\ S_{12} & 0 & S_{23} & 0 \\ 0 & S_{23} & 0 & S_{34} \\ S_{14} & 0 & S_{34} & 0 \end{bmatrix}$$

Identity,

$$\begin{bmatrix} 0 & S_{12} & 0 & S_{14} \\ S_{12} & 0 & S_{23} & 0 \\ 0 & S_{23} & 0 & S_{34} \\ S_{14} & 0 & S_{34} & 0 \end{bmatrix} \begin{bmatrix} 0 & S_{12}^* & 0 & S_{14}^* \\ S_{12}^* & 0 & S_{23}^* & 0 \\ 0 & S_{23}^* & 0 & S_{34}^* \\ S_{14}^* & 0 & S_{34}^* & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

* forward port: ① + ②

$$P_{12} = P_{21} = P_1, P_{23} = P_{32} = P_2$$

* coupled port

$$P_{23} = P_{32}, P_{24} = P_{42} = ① - ②$$

$$P_{14} = P_{41}$$

$$\begin{bmatrix} 0 & P & 0 & ① \\ P & 0 & ① & 0 \\ 0 & ① & 0 & P \\ ① & 0 & P & 0 \end{bmatrix}$$

19
Determine the [S] of a 3-port circulator given insertion loss of 0.5 dB, isolation of 20 dB and VSWR of 2.

Given : i) Insertion loss = 0.5 dB

$$= -20 \log [S_{21}]$$

$$|S_{21}| = 10^{-0.5/20}$$

$$S_{21} = 10^{-0.025}$$

$$ii) \text{ Isolation} = 20 \text{ dB}$$

$$= -20 \log [S_{212}]$$

$$S_{12} = 10^{-20/20}$$

$$S_{12} = 10^{-1} \quad S_{12} = 0.1$$

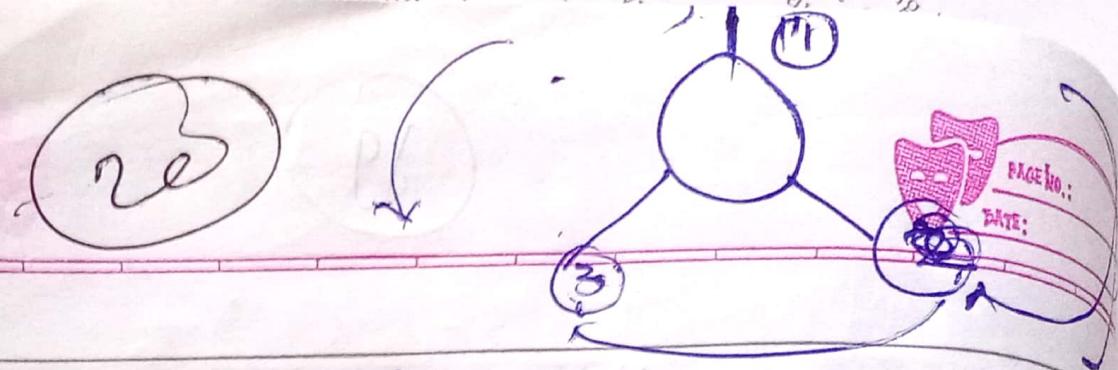
$$S_{12} = S_{23} = S_{31} = 0.1$$

$$P = \frac{VSWR - 1}{VSWR + 1}$$

$$= \frac{2-1}{2+1} = \frac{1}{3} = 0.333$$

$$S_{11} = S_{22} = S_{33} = 0.333$$

$$\begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{21} & S_{22} & S_{23} \\ S_{31} & S_{32} & S_{33} \end{bmatrix} \begin{bmatrix} 0.33 & 0.1 & 10^{-0.025} \\ 10^{-0.025} & 0.33 & 0.1 \\ 0.1 & 10^{-0.025} & 0.33 \end{bmatrix}$$



NON Reciprocal:

$$\begin{bmatrix} 0 & 0 & S_{13} \\ S_{21} & 0 & 0 \\ 0 & S_{32} & 0 \end{bmatrix}$$

$$\therefore S_{13} = S_{21} = S_{32} = 1$$

$$\begin{bmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}$$

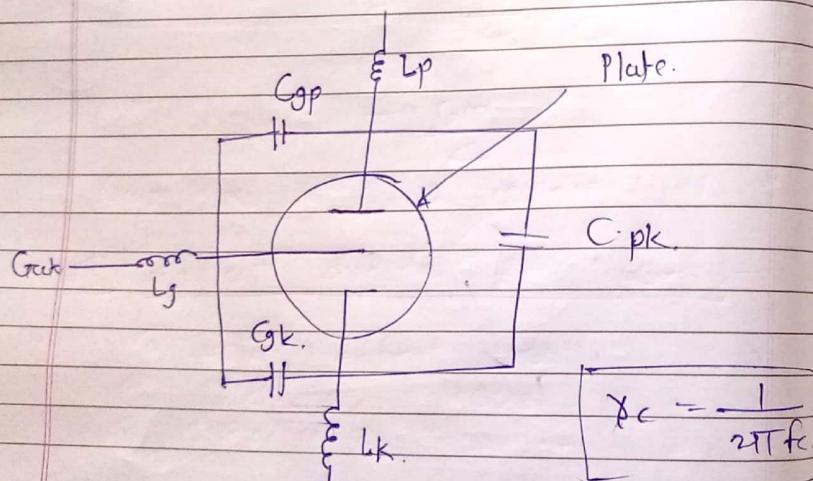
*

Q3. @ Elaborate on the HF limitation of conventional tube.

- following are the five reasons because which conventional tube does not use for High frequency more than 100MHz.

- ① Interelectrode Capacitance effect.
- ② lead Inductance effect.
- ③ Transit Time effect.
- ④ Gun Bandwidth limitation
- ⑤ effect due to RF losses.

① Interelectrode Capacitance effect.



operation. - if frequency ↑, $X_C \downarrow$ & OIP ↓ at sh due to shunt effect

- then X_C high X_C is short.

f - frequency
than → ↑ ince
 da.

→ $C_{gp} \downarrow$ & C_{pk}, C_{gk} is reduced. then area of electrode ↑ & distance of electrode ↑.

② lead Inductance effect (Same diagram)

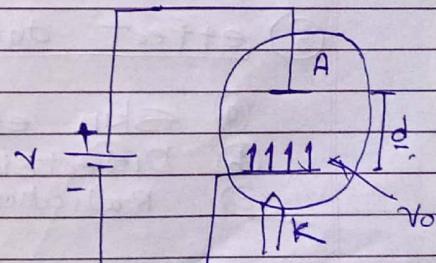
- frequency ↑ then $\rightarrow X_L = 2\pi f L$ ↑ → active electrode ↘ & base pins.
- L_p, L_g, L_k leading inductance.

