Software Requirements Specification for SynthEddy: Simulating Turbulent Flow with Synthetic Eddy

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September 11, 2024

Contents

Revision History

Date	Version	Notes
2024-02-01	1.0	Intro, problem, assumptions, goals, I/O and requirements
2024-02-05	1.1	Revisions based on presentation feedback. Finished theoretical models and matrices
2024-03-21	1.2	All issued from feedback addressed
2024-04-15	1.3	Update TM, GD and IM equations to more general forms
2024-08-16	1.4	Revised according to Summer 2024 meeting feedbacks

1 Reference Material

This section records information for easy reference.

1.1 Table of Units

Throughout this document SI (Système International d'Unités) is employed as the unit system. In addition to the basic units, several derived units are used as described below. For each unit, the symbol is given followed by a description of the unit and the SI name.

symbol	unit	SI
m	length	metre
m/s	velocity	metre per second
s	time	second

1.2 Table of Symbols

The table that follows summarizes the symbols used in this document along with their units. The choice of symbols was made to be consistent with the heat transfer literature and with existing documentation for solar water heating systems. The symbols are listed in alphabetical order.

symbol	unit	description
$\mathbf{x}$	m	3D vector of position in the flow field
t	s	time since the start of the simulation
$\mathbf{u}$	m/s	3D vector of flow velocity at given point and time
$\overline{\mathbf{u}}$	m/s	3D vector of mean flow velocity
$\mathbf{u}'$	m/s	3D vector of flow velocity fluctuation (on top of mean velocity)
u', v', w'	m/s	velocity fluctuation components in x, y, z directions
$\boldsymbol{\alpha}$	m/s	3D vector of eddy intensity
σ	m	eddy length-scale
N		total number of eddies
k		index of each eddy, used as a superscript
q_σ		shape function
L_x, L_y, L_z	m	x, y, z dimensions of the flow field

1.3 Abbreviations and Acronyms

symbol	description
A	Assumption
BC	Boundary Condition
CFD	Computational Fluid Dynamics
DD	Data Definition
GD	General Definition
GS	Goal Statement
IC	Initial Condition
IM	Instance Model
LC	Likely Change
PS	Physical System Description
R	Requirement
SRS	Software Requirements Specification
SynthEddy	Synthetic Eddy Generator
TM	Theoretical Model

Please refer to 4.1.1 for more detailed explanation of fluid related abbreviations and acronyms.

1.4 Mathematical Notation

In this document, the following notation is used:

- Bold font denotes vectors, such as $\mathbf{x}$.
- Superscript k indicates index of eddies, such as $\mathbf{x}^k$ (position of kth eddy).
- $|\ |$ denotes the modulus (magnitude) of a vector, such as $|\mathbf{r}^k|$.

2 Introduction

When using CFD (Computational Fluid Dynamics) to simulate turbulent flow, it is typical to start with a laminar flow upstream and let it develop into a turbulent flow downstream. For example, in a gas turbine simulation, it may be necessary to start with a clean laminar flow at the first turbine stage even if the interest is on a later stage that receives turbulent flow. This is computationally expensive as it requires simulations over a larger region and longer time, before the flow can develop into the desired state.

A potential approach to save computational time is to start with an artificially generated turbulent flow as Initial and Boundary Conditions (IC and BC) for further CFD simulations. Poletto et al. (2013) proposed a method to generate a velocity field of such flow with synthetic eddies, which this software, named SynthEddy, aims to implement.

This project is in collaboration Nikita Holyev, the domain expert in fluid theories. Nikita is a PhD student in Mechanical Engineering at McMaster University. He is currently working on the theoretical side of synthetic eddy methods, supervised by Dr. Marilyn Lightstone and Dr. Stephen Tullis.

If you find yourself with unfamiliar with the these fluid dynamics terminology, please refer to Section 4.1.1 for a brief overview of some background knowledge.

2.1 Purpose of Document

Since the theory behind this software is in a highly specialized field of study, this document helps the software development team to better understand the problem and any related requirements. It also facilitates communication between the software development team and the domain experts to ensure the correctness of implementation.

Users of this software can also refer to this document to understand its capabilities, assumptions and limitations. This document also serves as a reference for future maintenance and verification of the software.

2.2 Scope of Requirements

The scope of this software is limited to considering 3D space external flow scenarios only, although it is capable of modeling non-uniform mean flow velocity profile that can mimic some aspect of internal flow. It is also limited to one inlet and one outlet.

