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# ABSTRACT SPECIFICATION TOPIC FOR OGC DEFORMATION MODEL FUNCTIONAL MODEL

**ABSTRACT SPECIFICATION TOPIC** 

**CANDIDATE SWG DRAFT** 

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# ABSTRACT

All objects on the surface of the earth are moving. Apparently fixed features such as buildings are moving with the earth's crust — subject to ongoing plate tectonic movement and episodic deformation events such as earthquakes. Increasingly we rely on Global Navigation Satellite Systems (GNSS) which can precisely determine the coordinates of features — coordinates we then store in Geographic Information Systems (GIS) and other spatial databases. However, the coordinates from GNSS are referenced to global reference frames and coordinate systems In these reference frames the ongoing movement of apparently fixed objects means that the coordinates of these features are continually changing over time.

This creates a challenge for the geospatial and positioning community — how to account for this movement when comparing data sets observed at different times, or how to relocate an object located in the past.

One solution to this challenge is to use a deformation model — a mathematical model of the deformation of the crust. It allows the coordinates of an apparently fixed object to be propagated to different times so that they track the object's location.

Common uses of a deformation model include:

- determining the current location of an object based on a historic measurement of its location,
- transformation of the current observed location of an object to the reference epoch of a static coordinate system
- determining the correct spatial relationship of data sets observed at different times.

Currently many national geodetic agencies construct deformation models. However, these generally use customized formats and are typically only used by software developed by the agency.

This specification defines a functional model for describing a deformation model. It describes a way of parameterizing deformation such that it can be encoded into a data set and incorporated into software for use in coordinate transformations. It also defines how to calculate the displacement of a point between two different epochs using this parameterization. This specification allows producers of deformation models, such as national geodetic agencies, to publish these models in a consistent way. Users of coordinate transformation software can be confident that the model is being applied as intended by the producers.

# II KEYWORDS

The following are keywords to be used by search engines and document catalogues.

ogcdoc, OGC document, deformation model, crustal deformation, coordinate transformation, coordinate operation, specification



# SECURITY CONSIDERATIONS

No security considerations have been made for this document.



### SUBMITTING ORGANIZATIONS

The following organizations submitted this Document to the Open Geospatial Consortium (OGC):

- Land Information New Zealand
- ESRI



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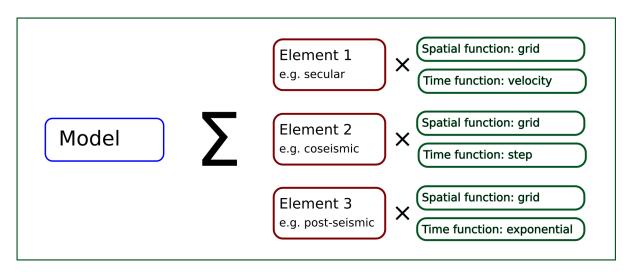


### INTRODUCTION

This specification has been developed by the OGC Coordinate Reference System (CRS) domain working group (DWG) in conjunction with the CRS DWG project team developing the "Gridded Geodetic Exchange Format (GGXF)" and with the International Association of Geodesy (IAG) Working group 1.3.1 on "Time-dependent transformations between reference frames in deforming regions".

This specification defines a general parameterization of deformation models as illustrated in Figure 1. The total deformation is decomposed into a set of elements, each of which is defined by a spatial function and a time function. The spatial function defines the displacement that applies at a given location, and the time function defines a scalar function that applies for the element at a given time. The displacement due to the element is the spatial function displacement multiplied by the time function scale factor. The total displacement at the location and time is the sum of the displacements from each element.

Figure 1 — Functional decomposition of a deformation model



Commonly elements represent identified geophysical causes, such as coseismic deformation due to an earthquake. However, an element could equally represent some measured displacement for which no physical cause has been ascribed. Also, several elements may represent different aspects of a single geophysical cause. For example, the horizontal deformation due to an earthquake may be represented by one element, and the vertical deformation by another.

This specification does not encompass other forms of deformation model such as:

- Rigid body transformation between reference frames such as time dependent Helmert or Bursa-Wolf transformations,
- Trajectory models for individual points, such as ITRF reference station coordinate models,
- Static distortion models used to represent the deformation between two datums
- Global plate tectonic models
- Three dimensional geophysical models of deformation in terms of dislocations on fault surfaces or using finite element models.

Also, this specification does not describe how the parameters and metadata of a deformation model should be encoded into a file.

