

# Quantitative approach to strain modelling using Python, Numpy and Matplotlib

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- Concept of homogeneous deformation
- From finite to continuous deformation
- Superposition of deformations

# Components of deformation

A change in the configuration of a continuum body results in a displacement from an **initial or undeformed configuration** to a current or **deformed configuration**. The displacement of a body has two components:

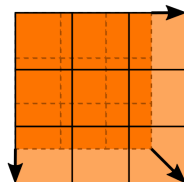
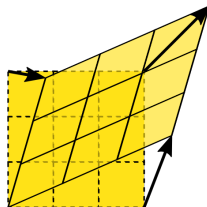
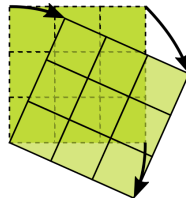
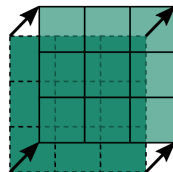
- **Rigid-body displacement**

- Translation
- Rotation

- **Deformation or strain**

- Distortion - isochoric change in shape
- Dilation - change in volume

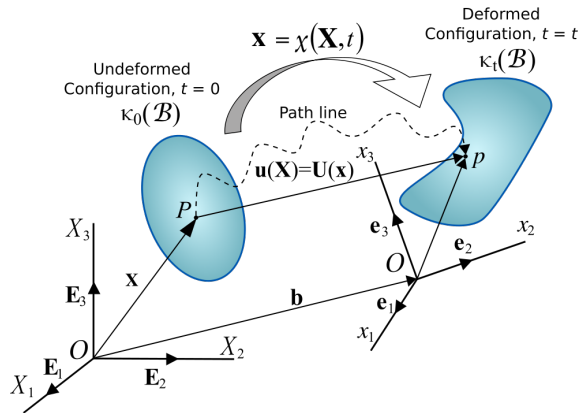
implies the change in shape and/or size of the body from an initial or undeformed configuration



# Kinematics of continuum body

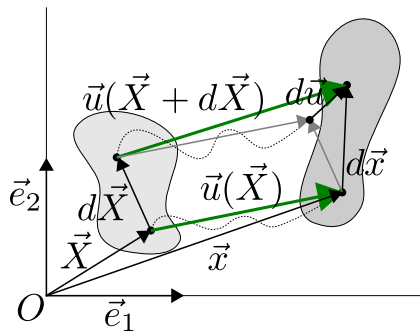
The motion of a continuum body is a **continuous** time sequence of displacements. Thus, the material body will occupy **different configurations** at different times so that a particle occupies a series of points in space which describe a **pathline**. There is **continuity** during deformation or motion of a continuum body in the sense that:

- The material points forming a closed curve at any instant will always form a closed curve at any subsequent time.
- The material points forming a closed surface at any instant will always form a closed surface at any subsequent time and the matter within the closed surface will always remain within.



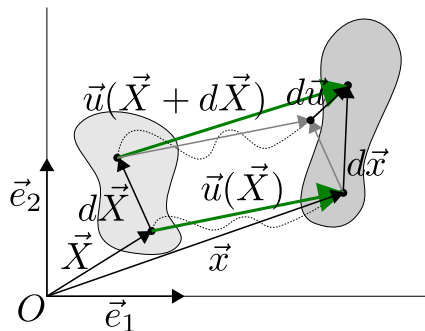
# Kinematics: deformation and motion I.

It is convenient to identify a **reference configuration** or **initial condition** which all subsequent **deformed configurations** are referenced from. Often, the configuration at  $t = 0$  is considered the reference configuration.



The components  $x_i$  of the position vector  $\vec{x}$  of a particle, taken with respect to the reference configuration, are called the **material or reference coordinates**.

# Kinematics of infinitesimal deformation I.



The displacement of first point is described as:

$$\vec{x} = \vec{X} + \vec{u}(\vec{X})$$

while displacement of second surrounding point is described as:

$$\vec{x} + d\vec{x} = \vec{X} + d\vec{X} + \vec{u}(\vec{X} + d\vec{X})$$

Substituting first equation into second we got:

$$\vec{X} + \vec{u}(\vec{X}) + d\vec{x} = \vec{X} + d\vec{X} + \vec{u}(\vec{X} + d\vec{X})$$

which simplifies to:

$$d\vec{x} = d\vec{X} + \vec{u}(\vec{X} + d\vec{X}) - \vec{u}(\vec{X})$$

## Detour on Taylor's theorem

Taylor's theorem states that any function that is infinitely differentiable may be represented by a Taylor series expansion:

$$f(X + dX) = f(X) + \frac{f'(X)}{1!}dX + \frac{f''(X)}{2!}dX^2 + \dots = \sum_{k=0}^{\infty} \frac{f^{(k)}(X)}{k!}dX^k$$

than

$$f(X + dX) - f(X) = \frac{f'(X)}{1!}dX + \frac{f''(X)}{2!}dX^2 + \dots = \sum_{k=0}^{\infty} \frac{f^{(k)}(X)}{k!}dX^k$$

neglecting higher terms as  $\left|d\vec{X}\right| \ll 1$  as  $dX^k$  is very small, it is:

$$f(X + dX) - f(X) = \frac{f'(X)}{1!}dX = (\nabla f)dX$$

where  $\nabla f$  is gradient of vector field.

# Kinematics of infinitesimal deformation II.

Using that for infinitesimal deformation equation

$$d\vec{x} = d\vec{X} + \vec{u}(\vec{X} + d\vec{X}) - \vec{u}(\vec{X})$$

it could be written in terms of gradient as:

$$d\vec{x} = d\vec{X} + (\nabla \mathbf{u})d\vec{X}$$

where  $\nabla \mathbf{u}$  is gradient of displacement field or **displacement gradient**.



# Displacement gradient

The **displacement gradient** is the derivative of each component of the linear element displacement  $d\vec{u}$  with respect to each component of the reference element  $d\vec{X}$ :

$$\nabla \mathbf{u} = u_{i,j} = \frac{\partial u_i}{\partial X_j} = \begin{bmatrix} \frac{\partial u_1}{\partial X_1} & \frac{\partial u_1}{\partial X_2} & \frac{\partial u_1}{\partial X_3} \\ \frac{\partial u_2}{\partial X_1} & \frac{\partial u_2}{\partial X_2} & \frac{\partial u_2}{\partial X_3} \\ \frac{\partial u_3}{\partial X_1} & \frac{\partial u_3}{\partial X_2} & \frac{\partial u_3}{\partial X_3} \end{bmatrix}$$

and characterise the local change of the displacement field at a material point with position vector  $\vec{X}$ . Knowing that:

$$d\vec{u} = d\vec{x} - d\vec{X}$$

it could be also written as:

$$d\vec{u} = (\nabla \mathbf{u})d\vec{X}$$

# Deformation gradient

Recalling that  $d\vec{u} = d\vec{x} - d\vec{X}$

$$(\nabla \mathbf{u}) = \frac{\partial u_i}{\partial X_j} = \frac{\partial (x_i - X_i)}{\partial X_j} = \frac{\partial x_i}{\partial X_j} - \frac{\partial X_i}{\partial X_j} = \mathbf{F} - \mathbf{I}$$

where  $\mathbf{F}$  is so called **deformation gradient**, i.e the derivative of each component of the deformed linear element  $d\vec{x}$  with respect to each component of the reference element  $d\vec{X}$ :

$$\mathbf{F} = x_{i,j} = \frac{\partial x_i}{\partial X_j} = \begin{bmatrix} \frac{\partial x_1}{\partial X_1} & \frac{\partial x_1}{\partial X_2} & \frac{\partial x_1}{\partial X_3} \\ \frac{\partial x_2}{\partial X_1} & \frac{\partial x_2}{\partial X_2} & \frac{\partial x_2}{\partial X_3} \\ \frac{\partial x_3}{\partial X_1} & \frac{\partial x_3}{\partial X_2} & \frac{\partial x_3}{\partial X_3} \end{bmatrix}$$

and characterizes the local deformation at a material point with position vector  $\vec{X}$ , assuming continuity. As

$$d\vec{u} = d\vec{x} - d\vec{X} = (\nabla \mathbf{u})d\vec{X} = (\mathbf{F} - \mathbf{I})d\vec{X} = \mathbf{F}d\vec{X} - d\vec{X}$$
$$d\vec{x} = \mathbf{F}d\vec{X}$$