As the first step of this project, the software will generate any velocity field based on user provided eddy profiles, regardless of whether they will lead to a realistic turbulent flow. This may change later, as theoretical work progresses allowing the software to provide realistic eddy profiles.

2.3 Characteristics of Intended Reader

The intended readers of this document are expected to have an undergraduate level understanding of fluid dynamics (from course such as Junior level Fluid Dynamics or equivalent) and aware of the general workflow when conducting CFD simulation. If not, a brief overview of relevant information needed to understand this document is provided in Section 4.1.1.

2.4 Organization of Document

The introduction section includes reader characteristics and necessary brief background knowledge needed to understand the scope of this project. The General System Description section (Section 3) provides a high-level view of what the user need to know to utilize this software. Detailed problem description and the theoretical behind the software are presented in Specific System Description (Section 4), followed by Requirements of the software (Section 5). Not all the requirements will be satisfied in the first version of the software. The development will gradually implement features as detailed in Development Plan (Section 9).

3 General System Description

This section provides general information about the system. It identifies the interfaces between the system and its environment, describes the user characteristics and lists the system constraints.

SynthEddy generates a velocity field for turbulent flow simulations. It can be used standalone or as an external tool for CFD software.

3.1 System Context

As illustrated by Figure 1, the software takes in user provided flow field dimensions, mean velocity and eddy profiles and generates a velocity field. The user can then query the software to get the velocity vector at any point of interest in space and time. This query can also be done by CFD software to use the generated velocity field as IC and BC.

The eddy profile include the intensity and length-scale of each eddy. This will be detailed in Section 4.2.4 and 4.2.6.

- User Responsibilities:
  - Provide flow field dimensions and mean velocity.
  - Provide eddy profiles that include density (number of eddies per unit volume), intensity and length-scale of each type of eddy in the field.
- SynthEddy Responsibilities:
  - Detect data type mismatch, such as a string of characters instead of a floating point number
  - (later) Suggest eddy profiles that will lead to a realistic turbulent flow.
  - Generate a divergence-free velocity field based on the eddy profiles.
  - Return the velocity vector at any point of interest in space and time.

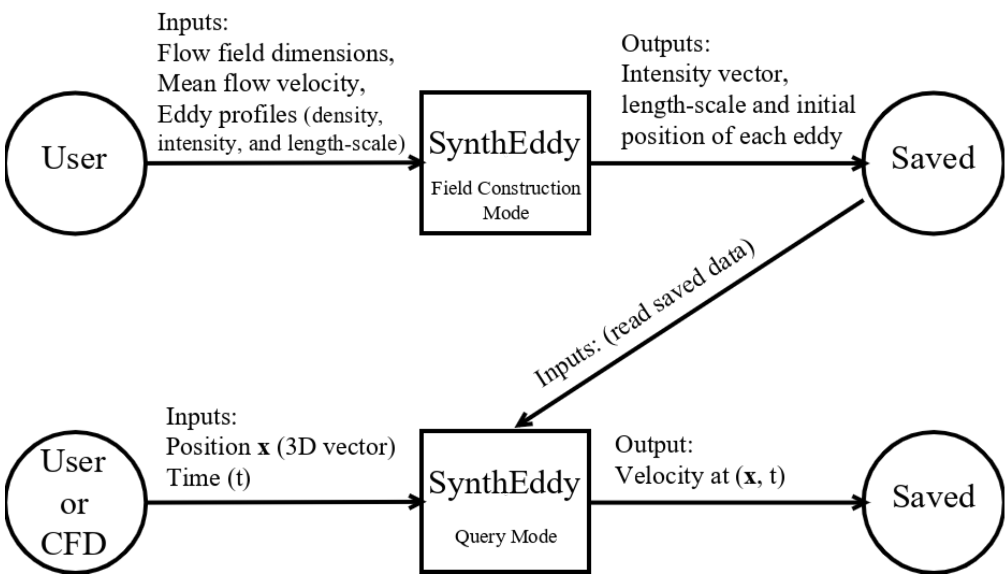

Figure 1: System Context

3.2 User Characteristics

The expected end users of SynthEddy are turbulent flow researchers and engineers looking to leverage SynthEddy in their CFD simulations. They should have a (at least) undergraduate Junior level understanding of Fluid Dynamics and can perform CFD without SynthEddy.

