MATLAB kode fra Optimalisering og regulering

0.1 Optimization - helicopter controllers

Optimal Control of Pitch/Travel without Feedback

```
1 % TTK4135 Optimization and Control - Helicopter lab
\mathbf{2} % Chapter 1, Optimal Control of Pitch/Travel without feedback
4 init;
5 dt = 0.25;
                                    % sampling time
6 \text{ sek\_forst} = 5;
8 % Continuous system model. x=[lambda r p p_dot]'
9 A = [ 0 1 0 0 ;

10 0 0 -K_2 0 ;

11 0 0 0 1 ;

12 0 0 -K_1*K_pp -K_1*K_pd ];
13 B = [0 \ 0 \ 0 \ K_1 * K_pp]';
15 % Number of states and inputs
16 mx = size(A, 2);
                                            % Number of states (number of ...
      columns in A)
                                           % Number of inputs (number of ...
17 mu = size(B,2);
      columns in B)
19 % Discrete system model
20 A1 = eye(mx) + dt*A;
B1 = dt *B;
23 % Initial values
24 x1_0 = pi;
                                               % Lambda
25 	 x2_0 = 0;
                                              % r
26 \times 3_0 = 0;
27 \times 4_0 = 0;
                                              % p_dot
x0 = [x1_0 \ x2_0 \ x3_0 \ x4_0]'; % Initial values
```

```
30 % Time horizon and initialization
31
32 N = 100;
                                         % Time horizon for states
33 M = N;
                                         % Time horizon for inputs
34 z = zeros(N*mx+M*mu,1);
                                        % Initialize z for the whole ...
      horizon
35 	 z0 = z;
                                         % Initial value for optimization
36
37 % Bounds
38
          = -30*pi/180;
39 ul
                                        % Lower bound on control -- u1
          = 30*pi/180;
                                         % Upper bound on control -- u1
41 xl
          = -Inf*ones(mx,1);
                                         % Lower bound on states (no bound)
         = Inf*ones(mx, 1);
                                         % Upper bound on states (no bound)
42 XU
         = ul;
43 xl(3)
                                         % Lower bound on state x3
         = uu;
                                         % Upper bound on state x3
44 xu(3)
45
46 % Generate constraints on measurements and inputs
47
48 [vlb, vub] = genbegr2(N, M, xl, xu, ul, uu);
49 vlb (N*mx+M*mu) = 0;
                                         % We want the last input to be ...
      zero
50 vub (N*mx+M*mu) = 0;
                                        % We want the last input to be ...
     zero
52 % Generate the matrix Q and the vector c (objective function weights ...
     in the QP problem)
93 	 Q1 = zeros(mx, mx);
54 Q1(1,1) = 1;
                                          % Weight on state x1
55 P1 = 1;
                                          % Input weight (0.1, 1 and 10)
S6 Q = geng2(Q1, P1, N, M, mu);
                                          % Generate Q
58 % Generate system matrixes for linear model
62 % Solve Qp problem with linear model
63 tic
64 [z,lambda] = quadprog(Q,c,[],[],Aeq,beq,vlb,vub,z0);
65 t1=toc;
67 % Calculate objective value
68 phi1 = 0.0;
69 PhiOut = zeros(N*mx+M*mu,1);
70 for i=1:N*mx+M*mu
71 phi1=phi1+Q(i,i)*z(i)*z(i);
72 PhiOut(i) = phi1;
73 end
74
75 % Extract control inputs and states
76 u = [z(N*mx+1:N*mx+M*mu);z(N*mx+M*mu)]; % Control input from solution
```

```
78 \times 1 = [x0(1); z(1:mx:N*mx)];
                                           % State x1 from solution
79 x2 = [x0(2); z(2:mx:N*mx)];
                                           % State x2 from solution
x3 = [x0(3); z(3:mx:N*mx)];
                                           % State x3 from solution
x4 = [x0(4); z(4:mx:N*mx)];
                                           % State x4 from solution
82
83 Antall = 5/dt;
84 Nuller = zeros(Antall,1);
85 Enere = ones(Antall,1);
86
       = [Nuller; u; Nuller];
87 u
88 x1
       = [pi*Enere; x1; Nuller];
89 \times 2 = [Nuller; \times 2; Nuller];
90 x3 = [Nuller; x3; Nuller];
91 \times 4 = [Nuller; \times 4; Nuller];
92
93 %save bane
94 t = 0:dt:dt*(length(u)-1); % real time
95 pitch_setpoint=[t' u];
97 figure(2)
98 subplot (511)
99 stairs(t,u),grid
100 ylabel('u')
101 subplot (512)
102 plot(t,x1,'m',t,x1,'mo'),grid
103 ylabel('lambda')
104 subplot (513)
105 plot(t,x2,'m',t,x2','mo'),grid
106 ylabel('r')
107 subplot (514)
108 plot(t,x3,'m',t,x3,'mo'),grid
109 ylabel('p')
110 subplot (515)
111 plot(t,x4,'m',t,x4','mo'),grid
112 xlabel('tid (s)'),ylabel('pdot')
```

Optimal Control of Pitch/Travel with Feedback (LQ)

```
1 % TTK4135 Optimization and Control - Helicopter lab
3 % Chapter 2, Optimal Control of Pitch/Travel with Feedback (LQ)
5 init;
6 dt = 0.25;
                                           % sampling time
7 \text{ sek\_forst} = 5;
9 % Continuous model
10 A = [0 0 1
      0
                           -K_2
                   0
                                       0
                                                    ;
              0
                  0
                           -K_1*K_pp -K_1*K_pd
14 B = [0 \ 0 \ 0 \ K_1 * K_pp]';
16 % Number of states and inputs
                                          % Number of states (number of ...
17 mx = size(A, 2);
      columns in A)
18 mu = size(B, 2);
                                         % Number of inputs (number of ...
      columns in B)
19
20 % Discrete system model
21 A1 = eye(mx) + dt \starA;
22 B1 = dt*B;
23
24 % Initial values
                                           % Lambda
25 \times 1_0 = pi;
26 	 x2_0 = 0;
                                            % r
                                           % p
27 \times 3_0 = 0;
28 \times 4_0 = 0;
                                            % p_dot
x_0 = [x_1_0 \ x_2_0 \ x_3_0 \ x_4_0]';
                                           % Initial values
31 % Time horizon and initialization
32 N = 100;
                                            % Time horizon for states
33 M = N;
                                           % Time horizon for inputs
z = zeros(N*mx+M*mu,1);
                                            % Initialize z for the whole ...
      horizon
35 	 z0 = z;
                                           % Initial value for optimization
37 % Bounds
38 \text{ ul} = -30 * \text{pi}/180;
                                           % Lower bound on control -- u1
         = 30*pi/180;
39 uu
                                           % Upper bound on control -- u1
         = -Inf*ones(mx,1);
                                           % Lower bound on states (no bound)
40 xl
          = Inf*ones(mx,1);
                                           % Upper bound on states (no bound)
41 XU
42 \times 1(3) = u1;
                                           % Lower bound on state x3
43 \times u(3) = uu;
                                           % Upper bound on state x3
45 % Generate constraints on measurements and inputs
46
47 [vlb, vub] = genbegr2(N, M, xl, xu, ul, uu);
```

```
48 vlb(N*mx+M*mu) = 0;
                                         % We want the last input to be ...
