

Particle Loading Characteristics of Two-stage Filtration System

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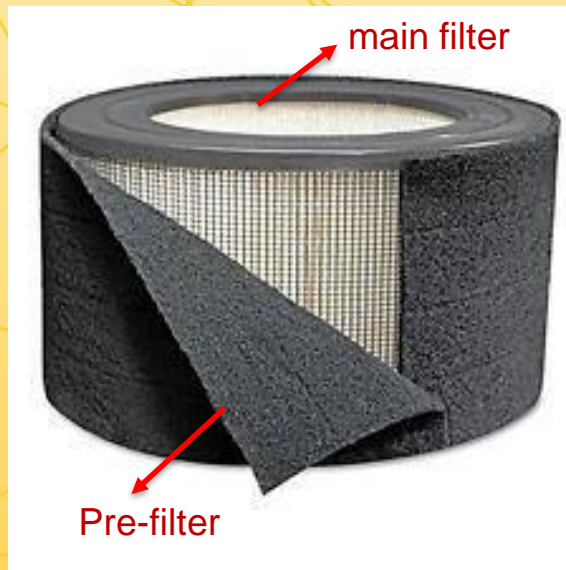


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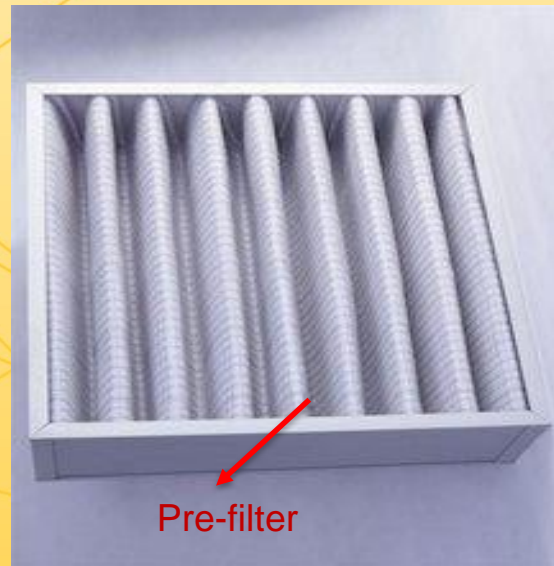
Introduction

- pre-filters used in two-stage filtration systems

Pre-filter wrap



Pre-filter panel



Pre-filter bag



Introduction

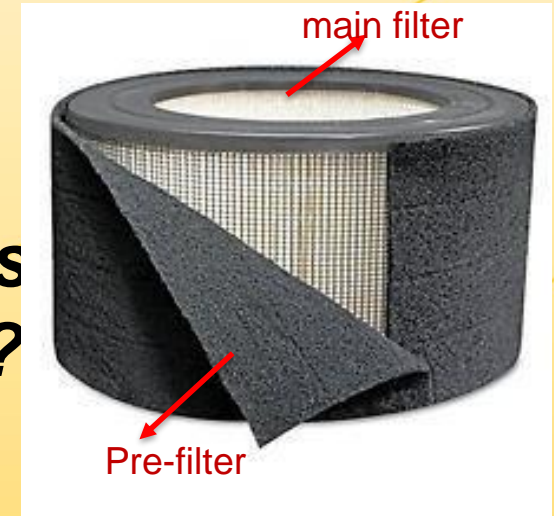
- **Issues** with **main** intake air **filters**:

- pressure drop often increases rapidly
- dust holding capacity is often low
- relatively expensive

Why we want to use the two-stage filter on the filtration system?

- **Solutions** with **pre-filters**:

- slows down pressure drop increase of main filters
- extra dust holding capacity
- inexpensive
- easy to change



Installing a pre-filter in front of the main filter, is a cost-effective way to extend the service life of the main filter.

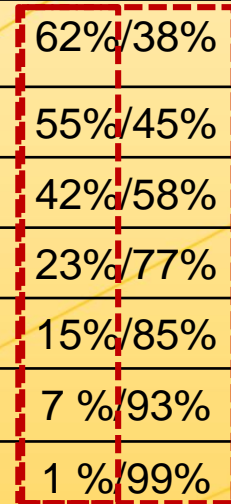
- **Factors influencing a two-stage filtration system performance:** incoming aerosol distribution, face velocity of each stage, filter combinations, and others.



Introduction

Ratios of fine and coarse particles in atmospheric environment

Category	Total Conc. ($\mu\text{m}/\text{cm}^3$) ³	Fine/Coarse by Volume
BK& aged urban plume	71.4	62%/38%
Urban Average	69.8	55%/45%
Urban and freeway	89.4	42%/58%
Clean continental BK	6.5	23%/77%
Average BK	30.4	15%/85%
BK& local sources	42.7	7 %/93%
Marine surface background	12.1	1 %/99%



BK- Back ground

(WS Poon, BYH Liu 1997)

- The ratio of fine and coarse particles varies greatly among ambient environments.
- Filters are evaluated in laboratories using either 100% fine or 100% coarse particles, which does not represent the environment where filters are used.

➤ *How does the particles size distribution in the environment affect the loading characteristics of a two-stage filter system?*

Objective

- To investigate the influence of installing a pre-filter on the loading characteristics of main filter.
- To compare loading characteristics of two-stage systems under different fine-coarse aerosol ratios and face velocity combinations of the two stages.
- To find the best scheme and to optimize the two-stage filtration system design.