- we can minimize the effect of X_L by ↓ L . that time reduce the HF power handling capacity.

③ Transit Time effect.

Transit time effect that time between electron flow from cathode to anode.

$$T = \frac{d}{v_0}$$



- $f \uparrow$ 'T' appears appreciable which $\downarrow v_0$.

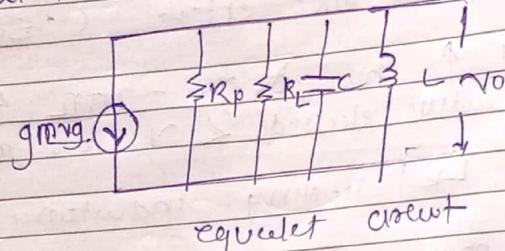
- to minimize $f \cdot T$ 'd' is separated → electrode is ↑ & v_0 ↑ →

- Interelectrode capacitance & T are composed

23

④ Gain Bandwidth product limitation.

- when the tuned circuit is not resonant at that time max. gain is achieved.



$$\text{Gain Bandwidth product} = \text{Amp.} \cdot B(\omega)$$

$$= \frac{G_m}{G_F} \cdot \frac{C}{C}$$

$$= \frac{G_m}{C}$$

Gain Bandwidth product is dependent upon frequency.

⑤ Effect due to RF losses:-

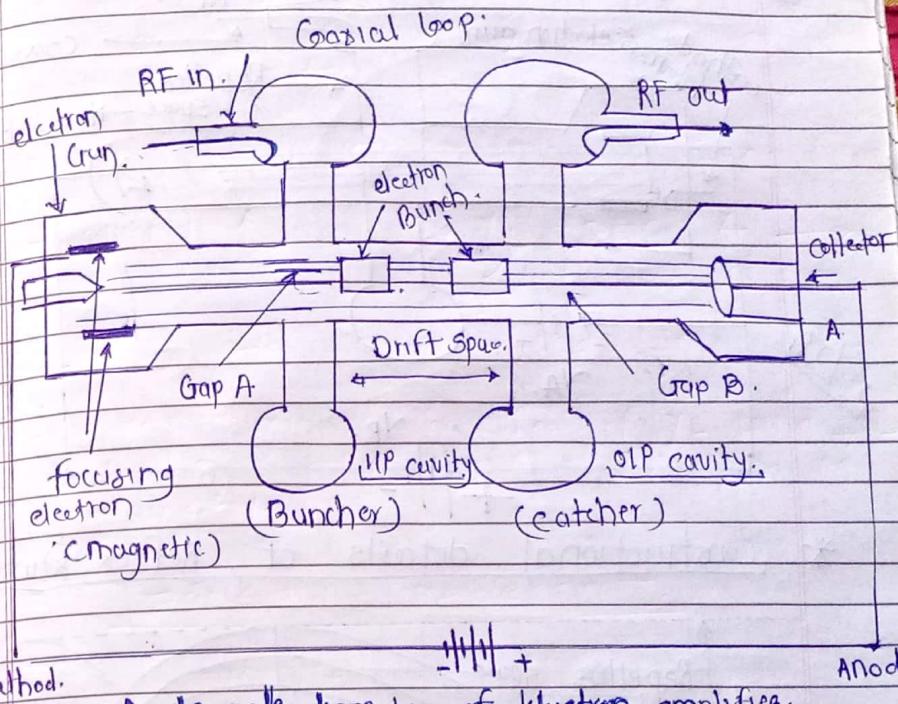
a) Skin effect losses.

b) Dielectric losses.

c) Radiation losses.

24

* two cavity klystron Amplifier.

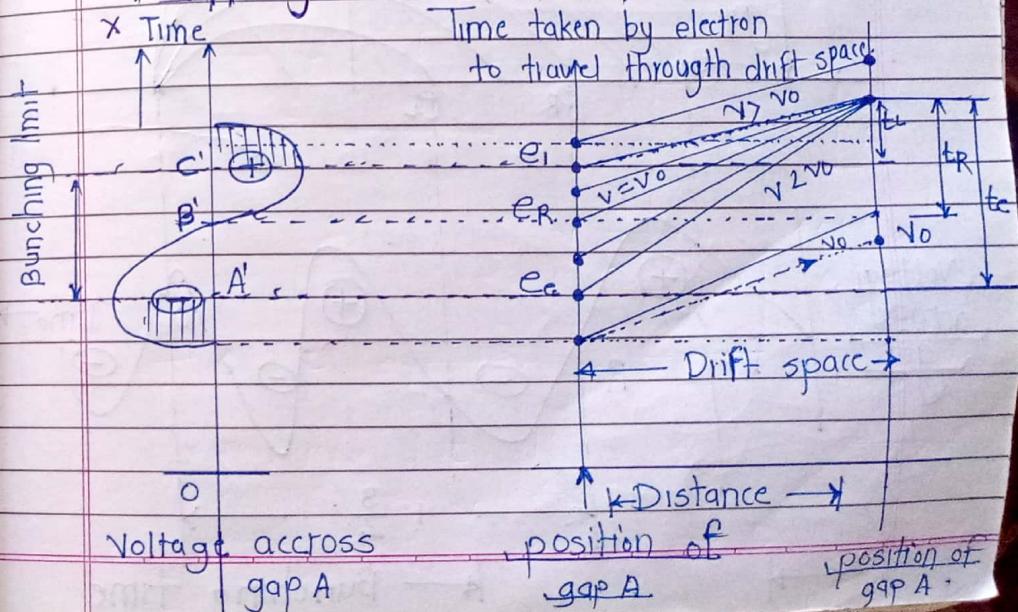


cathode.