49 vub(N*mx+M*mu) = 0;
                                         % We want the last input to be ...
     zero
51 % Generate the matrix Q and the vector c (objective function weights ...
    in the QP problem)
52
53 Q1 = zeros(mx, mx);
54 Q1(1,1) = 1;
                                          % Weight on state x1
55 P1 = 0.1;
                                          % Weight on input
Q = 2 * genq2(Q1, P1, N, M, mu);
                                          % Generate Q
58 % LQR tuning
59 Q_lqr = zeros(mx, mx);
60 Q_1qr(1,1)=1;
61 Q_lqr(2,2)=0;
62 Q_1qr(3,3)=1;
63 Q_1qr(4,4)=0;
64 P_lgr=1;
65 [K,P,E] = dlqr(A1,B1,2*Q_lqr,2*P_lqr);
67 % Generate system matrixes for linear model
68 Aeq =gena2(A1,B1,N,mx,mu); % Generate A
69 beq = [A1*x0; zeros((N-1)*mx,1)]; % Generate b
71 % Solve Qp problem with linear model
73 [z,lambda] = quadprog(Q,c,[],[],Aeq,beq,vlb,vub,z0);
74 t1=toc;
77 % Calculate objective value
78 phi1 = 0.0;
79 PhiOut = zeros(N*mx+M*mu,1);
80 for i=1:N*mx+M*mu
   phi1=phi1+Q(i,i)*z(i)*z(i);
PhiOut(i) = phi1;
83 end
85 % Extract control inputs and states
86 u = [z(N*mx+1:N*mx+M*mu);z(N*mx+M*mu)];% Control input from solution
88 x1 = [x0(1); z(1:mx:N*mx)];
                                          % State x1 from solution
89 x2 = [x0(2); z(2:mx:N*mx)];
                                         % State x2 from solution
90 \times 3 = [x0(3); z(3:mx:N*mx)];
                                         % State x3 from solution
91 x4 = [x0(4); z(4:mx:N*mx)];
                                         % State x4 from solution
92
93 Antall = 5/dt;
94 Nuller = zeros(Antall, 1);
95 Enere = ones(Antall,1);
97 u = [Nuller; u; Nuller];
```

```
98 x1 = [pi*Enere; x1; Nuller];
99 x2 = [Nuller; x2; Nuller];
100 x3 = [Nuller; x3; Nuller];
101 x4 = [Nuller; x4; Nuller];
102
103 x = [x1 x2 x3 x4]';
104
105 %saving trajectory
106 t = 0:dt:dt*(length(u)-1); % real time
107 pitch_setpoint = [t' u];
108 x_optimal = [t' x'];
```

Optimal Control of Pitch/Travel and Elevation with and without Feedback

```
1 % TTK4135 Optimization and Control - Helicopter lab
2  ^{\circ}
_{3} % Chapter 3, Optimal Control of Pitch/Travel and Elevation with and \dots
       without Feedback
4
5 init;
6 dt = 0.25;
                                               % sampling time
  sek_forst = 5;
   % Continuous model
10
                             0
                                                      0
            0
                              -K_2
                                           0
                                                      0
            0
                              0
                                                      0
                     0
                                           1
                                                                      0 ...
            0
                     0
                              -K_1*K_pp
                                           -K_1*K_pd 0
            0
                     0
                              0
                                                      0
                                                                     1 ...
                                                      -K_3*K_ep
                                                                     -K_3*K_ed] ...
            0
                              0
                                           K_1*K_pp 0
            0
                              0
                                           0
                                                      0
                                                                     K_3*K_ep]' ...
20 % Number of states and inputs
21
22 \text{ mx} = \text{size}(A, 2);
                                              % Number of states (number of ...
      columns in A)
23 mu = size(B, 2);
                                              % Number of inputs (number of ...
       columns in B)
25 % Discrete system model
26 A1 = eye(mx) + dt*A;
27 B1 = dt*B;
29 % Initial values
30 x1_0 = pi;
                                               % Lambda
31 \times 2_0 = 0;
                                               % r
32 \times 3_0 = 0;
                                               % p
33 \times 4_0 = 0;
                                               % p_dot
34 \times 5_0 = 0;
35 \times 6_0 = 0;
x0 = [x1_0 x2_0 x3_0 x4_0 x5_0 x6_0]'; Initial values
37
```

```
38 % Time horizon and initialization
40 N = 55;
                                           % Time horizon for states
41 M = N;
                                           % Time horizon for inputs
z = zeros(N*mx+M*mu, 1);
                                           % Initialize z for the whole ...
      horizon
43 	 z0 = z;
                                           % Initial value for optimization
44
45 % Bounds
       = [-30*pi/180 -30*pi/180]';
                                          % Lower bound on control -- ul
46 ul
          = [30*pi/180 30*pi/180]';
                                          % Upper bound on control -- u1
47 1111
49 xl
          = -Inf*ones(mx,1);
                                          % Lower bound on states (no bound)
          = Inf*ones(mx, 1);
                                           % Upper bound on states (no bound)
50 xu
         = ul(1);
                                           % Lower bound on state x3
51 xl(3)
         = uu(1);
                                           % Upper bound on state x3
52 xu(3)
54 % Generate constraints on measurements and inputs
[vlb, vub] = genBegr2(N, M, xl, xu, ul, uu);
57 vlb(N*mx+M*mu) = 0;
                                           % We want the last input to be ...
      zero
58 vub (N*mx+M*mu) = 0;
                                           % We want the last input to be ...
     zero
60 % Generate the matrix Q and the vector c (objective function weights ...
     in the QP problem)
61
62 Q1 = zeros(mx, mx);
63 Q1(1,1) = 10;
                                           % Weight on state x1
64 P1 = 0.1 * eye(2);
                                           % Weight on input
Q = 2*geng2(Q1,P1,N,M,mu);
                                           % Generate Q
66 FUN= @(z) z'*Q*z;
68 % LQR
69 Q_lqr = zeros(mx, mx);
70 Q_lqr(1,1)=1;
71 Q_1qr(2,2)=0;
72 Q_1qr(3,3)=1;
73 Q_1qr(4,4)=0;
74 Q_1qr(5,5)=1;
75 Q_lqr(6,6)=1;
76 \text{ r\_lqr} = 1 \star \text{eye}(2);
77 [K, P, E] = dlqr(A1, B1, 2*q_lqr, 2*r_lqr);
79 % Generate system matrixes for linear model
80 Aeq =gena2(A1,B1,N,mx,mu); % Generate A
81 beq = [A1*x0; zeros((N-1)*mx,1)];
                                          % Generate b
82
83 % Solve Qp problem with linear model
84 options = optimset('disp','iter','Algorithm','active-set');
86 [z,lambda] = fmincon(FUN,z0,[],[],Aeq,beq,vlb,vub,@el,options);
```

```
88 t1=toc;
90 % Calculate objective value
91 \text{ phi1} = 0.0;
92 PhiOut = zeros(N*mx+M*mu,1);
93 for i=1:N*mx+M*mu
94 phil=phil+Q(i,i)*z(i)*z(i);
    PhiOut(i) = phi1;
95
96 end
98 % Extract control inputs and states
100 u1 = [z(mx*N+1:mu:end);z(N*mx+M*mu)]; % Control input from solution
101 u2 = [z(mx*N+mu:mu:end); z(N*mx+M*mu)];
102
103 \times 1 = [x0(1); z(1:mx:N*mx)];
                                               % State x1 from solution
104 \times 2 = [x0(2); z(2:mx:N*mx)];
                                               % State x2 from solution
105 \times 3 = [x0(3); z(3:mx:N*mx)];
                                               % State x3 from solution
106 \times 4 = [x0(4); z(4:mx:N*mx)];
                                               % State x4 from solution
107 \times 5 = [x0(5); z(5:mx:N*mx)];
                                               % State x5 from solution
108 \times 6 = [x0(6); z(6:mx:N*mx)];
                                               % State x6 from solution
110 Antall = 5/dt;
111 Nuller = zeros(Antall,1);
112 Enere = ones(Antall, 1);
113
       = [Nuller; u1; Nuller];
114 u1
115 u2
       = [Nuller; u2; Nuller];
116 x1 = [pi*Enere; x1; Nuller];
117 x2
       = [Nuller; x2; Nuller];
118 x3
       = [Nuller; x3; Nuller];
119 x4
       = [Nuller; x4; Nuller];
120 \times 5 = [Nuller; \times 5; Nuller];
121 \times6 = [Nuller; \times6; Nuller];
122
123 \times = [x1 \times 2 \times 3 \times 4 \times 5 \times 6]';
124
125 %saving trajectory
126 t = 0:dt:dt*(length(u1)-1);
                                      % real time
127 setpoint = [t' u1 u2];
128 x_optimal = [t' x'];
```

MATLAB kode fra Fartøystyring

0.2 Guidance and Control of Vehicles (2014) / Fartøystyring

Satellite Angular Rates and Gyro Bias Estimation Using the Ekstended Kalman Filter

```
1
2 function [z,A]=jaccsd(fun,x,u,t)
3 % JACCSD Jacobian through complex step differentiation
4 % [z J] = jaccsd(@f,x, u, t)
5 % z = f(x, u, t)
6 % J = df/dx(x, u, t)
7 %
8 z=fun(x,u,t);
9 n=numel(x);
10 m=numel(z);
11 A=zeros(m,n);
12 h=n*eps;
13 for k=1:n
14     x1=x;
15     x1(k)=x1(k)+h*1i; %for bedre speed la jeg til 1-tall foran i.
