Software Requirements Specification for SynthEddy: Simulating Turbulent Flow with Synthetic Eddy

Phil Du (Software) Nikita Holyev (Theory)

 $March\ 21,\ 2024$

Contents

1.1 1.2 1.3	Table of Units	iv		
1.3		iv		
	Abbreviations and Acronyms	V		
1.4	Mathematical Notation	V		
Intr	roduction	1		
2.1	Purpose of Document	1		
2.2		1		
2.3	1 1	1		
2.4	Organization of Document	2		
Ger	neral System Description	2		
3.1		2		
3.2		3		
3.3	System Constraints	3		
Spe	cific System Description	3		
4.1		4		
	•	4		
		5		
		5		
4.2		6		
		6		
		6		
		6		
	•	8		
		10		
		12		
		13		
	4.2.8 Properties of a Correct Solution	13		
Rec	quirements	13		
5.1	Functional Requirements	13		
5.2	•	14		
5.3	Rationale	14		
Like	ely Changes	14		
\mathbf{Unl}	likely Changes	15		
3 Traceability Matrices and Graphs 15				
	1.4 Inti 2.1 2.2 2.3 2.4 Ger 3.1 3.2 3.3 Spe 4.1 4.2 Rec 5.1 5.2 5.3 Like Unl	Introduction 2.1 Purpose of Document . 2.2 Scope of Requirements . 2.3 Characteristics of Intended Reader . 2.4 Organization of Document . General System Description . 3.1 System Context . 3.2 User Characteristics . 3.3 System Constraints . Specific System Description . 4.1.1 Terminology and Definitions . 4.1.2 Physical System Description . 4.1.3 Goal Statements . 4.2 Solution Characteristics Specification . 4.2.1 Types . 4.2.2 Scope Decisions . 4.2.3 Assumptions . 4.2.4 Theoretical Models . 4.2.5 Data Definitions . 4.2.6 Instance Models . 4.2.7 Input Data Constraints . 4.2.8 Properties of a Correct Solution . Requirements . 5.1 Functional Requirements . 5.2 Nonfunctional Requirements .		

9 Development Plan

16

Revision History

Date	Version	Notes
2024-02-01 2024-02-05	1.0 1.1	Intro, problem, assumptions, goals, I/O and requirements Revisions based on presentation feedback. Finished the- oretical models and matrices

1 Reference Material

This section records information for easy reference.

1.1 Table of Units

Throughout this document SI (Système International d'Unités) is employed as the unit system. In addition to the basic units, several derived units are used as described below. For each unit, the symbol is given followed by a description of the unit and the SI name.

symbol	unit	SI
m	length	metre
m/s	velocity	metre per second
\mathbf{S}	time	second

1.2 Table of Symbols

The table that follows summarizes the symbols used in this document along with their units. The choice of symbols was made to be consistent with the heat transfer literature and with existing documentation for solar water heating systems. The symbols are listed in alphabetical order.

symbol	unit	description	
X	m	3D vector of position in the flow field	
t	S	time since the start of the simulation	
u	m/s	3D vector of flow velocity at given point and time	
$\mathbf{u}_{ ext{avg}}$	m/s	3D vector of average flow velocity	
\mathbf{u}'	m/s	3D vector of flow velocity fluctuation (on top of average velocity)	
lpha	m/s	3D vector of eddy intensity	
σ	m	eddy length-scale	
N		total number of eddies	
k		index of each eddy, used as a superscript	
q_{σ}		shape function	
L_x, L_y, L_z	m	x, y, z dimensions of the flow field	

1.3 Abbreviations and Acronyms

symbol	description
A	Assumption
BC	Boundary Condition
CFD	Computational Fluid Dynamics
DD	Data Definition
GD	General Definition
GS	Goal Statement
IC	Initial Condition
IM	Instance Model
LC	Likely Change
PS	Physical System Description
R	Requirement
SRS	Software Requirements Specification
SynthEddy	Synthetic Eddy Generator
TM	Theoretical Model

Please refer to 4.1.1 for more detailed explanation of fluid related abbreviations and acronyms.

1.4 Mathematical Notation

In this document, the following notation is used:

- \bullet Bold font denotes vectors, such as $\mathbf{x}.$
- Superscript k indicates index of eddies, such as \mathbf{x}^k (position of kth eddy).