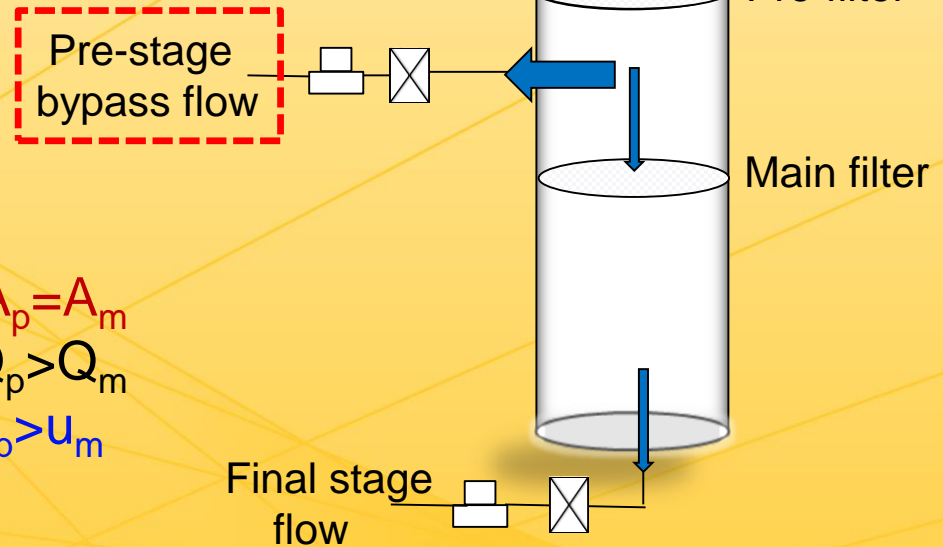


Methodology – simulating a two-stage filter

Practical application



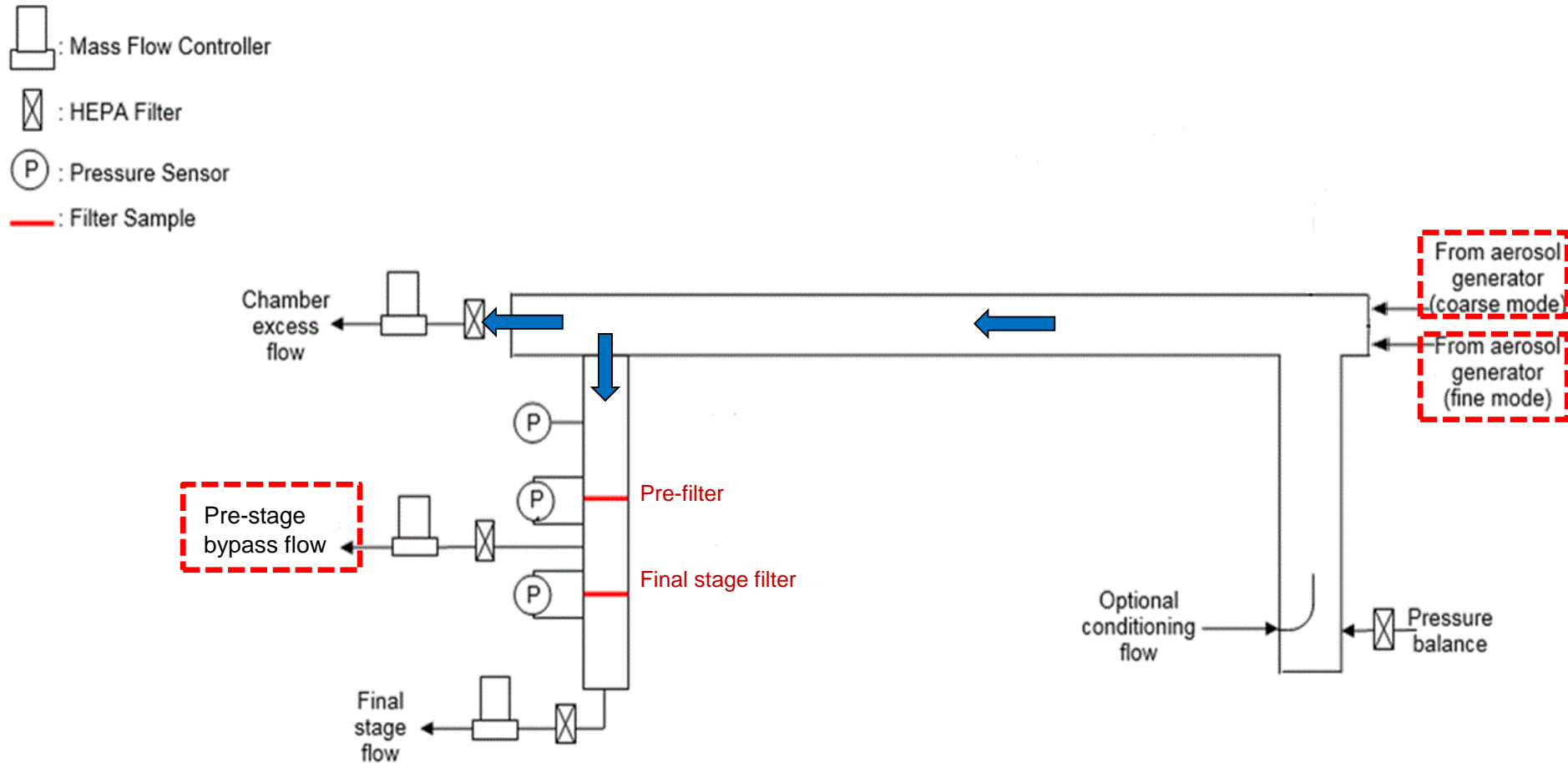
Experiment scenario



$$\begin{array}{ll} A_p < A_m & A_p = A_m \\ Q_p = Q_m & Q_p > Q_m \\ u_p > u_m & u_p > u_m \end{array}$$

p: pre-filter
m: main filter

Schematic of test system



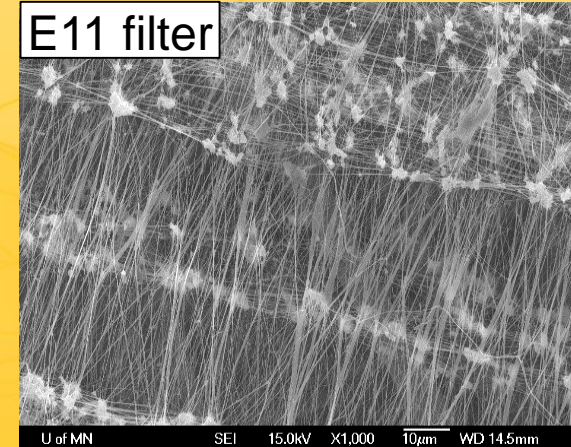
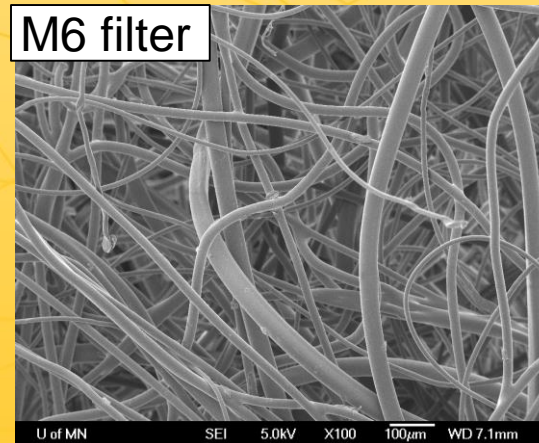
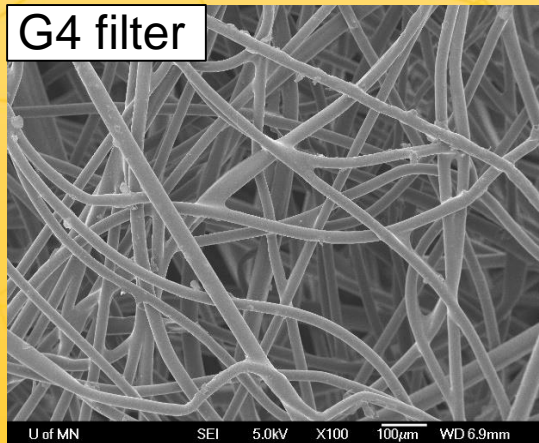
Testing condition

Properties of tested filter media

Filter		Areal weight (g m ⁻²)	Thickness (mm)	Permeability (mm s ⁻¹)	Average Diameter (μm)
Pre-stage	G4 filter	363±2	6.79	3100	28.3
	M6 filter	385±2	3.46	730	19.7
Final stage	E11 filter (PTFE membrane filter)	160±3	0.37	85	--

G4,M6: efficiency rating
E11 : efficiency rating

EN 779: 2012
EN 1822-1-2009
see the appendix



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Testing condition

Fine & Coarse Particles:

- **KCl:** 4% v/v potassium chloride aqueous solution
- **A2:** ISO 12103-1 Arizona test dust, A2 fine

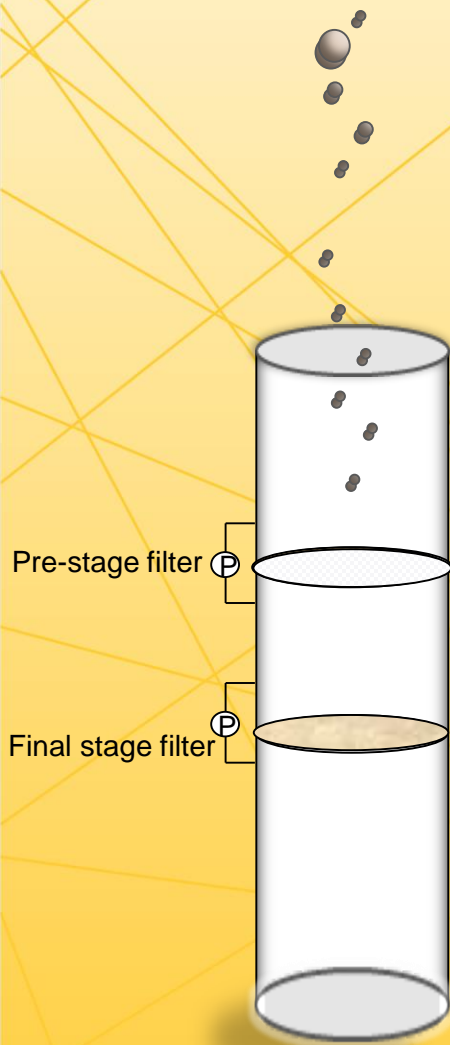
Aerosol mixing ratio	KCl/A2	0%/100%, 6%/94%, 11%/89%, 33%/67%, 100%/0%
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Pre-stage & Final stage face velocity:

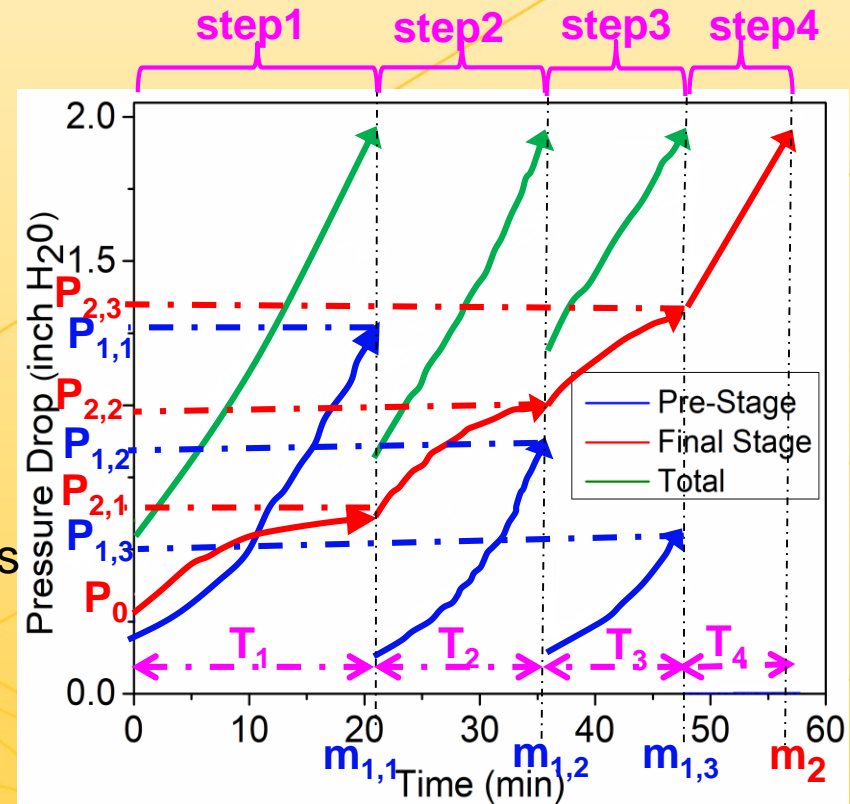
Face velocity (cm s ⁻¹)	Pre-stage/Final stage	G4 & E11	65.2/2.1, 65.2/3.1, 65.2/5.2
		M6 & E11	30.2/5.2, 50.2/5.2, 65.2/5.2



Testing Process



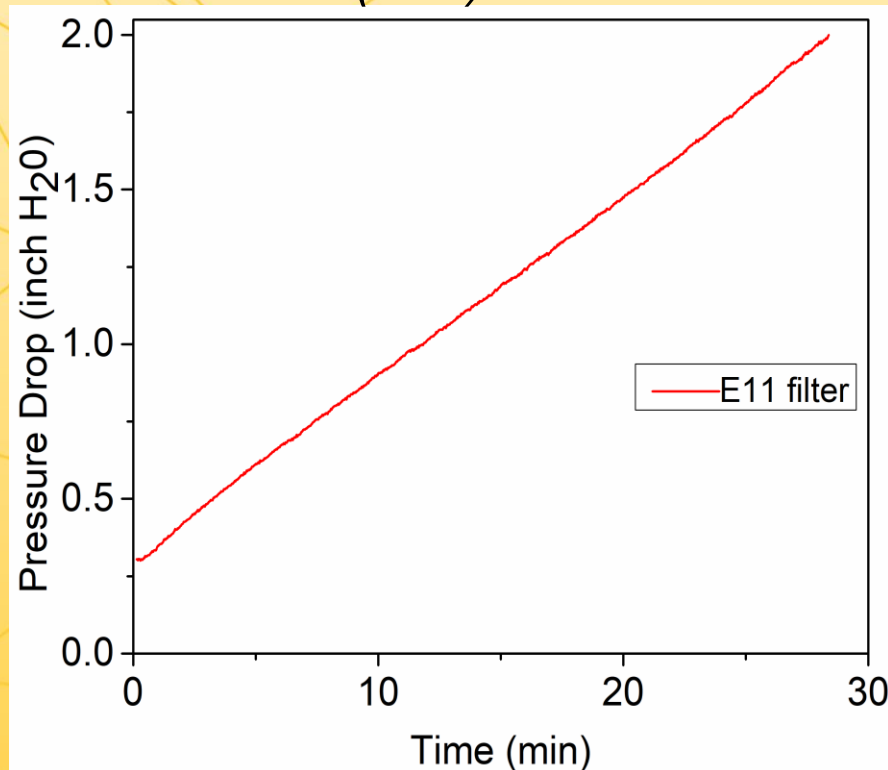
When $P_T = 2$ inch H_2O
 Remove pre-filter
 Install a new pre-filter
 Replace pre-filter three times
 Until $P_T = 2$ inch H_2O



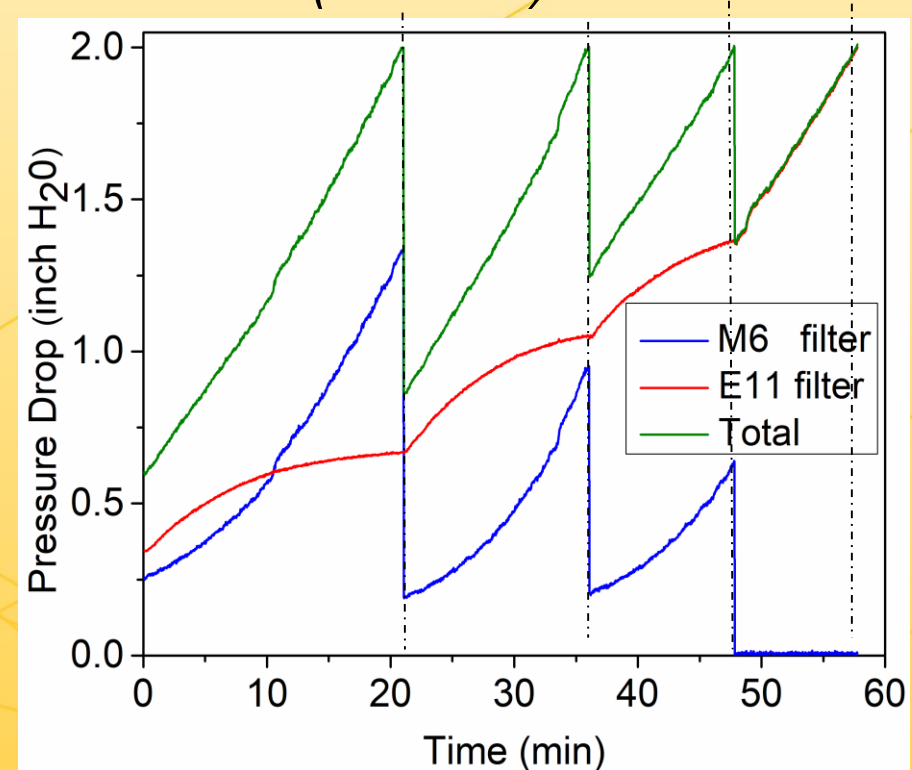
P_0 : initial pressure drop of main filter;
 $P_{1,n}$: pressure drop of the n^{th} pre-filter at the end of the n^{th} step;
 $P_{2,n}$: pressure drop of the main filter at the end of the n^{th} step;
 $m_{1,n}$: mass gain of the n^{th} pre-filter at the end of the n^{th} step;
 m_2 : mass gain of main filter at the end of the 4th step;
 T_n : time duration of the n^{th} step.