16     A(:,k)=imag(fun(x1,u,t))/h;
17 end
```

```
1 clear all;
2
3 h=0.01; %samplingtime
4 N=1000; %iterations
5 sigma=0.001; %sigma^2
6
7 %initial values
8 x=[0 0 0 0 0 0 0 0 0]';
9 xd=[0.1 0.3 0.2 0 0 0]'; %Desired Euler Angles
10 I=diag([0.0108 0.0113 0.0048]); %inertia matrix
11 b_g=[0.012;0.017;0.014]; %The constant Bias
12 x(7:9) = b_g; %adding bias to the states
```

```
14 %Initialization Controller from Task 2.1
15 Kp=diag([0.07 0.07 0.07]);
16 Kd=diag([0.1 0.1 0.1]);
17 e=[0;0;0];
18
19 %Initialization of Kalman filter
20 y=[0;0;0;0;0;0];
21 x_bar=[0 0 0 0 0 0 0 0 0];
22 p_bar= (x-x_bar)*(x-x_bar)' + 1e-9*eye(9); %Ensure pos def.
23 I_k = eye(9);
24 x_hat=[0 0 0 0 0 0 0 0 0]';
25 R=[1e-09*eye(3) zeros(3); zeros(3) sigma*eye(3)]; %6x6
26 H=[eye(3) zeros(3) zeros(3); zeros(3) eye(3) eye(3)]; %6x9
27 Q=10^-9*eye(9); %9x9 With small diag to avoid singularities and ensure ...
       keep pos def.
29 %Function for the system 9x1
30 f = 0(x, tau, t) [[1 sin(x(1))*tan(x(2)) cos(x(1))*tan(x(2));0 ...
       cos(x(1)) - sin(x(1)); 0 sin(x(1))/cos(x(2)) ...
       cos(x(1))/cos(x(2))]*x(4:6); ...
       inv(I)*(tau-(Smtrx(x(4:6))*(I*x(4:6)))); zeros(3,1)]; %function
32 %Used for data storing and plot
33 true=zeros(9,N);
34 est=zeros(9,N);
35 time=zeros(1,N);
36 %Loop
37 for i=1:N+1,
      t = (i-1) *h;
38
39
      %noise
40
41
      noise(:,i) = sqrt(0.001).*randn(3,1); %Computing noise
42
43
   %f(x_hat,tau_hat)+EW 9x1
44
     tau=-(Kp*e+Kd*x_hat(4:6)); %input with e=(x_hat_euler)-(x_d_euler)
45
46
47
       %measurement
      v = [zeros(3,1);
48
          noise(:,i)]; %Noise
49
      y = H * x + v;
50
51
      %%Kalman gain
53
54
      K=p_bar*H'*inv(H*p_bar*H'+R);
55
56
      %State estimate update
      x_hat=x_bar+K*(y-H*x_bar); %xbar+K(y-ybar). Ybar contains zero bias ...
57
          at the first iteration.
58
      P_hat = (I_k - K*H)*p_bar*(I_k - K*H)' + K*R*K';
59
60
```

```
61
      %linearization of f(x_{hat},tau_{hat}) inserting x_{hat} for [phi theta . . . .
          . .], df/dx
      [fev, df_xhat] = jaccsd(f,x_hat, tau, t);
63
64
      \$State estimate propagation and error covariance propagation \dots
65
          (predictor k+1)
      x_bar=x_hat+h*fev; %x_hat + h*x_dothat
66
67
      %discrete-time matrix PHI
68
      PHI=I_k+h*df_xhat; %(11.52)
69
      p_bar=PHI*P_hat*PHI'+Q; %with no process noise, we do not include ...
          gamma.
71
     %From Task 2.1
72
     e=(x_hat(1:3)-xd(1:3)); %error
73
74
75
     %Euler integration(k+1)
76
      x=x+h*f(x,tau,t);
77
      xest=x_hat;
78
79
      %data storing
82
      time(i)=i*h; %to update time table
83
      true(:,i)=x;
84
      est(:,i)=xest;
85
      yvector(:,i) = y; %used only for checking if measurement y is ...
86
          correct by ploting it
87
88 end
92 %plotting actual and estimated angular rates
93
94
95 %Plotting of actual and estimated bias
```

Autopilot design

Matlab kodene som følger er resultatet fra et formelt gruppearbeid som ble karaktersatt. Det er autopiloter for et skip som heter MS Fartøystyring. Skipet har begrenset bevegelse i North-East planet slik at autopiloter for fart og heading er det eneste som trengs. Autopilotene er deretter brukt til "path-following" og "path tracking". Kodene inkluderer implementering og simulering av skipet. Har ikke tatt med kode for skip-modell.

```
2 % TTK4190 - Guidance and Control
3 % Assignment 3
4 % 746072 - Bjorn-Olav H. Eiksen
5 % 746029 - Marius Hjertaker
6 % 705009 - Sveinung Ohrem
7 % 745621 - Ole Maurice Rabanal
9 % This is the code for task 1.4 of the assignment
11 clear; clc;
12 dispstat('','init')
                                 % Simulation progress. ...
     Initialization. Does not print anything.
13 dispstat('run_task_1_4','keepthis'); % Output first
14
15 %Integration values
16 sim_time=3000;
              %Simulation end time
                 %Steplength
17 dt=0.1;
18 L=sim_time/dt;
              %Simulation steps
System
     21
                 %Transfer function gain
22 K=-0.0598:
23 T=115.5667;
                 %Transfer function time constant
User parameters
     x_0=[6.63,0,0,0,0,0]; %x = [u v r x y psi]'
28 omega_b=0.06;
                    %Bandwith of controller
29 zeta=1;
                     %Damping coefficient
30
References
     32
33 t=0:dt:(sim_time);
                                 %Time steps
34 psi_d=-0.3*sin(0.008*t);
                                 %Desired heading(yaw)
r_d=-0.3*0.008*cos(0.008*t);
                                 %Desired yaw rate
36 r_d_{ot=0.3*0.008*0.008*sin(0.008*t)}; %Desired yaw acceleration
```

```
888888888888888888888
41 omega_n=omega_b/(sqrt(1-2*zeta^2+...
%Natural frequency
43
                                  %Proportional gain
44 Kp=(T/K)*omega_n^2;
45 Kd=(T/K) *2*zeta*omega_n-1/T;
                                  %Derivative gain
46 Ki=(omega_n/10) *Kp;
                                  %Integrator gain
47
888888888888888888888888
50 time=zeros(1,L+1);
                        %Time
51 x=zeros(6,L+1);
                        %States x=[ u v r x y psi]'
                        %Inputs to ms fartoystyring tau=[\Delta_c n_c]'
52 tau=zeros(2,L);
                        %Error
53 e=zeros(2,L);
55 \times (:,1) = x_0;
                        %Set first step equal to initial values
56 e_int=zeros(1,L+1);
                        %Error integrated
응응응응응응응응응응응응응응응응응응
60 for i=1:L
     if (mod(i, 100)) == 0
61
        Simulation progress in %
     end
63
     time(i+1) = time(i) + dt;
                          %Time
64
65
     %Control algorithm
66
     e(:,i) = [x(6,i)-psi_d(i);x(3,i)-r_d(i)]; %Error
67
     e_{int}(i+1) = e_{int}(i) + dt * e(1, i);
                                         %Error integrated
                                        %Feed forward input
70
     \Delta_{ff} = (1/K) * r_d(i) + (T/K) * r_d_dot(i);
     \Delta_{PID}=-Kp*e(1,i)-Kd*e(2,i)-Ki*e_int(i+1); %PID control input
71
72
                                    %Input with constant shaft ...
     tau(:,i)=[\Delta_ff+\Delta_PID ; 7.3];
73
       velocity
     x_{dot}=msfartoystyring(x(:,i),tau(:,i),1); %Send to ms ...