2 Introduction

When using CFD (Computational Fluid Dynamics) to simulate turbulent flow, it is typical to start with a laminar flow up stream and let it develop into a turbulent flow downstream. However, this is computationally expensive as it requires simulations over a larger region and longer time, before the flow can develop into the desired state.

A potential approach to save computational time is to start with a artificially generated turbulent flow as initial and boundary conditions (IC and BC) for further CFD simulations. Poletto et al. (2013) proposed a method to generate a velocity field of such flow with synthetic eddies, which this software aims to implement.

This project is in collaboration Nikita Holyev, the domain expert in fluid theories. Nikita is a PhD student in Mechanical Engineering at McMaster University, supervised by Dr. Marilyn Lightstone and Dr. Stephen Tullis. He is currently working on the theoretical side of synthetic eddy methods.

If you find yourself with unfamiliar with the these fluid dynamics terminology, please refer to Section 4.1.1 for a brief overview of some background knowledge.

2.1 Purpose of Document

Since the theory behind this software is in a highly specialized field of study, this document helps the software development team to better understand the problem and any related requirements. It also facilitates communication between the software development team and the domain experts to ensure the correctness of implantation.

User of this software can also refer to this document to understand the its capabilities, assumptions and limitations. It also serves as a reference for future maintenance and verification of the software.

2.2 Scope of Requirements

The scope of this software is limited to consider 3D space external flow scenarios only (for now, feasibility of internal flow such as within a pipe will be looked into with the domain expert.). It is also limited 1D flow direction with one inlet and one outlet.

As the first step of this project, the software will generate any velocity field based on user provided eddy profiles, regardless of whether they will lead to a realistic turbulent flow. This may change later as theoretical work progresses which allows the software to ensure realistic eddy profiles.

2.3 Characteristics of Intended Reader

The intended readers of this document are expected to have an undergraduate level understanding of fluid theories (from course such as Junior level Fluid Dynamics or equivalent) and aware of the general workflow when conducting CFD simulation. If not, a brief overview of relevant information needed to understand this document is provided in 4.1.1.

2.4 Organization of Document

The introduction section includes reader characteristics and necessary brief background knowledge needed to understand the scope of this project. The General System Description section (3) provides a high-level view of what the user need to know to utilize this software. Detailed problem description and the theoretical behind the software are presented in Specific System Description (4), followed by Requirements of the software (5). Not all the requirements will be satisfied in the first version of the software. The development will gradually implement features as detailed in Development Plan (9).

3 General System Description

This section provides general information about the system. It identifies the interfaces between the system and its environment, describes the user characteristics and lists the system constraints.

SynthEddy is a software that generates a velocity field for turbulent flow simulations. It can be used standalone or as a external tool for CFD software.

3.1 System Context

The software takes in user provided flow field dimensions, average velocity and eddy profiles and generates a velocity field. The user can then query the software to get the velocity vector at any point of interest in space and time. This query can also be done by CFD software to use the generated velocity field as IC and BC.

Eddy profile include the intensity and length-scale of each eddy, this will be detailed in 4.2.4 and 4.2.5.

• User Responsibilities:

- Provide flow field dimensions and average velocity.
- Provide eddy profiles. For now, the software will not check if the profiles will lead to a realistic turbulent flow, or suggest any profiles.

• SynthEddy Responsibilities:

- Detect data type mismatch, such as a string of characters instead of a floating point number
- (later) Suggest eddy profiles that will lead to a realistic turbulent flow.
- Generate a divergence-free velocity field based on the eddy profiles.
- Return the velocity vector at any point of interest in space and time.

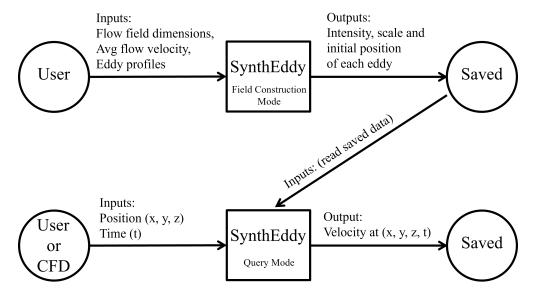


Figure 1: System Context

3.2 User Characteristics

The expected end users of SynthEddy are turbulent flow researchers and engineers looking to leverage SynthEddy in their CFD simulations. They should have a (at least) undergraduate Junior level understanding of Fluid Dynamics and can perform CFD without SynthEddy.

To provide suitable eddy profiles for SynthEddy, the user need to be aware of the synthetic eddy theories. This is detailed later in this document, with more information available in Poletto et al. (2013).