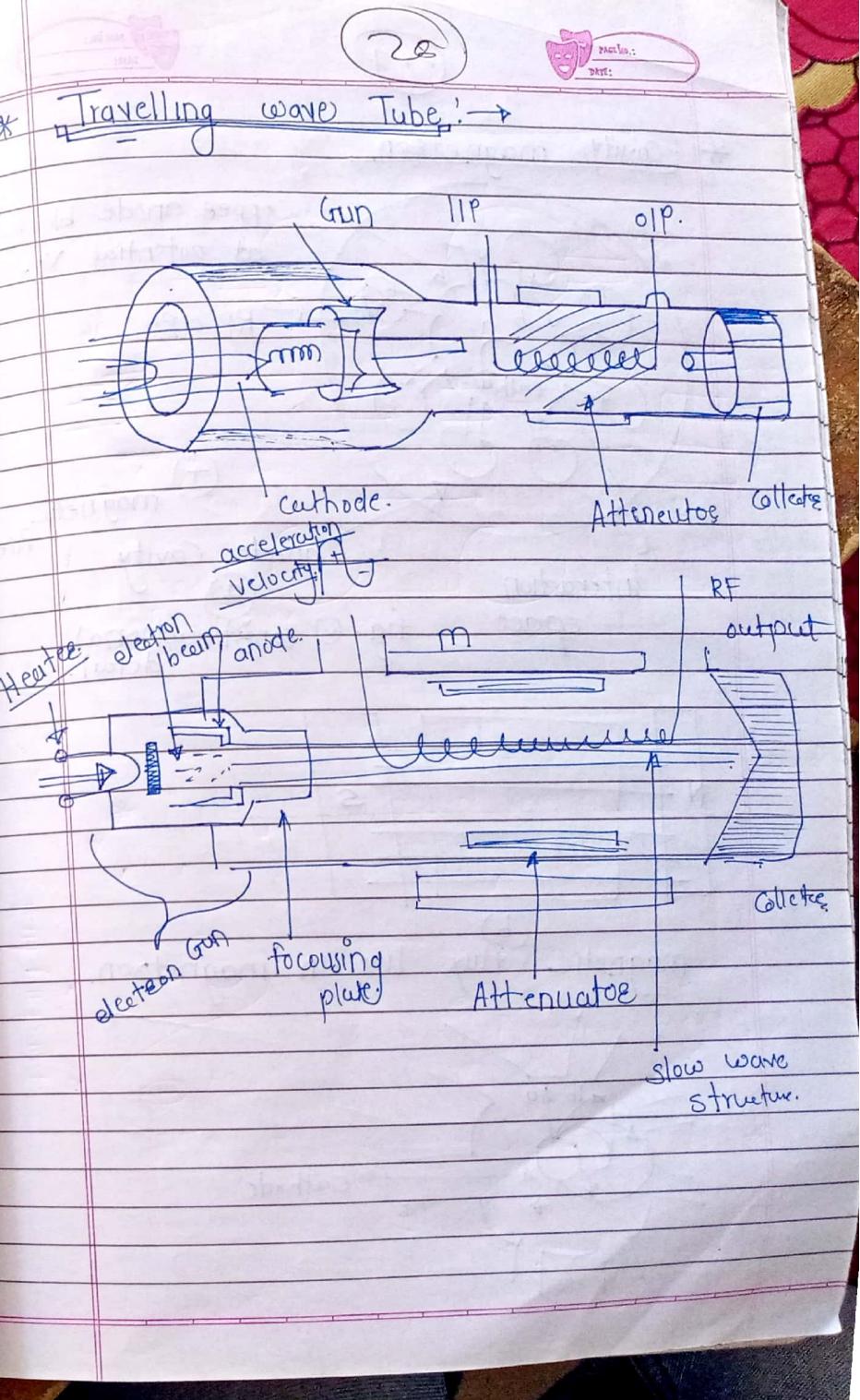
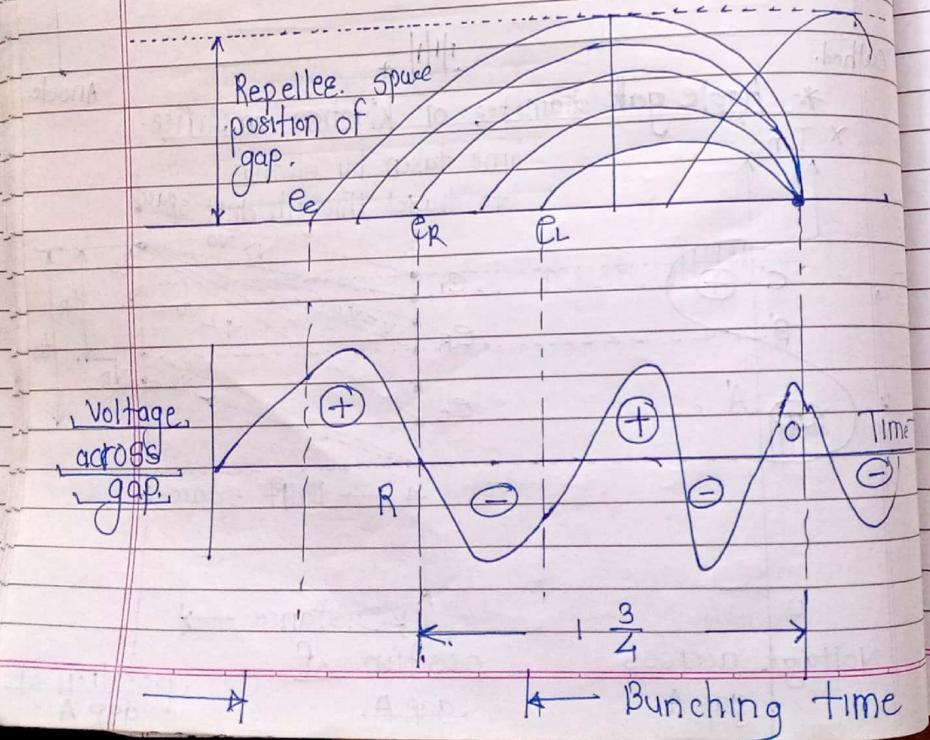
Anode.

* Apple gate diameter of klystron amplifier.





* Constructional details of Reflex klystron



27

* Cavity magnetron.

Copper anode block at potential V_0 .

RF OLP.

Interaction space

fig. @ configurational detail.

(+) magnetic anode Cavity.

$\Phi_v = \frac{2\pi n}{N}$, where $n=0, 1, 2 \pm \frac{(n-1)+N}{2}, \Phi_v = \pi$.

$N = \frac{N}{2}$

(b) magnetic flux line in magnetron.

cathode

(i) $P_{in} = \frac{V_1^2}{R_{sh}}$

$\therefore V_1^2 = P_{in} \times R_{sh}$

$$= 5 \times 10^{-3} \times 30 \times 10^3$$

$$\frac{V_1^2}{V_1} = \frac{150}{0.005}$$

$$V_1 = 12.247 \text{ V}$$

28

magnetic field.

electric field.

(i) A 2 cavity klystron amplifier has the following characteristics: $v_{tg} g_m = 15 \text{ dB}$.
 $I_{LP} = 5 \text{ mA}$,
 $R_{sh} \text{ of LP cavity} = 30 \text{ k}\Omega$
 $R_{sh} \text{ of OLP cavity} = 40 \text{ k}\Omega$
 $R_L \text{ (load impedance)} = 40 \text{ k}\Omega$

Determine :

- (i) The input e.m.s. voltage.
- (ii) The OLP e.m.s. voltage.
- (iii) The power delivered to the load.