74
       fartoystyring
75
76
     %Integrate
     x(:,i+1)=x(:,i)+dt*x_dot;
                                         %Update states
78 end
```

```
1 % TTK4190 - Guidance and Control
2 % Assignment 3
3 % 746072 - Bjorn-Olav H. Eiksen
```

```
4 % 746029 - Marius Hjertaker
5 % 705009 - Sveinung Ohrem
6 % 745621 - Ole Maurice Rabanal
7 %
8 % This is the code for task 1.8 of the assignment
10 clear; clc;
11 close all
12 dispstat('', 'init')
                                        % Simulation progress. ...
      Initialization. Does not print anything.
dispstat('run_task_1_8','keepthis'); % Output first
15 %Integration values
                                       %Simulation end time
16 sim_time=10000;
17 dt=1;
                                        %Steplength
                                        %Simulation steps
18 L=sim_time/dt;
19
21 %Heading
22 K=-0.0598;
23 T=115.5667;
24 %Surge
25 Ksurge=0.9820;
26 Tsurge=450.8367;
27 time=0:dt:sim_time;
29 %User parameters
30 x_0 = [4,0,0,0,0,0];
                                       %x = [uvrxypsi]'
31 omega_b=0.06;
                                        %Bandwith for heading controller
                                        %Bandwith for surge controller
32 omega_bs=0.015;
33 zeta=1;
                                        %Damping of system
n_c_{max}=85*2*pi/60;
                                        %Max shaft velocity[rad/s]
References
     888888888888888888888888888888888
37
38 %%Choose these for time varying reference in yaw
39 \% psi_d=-0.3*sin(0.008*time(1:L));
40 % r_d=-0.3*0.008*cos(0.008*time(1:L));
41 % r_d_dot=0.3*0.008*0.008*sin(0.008*time(1:L));
43 % psi_d=[psi_d(1:(L/2)) ones(1,L/2).*psi_d(end)];
44 % r_d=[r_d(1:(L/2)) zeros(1,L/2)];
45 % r_d_dot=[r_d_dot(1:(L/2)) zeros(1,L/2)];
47 %%Choose these for constant yaw and yaw rate:
48 psi_d=zeros(1,L);
49 r_d=zeros(1,L);
50 r_d_dot=zeros(1,L);
51
52 %%Choose between step input or time varying input for u:
u_r = [4.*ones(1,700/dt)...
```

```
7.*ones(1,L-700/dt)];
                                    %Step
u_r=4+abs(sin(0.001*time(1:L)));
                                   %Time varying
Controller parameters
     8888888888888888888888
58 %Heading controller
omega_n=omega_b/(sqrt(1-2*zeta^2+...
     sqrt(4*zeta^4-4*zeta^2+2)));
                                    %Natural frequency
60
61 Kp=(T/K) * omega_n^2;
                                    %Kp
62 Kd=(T/K)*2*zeta*omega_n;
                                    %Kd
63 Ki = (T/K) * ((omega_n^3)/10);
                                    %Ki
65 %Surge controller
omega_n_surge=omega_bs/(sqrt(1-2*...
67 zeta^2+sqrt(4*zeta^4-4*zeta^2+2)));
                                    %Natural frequency
68 Kp_surge=5.7388;
                                        %Kp
                                     %Ti
69 Ti_surge=Tsurge+50;
70
Data storage
     x=zeros(6,L+1);
                                    %x = [uvrxypsi]'
74 tau=zeros(2,L);
                                    tau = [\Delta_c n_c]'
75 e=zeros(3,L);
                                    %e=[psi,r,u]'
76 e_int=zeros(3,L+1);
                                    %Integrated error
                         Reference prefilter
888888888888888888888
79 omega_ref=0.05;
                                    %Natural frequency for ...
     reference model
80 zeta_ref=1;
                                    %Damping in prefilter
81 prefilter=ss([0 1;-omega_ref^2 ...
     -2*zeta_ref*omega_ref],[0;...
     omega_ref^2], eye(2), zeros(2,1));
                                    %Making state space for prefilter
84 [ref,¬]=lsim(prefilter,u_r,time...
    (1:end-1),[u_r(1);0]);
                                    %Simulate to get reference model
86 u_d=ref(:,1)';
                                    %Filtered desired value
87  u_d_dot=ref(:,2)';
                                    %Derivative of filtered ...
     desired value
90 x(:,1)=x_0;
                                    %Set x_0
91 for i=1:L
     if (mod(i, 100)) == 0
         Simulation progress in %
94
     end
95
     %Control algorithm
96
     e(:,i) = [x(6,i)-psi_d(i);...]
97
         x(3,i)-r_d(i);x(1,i)-u_d(i); %Error
98
99
     e_int(:,i+1)=e_int(:,i)+dt*e(:,i); %Error integrated
```

```
101
        %Heading
102
        \Delta_ff = (1/K) * r_d(i) + \dots
103
             (T/K)*r_d_dot(i);
                                                %Reference feed forward for ...
                heading
        \Delta_PID=-Kp*e(1,i)-Kd*...
104
             e(2,i)-Ki*e_int(1,i+1);
                                                %PID controller for heading
105
106
        %Surge
107
        n_c_ff=(1/Ksurge)*u_d(i)+...
108
109
             (Tsurge/Ksurge) *u_d_dot(i);
                                                %Reference feed forward for surge
        n_c=-Kp_surge*e(3,i)-(Kp_surge...
110
111
             /Ti_surge) *e_int(3,i+1);
                                                %PI controller for surge
112
        %Anti Windup
113
        if abs(n_c+n_c_ff)>n_c_max
114
             \Delta_{I}=-Ki*e_{int}(3,i+1)-(-Ki*e_{int}(3,i));
115
             if sign(\Delta_I) \neq sign(n_c+n_c_ff)
116
                 e_{int}(3,i+1) = e_{int}(3,i);
                                                          %Locks the integrator ...
117
                     if the
118
                      n_c = -Kp_surge * e(3, i) - ...
                                                         %Shaft speed reaches ...
                         max value
119
                      (Kp_surge/Ti_surge) ...
                      *e_int(3,i+1);
120
121
             end
122
        end
123
        %Set tau and send it to MS Fartoystyring
124
        tau(:,i) = [\Delta_ff + \Delta_PID... %Sets tau
125
            ;n_c_ff+n_c];
126
        x_{dot}=msfartoystyring(x(:,i),... %Send to MS Fartoystyring
127
128
            tau(:,i),1);
129
130
        %Integrate
131
        x(:,i+1)=x(:,i)+dt*x_dot;
                                                 %Integrates with forward Euler
132 end
```

```
'Lookahead-Based Steering', 'Exit');
         Steering method menu
no2=menu('Choose WP changing method','Circle of acceptance',...
      'Circle of acceptance ignoring cross-track error', 'Exit'); % WP ...
         changing menu
18 if no==3 || no2==3 % Exit?
      break
19
20 end
21 %Integration values
22 sim_time=2500;
                 %Simulation end time
23 dt=1;
                     %Steplength
24 L=sim_time/dt;
                     %Simulation steps
26 %System
27 K=-0.0598;
                     % Heading model gain
28 T=115.5667;
                     % Heading model time constant
                    % Surge model gain
29 Ksurge=0.9820;
30 Tsurge=450.8367;
                    % Surge model time constant
31
32 %User parameters
x_0 = [6.63, 0, 0, 0, 0, 0, 0]'; % Initial condition, x = [u v r x y psi]'
34 n_c_max=85*2*pi/60; % Max shaft velocity [rad/s]
35 \Delta_{max} = 25*pi/180; % max rudder angle [rad]
38 %Heading controller
39 zeta=1; % Damping coefficient
40 omega_b=0.03; % Bandwidth frequency
omega_n=omega_b/(sqrt(1-2*zeta^2+sqrt(4*zeta^4-4*zeta^2+2)));
     Natural frequency
42 Kp=(T/K)*omega_n^2;
                                % Heading controller proportional gain
42 Kp=(1/K) *0mega_.._,
43 Kd=(T/K) *2*zeta*omega_n-1/T;
                                % Heading controller derivative gain
44 Ki = (omega_n/10) *Kp;
                                % Heading controller integral gain
46 %Surge controller
                    % Surge controller proportional gain
47 Kp_surge=2.7388;
48 Ti_surge=Tsurge+50; % Surge controller integral time
51 time=zeros(1,L+1); % Time vector
                     % State vector, x = [ u v r x y psi]'
52 x=zeros(6,L+1);
53 tau=zeros(2,L);
                    % Input vector, tau = [\Delta n_c]'
                    % Control error vector, e = [psi¬ r¬ u¬]'
54 e=zeros(3,L);
                    % Integrated control error e_int = [psi¬_int ...
