



Global Sensitivity Analysis for Vector-Valued Responses of Mechanical Models

Master's Thesis Presentation

Technische

Prateek Bhustali, September 27, 2021

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Index

Goal

To study global sensitivities of models with vector-valued responses and demonstrate their efficient computation using surrogate models.

Outline

- 1. Uncertainty Quantification Primer
- 2. Surrogate modeling
- 3. Sensitivity Analysis
- 4. Chaboche Model
- 5. Results





Uncertainty Quantification (UQ) deals with the quantitative characterization and reduction of uncertainties in mathematical models [Sul15, LMK10, Xiu10].



What is Uncertainty Quantification?

Uncertainty Quantification (UQ) deals with the quantitative characterization and reduction of uncertainties in mathematical models [Sul15, LMK10, Xiu10].

Types of uncertainties:

- Aleatory Uncertainty: inherent, irreducible uncertainties
- Epistemic Uncertainty: lack of knowledge, reducible uncertainties





Example: Mechanical oscillator

$$\ddot{y} + 2\alpha \dot{y} + (\alpha^2 + \beta^2)y = 0,$$

 $y(0) = \ell, \dot{y}(0) = 0.$



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$$y(t; \alpha, \beta, \ell) = \ell e^{-\alpha t} (cos\beta t + \frac{\alpha}{\beta} sin\beta t).$$



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$$\alpha \sim U(3/8, 5/8),$$

$$\beta \sim U(10/4, 15/4),$$

$$\ell \sim \mathcal{U}(-5/4,-3/4).$$





Example: Mechanical oscillator

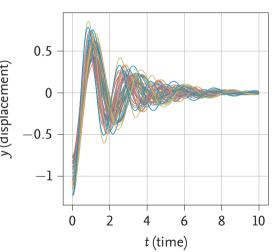
$$\ddot{y}+2\alpha\dot{y}+(\alpha^2+\beta^2)y=0,$$
 $\ddot{y}(0)=\ell,\ \dot{y}(0)=0.$ $y(t;\alpha,\beta,\ell)=\ell e^{-\alpha t}(cos\beta t+rac{\alpha}{\beta}sin\beta t)$

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Let's estimate the mean position of the block at t = 2s using N Monte Carlo (MC) samples,

$$\tilde{\mathbb{E}}[y_{t=2}] = \frac{1}{N} \sum_{k=1}^{N} y(t=2; \xi^{(k)})$$



Monte Carlo methods

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Due to the sampling error ϵ_N , the estimate above differs from the true mean $\mathbb{E}[y_{t=2}]$ given as:

$$\mathbb{E}[y_{t=2}] = \tilde{\mathbb{E}}[y_{t=2}] + \epsilon_N.$$



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- MC convergence rate: $\mathcal{O}(1/\sqrt{N})$
- → MC methods are slow and expensive



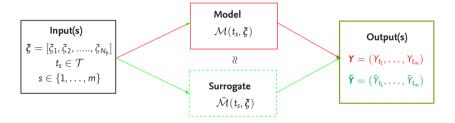


Surrogate modeling

Idea: Approximate the solution manifold Y using models that are computationally inexpensive to evaluate.

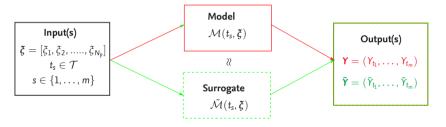


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Idea: Approximate the solution manifold \mathbf{Y} using models that are computationally inexpensive to evaluate.



For example: Polynomial Chaos Expansions, Karhunen-Loève Expansion with PCE approximated modes, Neural Networks, Gaussian Processes etc.





Polynomial Chaos Expansion (PCE)

A spectral method that approximates the solution manifold Y using a polynomial basis [LMK10].





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A spectral method that approximates the solution manifold Υ using a polynomial basis [LMK10].

$$\mathcal{M}(t,oldsymbol{\xi})pprox ilde{\mathcal{M}}^{PC}(t,oldsymbol{\xi})=\sum_{k=1}^{N_{PC}}c_k(t)\Psi_k(oldsymbol{\xi}),$$

 $\{\Psi_k(\xi)\}_{k=1}^{N_{PC}}$: multivariate orthonormal polynomial basis and $\{c_k\}_{k=1}^{N_{PC}}$: basis coefficients.