0.75

29

$$(ii) A_v = 20 \log \frac{V_2}{V_1} dB.$$

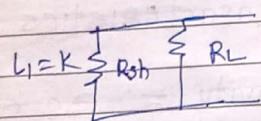
$$15 = 20 \log \frac{V_2}{12.28}$$

$$V_2 = 10^{15/20} \times 12.28$$

$$V_2 = 68.88 V.$$

$$(iii) P_{out} = \frac{V_2}{R_{sh.}}$$

$$P_{out} = \frac{68.88}{20 K} = 237.3 \text{ mW.}$$



Klystron Tube

- ① It is a narrowband device
② It is a wideband device

TWT.A.

③

- ① It is a narrowband device
② It is a wideband device

30

30

parameters

Klystron Tube.

TWT.A.

① devices

Narrowband

wideband.

② velocity modulation

using Cavity Resonator

using Non-resonant slow wave structure.

③ propagating wave

Not propagating

propagating wave.

④ average output power

about 30 dB
500 kWabout 60 dB
up to 10 kW.

⑤ efficiency.

about 20 dB
to 40 %

5 to 20 %

⑥ power gain

about 30 dB

about 60 dB

⑦ application

① Radar & satellite transmission

① RF
② microwave source.

② oscillator.

③ co-array cubic.

⑧

Interaction between electron beam & RF field occurs by across the cavity gap.

④ Continuous interaction between electron beam & RF field take place.

units

solid state microwave

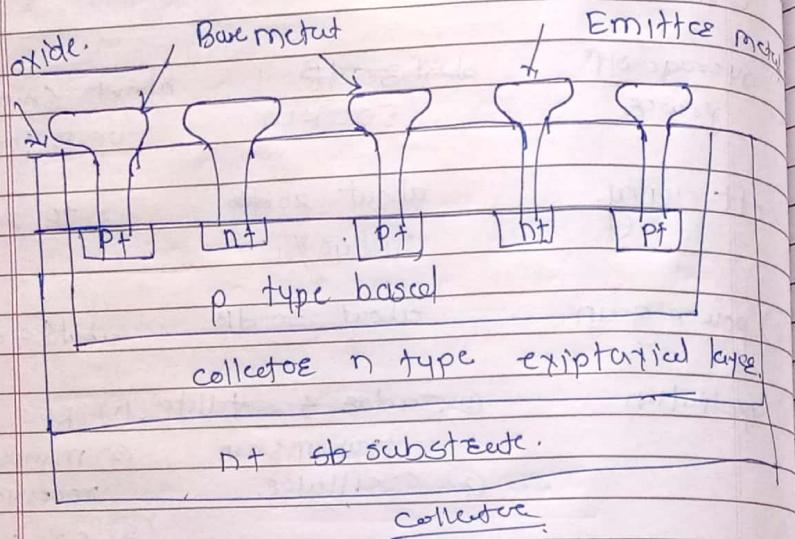
(31)

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Date:

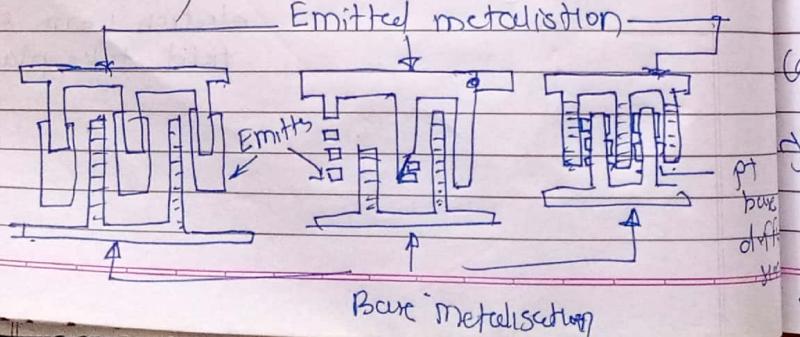
- * Explain the constructional detail and operation of microwave Transistor.

- n-p-n transistors which provide required power at the microwave frequency, 5 GHz f, 5 dB gain.

- It consists double diffused epitaxial device.



- Geometry surface of transistor →
 - (a) Interdigitated surface (C, L, S Band)
 - (b) Overlay
 - (c) matrix (Emitter grid) VHF, UHF region



(32)

Marked:
Date:

① Overlay Structure → - large number of emitters is overlaid through metal.

②

operation

→ In microwave transistors, In C condition E-B-S-C are reversed biased.

→ If microwave signal applied between → E & B is forward biased this junction is positive portion of the signal.

p-n-p transistors holes is p-region diffuse. Then this holes is drift or flow through the collector side. And collector is connected to the negative terminal of V_{cc} so current flow through collector circuit.

Performance parameters

α , B and cut-off frequency

f_{ab} , f_{afe}

$$\text{Where } B = \frac{d}{1-d} \text{ and } f_{afe} = \frac{f_{ab}}{B}$$

f_{ab} = Cut-off frequency
 f_{afe} = Cut-off frequency
 f_{max} = (m. f. of oscillator)

$$= \sqrt{\frac{f_F}{8\pi y_B' C_0}}$$

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Mach no.:
Date:

Performance characteristics: →

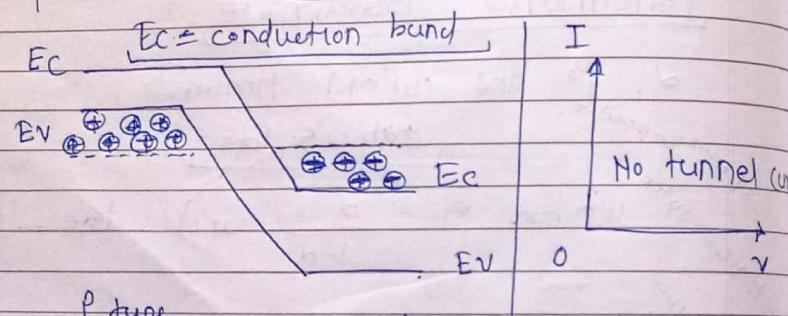
- ① High OIP power at the lower band of microwave region.
- ② High operating power efficiency.
- ③ Large operating bandwidth.
- ④ noise & distortion level is low.

Q(b) Tunnel diode

definition: → The tunnel diode is heavily doped in p-N junction, which is the electric current decreases as the voltage increases.