55 e_int=zeros(3,L);
     r-_int u-_int]'
56 LOS=zeros(2,L);
                    % LOS point for Enclosed-Based Steering, LOS = ...
     [xlos ylos]'
57 psi_r=zeros(1,L); % Requested heading
58 psi_d=zeros(3,L); % Filtered heading references psi_d = [psi_d ...
     psi_d_dot psi_d_ddot]'
59 u_r=zeros(1,L); % Requested surge speed
60 u_d=zeros(2,L);
                    % Filtered surge references u_d = [u_d u_d_dot]'
61
```

```
63 %Heading
omega_ref=0.15; % Natural frequency for reference model
65 zeta_ref=1; % Damping coefficient
66 A_h=[0 1 0;0 0 1;-omega_ref^3 -(2*zeta_ref+1)*omega_ref^2 ...
       -(2*zeta_ref+1)*omega_ref]; % Continous A matrix
67
                                 % Continous B matrix
68 B_h=[0;0;omega_ref^3];
69 psi_d_0 = [x_0(6) x_0(3) 0]'; % Initial state of filtered heading ...
       reference
70
71 %Surge
72 omega_ref=0.05; % Natural frequency for reference model
73 zeta_ref=1; % Damping coefficient
74 A_s=[0 1;-omega_ref^2 -2*zeta_ref*omega_ref];
                                                 % Continous A matrix
75 B_s=[0;omega_ref^2]; % Continous B matrix 76 u_d_0 = [x_0(1) 0]'; % Initial state of filtered surge references
77
78
79 x(:,1)=x_0;
                          % Set initial state
80 load('WP.mat');
                          % Load waypoints
                          % Next waypoint selector
81 k = 2;
82 R_LOS=4 * 305;
                          % LOS radius for Enclosed-Based steering
83 A_lookahead=3*305; % Lookahead distance for Lookahead-Based Steering
84 R = 2 * 305;
                          % Acceptance radius
85
87 AntiWU=zeros(2,L); % Anti wind-up log for the surge controller: 0 -> ...
       No action, 1 \rightarrow integrator hold, -1 \rightarrow Saturation, but no action, ...
       [AntiWU_heading AntiWU_surge]'
88 CurrentWP=zeros(1,L); % Current WP log
89 for i=1:L
90
       if (mod(i, 100)) == 0
           dispstat(sprintf('Progress %02d%%',round((i/L)*100)));
              Simulation progress in %
       end
       time(i+1)=time(i)+dt; % Update time vector
93
94
       %%%%%%% Waypoint selector %%%%%%%%
95
       if k < size(WP, 2) % More waypoints available?
96
                         % Circle of acceptance selected
           if no2==1
97
               if (((WP(1,k)-x(4,i))^2 + (WP(2,k)-x(5,i))^2) \le R^2)
98
                  k=k+1; % Select next waypoint
100
           error selected
102
               if NextWP(WP(:,k-1:k),x(4:5,i),R)
103
                  k=k+1; % Select next waypoint
104
               end
105
           else
               error('Invalid choice for WP changing method')
106
107
           end
108
       CurrentWP(i)=k; % Log current waypoint
```

```
110
111
        %%%%%%% Guidance system %%%%%%%%
112
        if no==1
                        % Enclosed-Based steering
113
            LOS(:,i) = LOSp(WP(:,k-1:k),x(4:5,i),R_LOS);
                Calculate LOS point
            Chi_d = atan2((LOS(2,i) - x(5,i)), (LOS(1,i) - x(4,i)));
114
                Calculate desired course
        elseif no==2
                        % Lookahead-Based steering
115
            Chi_d = Lookahead(WP(:,k-1:k),x(4:5,i),\Delta_lookahead); % ...
116
                Calculate desired course
117
        else
            error('Invalid choice for steering method')
118
119
120
        U_d = 6.63;
                            % Desired craft speed, constant
121
122
        %Mapping
        psi_r(i) = Chi_d;
123
                             % Requested heading
124
        u_r(i) = U_d;
                             % Requested surge speed
125
126
        %Prefilters
        if i==1 % First iteration, use initial state as psi_d_(i-1)
127
            psi_d(:,i) = (eye(3)+dt.*A_h)*psi_d_0+dt*B_h*psi_r(i);
128
                                                                             % ...
                Heading prefilter
129
            u_d(:,i) = (eye(2)+dt.*A_s)*u_d_0+dt*B_s*u_r(i);
                                                                             응 ...
                Surge prefilter
        else
130
            psi_d(:,i) = (eye(3)+dt.*A_h)*psi_d(:,i-1)+dt*B_h*psi_r(i);
131
                Heading prefilter
            u_d(:,i) = (eye(2)+dt.*A_s)*u_d(:,i-1)+dt*B_s*u_r(i);
                                                                             응 . . .
132
                Surge prefilter
        end
133
134
        %%%%%%% Control algorithm %%%%%%%%
        e(:,i) = [x(6,i) - psi_d(1,i);x(3,i) - psi_d(2,i);x(1,i) - u_d(1,i)]; % ...
            Control Error
        if i==1 % First iteration, use zero as e_int(i-1)
137
            e_{int}(:,i) = dt * e(:,i);
                                                  % Integrate error
138
139
        else
140
            e_{int}(:,i)=e_{int}(:,i-1)+dt*e(:,i); % Integrate error
        end
141
142
143
        %Heading controller
144
        \Delta_{ff} = (1/K) *psi_d(2,i) + (T/K) *psi_d(3,i);
                                                      % Heading reference ...
            feed forward
145
        \Delta_{PID}=-Kp*e(1,i)-Kd*e(2,i)-Ki*e_int(1,i); % Heading PID controller
146
147
        %Surge controller
148
        n_c_{ff} = (1/Ksurge) *u_d(1,i) + (Tsurge/Ksurge) *u_d(2,i);
            Surge reference feed forward
        n_c_{PI}=-Kp_surge*e(3,i)-(Kp_surge/Ti_surge)*e_int(3,i);
                                                                       응 ...
149
            Surge PI controller
150
151
        %Integrator Anti Wind-up
```

```
152
        %Heading
        if abs(\Delta_PID+\Delta_ff)>\Delta_max \&\& i>1 % Rudder saturated, and not ...
153
            first iteration
                                  % Log anti WU
154
            AntiWU(1,i)=-1;
            \Delta_{I}=-Ki*e_{int}(1,i)-(-Ki*e_{int}(1,i-1)); % Integrator direction
155
            if sign(\Delta_I) = sign(\Delta_PID + \Delta_ff) % Integrator direction is the ...
156
                same as the propellor speed (Integrates further into \dots
                saturation)
                 e_{int}(1,i) = e_{int}(1,i-1);
157
                                                            % Reset integrator ...
                     to previous value
                 \Delta_PID=-Kp*e(1,i)-Kd*e(2,i)-Ki*e_int(1,i);
158
                                                                  % Calculate ...
                     heading PID controller output again
                 AntiWU(1,i)=1; % Log anti WU
159
160
            end
161
        end
        %Surge
162
        if abs(n_c_PI+n_c_ff)>n_c_max && i>1
                                                   % Shaft speed saturated, ...
163
            and not first iteration
            AntiWU(2,i)=-1;
                                 % Log anti WU
164
165
            Δ_I=-(Kp_surge/Ti_surge) *e_int(3,i)-(-(Kp_surge/Ti_surge)...
166
                 *e_int(3,i-1)); % Integrator direction
167
            if sign(\Delta_I) = sign(n_c_PI + n_c_ff) % Integrator direction is ...
                the same as the propellor speed (Integrates further into ...
                saturation)
168
                 e_{int}(3,i) = e_{int}(3,i-1);
                                                        % Reset integrator to ...
                     previous value
                 n_c_PI=-Kp_surge*e(3,i)-(Kp_surge/Ti_surge)...