# Properties of deformation gradient

**Deformation gradient**  $\mathbf{F}$  contains all the required local information about the changes in length, volumes and angles due to the deformation as follows:

- When vector  $\vec{N}$  in the reference configuration is deformed into the vector  $\vec{n}$ , these vectors are related as:  $\vec{n} = \mathbf{F}\vec{N}$
- The ratio between the local volume of the deformed configuration to the local volume in the reference configuration is equal to the determinant of the deformation gradient tensor:  $J = \det \mathbf{F}$
- Two infinitesimal areas with  $da$  and  $dA$  being their magnitudes and  $\vec{n}$  and  $\vec{N}$  are unit vectors perpendicular to them, then the relationship is given by:  $(da)\vec{n} = \det(\mathbf{F})(dA)\mathbf{F}^{-T}\vec{N}$
- An isochoric deformation is a deformation preserving local volume, i.e.,  $\det \mathbf{F} = 1$
- A deformation is called homogeneous if  $\mathbf{F}$  is constant at every point. Otherwise, the deformation is called non-homogeneous
- The physical restriction of possible deformation:  $\det \mathbf{F} > 0$

# Homogeneous deformation

A **homogeneous deformation** is one where the deformation gradient is uniform, i.e. independent of the coordinates, and the associated motion is termed **affine**. Every part of the material deforms as the whole does, and straight parallel lines in the reference configuration map to straight parallel lines in the deformed configuration.

$$x = aX + bY + t_X$$

$$y = cX + dY + t_Y$$

or in matrix form:

$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} X \\ Y \end{bmatrix} + \begin{bmatrix} t_X \\ t_Y \end{bmatrix}$$

Properties of homogeneous deformation are not spatially dependent.

# Deformation gradient

Without translation the homogeneous deformation (rotation and strain) could be described as:

$$x = aX + bY$$

$$y = cX + dY$$

$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} X \\ Y \end{bmatrix}$$

or

$$\vec{x} = \mathbf{F} \vec{X}$$

where  $\mathbf{F}$  is so called **deformation gradient**.

Note, that as we excluded translation, the origin of coordinates do not change during deformation:

$$\begin{bmatrix} 0 \\ 0 \end{bmatrix} = \mathbf{F} \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

# Displacement gradient

Displacement of particle is vector between initial and final position, i.e:

$$u = x - X = aX + bY - X = (a - 1)X + bY$$

$$v = y - Y = cX + dY - Y = cX + (d - 1)Y$$

$$\begin{bmatrix} u \\ v \end{bmatrix} = \begin{bmatrix} a - 1 & b \\ c & d - 1 \end{bmatrix} \begin{bmatrix} X \\ Y \end{bmatrix}$$

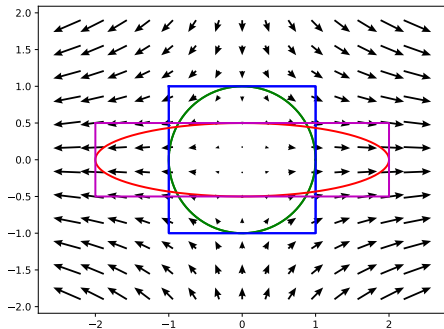
or

$$\vec{u} = (\mathbf{F} - \mathbf{I})\vec{X} = \nabla \mathbf{u} \vec{X}$$

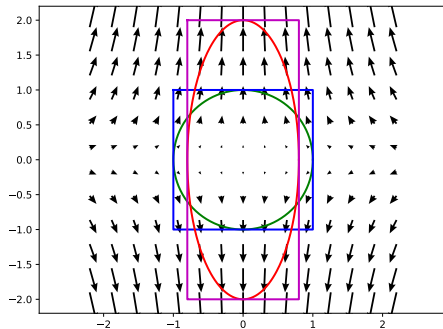
where  $\nabla \mathbf{u}$  is so called **displacement gradient**.

# Examples of pure shear

$$\mathbf{F} = \begin{bmatrix} 2 & 0 \\ 0 & 0.5 \end{bmatrix}$$
$$\nabla \mathbf{u} = \begin{bmatrix} 1 & 0 \\ 0 & -0.5 \end{bmatrix}$$

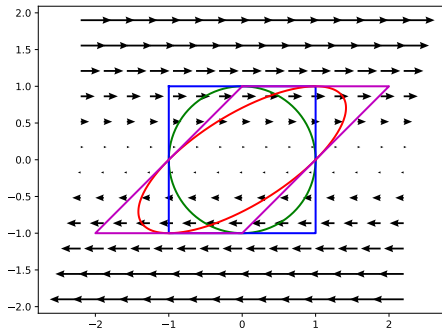


$$\mathbf{F} = \begin{bmatrix} 0.8 & 0 \\ 0 & 2 \end{bmatrix}$$
$$\nabla \mathbf{u} = \begin{bmatrix} -0.2 & 0 \\ 0 & 1 \end{bmatrix}$$

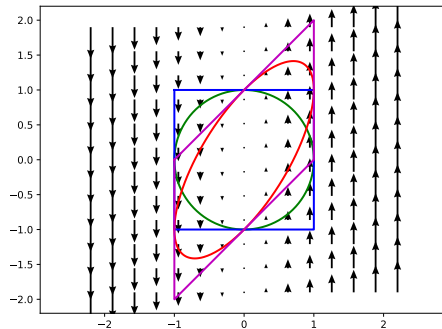


# Examples of simple shear

$$\mathbf{F} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$
$$\nabla \mathbf{u} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}$$



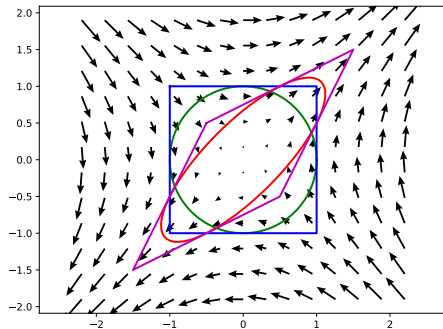
$$\mathbf{F} = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix}$$
$$\nabla \mathbf{u} = \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix}$$



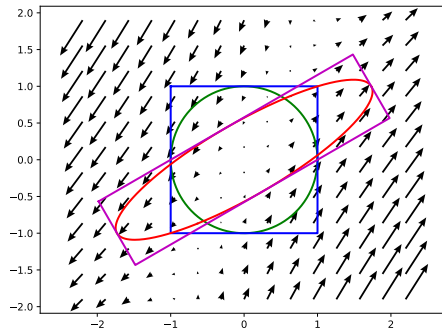


# Examples of general shear

$$\mathbf{F} = \begin{bmatrix} 1 & 0.5 \\ 0.5 & 1 \end{bmatrix}$$
$$\nabla \mathbf{u} = \begin{bmatrix} 0 & 0.5 \\ 0.5 & 0 \end{bmatrix}$$



$$\mathbf{F} = \begin{bmatrix} 1.732 & -0.25 \\ 1 & 0.433 \end{bmatrix}$$
$$\nabla \mathbf{u} = \begin{bmatrix} 0.732 & -0.25 \\ 1 & -0.567 \end{bmatrix}$$



## Time to think...

$\mathbf{F}$  maps any undeformed vector into its deformed state. This vector can also be a position vector of a point. Therefore  $\mathbf{F}$  also maps any point into its new position after deformation. Considering two successive deformations  $\mathbf{F}_1$  and  $\mathbf{F}_2$  write transformation equation....