Reference test cases

Without pre-filter (reference)
(E11) filter



With pre-filter (two-stage case)
(G4&E11) filter



For every two-stage test case, a **reference test case** was conducted, under exactly the same test condition as the two-stage case, but **without** a pre-filter in front of the main filter.



Examples of raw data

(G4&E11) filter

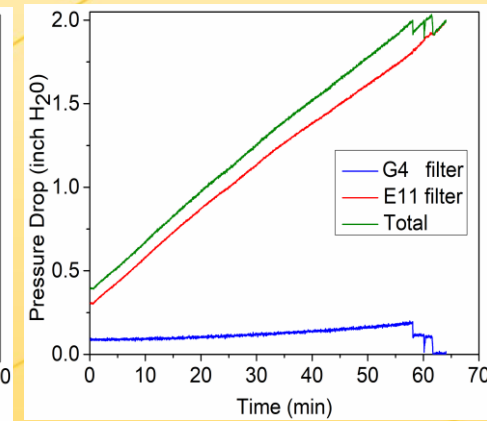
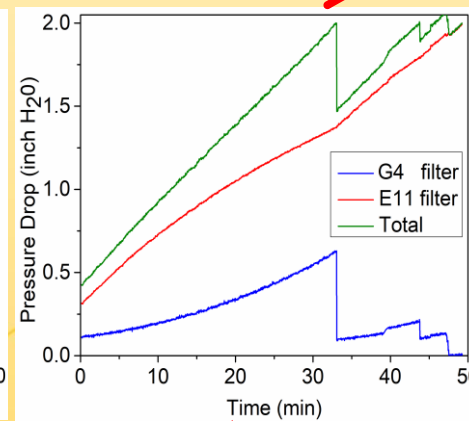
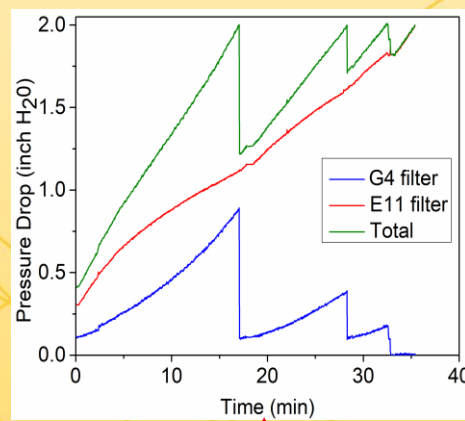
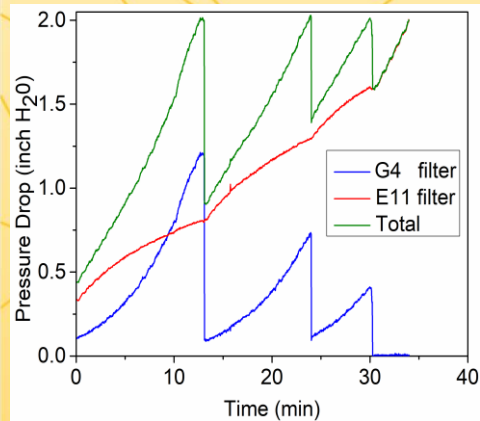
$U_1=65.2$ cm/s, $U_2=\underline{5.2}$ cm/s

KCl/A2 0%/100%

11%/89%

33%/67%

100%/0%



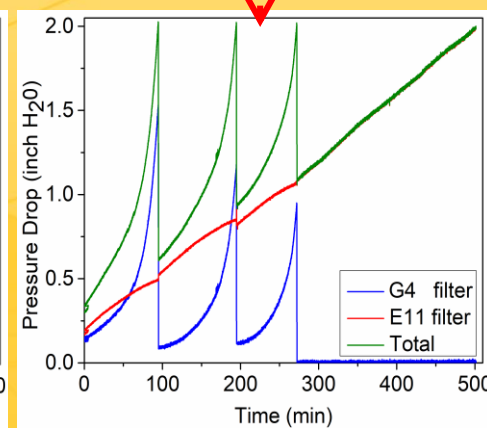
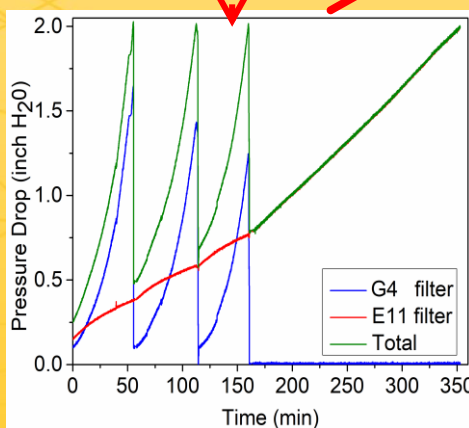
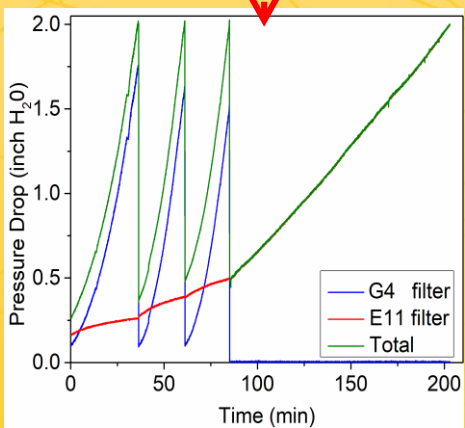
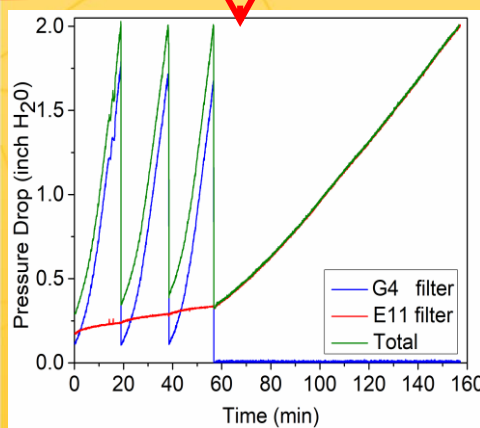
$U_1=65.2$ cm/s, $U_2=\underline{2.1}$ cm/s