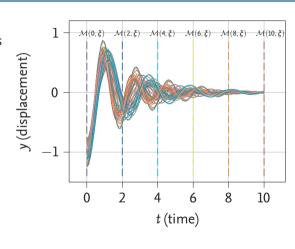


A spectral method that approximates the solution manifold \mathbf{Y} using a polynomial basis [LMK10].

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 $\{\Psi_k(\xi)\}_{k=1}^{N_{PC}}$: multivariate orthonormal polynomial basis and $\{c_k\}_{k=1}^{N_{PC}}$: basis coefficients.

- Local surrogate must be built at each point in time (time-frozen surrogates).



- PCE surrogates are known to deteriorate with time in some cases [MS17].



Karhunen-Loève Expansion

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Karhunen-Loève Expansion (KLE):

$$\mathcal{M}(t,oldsymbol{\xi})pprox ilde{\mathcal{M}}^{ extsf{KL}}(t,oldsymbol{\xi}) = \sum_{i=1}^{N_{kl}}\Phi_i(oldsymbol{\xi})oldsymbol{e}_i(t),$$

 $\{e_i(t)\}_{i=1}^{N_{kl}}$: eigenfunctions of the covariance operator of

 $\mathcal{M}(t, \boldsymbol{\xi})$ and $\{\Phi_i(\boldsymbol{\xi})\}_{i=1}^{N_{kl}}$: expansion coefficients.



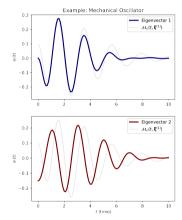


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However, $\Phi_i(\xi)$ are approximated using PCE, which leads to

$$\Phi_i(oldsymbol{\xi}) pprox \sum_{k=1}^{N_{PC}} \! f_{\Phi_i}^{(k)} \mathcal{F}_{\Phi_i}^{(k)}(oldsymbol{\xi}).$$



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The new surrogate model

$$ilde{\mathcal{M}}^{ ext{KL+PC}}(t,oldsymbol{\xi}) = \sum_{i=1}^{N_{kl}} \sum_{k=1}^{N_{PC}} f_{\Phi_i}^{(k)} \mathcal{F}_{\Phi_i}^{(k)}(oldsymbol{\xi}) e_i(t),$$

is called Karhunen-Loève Expansion with PCE approximated modes (KLE + PCE) [BS14].





How can the uncertainties in the model output be apportioned or allocated to the uncertainties in the model inputs? [Sal08]



Sensitivity Analysis

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Motivation:

- Which input variables make large contributions towards the output uncertainty?
 Factor Prioritisation ⇒ Reduce parameter uncertainty
- Which input variables have the least contribution towards the output uncertainty?
 Factor Fixing

 Model simplification
- Identify experimental settings under which a variable is most responsive
 Experiment Design
 Model calibration





Local v/s Global Sensitivity Analysis

Local Sensitivity Analysis

- Example: $\Delta_i y = f(\xi_i + \Delta \xi_i, \xi_{\alpha i}^0) f(\xi^0), \ \xi \in [0,1]^n$
- Provides local information about the model sensitivities
- Not meaningful if model inputs are uncertain



Local Sensitivity Analysis

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Global Sensitivity Analysis

Assign PDF(s) to input random variable(s) using domain knowledge



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Global Sensitivity Analysis

- Assign PDF(s) to input random variable(s) using domain knowledge
- Variance-based methods (Sobol indices), density-based methods (Borgonovo indices),
 Monte Carlo filtering, regression-based methods etc.





Sobol indices

• For non-additive, time-independent models $\mathcal{M}(\xi)$, we use the following generalisation: How much will the output variance decrease, if we know the value of an input with certainty?