The primary use case for this specification is for deformation model producers such as national geodetic agencies to encode regional deformation models for use in spatial data operations in geographic information systems and positioning systems. The purpose of this specification is to define the parameters that must be encoded in a compliant deformation model, and the formulae that compliant software should use to transform coordinates using the model.

SCOPE

# 1 SCOPE

This abstract specification defines a functional model that is used to define deformation models — models of the ongoing deformation of the earth's crust — to support their implementation into coordinate operations and transformations.

Within this context a deformation model is defined as follows:

A deformation model is a model of the displacement of the earth's surface within a defined spatial and temporal extent. It predicts the location of a point fixed to the surface at any time within the temporal extent in terms of an accessible coordinate system. The location of the point is represented as a displacement from a reference position for that point.

In the most abstract sense a deformation model is a mathematical function of a two dimensional coordinate and a time that defines a one, two, or three dimensional coordinate displacement. It may also express the uncertainty of the displacement.

This specification describes a means of representing a deformation model using a set of parameters and gridded data that defines this mathematical function. It specifies how the displacement is calculated from this data and how it is applied to a coordinate to apply the coordinate operation that the deformation model defines. It also specifies metadata attributes that should accompany the encoded model to allow users to understand its applicability and limitations.

2

# CONFORMANCE



# CONFORMANCE

**NOTE:** Provide a short description of the content approached in subsequent sections and the main subject of the document

3

# NORMATIVE REFERENCES



# NORMATIVE REFERENCES

There are no normative references in this document.

4

# TERMS AND DEFINITIONS



# TERMS AND DEFINITIONS

No terms and definitions are listed in this document.

5

# DEFORMATION MODEL DEFINITION

#### DEFORMATION MODEL DEFINITION

The deformation model is characterized as follows.

- a) The model defines deformation within a specified spatial and temporal extent. Beyond these extents the model is undefined and cannot be evaluated.
- b) The model partitions deformation into one or more elements. The total displacement at a specific time and position is calculated by summing the contribution from each element at that time and position, as described in Clause 6.3.
- c) Each element of the model comprises a spatial function and a time function. The spatial function evaluates displacement as a function of position. The time function evaluates a scale factor as a function of time. The deformation contribution for the element at a given position and time is obtained by multiplying the displacement from the spatial function by the scale factor from the time function.
- d) The spatial function may be defined over a subset of the total extent of the model. Where the spatial function is not defined it is assumed to be zero.
- e) The spatial function is represented by displacement vectors at the nodes of a grid or a set of grids.
  - If a set of grids is used then only one of the grids will be used to evaluate the function at a specific location. The implementation must unambiguously define which grid (if any) is to be used at a specific location.
  - The spatial function displacement components at a location are calculated from the selected grid using a specified interpolation method. The only interpolation method supported is bilinear interpolation, as described in Clause 6.1.
- f) The spatial function can define displacement and uncertainty components. This set of components must be defined at every node of every grid of the function. Different spatial functions may have different components. For example, the spatial function of one element might define horizontal displacement, and the spatial function of another may define vertical displacement.
- g) Displacement components of the spatial function may include:
  - horizontal displacement the east and north displacement in meters or degrees
  - vertical displacement the upwards vertical displacement in meters.

Displacement components not defined by the spatial function are assumed to be zero.

- h) Uncertainty components of the spatial function may be one of:
  - horizontal uncertainty specified as one of:
    - horizontal circular uncertainty e<sub>h</sub>
    - east and north uncertainty e<sub>e</sub>, e<sub>n</sub>
  - vertical uncertainty e<sub>v</sub>

The set of uncertainty components used to represent uncertainty are defined in the model metadata and must be used for all spatial functions which have uncertainty components. For example, the deformation metadata could specify that the model uses horizontal circular uncertainty and vertical uncertainty. A particular spatial component could define just horizontal circular uncertainty. Another could define vertical uncertainty. But it would not be valid for an element to define east and north uncertainty.

The probability level for the uncertainty is defined in the model metadata, e.g. "1 standard error", "95% confidence".

If the uncertainty of an element is not defined at a model node its value is defined by a default value element metadata or, if it is not defined there, in the model metadata.

- i) The displacement defined by the model is required to be continuous and invertible within the spatial and temporal extent of the model except where it evaluates to *no data*. This is not necessarily enforced by the mathematical formulation of a model. It is a compliance requirement on producers of functional models. Continuity can be assumed by software implementations of the model.
- j) The displacement and uncertainty components at a node of a spatial function may be assigned a *no data* value. This means that their value at that node is undefined. The model displacement and uncertainty is undefined at specific time and location if calculating it would require using a using a *no data* value.