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$$\vec{x}_1 = \mathbf{F}_1 \cdot \vec{X}$$

$$\vec{x}_2 = \mathbf{F}_2 \cdot \vec{x}_1$$

Substitute first equation to second gives:

$$\vec{x}_2 = \mathbf{F}_2 \cdot \mathbf{F}_1 \cdot \vec{X}$$

so

$$\vec{x}_2 = \mathbf{F} \cdot \vec{X}$$

where

$$\mathbf{F} = \mathbf{F}_2 \cdot \mathbf{F}_1$$

# Polar Decomposition I.

In last example the object has clearly been stretched and rotated. But by how much? the following two-step process of deformation followed by rigid body rotation gets you there...

$$\mathbf{F} = \begin{bmatrix} 1.732 & -0.25 \\ 1 & 0.433 \end{bmatrix} = \begin{bmatrix} \cos(30^\circ) & -\sin(30^\circ) \\ \sin(30^\circ) & \cos(30^\circ) \end{bmatrix} \begin{bmatrix} 2 & 0 \\ 0 & 0.5 \end{bmatrix}$$

or

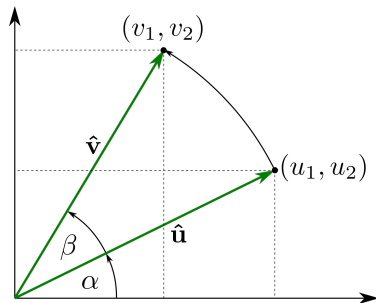
$$\mathbf{F} = \mathbf{R} \cdot \mathbf{U}$$

where  $\mathbf{R}$  is the **rotation matrix**, and  $\mathbf{U}$  is the **right stretch tensor** that is responsible for all the problems in life: stress, strain, fatigue, cracks, fracture, etc. Note that the process is read from right to left, not left to right.  $\mathbf{U}$  is applied first, then  $\mathbf{R}$ .

This partitioning of the **deformation gradient** into the product of a **rotation matrix** and **stretch tensor** is known as a **polar decomposition**.

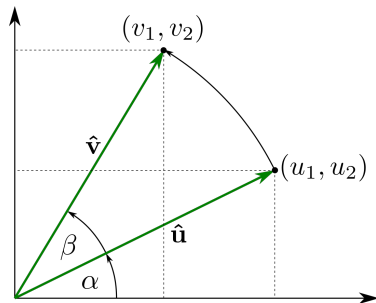
# Derivation of 2D rotation matrix

In order to rotate unit vector  $\hat{\mathbf{u}} = (u_1, u_2)$  to vector  $\hat{\mathbf{v}} = (v_1, v_2)$ , we can write following equations for  $\cos(\alpha)$ ,  $\sin(\alpha)$ ,  $\cos(\alpha + \beta)$  and  $\sin(\alpha + \beta)$ :



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$$\cos(\alpha) = u_1, \quad \sin(\alpha) = u_2$$

$$\cos(\alpha + \beta) = v_1, \quad \sin(\alpha + \beta) = v_2$$

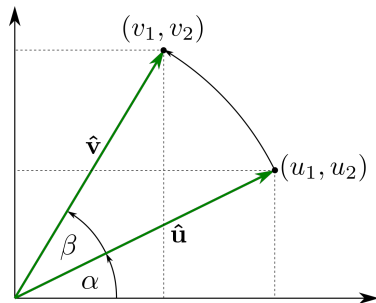
Substituting to the angle sum trigonometric identities:

$$\cos(\alpha + \beta) = \cos \alpha \cos \beta - \sin \alpha \sin \beta$$

$$\sin(\alpha + \beta) = \cos \alpha \sin \beta + \sin \alpha \cos \beta$$

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$$\cos(\alpha) = u_1, \quad \sin(\alpha) = u_2$$

$$\cos(\alpha + \beta) = v_1, \quad \sin(\alpha + \beta) = v_2$$

Substituting to the angle sum trigonometric identities:

$$\cos(\alpha + \beta) = \cos \alpha \cos \beta - \sin \alpha \sin \beta$$

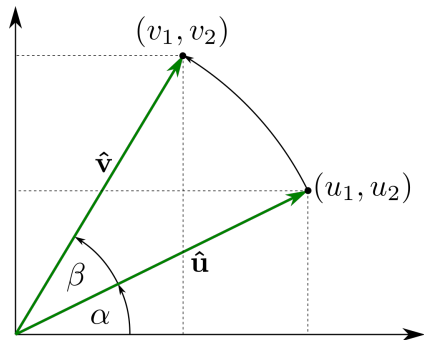
$$\sin(\alpha + \beta) = \cos \alpha \sin \beta + \sin \alpha \cos \beta$$

$$v_1 = u_1 \cos \beta - u_2 \sin \beta$$

$$v_2 = u_1 \sin \beta + u_2 \cos \beta$$

# Derivation of 2D rotation matrix

In order to rotate vector  $\hat{\mathbf{u}}$  by angle  $\beta$ , we can use the **rotation matrix  $\mathbf{R}$** :



$$v_1 = u_1 \cos \beta - u_2 \sin \beta$$

$$v_2 = u_1 \sin \beta + u_2 \cos \beta$$

or in matrix form

$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} \cos \beta & -\sin \beta \\ \sin \beta & \cos \beta \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

or

$$\hat{\mathbf{v}} = \mathbf{R} \cdot \hat{\mathbf{u}}$$



## Polar Decomposition II.

The deformed and rotated state could equally-well be arrived at by rotating it first, and then deforming it second. In this case, the reference configuration, is first rotated by the same  $30^\circ$  angle to arrive at an intermediate configuration and then the intermediate configuration is deformed to arrive at the final, deformed state.

The deformation gradient can be written as:

$$\mathbf{F} = \begin{bmatrix} 1.732 & -0.25 \\ 1 & 0.433 \end{bmatrix} = \begin{bmatrix} 1.625 & 0.65 \\ 0.65 & 0.875 \end{bmatrix} \begin{bmatrix} \cos(30^\circ) & -\sin(30^\circ) \\ \sin(30^\circ) & \cos(30^\circ) \end{bmatrix}$$

or

$$\mathbf{F} = \mathbf{V} \cdot \mathbf{R}$$

where  $\mathbf{R}$  is the same **rotation matrix**, and  $\mathbf{V}$  is the **left stretch tensor**.

## Polar Decomposition III.

It is relatively easy to develop a relationship between  $\mathbf{V}$  and  $\mathbf{U}$ . Since  $\mathbf{F} = \mathbf{V} \cdot \mathbf{R}$  and  $\mathbf{F} = \mathbf{R} \cdot \mathbf{U}$ , then

$$\mathbf{V} \cdot \mathbf{R} = \mathbf{R} \cdot \mathbf{U}$$

and post-multiplying through by  $\mathbf{R}^T$  gives

$$\mathbf{V} \cdot \mathbf{R} \cdot \mathbf{R}^T = \mathbf{R} \cdot \mathbf{U} \cdot \mathbf{R}^T$$

But since  $\mathbf{R} \cdot \mathbf{R}^T = \mathbf{I}$ , this leaves

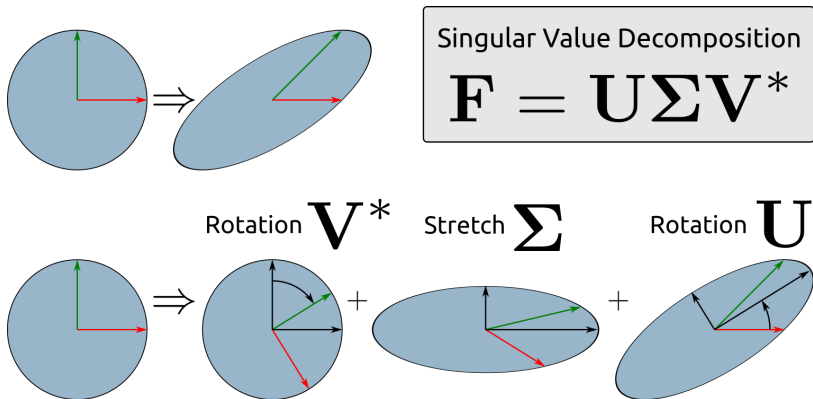
$$\mathbf{V} = \mathbf{R} \cdot \mathbf{U} \cdot \mathbf{R}^T$$

as the relationship between  $\mathbf{V}$  and  $\mathbf{U}$ . Alternatively, solving for  $\mathbf{U}$  gives

$$\mathbf{U} = \mathbf{R}^T \cdot \mathbf{V} \cdot \mathbf{R}$$

# Singular value decomposition

In linear algebra, the singular value decomposition (**SVD**) is a factorization of a real or complex matrix  $\mathbf{F} = \mathbf{U}\mathbf{\Sigma}\mathbf{V}^*$ . Thus the expression  $\mathbf{U}\mathbf{\Sigma}\mathbf{V}^*$  can be intuitively interpreted as a composition of three geometrical transformations: a **rotation or reflection**, a **scaling**, and another **rotation or reflection**.