169
                     *e_int(3,i);
                                     % Calculate surge PI controller output ...
170
                         again
                 AntiWU(2,i)=1; % Log anti WU
171
            end
172
173
        end
174
175
        %%%%%%% MS Fartoystyring %%%%%%%%
176
        tau(:,i) = [\Delta_ff + \Delta_PID; n_c_ff + n_c_PI];
                                                 % Define input
177
        if tau(2,i)<0
                           % Ensure non-negative propellor speed, ...
            msfartoystyring crashes if n_c < 0
            tau(2,i)=0;
178
            warning(['Desired propellor speed was negative at iteration ' ...
179
                num2str(i) '. Modified to zero.'])
        end
180
        x_{dot} = msfartoystyring(x(:,i),tau(:,i),1); % Simulate ship with ...
181
            current
182
        %Integrate
183
184
        x(:,i+1)=x(:,i)+dt*x_dot;
185 end
186
187 pathplotter(x(4,:), x(5,:), x(6,:), dt, 50, 0, sim_time, 0, WP)
188
189 %%%%%%%% Optional plots %%%%%%%%
```

```
1 % TTK4190 - Guidance and Control
2 % Assignment 3
_{3} % 746072 - Bjorn-Olav H. Eiksen
4 % 746029 - Marius Hjertaker
5 % 705009 - Sveinung Ohrem
6 % 745621 - Ole Maurice Rabanal
8 % This is the code for task 2.6 of the assignment
10 clear; clc;
11 dispstat('', 'init')
      Simulation progress. Initialization. Does not print anything.
12 dispstat('run_task_2_6. Path-tracking, with transformed assignment',...
      'keepthis');
                                                             % Output first
14 no=menu('Choose steering method', 'Enclosure-Based Steering',...
      'Lookahead-Based Steering', 'Exit');
         Steering method menu
16 no2=menu('Choose WP changing method','Circle of acceptance',...
      'Circle of acceptance ignoring cross-track error', 'Exit'); % WP ...
         changing menu
18 if no==3 || no2==3 % Exit?
     break
20 end
21 %Integration values
22 sim_time=2700; %Simulation end time
23 dt=1;
                     %Steplength
24 L=sim_time/dt;
                     %Simulation steps
25
26 %System
27 K=-0.0598;
                     % Heading model gain
28 T=115.5667;
                     % Heading model time constant
29 Ksurge=0.9820;
                    % Surge model gain
30 Tsurge=450.8367;
                     % Surge model time constant
31
32 %User parameters
33 x_0=[6.63,0,0,0,0,0]; % Initial condition, x = [u v r x y psi]
34 n_c_max=85*2*pi/60; % Max shaft velocity [rad/s]
35 \Delta_{\text{max}} = 25 * \text{pi}/180; \% \text{ max rudder angle [rad]}
38 %Heading controller
39 zeta=1; % Damping coefficient
40 omega_b=0.03; % Bandwidth frequency
41 omega_n=omega_b/(sqrt(1-2*zeta^2+sqrt(4*zeta^4-4*zeta^2+2))); % ...
      Natural frequency
42 Kp=(T/K) * omega_n^2;
                                 % Heading controller proportional gain
43 Kd=(T/K)*2*zeta*omega_n-1/T; % Heading controller derivative gain
44 Ki = (omega_n/10) *Kp;
                                % Heading controller integral gain
46 %Surge controller
47 Kp_surge=2.7388; % Surge controller proportional gain
48 Ti_surge=Tsurge+50; % Surge controller integral time
```

```
51 time=zeros(1,L+1); % Time vector
x=zeros(6,L+1);
                      % State vector, x = [ u v r x y psi]'
53 tau=zeros(2,L);
                      % Input vector, tau = [\Delta n_c]'
                      % Control error vector, e = [psi¬ r¬ u¬]'
54 e=zeros(3,L);
55 e_int=zeros(3,L); % Integrated control error e_int = [psi¬_int ...
      r-_int u-_int]'
                     % LOS point for Enclosed-Based Steering, LOS = ...
56 LOS=zeros(2,L);
      [xlos ylos]'
57 psi_r=zeros(1,L);
                      % Requested heading
58 psi_d=zeros(3,L); % Filtered heading references psi_d = [psi_d ...
      psi_d_dot psi_d_ddot]'
                   % Requested surge speed
59  u_r=zeros(1,L);
60 u_d=zeros(2,L);
                      % Filtered surge references u_d = [u_d u_d_dot]'
63 %Heading
64 omega_ref=0.15; % Natural frequency for reference model
65 zeta_ref=1; % Damping coefficient
66 A_h=[0 1 0;0 0 1;-omega_ref^3 -(2*zeta_ref+1)*omega_ref^2 ...
      -(2*zeta_ref+1)*omega_ref]; % Continous A matrix
68 B_h=[0;0;omega_ref^3]; % Continous B matrix
69 psi_d_0 = [x_0(6) x_0(3) 0]'; % Initial state of filtered heading ...
      reference
70
71 %Surge
72 omega_ref=0.05; % Natural frequency for reference model
73 zeta_ref=1; % Damping coefficient
74 A_s=[0 1;-omega_ref^2 -2*zeta_ref*omega_ref]; % Continous A matrix
75 B_s=[0; omega_ref^2]; % Continous B matrix
76 u d 0 = [x 0(1) 0]'; % Initial state of fi
u_d_0 = [x_0(1) 0]';
                          % Initial state of filtered surge references
77
79 x(:,1)=x_0;
                          % Set initial state
80 load('WP.mat');
                          % Load waypoints
81 k = 2;
                          % Next waypoint selector
                          % LOS radius for Enclosed-Based steering
82 R_LOS=4*305;
83 \Delta_lookahead=3*305; % Lookahead distance for Lookahead-Based Steering
84 R = 2 * 305;
                          % Acceptance radius
85
86
87 AntiWU=zeros(2,L); % Anti wind-up log for the surge controller: 0 -> ...
      No action, 1 \rightarrow integrator hold, -1 \rightarrow Saturation, but no action, ...
      [AntiWU_heading AntiWU_surge]'
88 CurrentWP=zeros(1,L); % Current WP log
89 for i=1:L
90
      if (mod(i, 100)) == 0
91
          dispstat(sprintf('Progress %02d%%',round((i/L)*100)));
              Simulation progress in \mbox{\ensuremath{\$}}
92
      end
      time(i+1)=time(i)+dt; % Update time vector
93
94
      %%%%%%% Waypoint selector %%%%%%%%
95
```

```
if k < size(WP, 2) % More waypoints available?
            if no2==1
                          % Circle of acceptance selected
98
                if (((WP(1,k)-x(4,i))^2 + (WP(2,k)-x(5,i))^2) \le R^2)
99
                    k=k+1; % Select next waypoint
100
                end
            elseif no2==2  % Circle of acceptance ignoring cross-track ...
101
                error selected
                if NextWP(WP(:,k-1:k),x(4:5,i),R)
102
103
                    k=k+1; % Select next waypoint
104
                end
105
            else
106
                error('Invalid choice for WP changing method')
107
            end
108
        end
        CurrentWP(i)=k; % Log current waypoint
109
110
111
        %%%%%%% Guidance system %%%%%%%%%
112
        if no==1 % Enclosure-Based steering
                                                                          % ...
113
            LOS(:,i) = LOSp(WP(:,k-1:k),x(4:5,i),R_LOS);
               Calculate LOS point
            Chi_d = atan2((LOS(2,i) - x(5,i)), (LOS(1,i) - x(4,i)));
114
               Calculate desired course
        elseif no==2
                       % Lookahead-Based steering
116
            Chi_d = Lookahead(WP(:,k-1:k),x(4:5,i),\Delta_lookahead); % ...