To provide suitable eddy profiles for SynthEddy, the user needs to be aware of the synthetic eddy theories. This is detailed later in this document, with more information available in Poletto et al. (2013).

3.3 System Constraints

According to the typical use case provided by the domain expert (1000^3 mesh grid points or more), memory usage is a concern. Current generation desktop platforms, such as Intel 14th generation CPUs support up to 192 GB of RAM (2023), with usual desktops computers having 16 to 64 GB. Research computing clusters, such as those provided by Compute Canada, typically allows hundreds of GB to a few TB of RAM per node (2024).

Memory saving considerations should be taken, so that small scale test runs can be performed on a typical desktop computer by a developer or researcher, while full scale "typical use case" runs are possible on a computing cluster.

4 Specific System Description

This section first presents the problem description, which gives a high-level view of the problem to be solved. This is followed by the solution characteristics specification, which presents the assumptions, theories, definitions and finally the instance models of the synthetic eddy methods used in SynthEddy.

4.1 Problem Description

SynthEddy is intended to alleviate high computational cost/time when simulating turbulent flow in CFD by providing turbulent flow initial conditions and boundary conditions (IC and BC). Since turbulent flow is chaotic and not as easily defined as a laminar flow, in CFD it is typically simulated by starting with a laminar flow and letting it develop over a larger region and longer time before it can develop into the desired state.

4.1.1 Terminology and Definitions

This subsection provides a list of terms that are used in this document and their meaning, with the purpose of reducing ambiguity and making it easier to correctly understand the requirements and the theories behind the software.

- **Fluid Dynamics:** The study of matters that can "flow", including gases (like air) and liquids (like water), and how they interact with other objects (such as an aircraft).
- **CFD:** Computational Fluid Dynamics. The use of computers to simulate the flow of fluids and their interaction with other objects. Commonly used in the both research and design of vehicles, fluid pipelines, etc.
- **Laminar Flow:** Calmly moving flow with no turbulence. The fluid acts as layers that slide over one another.
- **Turbulent Flow:** Chaotic flow with many random fluctuations within.
- **Eddy:** A swirling, circular movement of a fluid. A turbulent flow can be seen as consisting of many eddies.
- **Inlet**: Where the fluid enters the simulated flow field.
- **Outlet**: Where the fluid leaves the simulated flow field.
- **IC**: Initial Condition. The state of the entire flow field at the beginning of the simulation.
- **BC**: Boundary Condition. The state of the flow at the boundaries of the simulation region. In CFD, we need to specify the inlet BC.
- **External Flow**: Flow that is not confined by any solid physical boundaries. Think of the flow around an aircraft in open air.
- **Internal Flow**: Flow that is confined by solid physical boundaries. Think of the flow inside a pipe.

- **1D Flow**: Flow that is only in one general direction, which enters the flow field from one end (inlet) and leaves from the other (outlet).

4.1.2 Physical System Description

The physical system of SynthEddy, namely the entire flow field in question, as shown in Figure 2, includes the following elements:

PS1: 3D Flow Field

PS2: Inlet

PS3: Outlet

PS4: Mean Flow Velocity

PS5: Individual Eddies

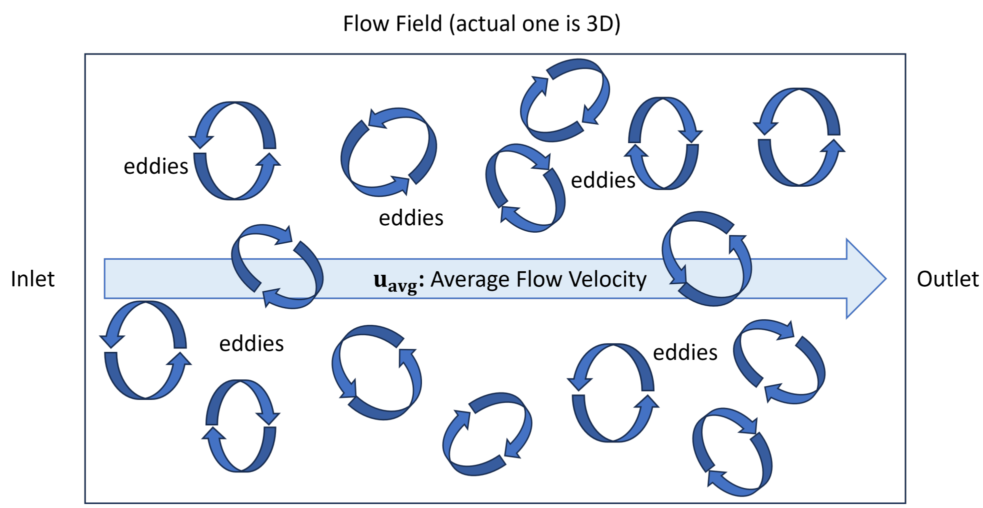

Figure 2: Physical System

4.1.3 Goal Statements

Given the flow field dimensions, mean velocity and eddy profile(s), the goal statements are:

GS1: Generate a velocity field over time that mimics a turbulent flow.

4.2 Solution Characteristics Specification

The instance models that govern SynthEddy are presented in Subsection 4.2.7. The information to understand the meaning of the instance models and their derivation is also presented, so that the instance models can be verified.

4.2.1 Types

- Vector $\mathbb{R}^3$: 3D vectors with components in x, y and z directions, as **bold** symbols.

4.2.2 Scope Decisions

- 3D rectangular box flow field.
- One inlet and one outlet.
- No wall boundaries.
- User provides eddy profiles. No consideration of whether such profiles will lead to realistic turbulent flow of the entire field.
- Spherical eddies.
- Homogeneous turbulence (same eddy profile throughout the field).
- Isotropic turbulence (eddies have no directional preference).

4.2.3 Assumptions

This section simplifies the original problem and helps in developing the theoretical model by filling in the missing information for the physical system. The numbers given in the square brackets refer to the theoretical model [TM], general definition [GD], data definition [DD], instance model [IM], or likely change [LC], in which the respective assumption is used.

A1: User can provide appropriate eddy profiles.

A2: At any location in the field, mean velocity is along the x-axis, from inlet to outlet (or zero). No mean velocity in y or z directions.

A3: Eddy centers always move with such prescribed mean velocity. [DD3]

A4: Eddies do not interact with each other.

4.2.4 Theoretical Models

This section focuses on the general equations and laws that SynthEddy is based on.

Number	TM1
Label	**Eddy Shape Function**
Equation	$q_\sigma(d^k(\mathbf{x})) = \begin{cases} \sigma^k(1 - \lvert\mathbf{r}^k(\mathbf{x})\rvert^2) & \text{if } d^k < 1 \\ 0 & \text{elsewhere} \end{cases}$ $q_\sigma(d^k(\mathbf{x})) = \begin{cases} 3.6276e^{-\frac{\pi}{2}(d^k)^2} & \text{if } d^k < 2 \\ 0 & \text{elsewhere} \end{cases}$
Description	Shape function (q_σ) describe the distribution of vorticity (strength of circular flow at that location) with respect to distance from the center of an eddy. These functions include a cut-off distance expressed in terms of multiples of length-scale (1 and 2 above). For locations outside such distance, the function value is set to 0, meaning the eddy has negligible influence to that location. • σ^k is the length-scale (similar to radius) of the kth eddy (m). • $\mathbf{r}^k$ is the normalized vector from a given point ($\mathbf{x}$) to the center of the kth eddy. [DD1] • d^k is the normalized distance from a given point ($\mathbf{x}$) to the center of the kth eddy, with 0 being the center and 1 being at σ^k. [DD1]
Notes	This are only two examples (quadratic and Gaussian) of many possible shape functions that can be used. But they should all be in the form with respect to a normalized distance.
Source	1st equation: Poletto et al. (2013), 2nd equation: Nikita Holyev
Uses	DD1, DD2
Ref. By	TM2, GD1, IM1

Number	TM2
Label	**Velocity Fluctuation Field**
Equation	$\mathbf{u}'(\mathbf{x}) = \frac{1}{\sqrt{N}} \sum_{k=1}^{N} q_\sigma(d^k(\mathbf{x}))\mathbf{r}^k(\mathbf{x}) \times \boldsymbol{\alpha}^k$
Description	The equation gives the fluctuation of velocity (the deviation from the mean flow velocity) at point $\mathbf{x}$ in the flow field. It is the normalized sum of the velocity fluctuation by each eddy, with shape function q_σ [TM1]. • N is the number of eddies. • $\mathbf{r}^k$ is the normalized distance to the center of the kth eddy [DD1]. • $\boldsymbol{\alpha}^k$ is the intensity vector of the kth eddy (m/s) [DD4].
Notes	According to TM1, at any single position, the fluctuation from most eddies will likely be 0, due to outside the boundaries of most eddies in the field.
Source	Poletto et al. (2013)
Uses	TM1, DD1, DD4
Ref. By	GD1

4.2.5 General Definitions

This section collects the laws and equations that will be used in building the instance models.