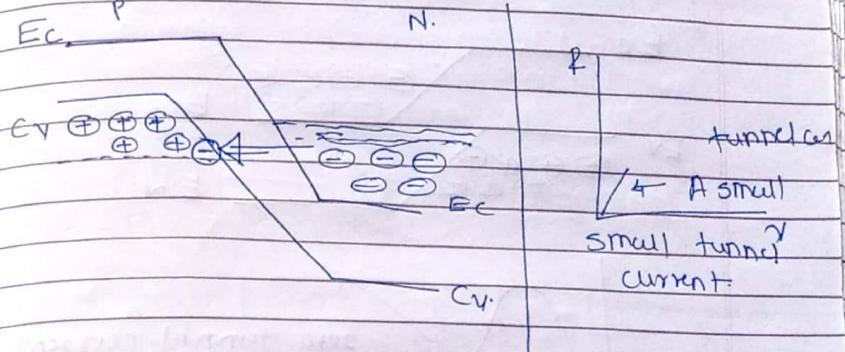
symbol: A  K

operation: $E_V = \text{valence band}$.

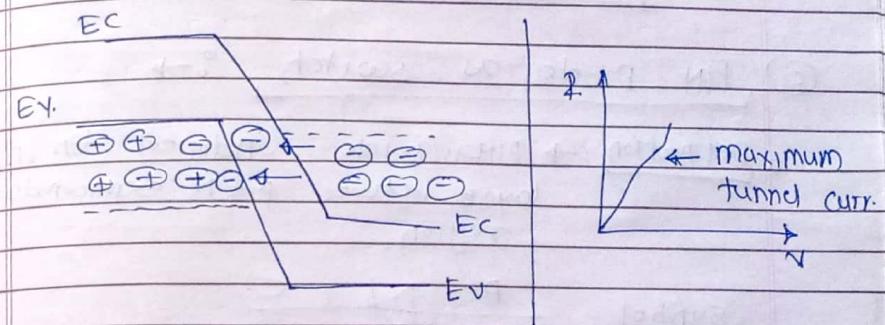


① Unbiased tunnel diode

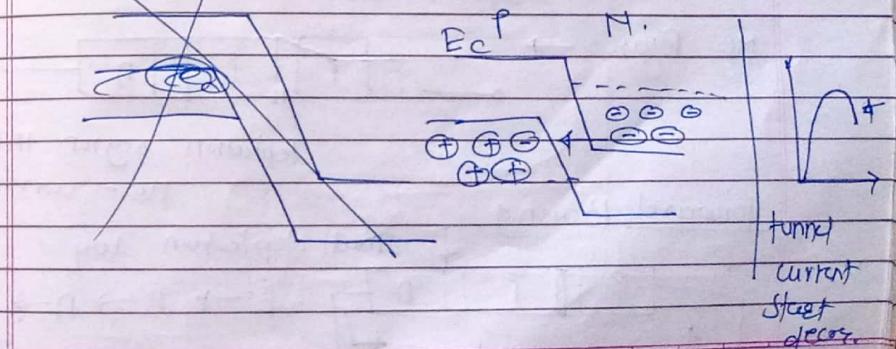
case → 2 Small V_{tg} applied to the tunnel diode.



Case - 3, Applied V_{tg} is slightly increase.



Case - 3, Applied High V_{tg} .

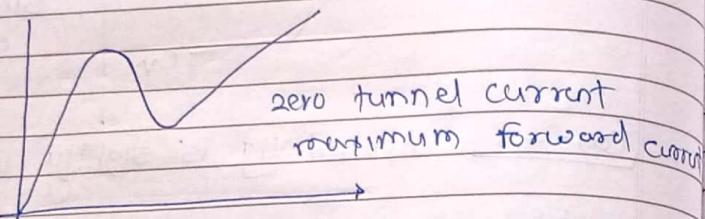


Case - 5 $|V_{tg}| \rightarrow$ largely increase.)

Ec

Ev

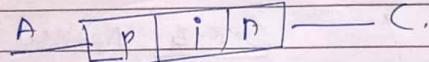
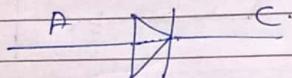
En



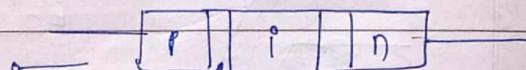
(c) PIN Diode as switch, $\text{O} \rightarrow$

① Definition: \rightarrow PIN is wide- Undoped Intrinsic layer between p & N semiconductor region.

Symbol



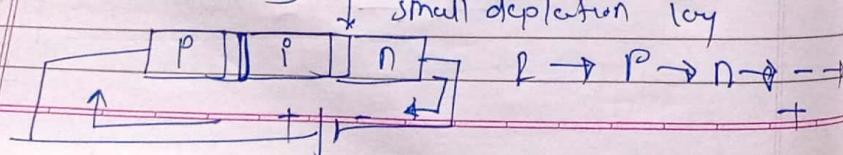
No Bias \rightarrow



depletion region increase
No current flow

forward biasing

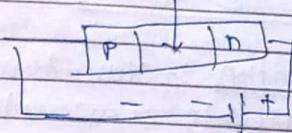
\downarrow small depletion layer



$$N = I R \quad \frac{1}{I} = R_A$$

36
net as. \downarrow ~~current~~
resistor

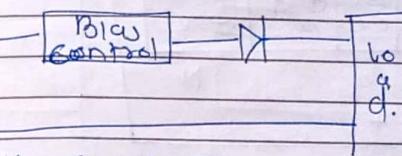
Raised bias,



$$C = \frac{\epsilon_0 A}{d}$$

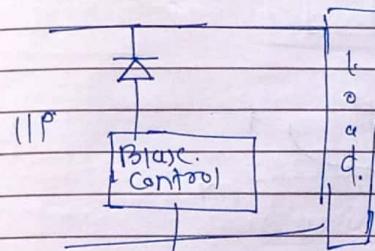
act as variable capacitance.

* PIN Diode as switch.

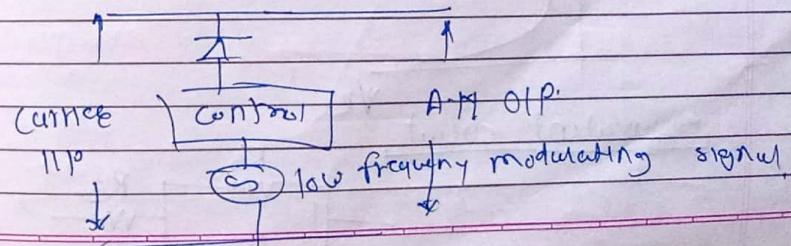


II P.

(f) PIN as series.