KCl/A2 0%/100%

11%/89%

33%/67%

100%/0%



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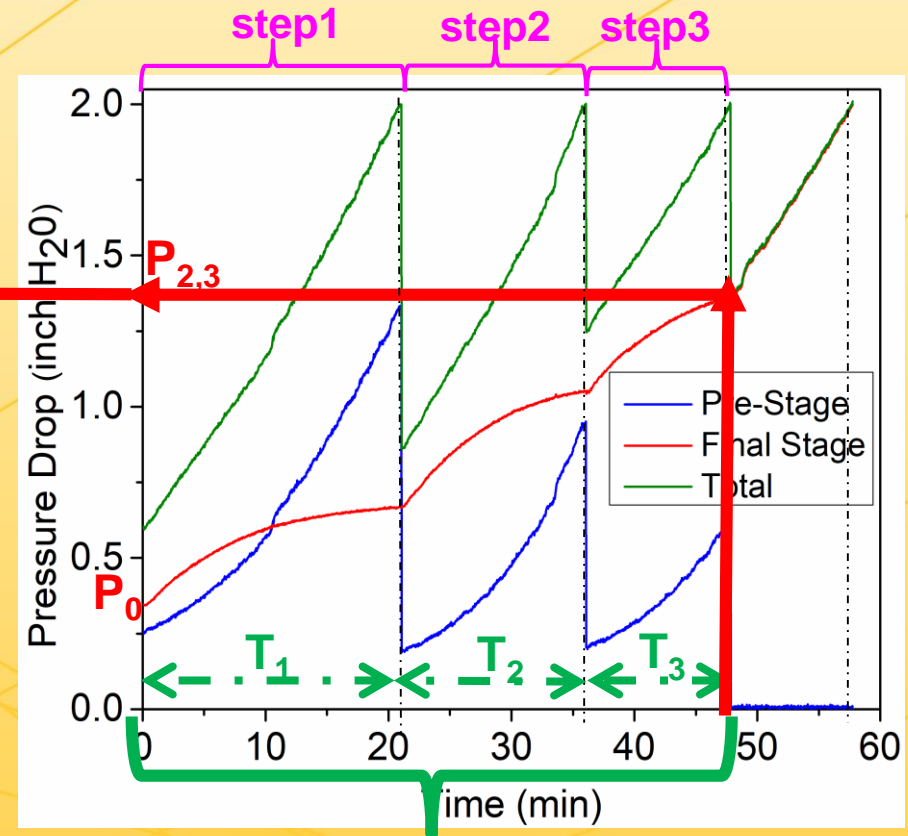
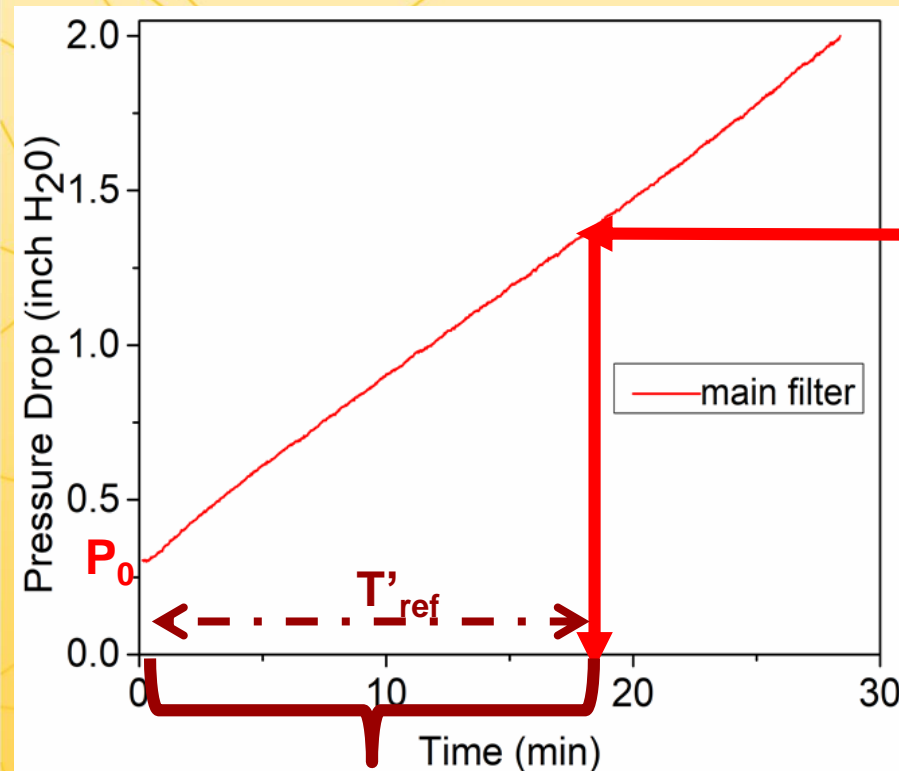


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Results analysis – Self-defined indexing parameters, T^*

Without pre-filter (reference)

With pre-filter (two-stage case)



$$T^* = \frac{(T_1 + T_2 + T_3)}{T'_{ref}} = \frac{48.7}{17.4} = 2.7$$

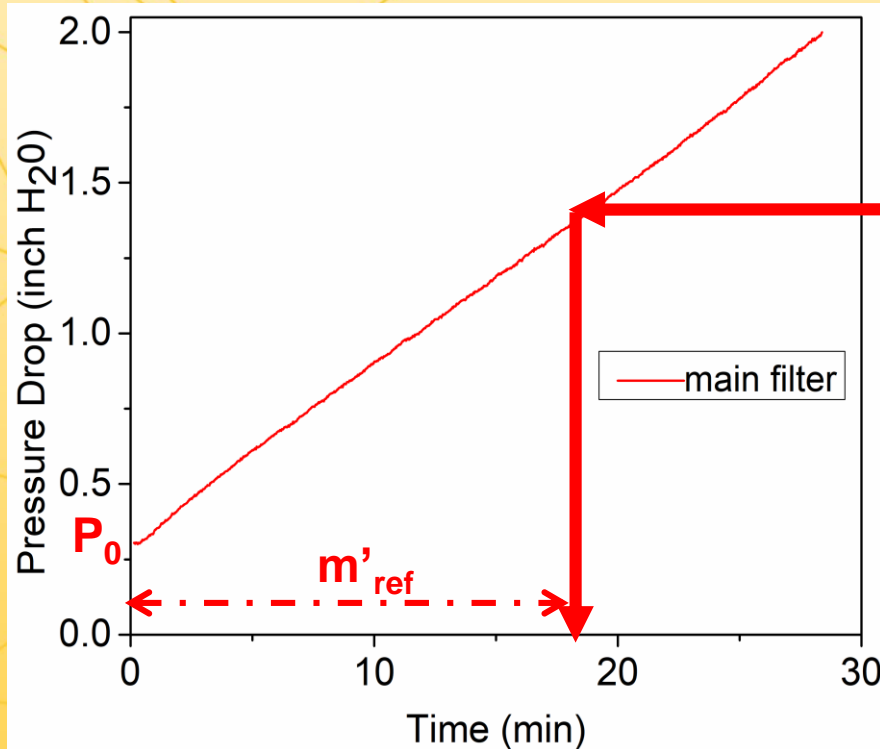
T^* : How long is the service life of the main filter extended by adding a pre-filter.

The **higher** T^* is, the **longer** of main filter service life is extended.

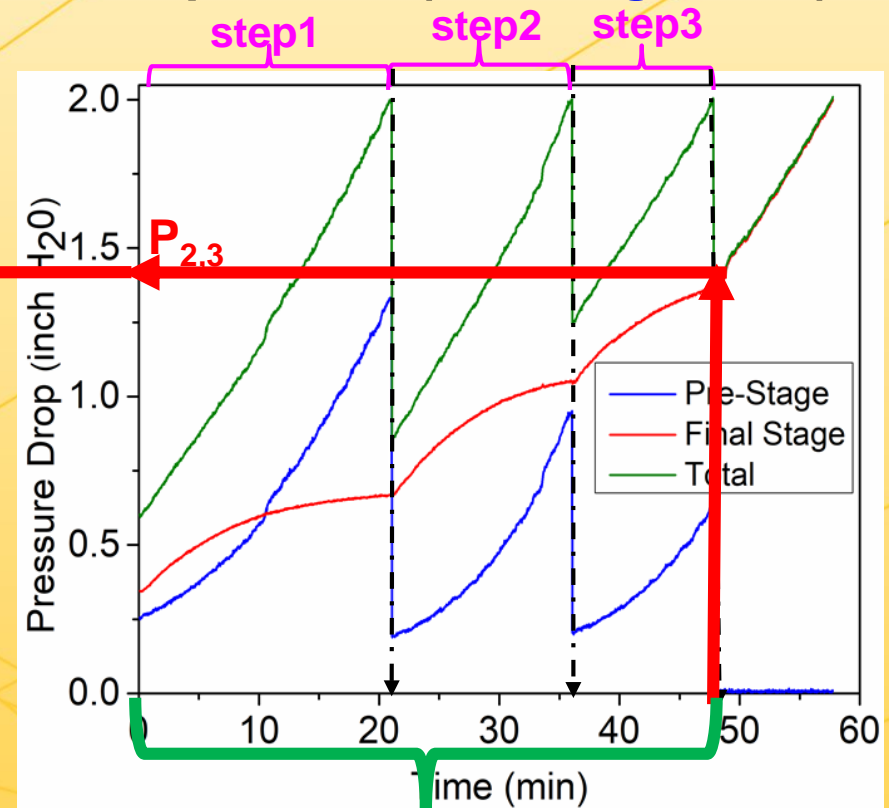


Results analysis – Self-defined indexing parameters, M^*

Without pre-filter(reference)