Calculate orientation and axial ratio of strain ellipse for deformation gradient  $\mathbf{F}$  using SVD.

```
>>> from pylab import *

>>> F = array([[1, 1], [0, 1]]) # deformation gradient

>>> # calculate singular value decomposition
>>> U, s, V = svd(F)
>>> # calculate axial ratio and orientation
>>> ar = s[0]/s[1]
>>> ori = degrees(arctan2(U[1, 0], U[0, 0]))
>>> print('Orientation:{:g} AR:{:g}'.format(ori, ar))
Orientation:31.7175 AR:2.61803
```

## Detour on conic sections

In mathematics, a **conic section** is a curve obtained as the intersection of the surface of a cone with a plane. The three types of conic section are the **hyperbola**, the **parabola**, and the **ellipse**. The circle is a special case of the ellipse sometimes called a fourth type of conic section. Conic sections are the sets of points whose coordinates satisfy a second-degree polynomial equation:

$$Q(x, y) = Ax^2 + 2Bxy + Cy^2 + Dx + Ey + F = 0$$

can be written in matrix notation as:

$$\begin{bmatrix} x & y \end{bmatrix} \begin{bmatrix} A & B \\ B & C \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} + \begin{bmatrix} D & E \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} + F = 0$$

The the first three terms  $Ax^2 + 2Bxy + Cy^2$  is the **quadratic form** associated with the equation and defined by **matrix of the quadratic form**.

$$Ax^2 + 2Bxy + Cy^2 = \begin{bmatrix} x & y \end{bmatrix} \begin{bmatrix} A & B \\ B & C \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = x^T \mathbf{A}_Q x$$

Note that  $Q$  is an ellipse if and only if  $\det \mathbf{A}_Q > 0$ .

# Strain ellipse or ellipsoid

According to definition, the **strain ellipse** results from transformation of unit circle, which in matrix form is given by equation:

$$\begin{bmatrix} X & Y \end{bmatrix} \begin{bmatrix} X \\ Y \end{bmatrix} = X^T X = 1$$

The deformation gradient equation could be written in terms of deformed coordinates as:

$$X = \mathbf{F}^{-1}x$$

Substituting into equation of unit circle we obtain:

$$(\mathbf{F}^{-1}x)^T \cdot \mathbf{F}^{-1}x = x^T (\mathbf{F}^{-1})^T \cdot \mathbf{F}^{-1}x = x^T (\mathbf{F} \cdot \mathbf{F}^T)^{-1}x = x^T \mathbf{B}^{-1}x = 1$$

where matrix  $\mathbf{B} = \mathbf{F} \cdot \mathbf{F}^T$  is called **Finger** or **Left Cauchy-Green** deformation tensor. It's inverse  $\mathbf{B}^{-1}$  represents ellipse or ellipsoid and is commonly called **ellipsoid tensor** or **Cauchy deformation tensor**.

According to definition, the **reciprocal ellipse** is transformed to unit circle, which in matrix form is given by equation:

$$\begin{bmatrix} x & y \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = x^T x = 1$$

Substituting equation for deformation gradient  $x = \mathbf{F}X$  into equation of unit circle in deformed coordinates we obtain:

$$(\mathbf{F}X)^T \cdot \mathbf{F}X = X^T \mathbf{F}^T \cdot \mathbf{F}X = X^T \mathbf{C}X = 1$$

where matrix  $\mathbf{C} = \mathbf{F}^T \cdot \mathbf{F}$  is called **Green's** or **Right Cauchy-Green** deformation tensor.

# Deformation tensors and polar decomposition

Plugging the polar decomposition into equations for above defined deformation tensors gives a rather surprising result. Using  $\mathbf{F} = \mathbf{V} \cdot \mathbf{R}$ :

$$\mathbf{B} = \mathbf{F} \cdot \mathbf{F}^T = (\mathbf{V} \cdot \mathbf{R}) \cdot (\mathbf{V} \cdot \mathbf{R})^T = \mathbf{V} \cdot \mathbf{R} \cdot \mathbf{R}^T \cdot \mathbf{V}^T = \mathbf{V} \cdot \mathbf{V}^T$$

Using  $\mathbf{F} = \mathbf{R} \cdot \mathbf{U}$ :

$$\mathbf{C} = \mathbf{F}^T \cdot \mathbf{F} = (\mathbf{R} \cdot \mathbf{U})^T \cdot (\mathbf{R} \cdot \mathbf{U}) = \mathbf{U}^T \cdot \mathbf{R}^T \cdot \mathbf{R} \cdot \mathbf{U} = \mathbf{U}^T \cdot \mathbf{U}$$

As  $\mathbf{U}$  and  $\mathbf{V}$  are both symmetric, so  $\mathbf{U} = \mathbf{U}^T$  and  $\mathbf{U}^T \cdot \mathbf{U} = \mathbf{U} \cdot \mathbf{U}$ . Likewise  $\mathbf{V} = \mathbf{V}^T$  and  $\mathbf{V} \cdot \mathbf{V}^T = \mathbf{V} \cdot \mathbf{V}$ . Finally,  $\mathbf{U} \cdot \mathbf{U}$  is sometimes written as  $\mathbf{U}^2$  and  $\mathbf{V} \cdot \mathbf{V}$  is sometimes written as  $\mathbf{V}^2$ . Therefore:

$$\mathbf{B} = \mathbf{V}^2 \text{ and } \mathbf{C} = \mathbf{U}^2$$

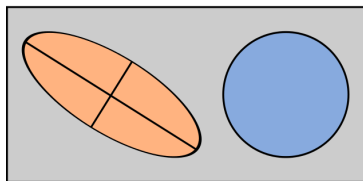
The surprising result here is that the rotation matrix,  $\mathbf{R}$ , has been eliminated from the problem in both cases.



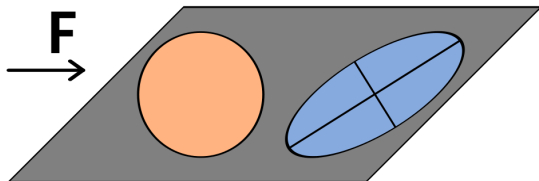
# Properties of strain and reciprocal deformation

The eigenvectors of  $\mathbf{B}$  define orientation of principal axes of the **strain ellipse/ellipsoid** in deformed state. The eigenvalues are quadratic elongations along principal directions, i.e. the lengths of semi-axes of the strain ellipse or ellipsoid are the square roots of the corresponding eigenvalues.

Reciprocal ellipse



Strain ellipse



The eigenvectors of  $\mathbf{C}$  define orientation of principal axes of the **reciprocal ellipse/ellipsoid** in undeformed state. The eigenvalues are quadratic elongations along principal directions, i.e. the lengths of semi-axes of the reciprocal ellipse or ellipsoid are the square roots of the corresponding eigenvalues.

# Actions of strain tensors

Consider two vectors in the reference configuration  $X_1$  and  $X_2$  which are mapped into the vectors  $x_1$  and  $x_2$  in the current configuration. Then for dot product:

$$x_1 \cdot x_2 = x_1^T x_2 = (\mathbf{F}X_1)^T \cdot \mathbf{F}X_2 = X_1^T \mathbf{F}^T \cdot \mathbf{F}X_2 = X_1^T \mathbf{C}X_2$$

Similarly for current configuration:

$$X_1 \cdot X_2 = X_1^T X_2 = (\mathbf{F}^{-1}x_1)^T \cdot \mathbf{F}^{-1}x_2 = x_1^T (\mathbf{F} \cdot \mathbf{F}^T)^{-1}x_2 = x_1^T \mathbf{B}^{-1}x_2$$

For dot product of vector with itself we can write:

$$x \cdot x = x^T x = (\mathbf{F}X)^T \cdot \mathbf{F}X = X^T \mathbf{F}^T \cdot \mathbf{F}X = X^T \mathbf{C}X$$

Similarly for current configuration:

$$X \cdot X = X^T X = (\mathbf{F}^{-1}x)^T \cdot \mathbf{F}^{-1}x = x^T (\mathbf{F} \cdot \mathbf{F}^T)^{-1}x = x^T \mathbf{B}^{-1}x$$

# Quadratic elongation

**Quadratic elongation**  $\lambda$  (square of the stretch) is defined as the square of ratio of the length of a deformed line element to the length of the corresponding undeformed line element:

$$\lambda = S^2 = \frac{|x|^2}{|X|^2}$$

As dot product of vector with itself is  $x \cdot x = x^T x = |x| |x| \cos(0) = |x|^2$ , the above equation could be written as:

$$\lambda_X = \frac{X^T \mathbf{C} X}{|X|^2} = \hat{X}^T \mathbf{C} \hat{X}$$

Similarly for  $X^T X = |X|^2$ :

$$\lambda_x^{-1} = \frac{x^T \mathbf{B}^{-1} x}{|x|^2} = \hat{x}^T \mathbf{B}^{-1} \hat{x}$$

where  $\hat{X} = \frac{X}{|X|}$  and  $\hat{x} = \frac{x}{|x|}$  are unit vector in the directions of  $X$  and  $x$ .