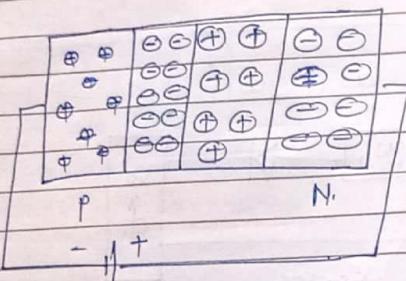
* PIN Diode as an Amplitude modulator



* Varactor diode.

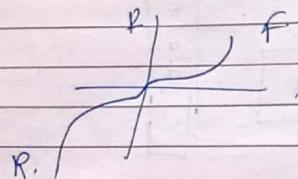
Definition :- Varactor diode is work as variable capacitor when but when it is in a reverse biased that called as varactor diode.

Symbol :-



$$C = \frac{EA}{d}$$

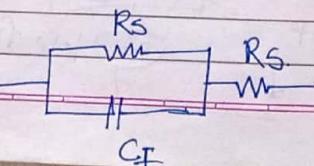
(b) V-I



(c) CP

doping profile.

equivalent circuit



* application :-

- ① Harmonic Generation.
- ② tuning circuit
- ③ Vtg Control oscillator, freq. multipl.
- ④ frequency multipliers.
- ⑤ active filters.
- ⑥ pulse.

what is TED ? (Transferred electron device)

- TED is two terminal device in which has no negative resistance and no junction.
- Negative resistance mean the voltage and current have a 180° phase shift. It generate high power signal.

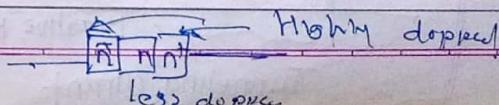
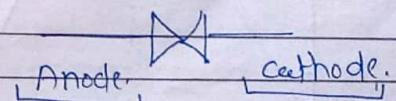
- It produced High power as compare to the MOSFET and BJT power.

- It also called as oscillator.

* Gunn Effect device diode.

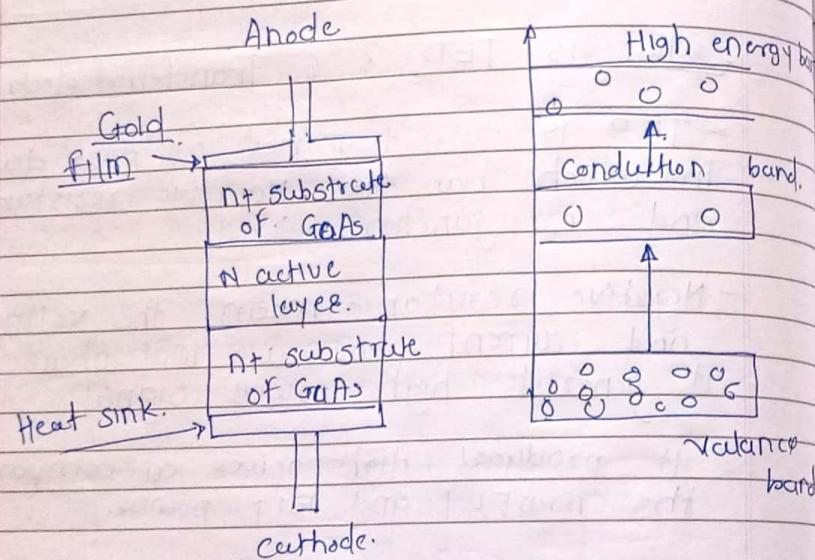
- It also known as TED.

- Symbol →

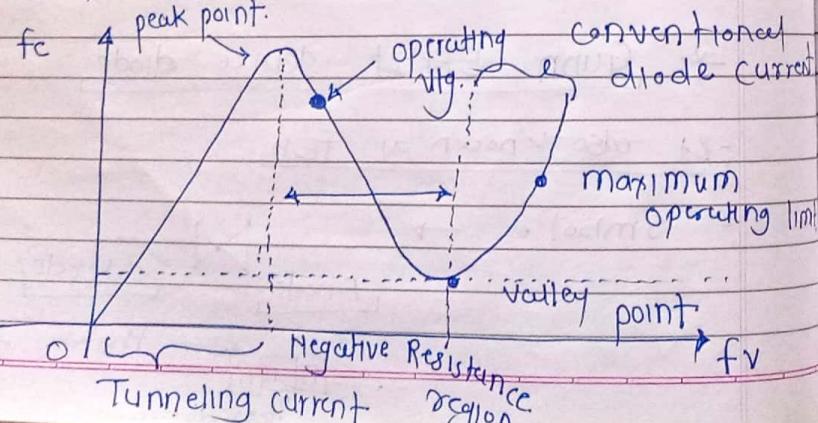


- The Gunn Effect is defined as generation of microwave whenever the voltage applied to the semiconductor device that temperature critical voltage is exceed the onset threshold voltage value.

Construction diagram,



Characteristics of Gunn diodes.



Advantages -

- compact in size.
- less noise.
- & cheaper source.
- operate on large BW & High frequency stability.

Application - RADAR

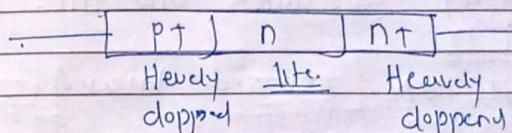
- Radio comm?
- Gunn diode oscillator.
- linear amplifier.

c) Explain TRAPATT diode.

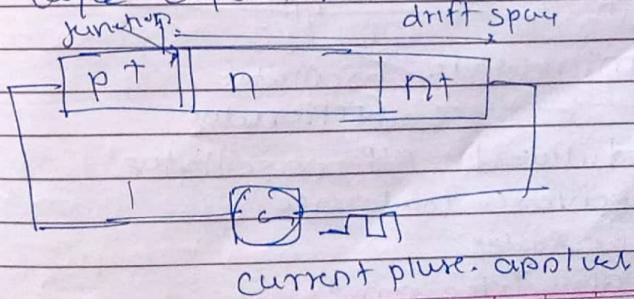
The TRAPATT - Trapped Plasma Avalanche Triggered transist.