3.3 System Constraints

SynthEddy should run on the same hardware and operating system that is capable of running the CFD software, which typically is a x86-64 based computer running Windows or Linux. It should have a relatively small CPU and memory footprint, as the CFD software would be computationally expensive and should have priority in system resources.

Certain CFD software may require the use of specific programming languages for any addons/extensions/libraries, but this does not mean the main process of SynthEddy is limited to those languages, as an interface in said language can be created to allow the two to communicate.

4 Specific System Description

This section first presents the problem description, which gives a high-level view of the problem to be solved. This is followed by the solution characteristics specification, which

presents the assumptions, theories, definitions and finally the instance models of the synthetic eddy methods used in SynthEddy.

4.1 Problem Description

SynthEddy is intended to alleviate high computational cost/time when simulating turbulent flow in CFD by providing turbulent flow initial conditions and boundary conditions (IC and BC). Since turbulent flow is chaotic and not as easily defined as a laminar flow, in CFD it is typically simulated by starting with a laminar flow and letting it develop over a larger region and longer time before it can develop into the desired state.

4.1.1 Terminology and Definitions

This subsection provides a list of terms that are used in the this document and their meaning, with the purpose of reducing ambiguity and making it easier to correctly understand the requirements and the theories behind the software:

- Fluid Dynamics: The study of matters that can "flow", including gases (like air) and liquids (like water), and how they interact with other objects (such as an aircraft).
- **CFD:** Computational Fluid Dynamics. The use of computers to simulate the flow of fluids and their interaction with other objects. Commonly used in the both research and design of vehicles, fluid pipelines, etc.
- Laminar Flow: Calmly moving flow with no turbulence.
- Turbulent Flow: Chaotic flow with many random fluctuations within.
- Eddy: A swirling, circular movement of a fluid. A turbulent flow can be seen as consisting of many eddies.
- **Inlet**: Where the fluid enters the simulated flow region.
- Outlet: Where the fluid leaves the simulated flow region.
- IC: Initial Condition. The state of the entire flow region at the beginning of the simulation.
- **BC**: Boundary Condition. The state of the flow at the boundaries of the simulation region. In CFD, we need to specify the inlet BC.
- External Flow: Flow that is not confined by any solid physical boundaries. Think of the flow around an aircraft in open air.
- **Internal Flow**: Flow that is confined by solid physical boundaries. Think of the flow inside a pipe.
- 1D Flow: Flow that is only in one general direction, which enters the flow region from one end (inlet) and leaves from the other (outlet).

4.1.2 Physical System Description

The physical system of SynthEddy, namely the entire flow field in question, as shown in Figure 2, includes the following elements:

PS1: 3D Flow Field

PS2: Inlet

PS3: Outlet

PS4: Average Flow Velocity

PS5: Individual Eddies

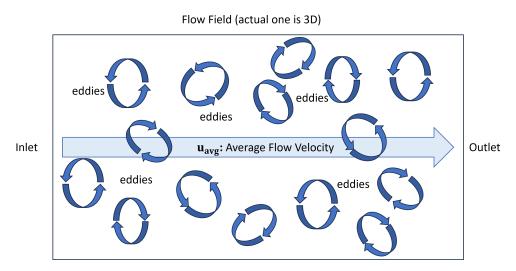


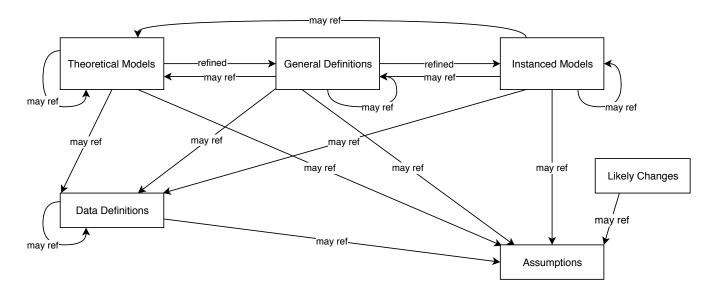
Figure 2: Physical System

4.1.3 Goal Statements

Given the flow field dimensions, average velocity and eddie profile(s), the goal statements are:

GS1: Generate a velocity field that mimics a turbulent flow.

4.2 Solution Characteristics Specification



The instance models that govern SynthEddy are presented in Subsection 4.2.6. The information to understand the meaning of the instance models and their derivation is also presented, so that the instance models can be verified.