Number	GD1
Label	**Velocity fluctuation without normalizing energy**
Equation	$\mathbf{u}'(\mathbf{x}) = \sum_{k=1}^{N} q_\sigma(d^k(\mathbf{x}))\mathbf{r}^k(\mathbf{x}) \times \boldsymbol{\alpha}^k$
Description	The equation in TM2 uses $\frac{1}{\sqrt{N}}$ to keep the total turbulent kinetic energy of the field constant when the number of eddies (N) changes. Holyev proposes the removal of this term, so that energy is simply the result of N and $\boldsymbol{\alpha}$. • N is the number of eddies. • $\mathbf{r}^k$ is the normalized distance to the center of the kth eddy [DD1]. • $\boldsymbol{\alpha}^k$ is the intensity vector of the kth eddy (m/s) [DD4].
Notes	In Poletto et al. (2013), more eddies means each eddy is weaker. Holyev removes such relation to find the optimal combination to fit a realistic turbulent flow, which SynthEddy will incorporate in the future.
Source	Nikita Holyev
Uses	TM1, TM2, DD1, DD4
Ref. By	DD5, IM1

4.2.6 Data Definitions

This section collects and defines all the data needed to build the instance models. The dimension of each quantity is also given.

Number	DD1
Label	**Normalized radial vector relative to an eddy center**
Symbol	$\mathbf{r}^k$
SI Units	none
Equation	$\mathbf{r}^k(\mathbf{x}) = \frac{\mathbf{x}-\mathbf{x}^k}{\sigma^k}$
Description	The positional vector relative to the center of the eddy, normalized by the length-scale (σ^k) of that eddy. • $\mathbf{x}$ is the given position (m). • $\mathbf{x}^k$ is the center position of the kth eddy (m) [DD3]. • σ^k is the length-scale of the kth eddy (m).
Source	Poletto et al. (2013)
Uses	DD3
Ref. By	TM1, TM2, GD1, DD2, IM1

Number	DD2
Label	**Normalized distance relative to an eddy center**
Symbol	d^k
SI Units	none
Equation	$d^k(\mathbf{x}) = \lvert \mathbf{r}^k(\mathbf{x}) \rvert$
Description	The positional vector relative to the center of the eddy, normalized by the length-scale (σ^k) of that eddy. • $\mathbf{x}$ is the given position (m). • $\mathbf{r}^k$ is the normalized radial vector relative to the center of kth eddy [DD1].
Source	Poletto et al. (2013)
Uses	DD1
Ref. By	TM1, IM1

Number	DD3
Label	**Center position of an eddy in the flow**
Symbol	$\mathbf{x}^k$
SI Units	m
Equation	$\mathbf{x}^k(t) = \mathbf{x}_0^k + \overline{\mathbf{u}}t$
Description	As the flow field has a constant mean velocity $\overline{\mathbf{u}}$, the center position of the kth eddy will move with the mean velocity over time t. • $\mathbf{x}^k(t)$ is the center position of the kth eddy at time t (m). • $\mathbf{x}_0^k$ is the initial center position of the kth eddy (m). • $\overline{\mathbf{u}}$ is the mean flow velocity, with zero y and z components (m/s). • t is time since start (s).
Uses	A2
Ref. By	DD1, IM1

Number	DD4
Label	**Eddy intensity vector**
Symbol	$\boldsymbol{\alpha}^{\boldsymbol{k}}$
SI Units	m/s
Equation	none
Description	A 3D vector that describes both the direction and intensity magnitude of the kth eddy. Fluid flows around this vector such that when looking against the vector (vector pointing at viewer), the flow is clockwise. The greater the vector magnitude, the stronger the flow.
Sources	Poletto et al. (2013)
Ref. By	TM2, GD1, IM1

Number	DD5
Label	**Velocity fluctuation components**
Symbol	u', v', w'
SI Units	m/s
Equation	$u' = \mathbf{u}'_x$, $v' = \mathbf{u}'_y$, $w' = \mathbf{u}'_z$
Description	The x, y and z components of the velocity fluctuation vector $\mathbf{u}'$ [GD1]. These are not used during the field calculation, but derived from the end result $\mathbf{u}$ for validation purposes [IM1].
Uses	GD1, IM1
Ref. By	Section 4.2.9

4.2.7 Instance Models

This section transforms the problem defined in Section 4.1 into one which is expressed in mathematical terms. It uses concrete symbols defined in Section 4.2.6 to replace the abstract symbols in the models identified in Sections 4.2.4 and 4.2.5.