With pre-filter (two-stage case)



$$M = \frac{m}{u}$$

$$(m_p)_{1-3} = m_{1,1} + m_{1,2} + m_{1,3}$$

$$(m_f)_{1-3} = m_{2,1} + m_{2,2} + m_{2,3}$$

$$(M_p + M_f)_{1-3} = \left(\frac{m_p}{u_1}\right)_{1-3} + \left(\frac{m_f}{u_2}\right)_{1-3}$$

$$M^* = \frac{(M_p + M_f)_{1-3}}{M'_{ref}}$$

$$= \frac{11.5}{3.2} = 3.6$$

$$(m_p + m_f)_{1-3}$$

M^* : How much is the mass collection increased by adding a pre-filter.

The **higher** of M^* , the **more** two-stage filters' dust holding capacity are increase.



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Results analysis – Self-defined indexing parameters, P^*

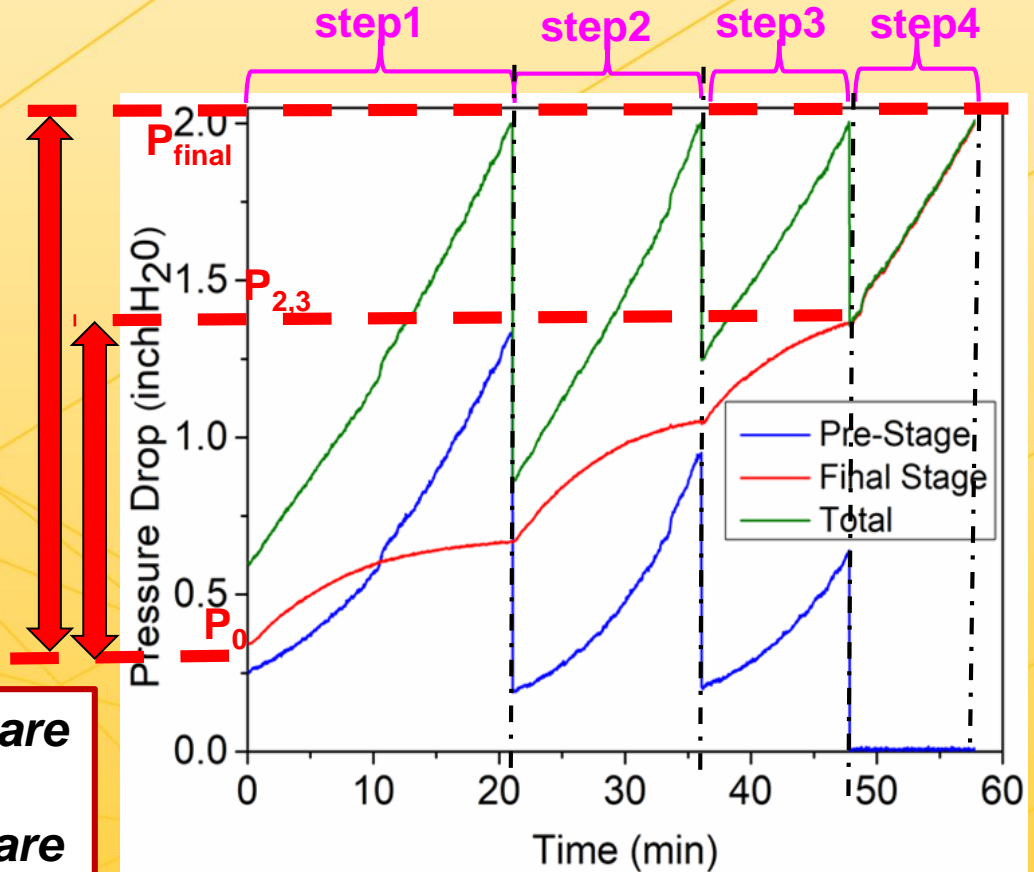
$$P^* = \frac{(P_{2,3} - P_0)}{(P_{final} - P_0)} = 62 \%$$

$$0 < P^* < 1$$

P^* : inversely-proportional to the contribution of pre-filter, in terms of pressure drop.

- **High P^*** means **fewer** particles are captured by the pre-filter;
- **Low P^*** means **more** particles are captured by the pre-filter.

With pre-filter (two-stage case)



Summarized Results (I) – Effect of *pre-filter*

Testing results with a pre-filter

$U_1=65.2$ cm/s, $U_2=2.1$ cm/s

Filter		Particles	$P_{2,3}$ (inch H ₂ O)	$(M_P+M_f)_{1-3}$ mg/(cm·s ⁻¹)	M'_{ref} mg/(cm·s ⁻¹)	$T_1+T_2+T_3$ (min)	T'_{ref} (min)	p^* (%)	M^* (--)	T^* (--)
Pre-stage	Final stage									
G4	E11	100% A2	0.35	39.6	11	55.6	14.6	<u>14</u>	<u>3.6</u>	<u>3.8</u>

Installing a pre-filter in front of a main filter can increase the dust holding capacity of a filtration system, and extend the service life of a main filter effectively.

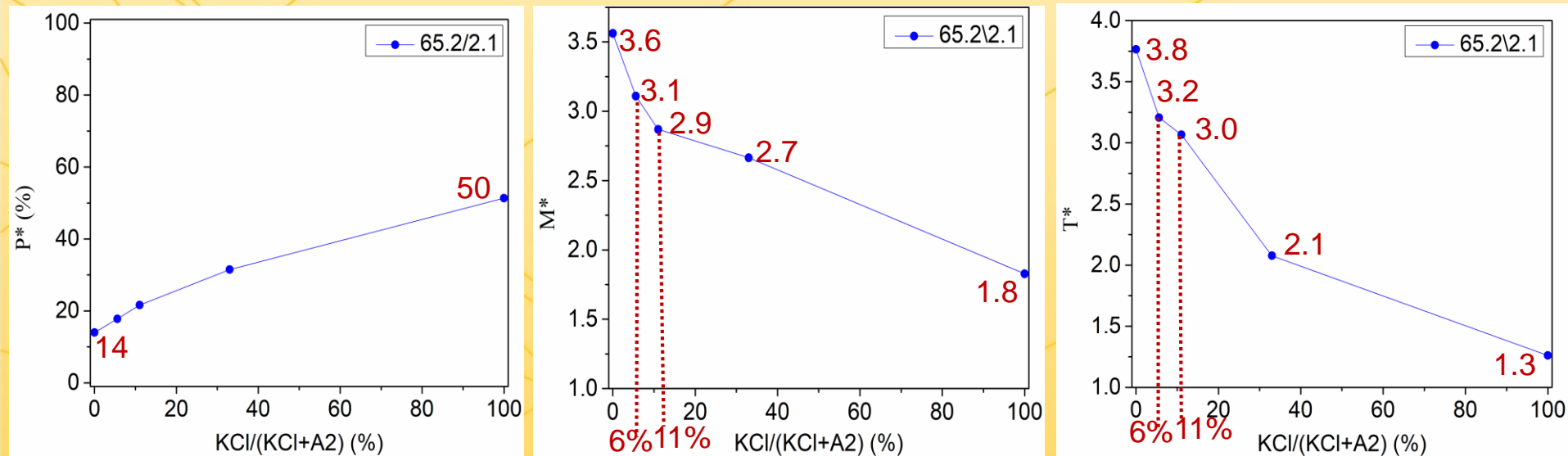


Summarized results (II)