4.2.1 Types

• Vector \mathbb{R}^3 : 3D vectors with components in x, y and z directions, as **bold** symbols.

4.2.2 Scope Decisions

- 3D flow region.
- (Possible removal) External flow only.
- (Currently) No consideration of whether the user provided eddy profiles will lead to a realistic turbulent flow.

4.2.3 Assumptions

This section simplifies the original problem and helps in developing the theoretical model by filling in the missing information for the physical system. The numbers given in the square brackets refer to the theoretical model [TM], general definition [GD], data definition [DD], instance model [IM], or likely change [LC], in which the respective assumption is used.

A1: The generated flow field is for CFD simulation in 3D space. [DD2]

A2: 1D flow with constant average velocity, from one inlet to one outlet. [DD2]

A3: (Currently) User can provide appropriate eddy profiles. $[\mathrm{TM1},\,\mathrm{TM2}]$

A4: (Possible removal) The simulation is for external flow. [TM1]

4.2.4 Theoretical Models

This section focuses on the general equations and laws that SynthEddy is based on.

Number	TM1	
Label	Eddy Shape Function	
Equation	$q_{\sigma}(\mathbf{r}^k) = \begin{cases} \sigma^k[1 - \mathbf{r}^k ^2] & \text{if } \mathbf{r}^k < 1\\ 0 & \text{elsewhere} \end{cases}$	
Description	 Shape function describe the distribution of vorticity with respect to distance from the center of an eddy. For distance outside the length-scale of said eddy, a zero vorticity is prescribed. • σ^k is the length-scale (radius) of the kth eddy (m). • r^k is the normalized distance from a given point to the center of the kth eddy, with 0 being the center and 1 being the edge. [DD1] 	
Notes	This is only one of many possible shape functions that can be used. But they should all be in the form with respect to a normalized distance.	
Source	Poletto et al. (2013), DD1	
Ref. By	TM2	

Number	TM2				
Label	Velocity Fluctuation Field				
Equation	$\mathbf{u}'(\mathbf{x}) = rac{1}{\sqrt{N}} \sum_{k=1}^N rac{q_{\sigma}(\mathbf{r}^k(\mathbf{x}))}{ \mathbf{r}^k(\mathbf{x}) ^3} \mathbf{r}^k(\mathbf{x}) imes oldsymbol{lpha}^k$				
Description	The equation gives the fluctuation of velocity (the deviation from the average flow velocity) at point \mathbf{x} in the flow field. It is the normalized sum of the velocity fluctuation due to influence by each eddy at that point.				
	\bullet N is the number of eddies.				
	• \mathbf{r}^k is the normalized distance to the center of the kth eddy [DD1].				
	• α^k is the intensity vector of the kth eddy (m/s) [DD3].				
Notes	According to TM1, at any given position, the fluctuation from most eddies will likely be 0, as any single position is likely outside the boundaries of most eddies in the field.				
Source	Poletto et al. (2013), DD1, DD3				
Ref. By	IM1				

4.2.5 Data Definitions

This section collects and defines all the data needed to build the instance models. The dimension of each quantity is also given.

Number	DD1
Label	Normalized radial vector relative to an eddy center
Symbol	\mathbf{r}^k
SI Units	none
Equation	$\mathbf{r}^k(\mathbf{x}) = rac{\mathbf{x} - \mathbf{x}^k}{\sigma^k}$
Description	The positional vector relative to the center of the eddy, normalized by the length-scale (σ^k) of that eddy.
	• x is the given position (m).
	• \mathbf{x}^k is the center position of the kth eddy (m).
	• σ^k is the length-scale of the kth eddy (m).
Source	Poletto et al. (2013)
Ref. By	TM1, TM2, IM1

Number	DD2			
Label	Center position of an eddy in the flow			
Symbol	$ \mathbf{x}^k $			
SI Units	m			
Equation	$\mathbf{x}^k(t) = \mathbf{x}_0^k + \mathbf{u}_{\mathrm{avg}}t$			
Description	As the flow field has a constant average velocity \mathbf{u}_{avg} , the center position the k th eddy will move with the average velocity over time t .			
	• $\mathbf{x}^{k}(t)$ is the center position of the kth eddy at time t (m).			
	• \mathbf{x}_0^k is the initial center position of the kth eddy (m).			
	• \mathbf{u}_{avg} is the average flow velocity, with zero y and z components (m/s).			
	• t is time since start (s).			
Sources	A1, A2			
Ref. By	DD1, IM1			

Number	DD3
Label	Eddy intensity vector
Symbol	$lpha^k$
SI Units	m/s
Equation	none
Description	A 3D vector that describes both the direction and intensity magnitude of the k th eddy. Fluid flows around such a vector with right hand rule.
Sources	Poletto et al. (2013)
Ref. By	TM2

4.2.6 Instance Models

This section transforms the problem defined in Section 4.1 into one which is expressed in mathematical terms. It uses concrete symbols defined in Section 4.2.5 to replace the abstract symbols in the models identified in Sections 4.2.4.