## Change of angle I.

The change in angle between any two vectors may also be given in terms of stretch. Let  $X_1$  and  $X_2$  be arbitrary vectors which become  $x_1$  and  $x_2$ , respectively, during a deformation. By the dot product,

$$x_1 \cdot x_2 = x_1^T x_2 = |x_1| |x_2| \cos(\theta)$$

we may compute the angle  $\theta$  between  $x_1$  and  $x_2$  from its cosine

$$\cos(\theta) = \frac{x_1 \cdot x_2}{|x_1| |x_2|} = \frac{X_1^T \mathbf{C} X_2}{|x_1| |x_2|} = \frac{X_1^T \mathbf{C} X_2}{\sqrt{X_1^T \mathbf{C} X_1} \sqrt{X_2^T \mathbf{C} X_2}}$$

Dividing both the numerator and denominator by the  $|X_1| |X_2|$  we got:

$$\cos(\theta) = \frac{\hat{X}_1^T \mathbf{C} \hat{X}_2}{S_{X_1} S_{X_2}}$$

where  $\hat{X}_1 = \frac{X_1}{|X_1|}$ ,  $\hat{X}_2 = \frac{X_2}{|X_2|}$  are unit vector in the directions of  $X_1$ ,  $X_2$ .

## Change of angle II.

Similarly for current configuration

$$X_1 \cdot X_2 = X_1^T X_2 = |X_1| |X_2| \cos(\phi)$$

we may compute the angle  $\phi$  between  $X_1$  and  $X_2$  from its cosine

$$\cos(\phi) = \frac{X_1 \cdot X_2}{|X_1| |X_2|} = \frac{x_1^T \mathbf{B}^{-1} x_2}{|X_1| |X_2|} = \frac{x_1^T \mathbf{B}^{-1} x_2}{\sqrt{x_1^T \mathbf{B}^{-1} x_1} \sqrt{x_2^T \mathbf{B}^{-1} x_2}}$$

Dividing both the numerator and denominator by the  $|x_1| |x_2|$  we got:

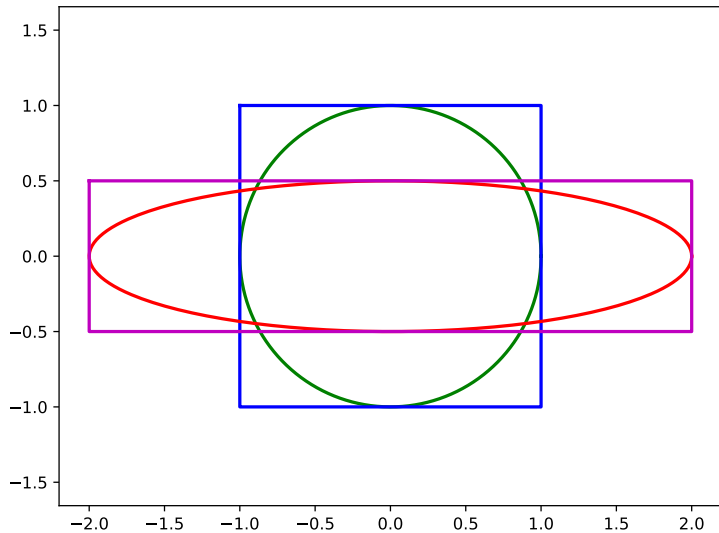
$$\cos(\phi) = \frac{\hat{x}_1^T \mathbf{B}^{-1} \hat{x}_2}{S_{x_1}^{-1} S_{x_2}^{-1}} = S_{x_1} S_{x_2} \hat{x}_1^T \mathbf{B}^{-1} \hat{x}_2$$

where  $\hat{x}_1 = \frac{x_1}{|x_1|}$ ,  $\hat{x}_2 = \frac{x_2}{|x_2|}$  are unit vector in the directions of  $x_1$ ,  $x_2$ .

Lets try to visualize how unit circle deforms during homogeneous deformation:

```
# parametric definition of unit circle
theta = linspace(0, 2*pi, 300)
c = cos(theta), sin(theta)
s = [-1, 1, 1, -1, -1], [1, 1, -1, -1, 1]
plot(c[0], c[1], 'g', s[0], s[1], 'b', lw=2)
# Apply deformation gradient and plot ellipse
F = array([[2, 0], [0, 0.5]])
e = dot(F, c)
q = dot(F, s)
plot(e[0], e[1], 'r', q[0], q[1], 'm', lw=2)
axis('equal')
```

# Python exercise



# Python exercise

To visualize displacement field we have to calculate it for points on regular grid and plot it using command **quiver**.

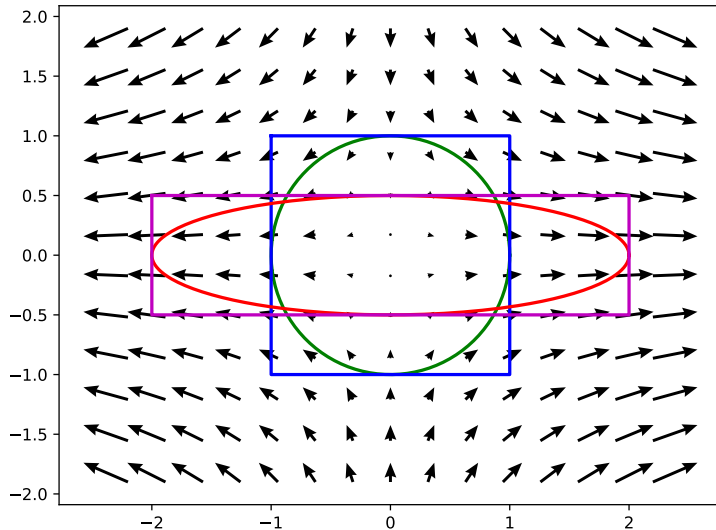
```
# create rectangular grid
X = meshgrid(linspace(-2.2, 2.2, 15),
             linspace(-1.9, 1.9, 12))

# calculate displacements
J = F - eye(2)
u = tensordot(J, X, axes=1)

# plot
quiver(X[0], X[1], u[0], u[1],
       angles='xy', lw=0.5, headwidth=4)
plot(c[0], c[1], 'g', s[0], s[1], 'b',
     e[0], e[1], 'r', q[0], q[1], 'm', lw=2)
axis('equal')
```



# Python exercise



Find orientation and axial ratio of strain ellipse for deformation gradient  $\mathbf{F}$ .

```
>>> from pylab import *
>>> # deformation gradient
>>> F = array([[1, 1], [0, 1]])
>>> # calculate Left Cauchy-Green deformation tensor
>>> B = dot(F, F.T)
>>> s, U = eig(B)
>>> # calculate axial ratio and orientation
>>> ar = sqrt(s[0]/s[1])
>>> ori = degrees(arctan2(U[1, 0], U[0, 0]))
>>> print('Orientation:{:g} AR:{:g}'.format(ori, ar))
Orientation:31.7175 AR:2.61803
```