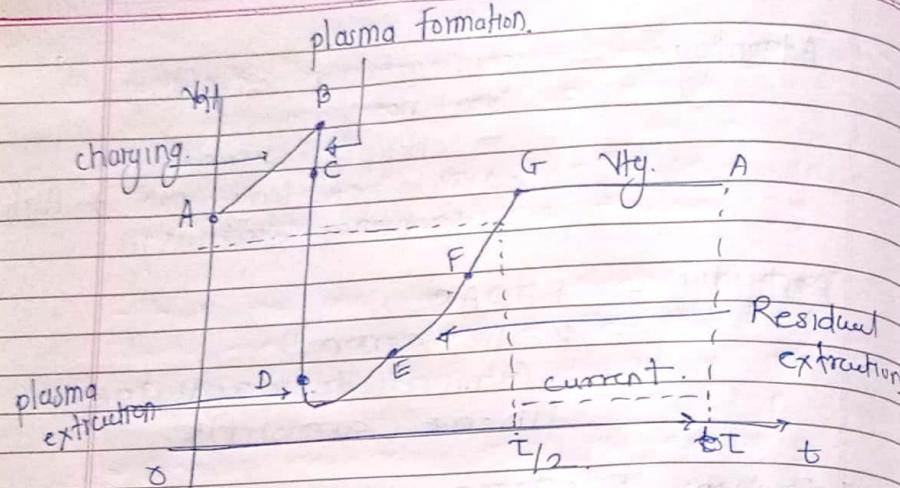
diode.

- It operates efficiently below 10 GHz.



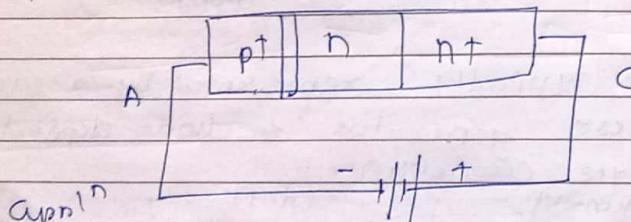
- It is typically represented by a current pulse generator. & diode depletion layer capacitance.



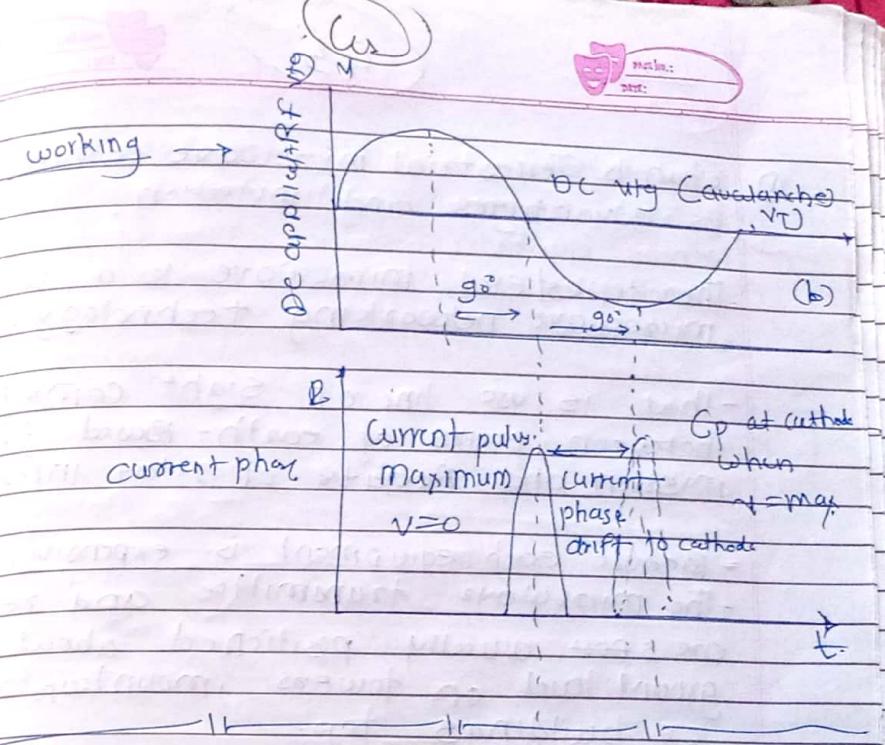


* IMPATT diode! —

- impact ionization avalanche transit time diode
- It is RF semiconductor devices.
- It made by Si, GaAs and InP.
- TIED
- It work on reversed biased

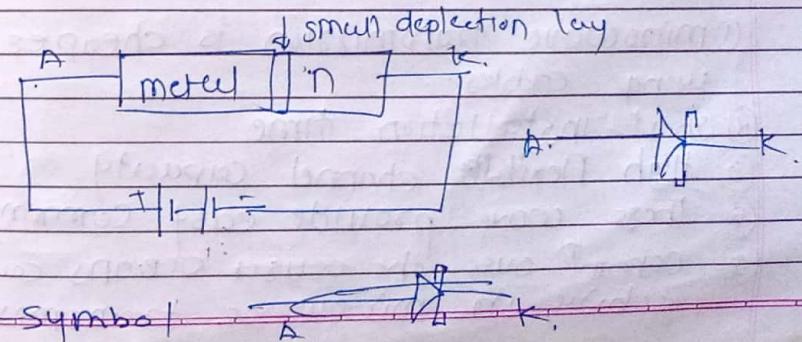


- microwave oscillator
- Generator
- modulated OIP oscillator.
- Receiver load osc.
- Police Radar.
- PCN Telecomm.



SCHOTTKY BARRIER DIODE (SBD)

- It is metal semiconductor devices with low forward V_f drop and very fast switching speed.
- It is used very high frequency and very high switching speed.



Unit - 6

GB

Page No.:
Date:

- ① what is Terrestrial microwave comm sys. its advantages and limitation.

The terrestrial microwave is a wireless microwave networking technology.

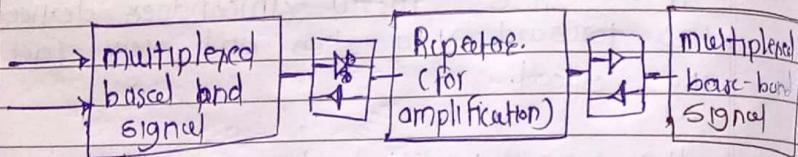
- That is use line of sight comm between pairs of earth-based transmission and receiver of relay information.

- Because each equipment is expensive.

- The microwave transmitter and receiver are most usually positioned about ground level on towers, mountain tops, or buildings top.

→ advantages:-

① MI



→ advantages:-

- ① microwave transmission is cheaper than using cables.
 ② short installation time.
 ③ high flexible channel capacity.
 ④ these come provide easy comm.
 ⑤ comm over the oceans can be achieve in microwave transmission.