Sobol indices

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- First-order Sobol index

$$\mathcal{S}_i := 1 - rac{\mathbb{E}_{oldsymbol{\xi}_i}[\mathbb{V}_{oldsymbol{\xi}|oldsymbol{\xi}_i}[\mathcal{M}(oldsymbol{\xi}) \mid oldsymbol{\xi}_i]]}{\mathbb{V}[\mathcal{M}(oldsymbol{\xi})]} = rac{\mathbb{V}_{oldsymbol{\xi}_i}[\mathbb{E}_{oldsymbol{\xi}|oldsymbol{\xi}_i}[\mathcal{M}(oldsymbol{\xi}) \mid oldsymbol{\xi}_i]]}{\mathbb{V}[\mathcal{M}(oldsymbol{\xi})]}.$$

• $0 \leq S_i \leq 1$.



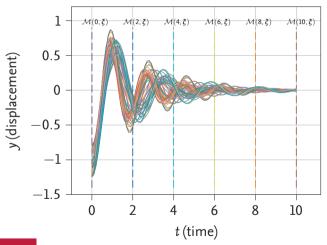
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- $0 \leq S_i \leq 1$.
- Computing using PCE surrogate: $S_i = \sum_{k \in \mathcal{K}_i} c_k^2$.

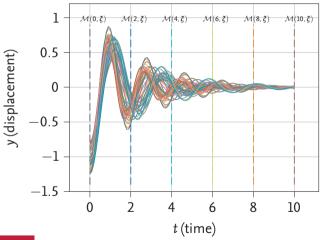




$$\mathcal{M}(t_{ extsf{s}},oldsymbol{\xi}) = \ell e^{-lpha t_{ extsf{s}}}(coseta t_{ extsf{s}} + rac{lpha}{eta} sineta t_{ extsf{s}})$$



Example: Mechanical oscillator



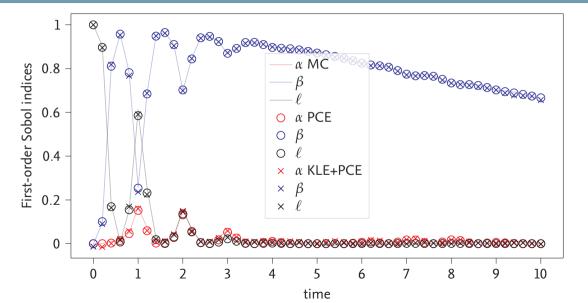
$$\mathcal{M}(t_{\mathrm{s}},\xi) = \ell e^{-lpha t_{\mathrm{s}}}(\cos\!eta t_{\mathrm{s}} + rac{lpha}{eta}\!\sin\!eta t_{\mathrm{s}})$$

$$\mathcal{S}_{\textit{i}}(t_{\textit{s}}) = rac{\mathbb{V}_{\xi_{\textit{i}}}[\mathbb{E}_{\xi|\xi_{\textit{i}}}[\mathcal{M}(t_{\textit{s}},\xi)|\xi_{\textit{i}}]]}{\mathbb{V}[\mathcal{M}(t_{\textit{s}},\xi)]}$$

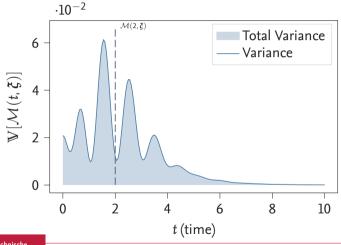




Pointwise-in-time Sobol indices



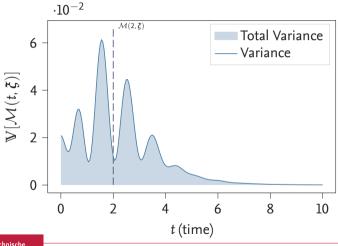
Shortcomings



- Sensitivity metric variance, changes over time
- Cannot provide holistic overview of sensitivities



Shortcomings



- Sensitivity metric variance, changes over time
- Cannot provide holistic overview of sensitivities
- Solution: Use total integrated variance as a metric [AGS20, GJKL13].



For time-dependent processes, the generalised Sobol indices are the ratio of the time integrals of the numerator and denominator of the Sobol indices [AGS20].

$$\mathcal{G}_i(\mathcal{T}) := rac{\int_{\mathcal{T}} \mathcal{S}_i^{num}(\mathcal{M};t) \; \mathrm{d}t}{\int_{\mathcal{T}} \mathsf{V}(\mathcal{M};t) \; \mathrm{d}t} = rac{\int_{\mathcal{T}} \mathbb{V}_{\xi_i}[\mathbb{E}_{\xi|\xi_i}[\mathcal{M}(t,oldsymbol{\xi}) \mid \xi_i]] \; \mathrm{d}t}{\int_{\mathcal{T}} \mathbb{V}[\mathcal{M}(t,oldsymbol{\xi})] \; \mathrm{d}t},$$

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where \mathcal{T} is the time interval.