# Superposed strain

Similarly, we can obtain ellipse or ellipsoid equation resulting from two superposed deformation. When first deformation  $\mathbf{F}_1$  results in intermediate ellipse or ellipsoid  $\mathbf{B}_1$ , i.e.:

$$x^T \mathbf{B}_1^{-1} x = 1$$

then substituting equation for deformation  $\mathbf{D}_2$  we obtain:

$$x^T \mathbf{F}_2^{-T} \mathbf{B}_1^{-1} \mathbf{F}_2^{-1} x = x^T \mathbf{B}_{12}^{-1} x$$

where  $\mathbf{B}_{12}^{-1}$  is:

$$\begin{aligned} \mathbf{B}_{12}^{-1} &= \mathbf{F}_2^{-T} \mathbf{B}_1^{-1} \mathbf{F}_2^{-1} \\ &= \mathbf{F}_2^{-T} \mathbf{F}_1^{-T} \mathbf{F}_1^{-1} \mathbf{F}_2^{-1} \\ &= (\mathbf{F}_2 \mathbf{F}_1)^{-T} (\mathbf{F}_2 \mathbf{F}_1)^{-1} \\ &= \mathbf{F}_{12}^{-T} \mathbf{F}_{12}^{-1} \end{aligned}$$

where  $\mathbf{F}_{12} = \mathbf{F}_2 \mathbf{F}_1$ . Consequently  $\mathbf{B}_{12}$  could be written as

$$\mathbf{B}_{12} = \mathbf{F}_{12} \mathbf{F}_{12}^T$$

# Python exercise - our first library

Function to plot unit circle and strain ellipse from deformation gradient:

```
import numpy as np
import matplotlib.pyplot as plt

def def_ellipse(F):
    # Draw ellipse from deformation gradient
    theta = np.linspace(0, 2*np.pi, 180)
    c = np.cos(theta), np.sin(theta)
    e = np.dot(F, c)
    plt.plot(c[0], c[1], 'r', e[0], e[1], 'g')
    plt.axis('equal')
```

Function to visualize displacement field from displacement gradient:

```
def dis_field(J):  
    # Visualize displacement gradient  
    X = np.meshgrid(np.linspace(-3, 3, 21),  
                    np.linspace(-2, 2, 17))  
    u = u = tensordot(J, X, axes=1)  
    plt.quiver(X[0], X[1], u[0], u[1], angles='xy')
```

Function to plot unit circle and strain ellipse from displacement gradient:

```
def dis_ellipse(J):  
    # Draw ellipse from displacement gradient  
    F = np.asarray(J) + np.eye(J.ndim)  
    dis_ellipse(F)
```

Function to visualize displacement field from deformation gradient:

```
def def_field(F):  
    # Visualize deformation gradient  
    J = np.asarray(F) - np.eye(F.ndim)  
    dis_field(J)
```

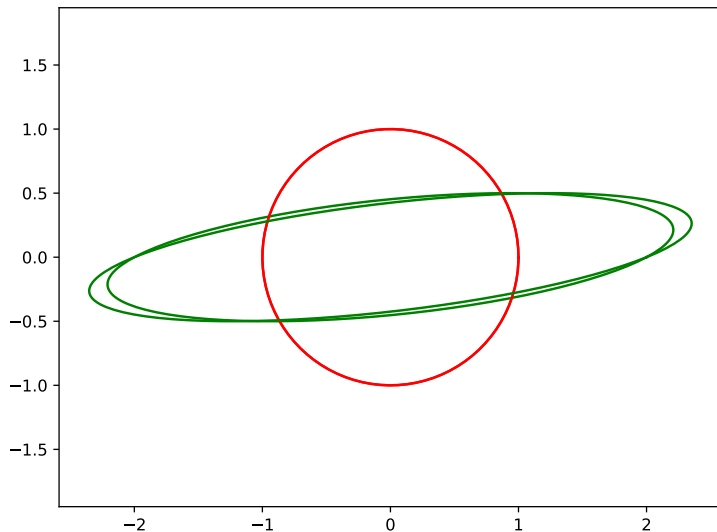
# Python exercise

Script to simulate simultaneous simple and pure shear by mutual combination of incremental deformations:

```
n = 5  # number of increments
SS = np.array([[1, 1./n], [0, 1]])  # simple shear increment
PS = np.array([[2**(1./n), 0], [0, 0.5**(1/n)]])  # pure shear increment
# initial stage
F1 = F2 = np.array([[1,0],[0,1]])
# both orders of superpositions of increments
for i in range(n):
    F1 = np.dot(SS, np.dot(PS, F1))
    F2 = np.dot(PS, np.dot(SS, F2))

def_ellipse(F1)
def_ellipse(F2)
```

# Python exercise





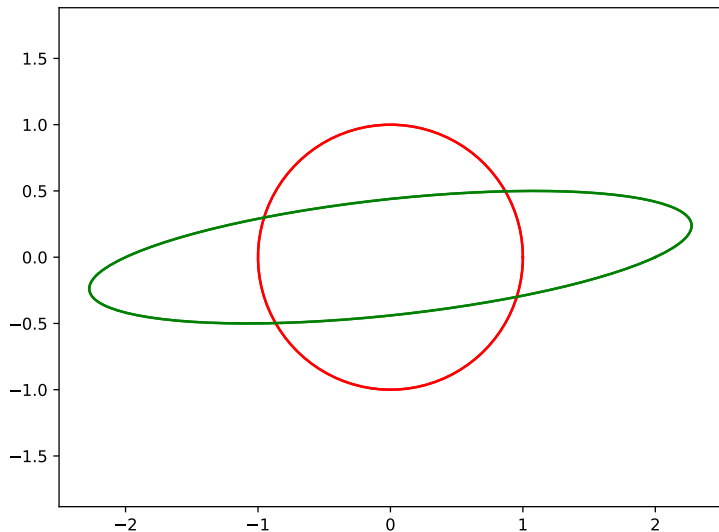
# Python exercise

Script to simulate simultaneous simple and pure shear by mutual combination of incremental deformations:

```
n = 500  # number of increments
SS = np.array([[1, 1./n], [0, 1]])  # simple shear increment
PS = np.array([[2**(1./n), 0], [0, 0.5**(1/n)]])  # pure shear increment
# initial stage
F1 = F2 = np.array([[1,0],[0,1]])
# both orders of superposition
for i in range(n):
    F1 = np.dot(SS, np.dot(PS, F1))
    F2 = np.dot(PS, np.dot(SS, F2))

def_ellipse(F1)
def_ellipse(F2)
```

# Python exercise



## Volume change and area change I.

Consider an infinitesimal volume element  $(dX_1, dX_2, dX_3)$  in the reference configuration  $(\mathbf{E}_1, \mathbf{E}_2, \mathbf{E}_3)$  so the vectors representing the edges of the element are  $d\mathbf{X}_1 = dX_1 \mathbf{E}_1$ ;  $d\mathbf{X}_2 = dX_2 \mathbf{E}_2$ ;  $d\mathbf{X}_3 = dX_3 \mathbf{E}_3$ . The volume of the element is given by triple product of it's edges:

$$dV = d\mathbf{X}_1 \cdot (d\mathbf{X}_2 \times d\mathbf{X}_3) = dX_1 dX_2 dX_3 \mathbf{E}_1 \cdot (\mathbf{E}_2 \times \mathbf{E}_3) = dX_1 dX_2 dX_3$$

Upon deformation, these edges go to  $(d\mathbf{x}_1, d\mathbf{x}_2, d\mathbf{x}_3)$  where:

$$d\mathbf{x}_1 = \mathbf{F} \cdot d\mathbf{X}_1 = \left[ \frac{\partial x_i}{\partial X_j} \right] \cdot d\mathbf{X}_1 = dX_1 \left[ \frac{\partial x_i}{\partial X_j} \right] \cdot \mathbf{E}_1 = dX_1 \left[ \frac{\partial x_i}{\partial X_1} \right]$$

$$d\mathbf{x}_2 = \mathbf{F} \cdot d\mathbf{X}_2 = \left[ \frac{\partial x_i}{\partial X_j} \right] \cdot d\mathbf{X}_2 = dX_2 \left[ \frac{\partial x_i}{\partial X_j} \right] \cdot \mathbf{E}_2 = dX_2 \left[ \frac{\partial x_i}{\partial X_2} \right]$$

$$d\mathbf{x}_3 = \mathbf{F} \cdot d\mathbf{X}_3 = \left[ \frac{\partial x_i}{\partial X_j} \right] \cdot d\mathbf{X}_3 = dX_3 \left[ \frac{\partial x_i}{\partial X_j} \right] \cdot \mathbf{E}_3 = dX_3 \left[ \frac{\partial x_i}{\partial X_3} \right]$$

## Volume change and area change II.

The deformed volume is given by triple product of deformed edges:

$$dv = d\mathbf{x}_1 \cdot (d\mathbf{x}_2 \times d\mathbf{x}_3) = \left[ \frac{\partial x_i}{\partial X_1} \right] \cdot \left( \left[ \frac{\partial x_i}{\partial X_2} \right] \times \left[ \frac{\partial x_i}{\partial X_3} \right] \right) dX_1 dX_2 dX_3$$