Number	IM1
Label	**Velocity at any position and time in the flow field**
Input	$\overline{\mathbf{u}}$: Mean flow velocity, with zero y and z components (m/s) N: Number of eddies $\mathbf{x}_0^k$: Initial center position of each eddy (m) σ^k: Length-scale of each eddy (m) $\boldsymbol{\alpha}^k$: Intensity vector of each eddy (m/s) [DD4] $\mathbf{x}$: Any position in the flow field (m) t: Any time since start (s)
Output	$\mathbf{u}$, the velocity at any position and time
Equation	$\mathbf{u}(\mathbf{x}, t) = \overline{\mathbf{u}} + \mathbf{u}'(\mathbf{x}, t)$ where $\mathbf{u}'(\mathbf{x}, t) = \sum_{k=1}^{N} q_\sigma(d^k(\mathbf{x}, t))\mathbf{r}^k(\mathbf{x}, t) \times \boldsymbol{\alpha}^k$ from [GD1] q_σ is any satisfying shape function as per [TM1] $\mathbf{r}^k(\mathbf{x}, t) = \frac{\mathbf{x} - \mathbf{x}^k(t)}{\sigma^k}$ from [DD1] $d^k(\mathbf{x}, t) = \lvert\mathbf{r}^k(\mathbf{x}, t)\rvert$ from [DD2] $\mathbf{x}^k(t) = \mathbf{x}_0^k + \overline{\mathbf{u}}t$ from [DD3]
Description	The above model gives the velocity vector at any position within the flow field at any given time, by combining the influence from each eddy at such time as they move down the flow field with mean velocity. Such influence is calculated by the relative position of that point to the center of each eddy, according to its length-scale, intensity and shape function.
Uses	GD1, TM1, DD1, DD2, DD3, DD4
Ref. By	DD5

4.2.8 Input Data Constraints

Table 1 shows the data constraints on the input output variables. The column for physical constraints gives the physical limitations on the range of values that can be taken by the variable. The column for software constraints restricts the range of inputs to reasonable values. The software constraints will be helpful in the design stage for picking suitable algorithms. The constraints are conservative, to give the user of the model the flexibility to experiment with unusual situations. The column of typical values is intended to provide a feel for a common scenario. The uncertainty column provides an estimate of the confidence with which the physical quantities can be measured. This information would be part of the input if one were performing an uncertainty quantification exercise.

Table 1: Input Variables

Var	Physical Constraints	Software Constraints	Typical Value	Uncertainty
σ	$\sigma > 0$	-	0.01 m	0%
$\mathbf{x}$	$\mathbf{x} \in field(L_x, L_y, L_z)$	-	1 m	0%
t	$t \geq 0$	-	5 s	0%

4.2.9 Properties of a Correct Solution

A correct solution must be a divergence-free velocity field, obeying conservation of mass. Products of velocity fluctuations components u', v' and w' (derived from output $\mathbf{u}$), when averaged across the entire field, should satisfy the current assumption of homogeneous isotropic turbulence.

Table 2: Output Variables

Var	Physical Constraints
$\mathbf{u}$	$\text{div}(\mathbf{u}\|_{\text{field}}) = 0$
u', v', w'	$\overline{u'u'} = \overline{v'v'} = \overline{w'w'}$
u', v', w'	$\overline{u'v'} = \overline{v'w'} = \overline{w'u'} = 0$

5 Requirements

5.1 Functional Requirements

R1: Must verify that the queried point is within the flow field [Table 1].

R2: Can generate a velocity field given any valid eddy profiles input, which include density (number of eddies per unit volume), intensity magnitude and length-scale of each type of eddy in the field (IM1).