Number	IM1				
Label	Velocity at any position and time in the flow field				
Input	$\mathbf{u}_{\mathrm{avg}}$: Average flow velocity (m/s)				
	N: Number of eddies				
	\mathbf{x}_0^k : Initial center position of each eddy (m)				
	σ^k : Length-scale of each eddy (m)				
	α^k : Intensity vector of each eddy (m/s) [DD3]				
	x : Any position in the flow field (m)				
	t: Any time since start (s)				
Output	u				
Equation	$\mathbf{u}(\mathbf{x},t) = \mathbf{u}_{\text{avg}} + \mathbf{u}'(\mathbf{x},t)$				
	where				
	$\mathbf{u}'(\mathbf{x},t) = \frac{1}{\sqrt{N}} \sum_{k=1}^{N} \frac{q_{\sigma}(\mathbf{r}^{k}(\mathbf{x},t))}{ \mathbf{r}^{k}(\mathbf{x},t) ^{3}} \mathbf{r}^{k}(\mathbf{x},t) \times \boldsymbol{\alpha}^{k} \text{ [TM2]}$				
	$q_{\sigma}(\mathbf{r}^k(\mathbf{x},t)) = \sigma^k[1- \mathbf{r}^k(\mathbf{x},t) ^2] \text{ if } \mathbf{r}^k(\mathbf{x},t) < 1 \text{ , otherwise } 0 \text{ [TM1]}$				
	$\mathbf{r}^k(\mathbf{x},t) = \frac{\mathbf{x} - \mathbf{x}^k(t)}{\sigma^k} \text{ [DD1]}$				
	$\mathbf{x}^k(t) = \mathbf{x}_0^k + \mathbf{u}_{\mathrm{avg}}t \; [\mathrm{DD2}]$				
Description	The above model gives the velocity vector at any position within the flow field at any given time, by combining the influence from each eddy at such time as they move down the flow field with average velocity.				
	Such influence is calculated by the relative position of that point to the center of each eddy, according to its length-scale, intensity and shape function.				
Sources	Poletto et al. (2013), TM1, TM2, DD1, DD2, DD3				
Ref. By	None				

4.2.7 Input Data Constraints

Table 1 shows the data constraints on the input output variables. The column for physical constraints gives the physical limitations on the range of values that can be taken by the variable. The column for software constraints restricts the range of inputs to reasonable values. The software constraints will be helpful in the design stage for picking suitable algorithms. The constraints are conservative, to give the user of the model the flexibility to experiment with unusual situations. The column of typical values is intended to provide a feel for a common scenario. The uncertainty column provides an estimate of the confidence with which the physical quantities can be measured. This information would be part of the input if one were performing an uncertainty quantification exercise.

Table 1: Input Variables

Var	Physical Constraints	Software Constraints	Typical Value	Uncertainty
σ	$\sigma > 0$	-	0.01 m	0%
\mathbf{x}	$\mathbf{x} \in region(L_x, L_y, L_z)$	-	1 m	0%
t	$t \ge 0$	-	5 s	0%

4.2.8 Properties of a Correct Solution

A correct solution must exhibit a zero-sum velocity fluctuation across the entire field, i.e. velocity field is divergence-free, obeying conservation of mass.

Table 2: Output Variables

Var	Physical Constraints
u	$\int_{field} \mathbf{u}(\mathbf{x}) - \mathbf{u}_{avg} = 0 \text{ (by R3)}$

5 Requirements

5.1 Functional Requirements

R1: Must verify that the queried point is within the flow region [Table 1].

- R2: Can generate a velocity field given any valid eddy profiles input (length-scale and intensity of each eddy) (IM1).
- R3: Generated velocity field must be divergence-free (zero sum of velocity fluctuation, conservation of mass, required by the theory Poletto et al. (2013)) (IM1).
- R4: (Future) Allow CFD software to interface with this software to obtain IC and BC.