Knowing that scalar triple product can also be understood as the determinant of the  $3 \times 3$  matrix also known as **Jacobian of the deformation gradient**:

$$\left[ \frac{\partial x_i}{\partial X_1} \right] \cdot \left( \left[ \frac{\partial x_i}{\partial X_2} \right] \times \left[ \frac{\partial x_i}{\partial X_3} \right] \right) = \det \left( \left[ \frac{\partial x_i}{\partial X_j} \right] \right) = \det (\mathbf{F}) = J$$

Therefore:

$$dv = \det (\mathbf{F}) dV = J dV$$

## Area change - Nanson's formula

**Nanson's formula** is an important relation that can be used to go from areas in the current configuration to areas in the reference configuration and vice versa. Using area elements ( $d\mathbf{A} = dA \mathbf{N}$ ;  $d\mathbf{a} = da \mathbf{n}$ ) and above derived equation for volume change, we can write:

$$dv = J dV$$

$$d\mathbf{l} \cdot d\mathbf{a} = J d\mathbf{L} \cdot d\mathbf{A}$$

$$\mathbf{F} \cdot d\mathbf{L} \cdot d\mathbf{a} = J d\mathbf{L} \cdot d\mathbf{A}$$

$$d\mathbf{L} \cdot (\mathbf{F}^T \cdot d\mathbf{a}) = d\mathbf{L} \cdot J d\mathbf{A}$$

$$\mathbf{F}^T \cdot d\mathbf{a} = J d\mathbf{A}$$

$$d\mathbf{a} = J \mathbf{F}^{-T} \cdot d\mathbf{A}$$

$$da \mathbf{n} = \det(\mathbf{F}) dA \mathbf{F}^{-T} \cdot \mathbf{N}$$

where  $da$  is an area of a region in the current configuration,  $dA$  is the same area in the reference configuration, and  $\mathbf{n}$  is the outward normal to the area element in the current configuration while  $\mathbf{N}$  is the outward normal in the reference configuration.

Script to volume change and area changes in principal coordinate planes:

```
>>> F = array([[1, 0, 1],[0, 2, 0],[0, 0, 0.5]])
>>> print('Volume change: {:.0%}'.format(det(F) - 1))
Volume change: 0%
>>> dA1, dA2, dA3 = eye(3)  # unit length basis vectors
>>> da = lambda n: norm(dot(det(F)*inv(F).T, n))
>>> tmpl = 'Area change within plane {}: {:.0%}'
>>> print(tmpl.format(dA1, da(dA1) - 1))
Area change within plane [1. 0. 0.]: 124%
>>> print(tmpl.format(dA2, da(dA2) - 1))
Area change within plane [0. 1. 0.]: -50%
>>> print(tmpl.format(dA3, da(dA3) - 1))
Area change within plane [0. 0. 1.]: 100%
```

# Velocity gradient I.

Velocity gradients are absolutely essential to analyses involving path dependent materials and are useful to better understanding deformations. The **velocity gradient** is to velocities what the deformation gradient is to displacements. The **velocity gradient** is used as a measure of the rate at which a material is deforming. Consider two fixed neighbouring points,  $x$  and  $x + dx$ . The velocities of the material particles at these points at any given time instant are  $\mathbf{v}(x)$  and  $\mathbf{v}(x + dx)$ , and

$$\mathbf{v}(x + dx) = \mathbf{v}(x) + \frac{\partial \mathbf{v}}{\partial x} dx$$

The relative velocity between the points is

$$d\mathbf{v} = \frac{\partial \mathbf{v}}{\partial x} dx = \mathbf{L} dx$$

where  $\mathbf{L}$  is defined to be the **spatial velocity gradient**.

## Velocity gradient II.

The **spatial velocity gradient**  $\mathbf{L}$  is defined as:

$$\mathbf{L} = \frac{\partial v_i}{\partial x_j} = \begin{bmatrix} \frac{\partial v_1}{\partial x_1} & \frac{\partial v_1}{\partial x_2} & \frac{\partial v_1}{\partial x_3} \\ \frac{\partial v_2}{\partial x_1} & \frac{\partial v_2}{\partial x_2} & \frac{\partial v_2}{\partial x_3} \\ \frac{\partial v_3}{\partial x_1} & \frac{\partial v_3}{\partial x_2} & \frac{\partial v_3}{\partial x_3} \end{bmatrix}$$

Note that the derivative is with respect to the current coordinates,  $x$ , not the reference coordinates  $X$ .



## Velocity gradient III.

Calculations that involve the time-dependent deformation of a body often require a time derivative of the deformation gradient to be calculated. The time derivative of  $\mathbf{F}$  is:

$$\dot{\mathbf{F}} = \frac{\partial \mathbf{F}}{\partial t} = \frac{\partial}{\partial t} \frac{\partial \mathbf{x}}{\partial \mathbf{X}} = \frac{\partial}{\partial \mathbf{X}} \frac{\partial \mathbf{x}}{\partial t} = \frac{\partial}{\partial \mathbf{X}} \mathbf{v} = \frac{\partial \mathbf{v}}{\partial \mathbf{X}}$$

where  $\mathbf{v}$  is the velocity in reference frame and the derivative on the right hand side represents a *material velocity gradient*. It is common to convert that into a spatial gradient applying the chain rule to the above result, i.e.,

$$\dot{\mathbf{F}} = \frac{\partial \mathbf{v}}{\partial \mathbf{X}} = \frac{\partial \mathbf{v}}{\partial \mathbf{x}} \cdot \frac{\partial \mathbf{x}}{\partial \mathbf{X}} = \mathbf{L} \cdot \mathbf{F}$$

where  $\mathbf{L}$  is the *spatial velocity gradient*. Post multiplying both sides by  $\mathbf{F}^{-1}$  gives the equation for  $\mathbf{L}$  in terms of  $\mathbf{F}$ :

$$\mathbf{L} = \dot{\mathbf{F}} \cdot \mathbf{F}^{-1}$$

## Velocity gradient IV.

If the **spatial velocity gradient** is constant, the above equation can be solved exactly using *matrix exponential*:

$$\mathbf{F} = e^{\mathbf{L}t}$$

where  $t$  is time. Similarly, the spatial velocity gradient could be calculated from deformation gradient using *matrix logarithm*:

$$\mathbf{L} = \ln(\mathbf{F})$$

We can use these equation to calculate deformation gradient for any intermediate deformation. When deformation in time  $t = 1$  is defined by  $\mathbf{F}$ , than for any time  $t = [0, 1]$ :

$$\mathbf{F}(t) = e^{\ln(\mathbf{F})t}$$

# Decomposition of velocity gradient

The **spatial velocity gradient** can be decomposed into symmetric and antisymmetric parts as follows.

$$\mathbf{L} = \frac{1}{2} (\mathbf{L} + \mathbf{L}^T) + \frac{1}{2} (\mathbf{L} - \mathbf{L}^T) = \mathbf{D} + \mathbf{W}$$

The first symmetric term is called **rate of deformation tensor** ( $\mathbf{D}$ ), while second antisymmetric term is known as **spin tensor** ( $\mathbf{W}$ ).

$$\mathbf{D} = \begin{bmatrix} \dot{\epsilon}_{xx} & \dot{\gamma}_{xy} & \dot{\gamma}_{xz} \\ \dot{\gamma}_{xy} & \dot{\epsilon}_{yy} & \dot{\gamma}_{yz} \\ \dot{\gamma}_{xz} & \dot{\gamma}_{yz} & \dot{\epsilon}_{zz} \end{bmatrix}$$

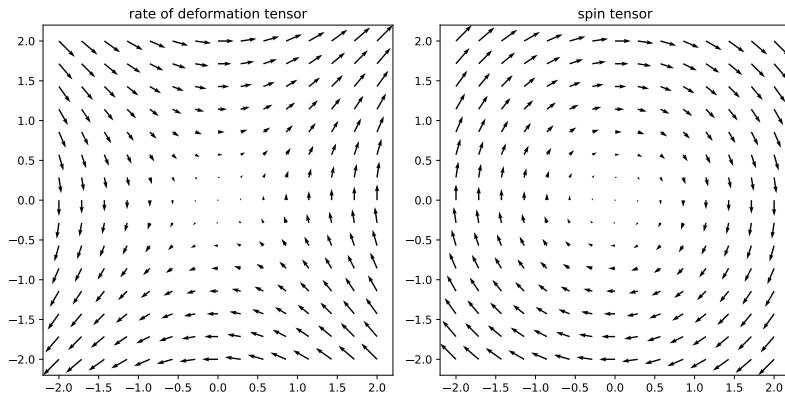
where 6 independent components are referred as **stretching and shearing strain rates**.

$$\mathbf{W} = \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix}$$

where  $\boldsymbol{\omega} = (\omega_1, \omega_2, \omega_3) = \frac{d\phi}{dt} \mathbf{u}$  is the angular velocity vector defining rate of rotation  $\frac{d\phi}{dt}$  about an axis  $\mathbf{u}$ .