–Effect of aerosol mixing ratio

(G4&E11) filter

$U_1=65.2$ cm/s, $U_2=2.1$ cm/s



With the fraction of fine particles **increases** (0%→ 6%→ 11%→ 33%→ 100%):

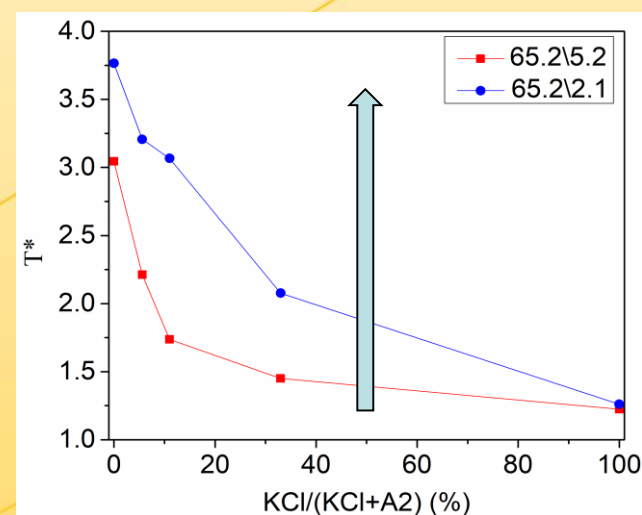
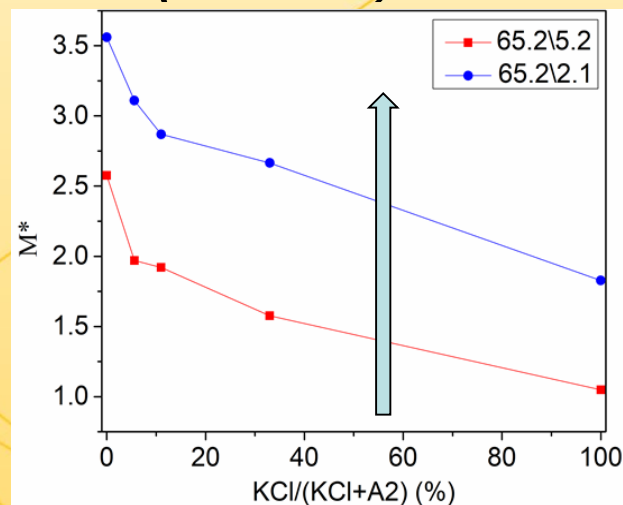
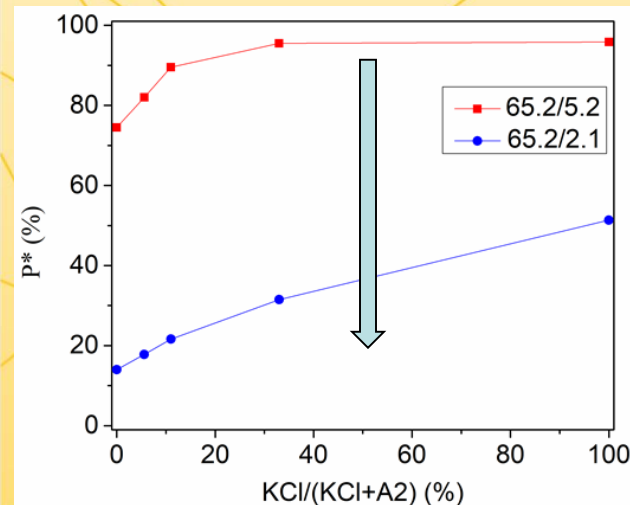
- **More** particles are captured by the main filter;
- The total dust holding capacity of the two stages **decreases**;
- The service life of the main filter **decreases**.

Even a small fraction of fine particles can reduce the dust holding capacity of a two-stage system and the service life of the main filter.



Summarized Results (III)

– Effect of face velocity ratio (G4&E11) filter



At **higher** face velocity ratio, **more** particles are collected on pre-filter, leading to:

- **Slower** increase of main stage pressure drop;
- **Higher** total dust holding capacity of two-stage filter;
- **Longer** service time of the main filter.

The detailed relationship between the velocity ratio and the absolute velocity values of each stage requires more investigation.



Summary

- A simple two-stage filter loading test system was successfully developed, capable of being used to investigate the loading characteristics of a two-stage filtration system cost- and time-effectively.
- Installing a pre-filter in front of a main filter can effectively increase the total particle holding capacity of the filtration system, and extend the service life of the main filter.
- The effectiveness of the pre-filter is strongly affected by the incoming particle size distribution. Even a small fraction of fine particles can reduce the dust holding capacity of a two-stage filtration system, and can reduce the main filter's service life significantly.
- The selection of face velocities of the two stages can affect the performance of a two-stage filtration system. Higher velocity difference between two stages results in longer service time of the main stage, but requires more frequent replacement of the pre-filter.



Future work

- To investigate how the selection of pre-filter media and main filter media influence the loading characteristics of a two-stage filtration system.
- To investigate more in details on how the velocity ratio and the absolute velocity values of each stage influence the loading characteristics of a two-stage filtration system.
- To develop a evaluation formula, based on those self-defined indexing parameters and the information of filter cost and replacement cost, which can be used as a guideline of selection and optimization of a two-stage filtration system.



Thank you!
Q&A



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EN 779: 2012

Table 1— Classification of air filters ¹⁾

Group	Class	Final test pressure drop Pa	Average arrestance (A_m) of synthetic dust %	Average efficiency (E_m) of 0,4 μ m particles %	Minimum Efficiency ^a of 0,4 μ m particles %
Coarse	G1	250	$50 \leq A_m < 65$	-	-
	G2	250	$65 \leq A_m < 80$	-	-
	G3	250	$80 \leq A_m < 90$	-	-
	G4	250	$90 \leq A_m$	-	-
Medium	M5	450	-	$40 \leq E_m < 60$	-
	M6	450	-	$60 \leq E_m < 80$	-
Fine	F7	450	-	$80 \leq E_m < 90$	35
	F8	450	-	$90 \leq E_m < 95$	55
	F9	450	-	$95 \leq E_m$	70

^a Minimum efficiency is the lowest efficiency among the initial efficiency, discharged efficiency and the lowest efficiency throughout the loading procedure of the test.

EN 1822-1-2009

Table 1 — Classification of EPA, HEPA and ULPA filters

Filter Group Filter Class	Integral value		Local value ^{a b}	
	Efficiency (%)	Penetration (%)	Efficiency (%)	Penetration (%)
E 10	≥ 85	≤ 15	--- ^c	--- ^c
E 11	≥ 95	≤ 5	--- ^c	--- ^c
E 12	$\geq 99,5$	$\leq 0,5$	--- ^c	--- ^c
H 13	$\geq 99,95$	$\leq 0,05$	$\geq 99,75$	$\leq 0,25$
H 14	$\geq 99,995$	$\leq 0,005$	$\geq 99,975$	$\leq 0,025$
U 15	$\geq 99,999\ 5$	$\leq 0,000\ 5$	$\geq 99,997\ 5$	$\leq 0,002\ 5$
U 16	$\geq 99,999\ 95$	$\leq 0,000\ 05$	$\geq 99,999\ 75$	$\leq 0,000\ 25$
U 17	$\geq 99,999\ 995$	$\leq 0,000\ 005$	$\geq 99,999\ 9$	$\leq 0,000\ 1$

^a See 7.5.2 and EN 1822-4.