5.2 Nonfunctional Requirements

NFR1: **Accuracy** The accuracy of the computed solutions, namely the how realistically the flow field mimics a turbulent flow, should meet the level needed for being used as IC and BC in CFD simulation. Given the current assumptions, the result should exhibit characteristics of homogeneous isotropic turbulence (below certain threshold), as detailed in Section 4.2.9.

NFR2: **Usability** The input and output of the software should be in terms understandable by those familiar with CFD. Later, it should provide easy setup for integration with CFD software.

NFR3: **Maintainability** The source code should be clear and well-documented. Potential changes to the eddy generation algorithm should be understandable and modifiable by a CFD user if they wish to review the generation method or adapt this software for another theoretical model.

NFR4: **Portability** SynthEddy should be able to run on any x86-64 based computer with Windows or Linux systems.

NFR5: **Performance** SynthEddy should require less memory for typical use cases, as detailed in Section 3.3 System Constraints.

5.3 Rationale

SynthEddy is based on the proposed method by Poletto et al. (2013) to synthetically generate eddies to form a velocity field that mimics turbulent flow. However, if such method can truly lead to a realistic turbulent flow (given proper inputs) suitable for the purpose of CFD is outside the concern of this software. However, NFR3 makes it possible for a CFD user to review and improve the method or adapt it for another theoretical model if they wish so.

6 Likely Changes

LC1: When theoretical work by Nikita Holyev progress, the software update to incorporate the new method to obtain realistic eddy profiles before generating velocity field (A1). The will allow user to input only a few parameters related to the energy spectrum of the flow, instead of details of each eddy type.

LC2: Additional interfaces can be developed to facilitate communication between any CFD software and SynthEddy, for obtaining IC and BC automatically.

7 Unlikely Changes

LC3: Support for 2D flow field is unlikely to be add, as most computational cost of 2D is significantly less than 3D. Thus, the need for this software is limited (A**??**).

8 Traceability Matrices and Graphs

The purpose of the traceability matrices is to provide easy references on what has to be additionally modified if a certain component is changed. Every time a component is changed, the items in the column of that component that are marked with an "X" may have to be modified as well. Table 3 shows the dependencies of theoretical models, general definitions, data definitions, and instance models with each other. Table 4 shows the dependencies of instance models, requirements, and data constraints on each other. Table **??** shows the dependencies of theoretical models, general definitions, data definitions, instance models, and likely changes on the assumptions.

	TM1	TM2	GD1	DD1	DD2	DD3	DD4	DD5	IM1
TM1				X	X				
TM2	X			X			X		
GD1	X	X		X			X		
DD1						X			
DD2				X					
DD3									
DD4									
DD5			X						X
IM1	X		X	X	X	X	X		

Table 3: Traceability Matrix Showing the Connections Between Items of Different Sections

	IM1	R1	R2
IM1			
R1			
R2	X		

Table 4: Traceability Matrix Showing the Connections Between Requirements and Instance Models

9 Development Plan

The first step would be to implement R2 given any user provided eddy profiles, and ensure divergence-free field generation. At this point, the software allows the user to manually query the velocity field at any point within the velocity field (R1).

Later as theoretical work by Nikita progresses, the software will be updated to incorporate the new method to obtain realistic eddy profiles before generating velocity field (NFR1).

References

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Cedar - digital research alliance of canada, 2024. URL https://docs.alliancecan.ca/wiki/Cedar.

Ruggero Poletto, T. Craft, and Alistair Revell. A new divergence free synthetic eddy method for the reproduction of inlet flow conditions for LES. *Flow, Turbulence and Combustion*, 91:1–21, 10 2013. doi: 10.1007/s10494-013-9488-2.

Appendix — Reflection

The information in this section will be used to evaluate the team members on the graduate attribute of Lifelong Learning. Please answer the following questions:

1. Which of the courses you have taken, or are currently taking, will help your team to be successful with your capstone project.
2. What knowledge and skills will the team collectively need to acquire to successfully complete this capstone project? Examples of possible knowledge to acquire include domain specific knowledge from the domain of your application, or software engineering knowledge, mechatronics knowledge or computer science knowledge. Skills may be related to technology, or writing, or presentation, or team management, etc. You should look to identify at least one item for each team member.
3. For each of the knowledge areas and skills identified in the previous question, what are at least two approaches to acquiring the knowledge or mastering the skill? Of the identified approaches, which will each team member pursue, and why did they make this choice?