Lets visualize symmetric and antisymmetric parts of L for simple shear:

```
import scipy.linalg as la
X = meshgrid(linspace(-2, 2, 15), linspace(-2, 2, 15))
F = array([[1, 1], [0, 1]])
L = la.logm(F)
D, W = (L + L.T)/2, (L - L.T)/2
f, (ax1, ax2) = plt.subplots(1,2,figsize=(10, 6))
u = tensordot(D, X, axes=1)
ax1.quiver(X[0], X[1], u[0], u[1], angles='xy')
ax1.set_aspect('equal', adjustable='box')
ax1.set_title('rate of deformation tensor')
u = tensordot(W, X, axes=1)
ax2.quiver(X[0], X[1], u[0], u[1], angles='xy')
ax2.set_aspect('equal', adjustable='box')
ax2.set_title('spin tensor')
```



**Figure:** Velocity field for symmetric and antisymmetric parts of  $\mathbf{L}$  for simple shear with  $\gamma = 1$ .

# Python exercise

Script to plot evolution of axial ratio of finite strain ellipse during progressive deformation:

```
gdot = 1e-14
yearsec = 365.25*24*3600
times = linspace(0, 5, 100)[1:]
ar = []
L = array([[0, gdot], [0, 0]])
for t in times:
    F = la.expm(L*t*1e6*yearsec)
    U, s, V = svd(F)
    ar.append(s.max()/s.min())

plot(times, ar)
xlabel('Time [Ma]')
ylabel('Axial ratio')
```

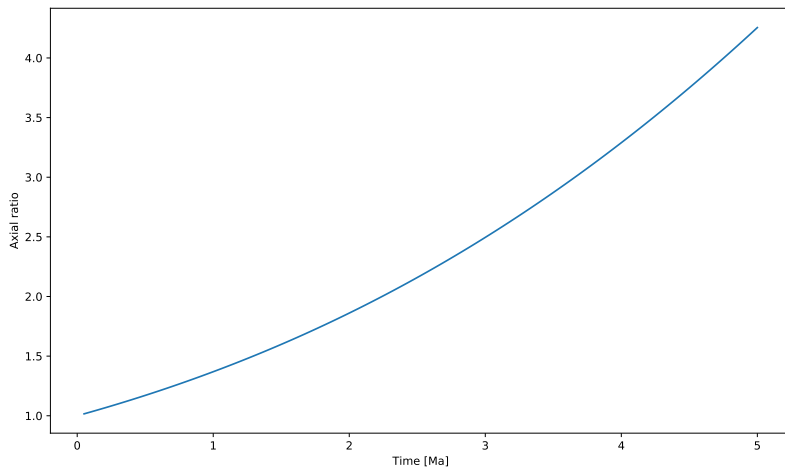


Figure: Axial ratio of finite strain ellipse during simple shear.

# Simultaneous deformation

As velocity gradient represents vector field, the velocity gradient of simultaneous deformation could be described as addition of individual velocity gradients, i.e:

$$\mathbf{L} = \mathbf{L}_1 + \mathbf{L}_2$$

and finite deformation could be calculated as:

$$\mathbf{F} = e^{\mathbf{L}_1 + \mathbf{L}_2}$$

In case we know individual deformation gradients, the simultaneous deformation could be calculated as:

$$\mathbf{F} = e^{\ln(\mathbf{F}_1) + \ln(\mathbf{F}_2)}$$



## Python exercise

Calculate deformation gradient for simultaneous pure shear with  $S_x = 2$  and  $S_y = 0.5$  and simple shear with  $\gamma = 1$ :

```
>>> F1 = array([[2, 0], [0, 0.5]])
>>> F2 = array([[1, 1], [0, 1]])

>>> F = la.expm(la.logm(F1) + la.logm(F2))
Traceback (most recent call last):
  File "<stdin>", line 1, in <module>
NameError: name 'la' is not defined

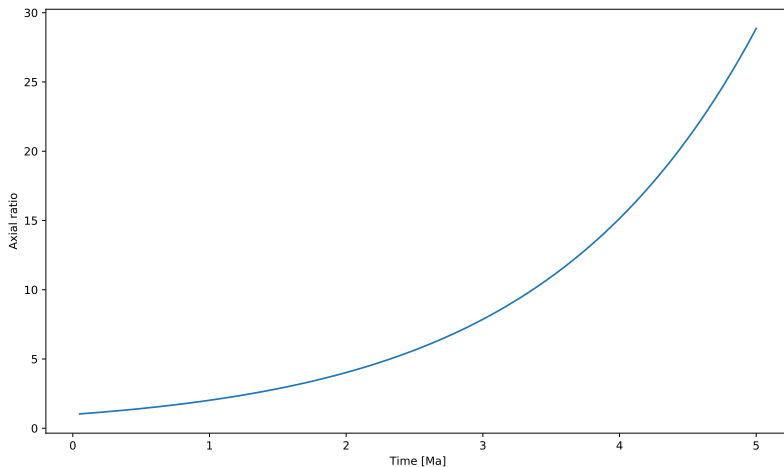
>>> print(F)
[[1.  0.  1. ]
 [0.  2.  0. ]
 [0.  0.  0.5]]
```

# Python exercise

Script to plot evolution of axial ratio of finite strain ellipse during progressive simultaneous pure shear and simple shear:

```
edot = 1e-14
ar = []
L = array([[edot, gdot],[0, -edot]])
for t in times:
    F = la.expm(L*t*1e6*yearsec)
    U, s, V = svd(F)
    ar.append(s.max()/s.min())

plot(times, ar)
xlabel('Time [Ma]')
ylabel('Axial ratio')
```



**Figure:** Axial ratio of progressive simultaneous deformation.

Plot evolution of deformation intensity (D) and symmetry (K) within transpression zone defined by convergence angle  $\alpha = 30^\circ$ ,  $\dot{\gamma}_{xy} = 10^{-14} s^{-1}$ ,  $\dot{e}_{yy} = -10^{-14} s^{-1}$  and  $\dot{e}_{zz} = 10^{-14} s^{-1}$  during 5Ma years.

# Python exercise

```
K, D = [], []
L = array([[0, gdot, 0 ],
           [0,-edot, 0 ],
           [0,  0, edot]])

for t in times:
    F = la.expm(L * t * 1e6*yearsec)
    U, s, V = svd(F)
    xy, yz = s[:-1]/s[1:] - 1
    K.append(xy/yz)
    D.append(sqrt(xy**2 + yz**2))

plot(times, D, times, K)
xlabel('Time [Ma]')
ylabel('D and K')
```

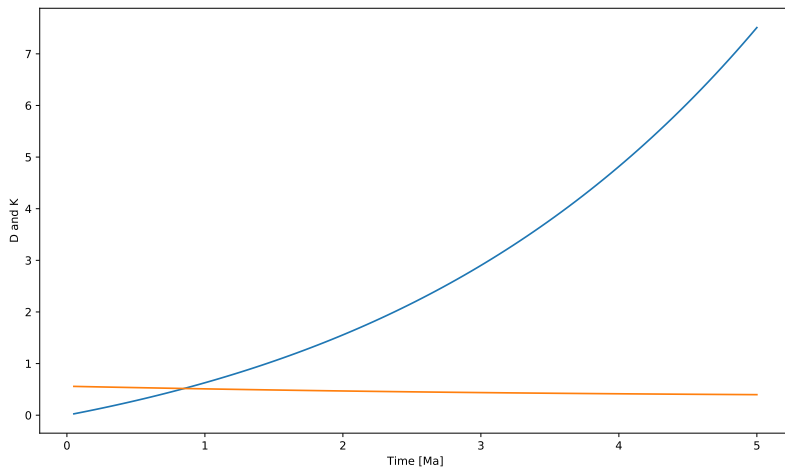


Figure: Intensity (D) and symmetry (K) during transpression.