               Calculate desired course
117
        else
            error('Invalid choice for steering method')
118
        end
119
        U_d = 6.63;
                           % Desired craft speed, constant
120
121
122
        %Mapping
123
        u=x(1,i);
124
        v=x(2,i);
125
        U=sqrt(u^2+v^2);
126
        beta=asin(v/U);
        psi_r(i) = Chi_d-beta; % Requested heading
127
128
129
        u_r(i) = sqrt(U_d^2-v^2);
                                        % Requested surge speed
130
131
        %Prefilters
        if i==1 % First iteration, use initial state as psi_d_(i-1)
132
133
            psi_d(:,i) = (eye(3)+dt.*A_h)*psi_d_0+dt*B_h*psi_r(i);
                                                                           응 ...
               Heading prefilter
            u_d(:,i) = (eye(2)+dt.*A_s)*u_d_0+dt*B_s*u_r(i);
                                                                           응 ...
                Surge prefilter
135
        else
136
            psi_d(:, i) = (eye(3) + dt.*A_h)*psi_d(:, i-1) + dt*B_h*psi_r(i);
                Heading prefilter
            u_d(:,i) = (eye(2)+dt.*A_s)*u_d(:,i-1)+dt*B_s*u_r(i);
137
                                                                           응 ...
                Surge prefilter
        end
138
139
        %%%%%%% Control algorithm %%%%%%%%
```

```
e(:,i) = [x(6,i)-psi_d(1,i);x(3,i)-psi_d(2,i);x(1,i)-u_d(1,i)];
141
            Control Error
142
        if i==1 % First iteration, use zero as e_int(i-1)
143
             e_{int}(:,i) = dt * e(:,i);
                                                    % Integrate error
144
        else
             e_int(:,i)=e_int(:,i-1)+dt*e(:,i); % Integrate error
145
146
147
148
        %Heading controller
        \Delta_{ff}=(1/K)*psi_d(2,i)+(T/K)*psi_d(3,i);
                                                         % Heading reference ...
149
            feed forward
        \Delta_{PID} = -Kp * e (1, i) - Kd * e (2, i) - Ki * e_int (1, i); % Heading PID controller
150
151
152
        %Surge controller
        n_c_{ff} = (1/Ksurge) *u_d(1,i) + (Tsurge/Ksurge) *u_d(2,i);
153
            Surge reference feed forward
        n_c_PI=-Kp_surge*e(3,i)-(Kp_surge/Ti_surge)*e_int(3,i);
154
            Surge PI controller
155
156
        %Integrator Anti Wind-up
157
        %Heading
        if abs(\Delta_{PID}+\Delta_{ff})>\Delta_{max \&\& i>1
158
                                               % Rudder saturated, and not ...
            first iteration
            AntiWU(1,i)=-1;
                                  % Log anti WU
159
             \Delta_{I}=-Ki*e_{int}(1,i)-(-Ki*e_{int}(1,i-1)); % Integrator direction
160
             if sign(\Delta_I) == sign(\Delta_PID+\Delta_ff) % Integrator direction is the ...
161
                 same as the propellor speed (Integrates further into ...
                 saturation)
                 e_{int}(1,i) = e_{int}(1,i-1);
                                                              % Reset integrator ...
162
                     to previous value
                 \Delta_PID=-Kp*e(1,i)-Kd*e(2,i)-Ki*e_int(1,i);
                                                                   % Calculate ...
163
                     heading PID controller output again
164
                 AntiWU(1,i)=1; % Log anti WU
165
             end
166
        end
167
        %Surge
        if abs(n_c_PI+n_c_ff)>n_c_max && i>1
168
                                                         % Shaft speed ...
            saturated, and not first iteration
                                  % Log anti WU
             AntiWU(2,i)=-1;
169
             \Delta_{I}=-(Kp\_surge/Ti\_surge)*e\_int(3,i)-(-(Kp\_surge/Ti\_surge)...
170
171
                 *e_int(3,i-1)); % Integrator direction
172
             if sign(\Delta_I) == sign(n_c_PI + n_c_ff)
                                                   % Integrator direction is ...
                the same as the propellor speed (Integrates further into ...
                 saturation)
                 e_{int}(3,i) = e_{int}(3,i-1);
                                                         % Reset integrator to ...
173
                     previous value
174
                 n_c_PI=-Kp_surge*e(3,i)-(Kp_surge/Ti_surge)...
175
                      *e_int(3,i);
                                      % Calculate surge PI controller output ...
                          again
                 AntiWU(2,i)=1; % Log anti WU
176
             end
177
178
        end
179
```

```
180
        %%%%%%% MS Fartoystyring %%%%%%%%
                                                % Define input
181
        tau(:,i) = [\Delta_ff + \Delta_PID; n_c_ff + n_c_PI];
                           % Ensure non-negative propellor speed, ...
182
        if tau(2,i)<0
           msfartoystyring crashes if n_c < 0
            tau(2,i)=0;
183
            warning(['Desired propellor speed was negative at iteration ' ...
184
                num2str(i) '. Modified to zero.'])
185
        end
        x_{dot}=msfartoystyring(x(:,i),tau(:,i),1); % Simulate ship with ...
186
           current
187
        %Integrate
        x(:,i+1)=x(:,i)+dt*x_dot;
189
190 end
191
192 pathplotter(x(4,:), x(5,:), x(6,:), dt, 50, 0, sim_time, 0, WP)
```

```
1 % TTK4190 - Guidance and Control
2 % Assignment 3
3 % 105334 - Bjorn-Olav H. Eiksen
4 % 746029 - Marius Hjertaker
5 % 705009 - Sveinung Ohrem
6 % 745621 - Ole Maurice Rabanal
8 % This is the code for task 2.7 of the assignment
10 clear; clc;
11 dispstat('','init')
      Simulation progress. Initialization. Does not print anything.
12 dispstat('run_task_2_7. Path-tracking','keepthis');
                                                              % Output first
14 %Integration values
15 sim_time=12000; % Simulation end time
16 dt=1;
                      % Steplength
17 L=sim_time/dt;
                      % Simulation steps
18
19 %System
20 K=-0.0261;
                      % Heading model gain, modified from -0.0598
21 T=261.348;
                       % Heading model time constant, modified from 115.5667
                      % Surge model gain
22 Ksurge=0.9820;
23 Tsurge=450.8367;
                      % Surge model time constant
25 %User parameters
26 load('WP.mat');
                           % Load waypoints
x_0=[6.63,0,0,0,0,0]; % Initial condition, x = [u v r x y psi]
                           % Max shaft velocity [rad/s]
28 n_c_max=85*2*pi/60;
29 \Delta_{max} = 25*pi/180; % max rudder angle [rad]
30 \text{ s\_d}=2 \times 305;
                           % Desired lateral distance
31 e_d=200;
                           % Desired cross-track error, e_d=0 causes the ...
      boat to line up with the target
U_a_max=4;
                           % Maximum approach speed
                           % Target speed
33 U_target=3;
```

```
34 target_0 = [WP(:,2)' atan2(WP(2,2)-WP(2,1),WP(1,2)-WP(1,1))]'; % ...
     Initial position target, target = [x_t y_t psi_t]'
37 %Heading controller
38 zeta=1; % Damping coefficient
39 omega_b=0.06; % Bandwidth frequency
40 omega_n=omega_b/(sqrt(1-2*zeta^2+sqrt(4*zeta^4-4*zeta^2+2))); % ...
     Natural frequency
41 Kp=(T/K)*omega_n^2;
                               % Heading controller proportional gain
                              % Heading controller derivative gain
42 Kd=(T/K) *2*zeta*omega_n-1/T;
43 Ki = (omega_n/10) *Kp;
                               % Heading controller integral gain
45 %Surge controller
46 Kp_surge=2.7388; % Surge controller proportional gain
47 Ti_surge=Tsurge+50; % Surge controller integral time
50 time=zeros(1,L+1); % Time vector
51 x=zeros(6,L+1); % State vector, x = [u v r x y psi]'
                   % Input vector, tau = [\Delta n_c]'
52 tau=zeros(2,L);
53 e=zeros(3,L); % Control error vector, e = [psi¬ r¬ u¬]'
54 e_int=zeros(3,L); % Integrated control error e_int = [psi¬_int ...
     r-_int u-_int]'
55 psi_r=zeros(1,L); % Requested heading
                   % Filtered heading references psi_d = [psi_d ...