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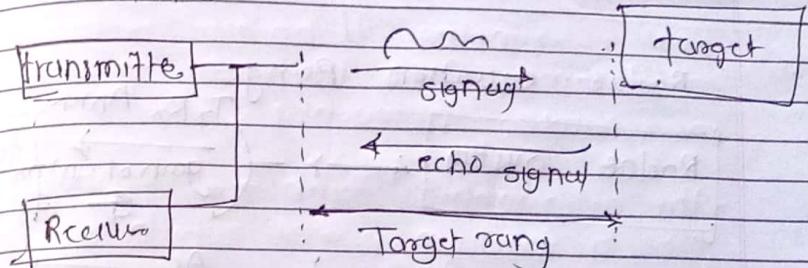
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disadvantages:-

- ① Eavesdropping.
- ② off out of phase signal
- ③ Bandwidth is limited.

(b) block diagram of Radar.

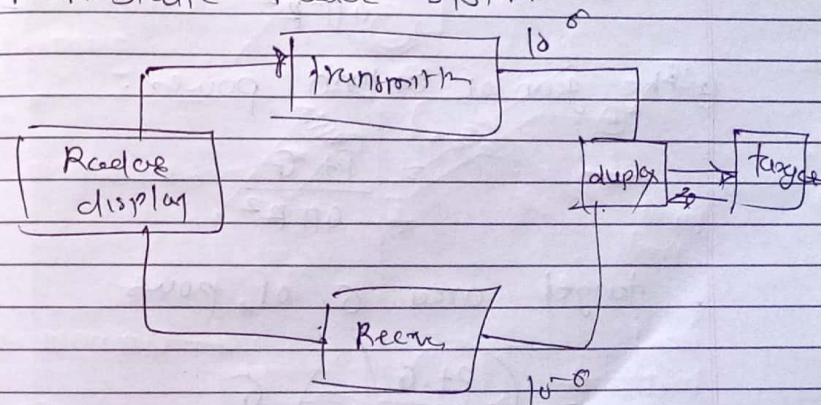
Antenna.



Basic principle of Radar, Bistatic

Radio detection and

monostatic Radar system.



Q1

$$T = \frac{P}{S} \quad S = \frac{P}{T}$$

margin: 2D = SXT

monostatic

- (1) single antenna
- (2) need duplex
- (3) need less space
- (4) complex
- (5) costly

bi-static.

do two antenna

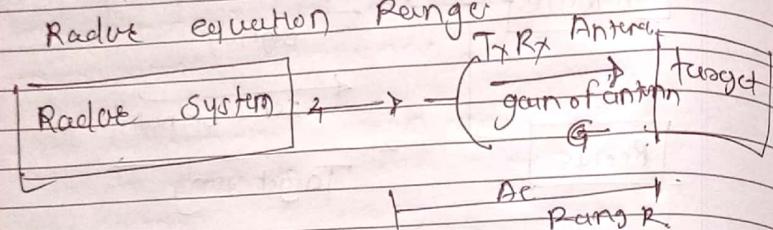
No need duplex

more space.

simple.

low cost system

Radius equation Range



(1) power density by isotropic source

$$= \frac{P_t}{4\pi r^2}$$

(2) the gain of antenna power.

$$= \frac{P_t G}{4\pi r^2}$$

- target area σ of power

$$= \left(\frac{P_t G}{4\pi r^2} \right) \sigma$$

Left

- Repeated power density.

$$= \left(\frac{P_t G G}{4\pi r^2} \right) \times \frac{1}{4\pi r^2} = \frac{P_t G G}{(4\pi r^2)^2}$$

effective area. of antenna A_e , receive power

$$P_r = \frac{P_t G G A_e}{(4\pi r^2)^2}$$

for maximum range R_{max} , $P_r = S_{min}$

$$S_{min} = \frac{P_t G G A_e}{(4\pi r^2)^2 R_{max}^4} \Rightarrow R_{max} = \sqrt{\frac{P_t G G A_e}{(4\pi r^2)^2 S_{min}}}$$

Hence

$$\text{parabolic antenna } \left[G = \frac{4\pi A_e}{\lambda^2} \right]$$

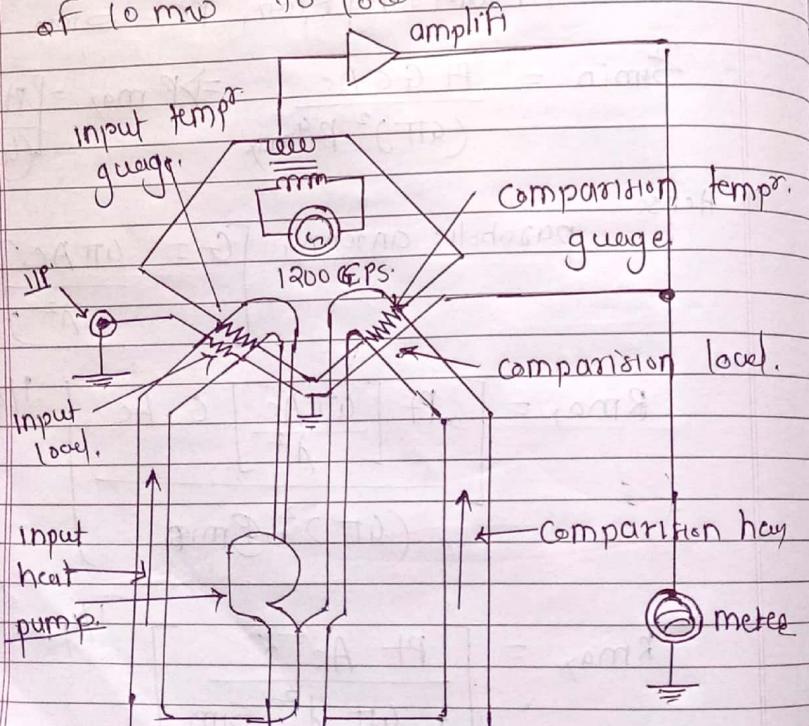
$$R_{max} = \left[\frac{P_t \left[\frac{4\pi A_e}{\lambda^2} \right] G \cdot A_e}{(4\pi)^2 P_{min}} \right]^{1/4}$$

$$R_{max} = \left[\frac{P_t A_e^2 \sigma}{(4\pi)^2 S_{min}} \right]^{1/4}$$

- application :-
- ① military
 - ② A.R.E. traffic controlling
 - ③ ship safety
 - ④ Remote sensing.
 - ⑤ R.F.T.

(c) How calorimetric technique is used for measurement of medium power at microwave frequency.

- The calorimetric technique is measured the a medium power which is range of 10 mW to 10W.



Heat Exchanger.

Self balancing bridge technique.

- unknown IIP microwave power is sensed by the IIP loop.
- when IIP applied to the compensation load R_{comp} it produce heat it transfer to the bridge.
- large amount of power applied to the compensation load Resistor . it is balanced bridge. It measure the the directly in form of IIP microwave power.

(d) medical application such as microwave Diathermy.