5.2 Nonfunctional Requirements

- NFR1: Accuracy (Future) The accuracy of the computed solutions, namely the how realistically the flow field mimics a turbulent flow, should meet the level needed for being used as IC and BC in CFD simulation. Specifically, SynthEddy should be suggest realistic eddy profiles if the user cannot provide one.
- NFR2: **Usability** The input and output of the software should be easily understandable by those familiar with CFD. Later, it should provide easy setup for integration with CFD software.
- NFR3: **Maintainability** The source code should be clear and well-documented. Potential changes to the eddy generation algorithm should be understandable and modifiable by a CFD user if they wish to review the generation method or adapt this software for another theoretical model.
- NFR4: **Portability** SynthEddy should be able to run on any x86-64 based computer with Windows or Linux systems.
- NFR5: **Performance** SynthEddy should require minimal computing an memory resources compared to typical CFD software to avoid impacting CFD simulation performance.

5.3 Rationale

SynthEddy is based on the proposed method by Poletto et al. (2013) to synthetically generate eddies to form a velocity field that mimics turbulent flow. However, if such method can truly lead to a realistic turbulent flow (given proper inputs) suitable for the purpose of CFD is outside the concern of this software. However, NFR3 makes it possible for a CFD user to review and improve the method or adapt it for another theoretical model if they wish so.

6 Likely Changes

- LC1: When theoretical work by Nikita progress, the software will be updated to incorporate the new method to obtain realistic eddy profiles before generating velocity field (A3).
- LC2: Possibility to use this software for internal flow will be looked into. This can be valuable as most turbulent flow scenarios are internal (e.g. within a pipe) (A4).

7 Unlikely Changes

LC3: Support for 2D flow field is unlikely to be add, as most computational cost of 2D is significantly less than 3D. Thus, the need for this software is limited (A1).

8 Traceability Matrices and Graphs

The purpose of the traceability matrices is to provide easy references on what has to be additionally modified if a certain component is changed. Every time a component is changed, the items in the column of that component that are marked with an "X" may have to be modified as well. Table 3 shows the dependencies of theoretical models, general definitions, data definitions, and instance models with each other. Table 4 shows the dependencies of instance models, requirements, and data constraints on each other. Table 5 shows the dependencies of theoretical models, general definitions, data definitions, instance models, and likely changes on the assumptions.

	TM1	TM2	DD1	DD_2	IM1
TM1			X		
TM2	X		X		
DD1				X	
DD2					
IM1		X	X	X	

Table 3: Traceability Matrix Showing the Connections Between Items of Different Sections

	IM1	R1	R2	R??	R3	R4
IM1						
R1						
R2	X					
R??						
R3	X					
R4						

Table 4: Traceability Matrix Showing the Connections Between Requirements and Instance Models

	A1	A2	A3	A4
TM1			X	X
TM2			X	
DD1				
DD2	X	X		
IM1				

Table 5: Traceability Matrix Showing the Connections Between Assumptions and Other Items

9 Development Plan

The first step would be to implement R2 given any user provided eddy profiles, and ensure R3 divergence-free field generation. At this point, the software allows the user to manually query the velocity field at any point within the velocity field (R1).

Later as theoretical work by Nikita progresses, the software will be updated to incorporate the new method to obtain realistic eddy profiles before generating velocity field (R??).

References

Ruggero Poletto, T. Craft, and Alistair Revell. A new divergence free synthetic eddy method for the reproduction of inlet flow conditions for les. *Flow, Turbulence and Combustion*, 91:1–21, 10 2013. doi: 10.1007/s10494-013-9488-2.

Appendix — Reflection

The information in this section will be used to evaluate the team members on the graduate attribute of Lifelong Learning. Please answer the following questions:

- 1. Which of the courses you have taken, or are currently taking, will help your team to be successful with your capstone project.
- 2. What knowledge and skills will the team collectively need to acquire to successfully complete this capstone project? Examples of possible knowledge to acquire include domain specific knowledge from the domain of your application, or software engineering knowledge, mechatronics knowledge or computer science knowledge. Skills may be related to technology, or writing, or presentation, or team management, etc. You should look to identify at least one item for each team member.
- 3. For each of the knowledge areas and skills identified in the previous question, what are at least two approaches to acquiring the knowledge or mastering the skill? Of the identified approaches, which will each team member pursue, and why did they make this choice?