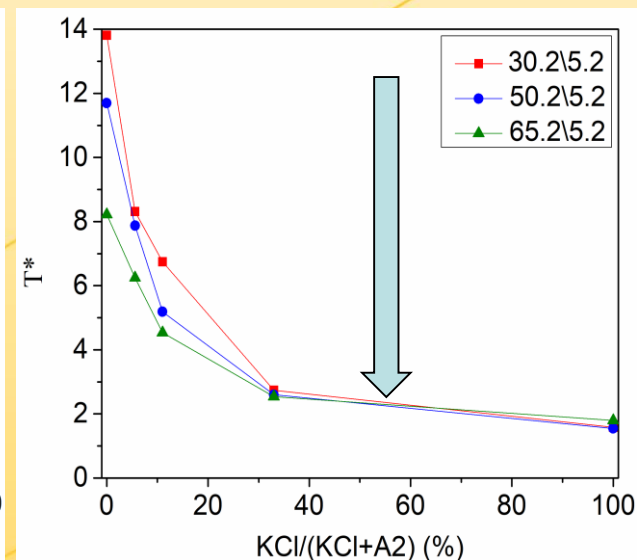
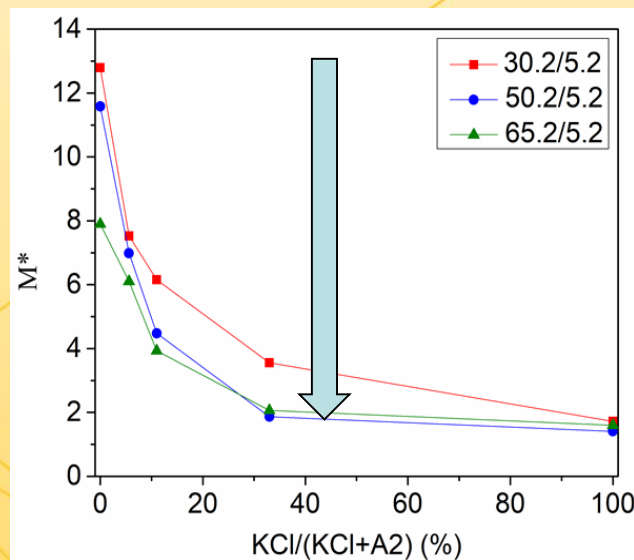
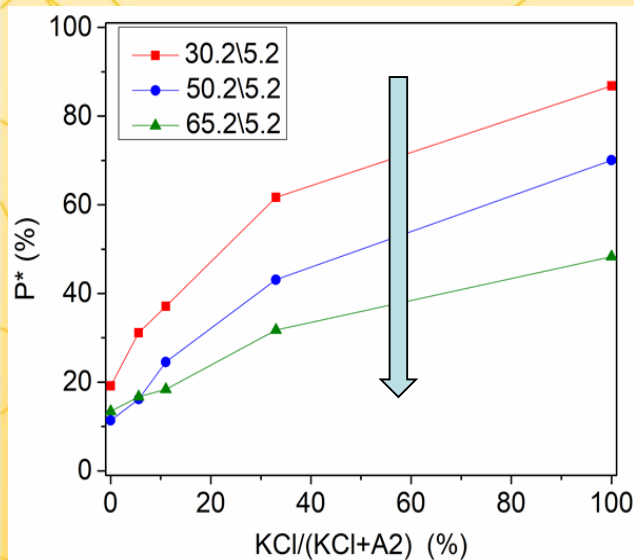
^b Local penetration values lower than those given in the table may be agreed between supplier and purchaser.

^c Group E filters (Classes E10, E11 and E12) cannot and shall not be leak tested for classification purposes.



Summarized Results

(M6&E11) filter



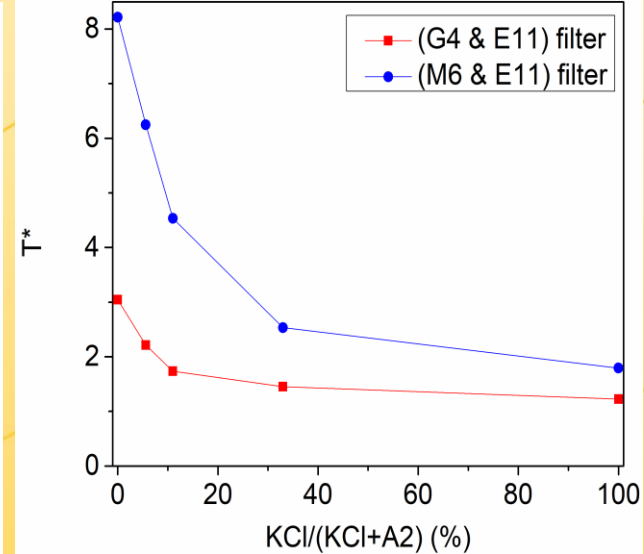
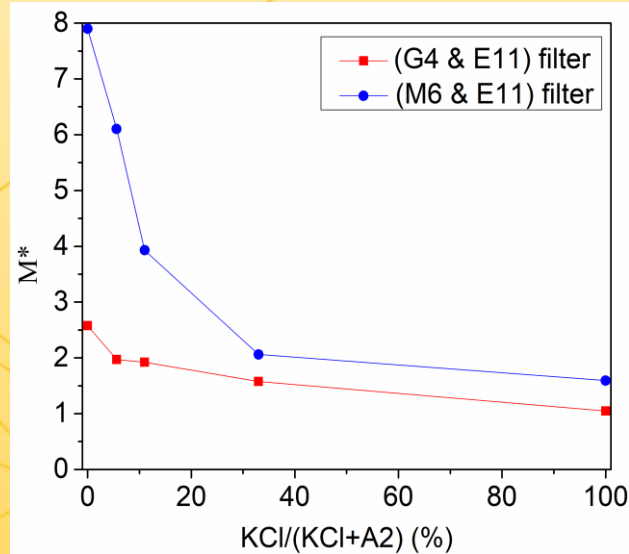
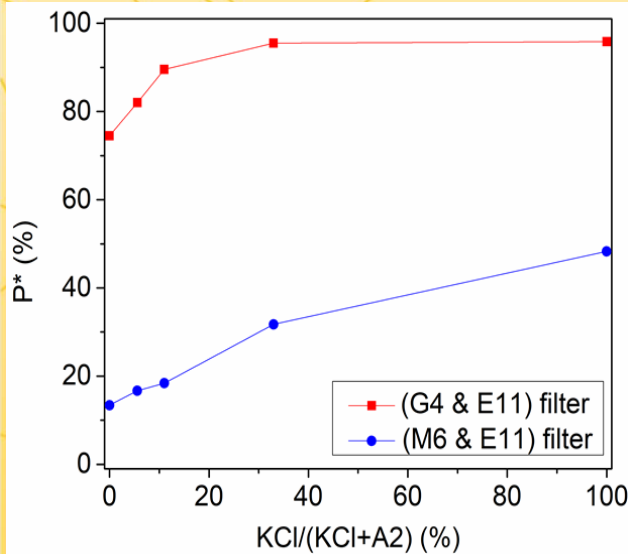
- When using M6 media instead of G4 media as the pre-filter, similar trend was found for the effectiveness of pre-filter, and the effectiveness of fine-coarse aerosol ratio;
- When we increase the face velocity of pre-stage, though the pressure drop of E11 filter increases slowly, the dust holding capacity of two-stage filtration system and service life of E11 filter decrease.



Summarized Results – Effect of filter combination

(G4&E11) filter vs (M6&E11) filter

$U_1 = \underline{65.2}$ cm/s, $U_2 = \underline{5.2}$ cm/s



When replacing pre-filter from G4 to M6:

- More particles are captured by the pre-stage (M6) filter;
- M6 filter increase more dust holding capacity than G4 filter;
- The service life of main filter are extended longer.
- Requiring more replacements of pre-filter in order to fully utilize the main filter;
- More investigating and **cost information** are needed for better system optimization