56 psi_d=zeros(3,L);
     psi_d_dot psi_d_ddot]'
57 u_r=zeros(1,L); % Requested surge speed
58 u_d=zeros(2,L);
                   % Filtered surge references u_d = [u_d u_d_dot]'
59 target=zeros(3,L+1);% Target position target = [x_t y_t psi_t]'
60 track=zeros(2,L); % Tracking distance track = [s e]'
63 %Heading
omega_ref=0.15; % Natural frequency for reference model
65 zeta_ref=1; % Damping coefficient
66 A_h=[0 1 0;0 0 1;-omega_ref^3 -(2*zeta_ref+1)*omega_ref^2 ...
   -(2*zeta_ref+1)*omega_ref]; % Continous A matrix
68 B_h=[0;0;omega_ref^3]; % Continous B matrix
69 psi_d_0 = [x_0(6) x_0(3) 0]'; % Initial state of filtered heading ...
     reference
71 %Surge
72 omega_ref=0.05; % Natural frequency for reference model
73 zeta_ref=1; % Damping coefficient
74 A_s=[0 1;-omega_ref^2 -2*zeta_ref*omega_ref]; % Continous A matrix
75 B_s=[0;omega_ref^2]; % Continous B matrix
76 u_d_0 = [x_0(1) \ 0]'; % Initial state of filtered surge references
77
78
                        % Set initial state
79 x(:,1)=x_0;
80 target(:,1)=target_0; % Initial position target
81 A_lookahead=8*305; % Lookahead distance for Lookahead-Based Steering
```

```
82 \Delta_s=2400;
                        % Speed tuning parameter
84 AntiWU=zeros(2,L); % Anti wind-up log for the surge controller: 0 -> ...
       No action, 1 \rightarrow integrator hold, -1 \rightarrow Saturation, but no action, ...
        [AntiWU_heading AntiWU_surge]'
85 for i=1:L
        if \mod(i, 100) == 0
86
            dispstat(sprintf('Progress %02d%%', round((i/L)*100)));
87
                Simulation progress in %
        end
88
        time(i+1)=time(i)+dt; % Update time vector
89
        %%%%%%% Guidance system %%%%%%%%
        Chi_t=target(3,i);
                                                                    % Target ...
            heading
        R_p=[cos(Chi_t) -sin(Chi_t); sin(Chi_t) cos(Chi_t)];
93
            Tansformation matrix from ned to path-fixed frame
        track(:,i)=[s_d e_d]'+R_p'*[x(4,i)-target(1,i) ; ...
94
            x(5,i)-target(2,i)]; % Tracking error
95
96
        Chi_r = atan(-track(2,i)/\Delta_lookahead);
                                                                            응 ...
           Lookahead LOS steering law
        Chi_d = Chi_r + target(3,i); ...
                                                     % Desired course
        U_d = U_{target} - U_{a_max} (track(1,i)/sqrt(track(1,i)^2 + \Delta_s^2));
                                                                            응 ...
98
           Desired ship speed
aa
        %Mapping
100
        u=x(1,i);
                             % Surge speed
101
        v=x(2,i);
                             % Sway speed
102
103
        U=sqrt(u^2+v^2);
                             % Course speed
104
        beta=asin(v/U);
                            % Sideslip angle
105
106
        psi_r(i) = Chi_d-beta;
                                     % Requested heading
        u_r(i) = sqrt(U_d^2-v^2); % Requested surge speed
107
108
        %Prefilters
109
        if i==1 % First iteration, use initial state as psi_d_(i-1)
110
            psi_d(:,i) = (eye(3)+dt.*A_h)*psi_d_0+dt*B_h*psi_r(i);
111
                                                                            응 ...
                Heading prefilter
            u_d(:,i) = (eye(2)+dt.*A_s)*u_d_0+dt*B_s*u_r(i);
112
                                                                            응 . . .
                Surge prefilter
113
        else
            psi_d(:,i) = (eye(3)+dt.*A_h)*psi_d(:,i-1)+dt*B_h*psi_r(i);
                                                                            응 ...
                Heading prefilter
115
            u_d(:,i) = (eye(2)+dt.*A_s)*u_d(:,i-1)+dt*B_s*u_r(i);
                Surge prefilter
116
        end
117
        %%%%%%% Control algorithm %%%%%%%%
118
        e(:,i) = [x(6,i)-psi_d(1,i);x(3,i)-psi_d(2,i);x(1,i)-u_d(1,i)]; % ...
119
            Control Error
        if i==1 % First iteration, use zero as e_int(i-1)
```

```
121
             e_{int}(:,i) = dt * e(:,i);
                                                     % Integrate error
122
        else
123
             e_int(:,i)=e_int(:,i-1)+dt*e(:,i); % Integrate error
124
        end
125
        %Heading controller
126
                                                          % Heading reference ...
127
        \Delta_{ff}=(1/K)*psi_d(2,i)+(T/K)*psi_d(3,i);
            feed forward
        \Delta_{PID} = -Kp * e (1, i) - Kd * e (2, i) - Ki * e_int (1, i); % Heading PID controller
128
129
130
        %Surge controller
        n_c_{ff} = (1/Ksurge) *u_d(1,i) + (Tsurge/Ksurge) *u_d(2,i);
             Surge reference feed forward
        n_c_{PI}=-Kp_surge*e(3,i)-(Kp_surge/Ti_surge)*e_int(3,i);
132
            Surge PI controller
133
        %Integrator Anti Wind-up
134
135
        %Heading
136
        if abs(\Delta_{PID}+\Delta_{ff})>\Delta_{max \&\& i>1
                                             % Rudder saturated, and not ...
            first iteration
137
             AntiWU(1,i)=-1;
                                  % Log anti WU
             \Delta_{I}=-Ki*e_{int}(1,i)-(-Ki*e_{int}(1,i-1)); % Integrator direction
138
             if sign(\Delta_I) = sign(\Delta_PID + \Delta_ff) % Integrator direction is the ...
139
                 same as the propellor speed (Integrates further into ...
                 saturation)
140
                 e_{int}(1,i) = e_{int}(1,i-1);
                                                              % Reset integrator ...
                     to previous value
                 \Delta_PID=-Kp*e(1,i)-Kd*e(2,i)-Ki*e_int(1,i);
                                                                  % Calculate ...
141
                     heading PID controller output again
                 AntiWU(1,i)=1; % Log anti WU
142
             end
143
144
        end
145
        %Surge
146
        if abs(n_c_PI+n_c_ff)>n_c_max && i>1
                                                        % Shaft speed ...
            saturated, and not first iteration
                                  % Log anti WU
147
             AntiWU(2,i)=-1;
             \Delta_{I}=-(Kp\_surge/Ti\_surge)*e\_int(3,i)-(-(Kp\_surge/Ti\_surge)...
148
                 *e_int(3,i-1)); % Integrator direction
149
             if sign(\Delta_I) = sign(n_c_PI + n_c_ff) % Integrator direction is ...
150
                 the same as the propellor speed (Integrates further into ...
                 saturation)
                 e_{int}(3,i) = e_{int}(3,i-1);
                                                          % Reset integrator to ...
151
                     previous value
                 n_c_PI=-Kp_surge*e(3,i)-(Kp_surge/Ti_surge)...
153
                                      % Calculate surge PI controller output ...
                      *e_int(3,i);
                          again
154
                 AntiWU(2,i)=1; % Log anti WU
155
             end
        end
156
157
        %%%%%%% MS Fartoystyring %%%%%%%%
158
        tau(:,i) = [\Delta_ff + \Delta_PID; n_c_ff + n_c_PI];
                                                   % Define input
159
```

```
160
        if tau(2,i)<0
                          % Ensure non-negative propellor speed, ...
           msfartoystyring crashes if n_c < 0
           tau(2,i)=0;
161
            warning(['Desired propellor speed was negative at iteration ' ...
162
               num2str(i) '. Modified to zero.'])
        end
163
        x_{dot}=msfartoystyring(x(:,i),tau(:,i),0); % Simulate ship with ...
164
           current
165
        %Integrate
166
167
        x(:,i+1)=x(:,i)+dt*x_dot;
        target(:,i+1) = target(:,i) + dt*U_target*[cos(target(3,i)) ...
           sin(target(3,i)) 0]';
169 end
170
171 pathplotter(x(4,:), x(5,:), x(6,:), dt, 50, 0, sim_time, 1, WP)
```