- k) The time function of an element is a scalar function of time calculated as the sum of one or more base functions. Each base function is one of:
  - a velocity function
  - a step function
  - a reverse step function
  - a ramp function
  - an exponential decay function
  - a logarithmic function
  - an acceleration function
  - a hyperbolic tangent function
  - a sine or cosine function

These base time functions are defined mathematically in Clause 6.2.

- l) Each element definition specifies:
  - The spatial interpolation method to use (bilinear)
  - The quantities it defines (displacement components, uncertainty components)
  - A spatial definition of the extent of the spatial function (to determine if it is required at a specific position)

#### It may also include:

- The default uncertainty, which applies if the spatial function does not explicitly define uncertainty.
- Other metadata required by the implementation
- Other producer metadata

- m) The model definition specifies:
  - The source CRS definition (e.g., EPSG:xxxx)
  - The target CRS definition (if the model is implemented as a point motion model this will be the same as the source CRS).
  - The spatial function definition CRS
  - The valid spatial extent of the model (defined in terms of the definition CRS)
  - The valid time extent of the model
  - The units of horizontal displacement
  - The units of vertical displacement
  - The parameters used to represent uncertainty, for example, horizontal 95% circular confidence, vertical 95% confidence level.
  - The default uncertainty for each element of the model, if the model does not explicitly define uncertainty

#### It may also include:

- Other metadata required by the implementation, such as discovery metadata and licence information.
- Other producer metadata, such as model name, model version and publication date.

6

# CALCULATION FORMULAE

#### CALCULATION FORMULAE

The formulae below define the expected behavior of software implementations of the deformation model. Whatever algorithm a software implementation may use it should produce numerically indistinguishable results to be a compliant implementation. This ensures the software implementation applies the model as intended by the producers.

In this specification the grid can be defined either in terms of a geographic (longitude/latitude) or projected (easting/northing) coordinate system. Displacements and uncertainties are expressed as linear distance except that the horizontal displacement may be an angular distance if the source and target coordinate systems are geographic.

#### 6.1. SPATIAL INTERPOLATION

This specification defines spatial functions by bilinear interpolation on a grid or set of grids. In the future other interpolation methods or spatial representations may be supported.

#### 6.1.1. Selection of spatial function grid

Spatial functions are using a set of one or more grids. At a given position only one of the grids is used to calculate the spatial function displacement or uncertainty. The implementation must uniquely identify the grid, if any, that applies at any location within the valid extents of the model. If no grid applies at a location then the displacement and uncertainty of the element at that location are both zero.

#### 6.1.2. Bilinear grid interpolation

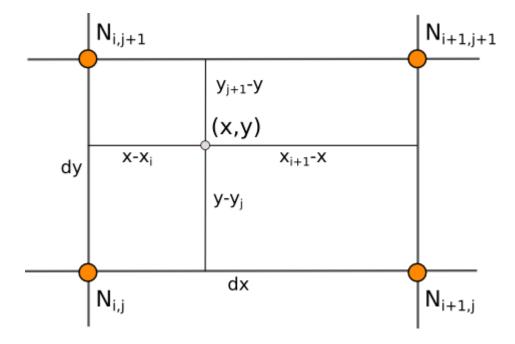
Each grid of a spatial function is a regular grids defined in an interpolation CRS. The coordinates of a grid node are given by

$$x_i = x_o + i.x_s$$
  
 $y_i = y_o + j.y_s$ 

where  $x_o$ ,  $y_o$  are the coordinates of a reference point of the grid,  $x_s$  and  $y_s$  are the grid spacing along the x and y axes respectively, and i and j are the column and row number of the grid node. Note that the x and y grid spacing need not be equal. For example, in a geographic interpolation coordinate system where x is longitude and y is latitude it may be preferable that  $x_s$  is approximately equal to  $y_s/\cos(y_m)$ , where  $y_m$  is the latitude of the middle of the grid, as this makes the grid cells approximately square (except at polar latitudes).

Model components are calculated using bilinear interpolation with respect to x and y between the nodes at the corners of the grid cell within which the calculation point lies, as shown in Figure 2. Each component of the displacement is calculated independently.