Computing using PCE surrogates:

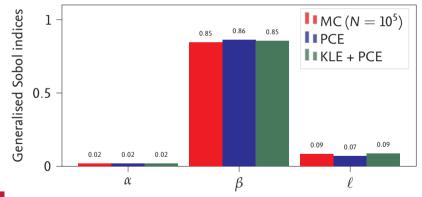
$$\mathcal{G}_i^{PC}(\mathcal{T}) pprox \left(\sum_{j=1}^{N_{ ext{quad}}} \sum_{k \in \mathcal{K}_i} w_j \, c_k^2(t_j) \right) \Bigg/ \left(\sum_{j=1}^{N_{ ext{quad}}} \sum_{k=2}^{N_{PC}} w_j \, c_k^2(t_j)
ight).$$





Example: Mechanical oscillator

- Generalised Sobol indices for $\mathcal{T} = [0, 10]s$.
- Computed using MC simulation, PCE and KLE+PCE surrogate.





Chaboche Model

 A constitutive material model that describes the behaviour of viscoplastic materials (such as steel) when subjected to time-dependent loading.



- A constitutive material model that describes the behaviour of viscoplastic materials (such as steel) when subjected to time-dependent loading.
- System of ODEs for a 1D bar:

$$\begin{bmatrix} \dot{\varepsilon}_{xx} \\ \dot{K} \\ \dot{X}_{xx} \end{bmatrix} = \begin{bmatrix} E^{-1} \cdot \dot{\sigma}_{xx} + \frac{1}{\sigma_{\nu}} (\sigma_{xx} - X_{xx}) \cdot \left\langle \frac{\sigma_{ex}}{D} \right\rangle^{n} \cdot \dot{\varepsilon}_{0} \\ b_{iso} \cdot (Q_{iso} - K) \cdot \left\langle \frac{\sigma_{ex}}{D} \right\rangle^{n} \\ b_{kin} \left(\frac{2}{3} Q_{kin} \cdot \frac{1}{\sigma_{\nu}} (\sigma_{xx} - X_{xx}) - X_{xx} \right) \cdot \left\langle \frac{\sigma_{ex}}{D} \right\rangle^{n} \end{bmatrix}$$



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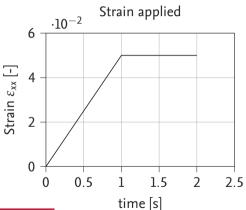
• Stress response: $\mathcal{M}(t, \xi) = \sigma_{xx}(t; E, \sigma_{y_0}, Q_{iso}, b_{iso}, n, D, Q_{kin}, b_{kin})$, when subjected to strain $\varepsilon_{xx}(t)$.





• Monotonic loading: $\mathcal{M}(t, \xi) = \sigma_{xx}(t; E, \sigma_{y_0}, Q_{iso}, b_{iso}, n, D)$

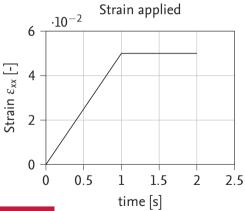
• Monotonic loading: $\mathcal{M}(t, \xi) = \sigma_{xx}(t; E, \sigma_{y_0}, Q_{iso}, b_{iso}, n, D)$





Physical Model setup [Hei21]

• Monotonic loading: $\mathcal{M}(t, \xi) = \sigma_{xx}(t; E, \sigma_{y_0}, Q_{iso}, b_{iso}, n, D)$

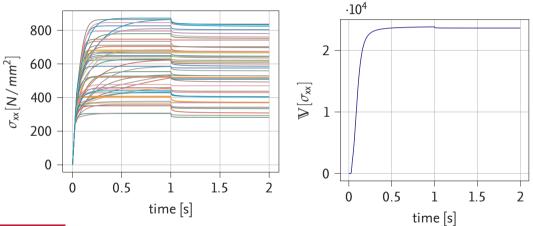


#	ξ	Distribution	a	Ь	Mean	Variance	Unit
1	Ε	Uniform	200,000	210,000	205,000	8, 333, 333.33	N/mm ²
2	σ_{y_0}	Uniform	200	400	300	3, 333.33	N/mm ²
3	Qiso	Uniform	0	500	250	20, 833.33	N/mm ²
4	biso	Uniform	0	1000	500	83, 333.33	-
5	n	Uniform	1	6	3.5	2.08	-
6	D	Uniform	1	100	50.5	816.75	N/mm ²



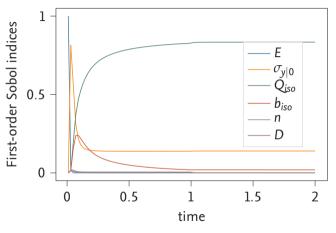


Chaboche Model Response





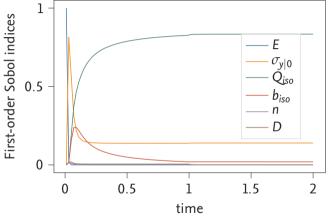




Estimated using time-frozen PCE surrogates.

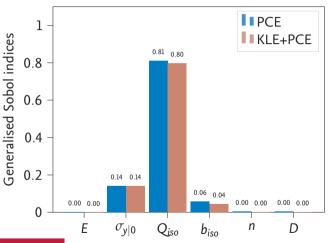


Pointwise-in-time Sobol indices



- Estimated using time-frozen PCE surrogates.
- In literature [GR18, WSK19], it has been observed that sensitivity can be a good indicator for parameter identifiability ⇒ calibration time-points are now available.

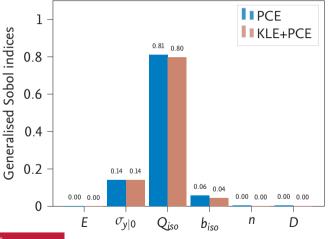




 Estimation using MC simulations not feasible.



Generalised Sobol indices



- Estimation using MC simulations not feasible.
- The uncertainty in parameter Q_{iso} must be reduced to reduce overall output uncertainty.



Bayes' rule:

$$\underbrace{\pi(\boldsymbol{\xi} \mid \boldsymbol{\mathcal{Y}})}_{\text{Posterior}} = \underbrace{\frac{\underbrace{\mathcal{L}(\boldsymbol{\xi}, \boldsymbol{\mathcal{Y}})}_{\text{Evidence}} \underbrace{\pi(\boldsymbol{\xi})}_{\text{Evidence}} \underbrace{\mathbb{E}_{\pi}(\boldsymbol{y})}_{\text{Evidence}}}_{\text{Evidence}}$$

■ Young's Modulus E has sensitivity highest in the initial elastic region [0, 0.019]s, therefore calibrated at t = 0.01s.



Bayesian Calibration

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- Young's Modulus E has sensitivity highest in the initial elastic region [0, 0.019]s, therefore calibrated at t = 0.01s.
- True parameter value assumed $E = 200,000 \text{ N/mm}^2$ and thus model response $\hat{\sigma}_{xx} = E \cdot \dot{\varepsilon} \cdot t_1 = 200,000 \cdot 5 \times 10^{-2} \cdot 0.01 = 100 \text{ N/mm}^2$.



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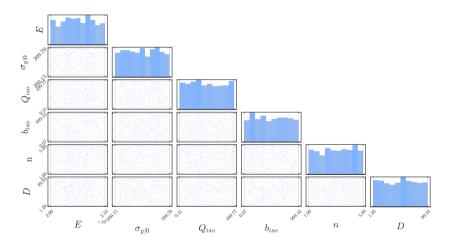
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- Calibrated *E* using 10 samples from mock data: $y_i \sim \mathcal{N}(100, 10^{-4})$ (coefficient of variation = 0.01%).



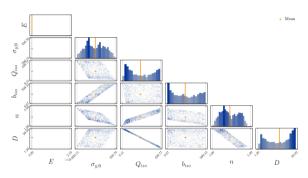


Model Priors

Prior Sample







Successfully calibrated E using PCE surrogate to replace model evaluations in MCMC.









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