Figure 2 — Bilinear interpolation on a grid cell



Bilinear interpolation is defined as follows:

The calculation point (x,y) is located in the grid cell between columns i and i+1, and rows j and j +1.

The weights are assigned to these nodes using the formulae:

$$\begin{split} W_{i,j} &= ((x_{i+1}\text{-}x)/x_s) * ((y_{j+1}\text{-}y)/y_s) \\ W_{i+1,j} &= ((x\text{-}x_i)/x_s) * ((y_{j+1}\text{-}y)/y_s) \\ W_{i,j+1} &= ((x_{i+1}\text{-}x)/x_s) * ((y\text{-}y_j)/y_s) \\ W_{i+1,j+1} &= ((x\text{-}x_i)/x_s) * ((y\text{-}y_j)/y_s) \end{split}$$

The model components at (x,y) are calculated as the weighted average of the values at the nodes as, e.g.:

$$de = W_{i,j}.de_{i,j} + W_{i+1,j}.de_{i+1,j} + W_{i,j+1}.de_{i,j+1} + W_{i+1,j+1}.de_{i+1,j+1}$$

Uncertainties are interpolated from the grid node values using the same formulae.

### 6.2. TIME FUNCTIONS

The time function f(t) for an element evaluates a scalar value by which the spatial function displacement is multiplied to determine the displacement at time t. For example, in a velocity

model the spatial model represents the displacement that happens in one year and the time function evaluates the scale factor f(t) applied to the displacement at time t as the number of years since a function reference epoch  $t_0$ , i.e.  $f(t)=(t-t_0)$ .

The deformation model metadata defines a temporal extent for the model from  $T_{min}$  to  $T_{max}$ . At times before  $T_{min}$  and after  $T_{max}$  every time function is considered undefined and the model cannot be evaluated.

The time function is defined as the sum of one or more base functions.

Each base time function is one of the types listed in the following table.

Table 1 — Base time function types

TIME FUNCTION TYPE	DESCRIPTION
velocity	Defines a scale factor that is linear with time. When multiplied by the spatial function this defines a constant velocity field, typically used to represent secular tectonic velocity.
acceleration	Defines a rate of change of the velocity function. This may be used where the velocity is changing at a constant rate. This is sometimes used to model glacial isostatic adjustment.
step	Defines an instantaneous change of displacement, typically used to model coseismic earthquake deformation.
ramp	Defines displacement accumulating at a linear rate over a fixed period of time. This can be used to simplistically represent post-seismic deformation. In particular, combining several ramp functions can be used to create a piecewise linear time function that can emulate any time behavior to an arbitrary level of accuracy.
exponential	Defines a displacement accumulating at an exponentially decaying rate after an event. This is commonly used to approximate post-seismic deformation. Often used in conjunction with a logarithmic model.
logarithmic	Defines a displacement accumulating proportionally to the logarithm of elapsed time since an event. This is commonly used to approximate post-seismic deformation. It is often used in conjunction with an exponential model.
hyperbolic tangent	Approximates a time behavior observed in slow slip events.
cyclic	Represents cyclic behavior, such as deformation due to seasonal groundwater loading.

The following table lists the reference formulae for each type of time function.

Table 2 — Time function reference formulae

TIME FUNCTION TYPE	PARAMETERS	FORMULA (T <sub>I,MIN</sub> ≤ T < T <sub>I,MAX</sub> )
velocity	Function reference epoch t <sub>0</sub>	$f_r(t) = (t - t_0)$
acceleration	Function reference epoch t <sub>0</sub>	$f_r(t) = (t - t_0)^2$
step	Event epoch t <sub>v</sub>	$f_r(t) = 0$ when $t < t_v$ , $f_r(t) = 1$ when $t \ge t_v$

TIME FUNCTION TYPE	PARAMETERS	FORMULA $(T_{I,MIN} \le T < T_{I,MAX})$
ramp	Start epoch t <sub>s</sub>	$f_r(t) = 0$ for $t < t_s$
	End epoch t <sub>e</sub>	$f_r(t) = (t-t_s)/(t_e-t_s)$ for $t_s \le t < t_e$
		$f_r(t) = 1.0 \text{ for } t \ge t_e$
exponential	Event epoch t <sub>v</sub>	$f_r(t) = 0 \text{ for } t < t_v$
	Time constant $\tau$	$f_r(t) = (1 - \exp(-(t-t_v)/\tau) \text{ for } t \ge t_v$
logarithmic	Event epoch t <sub>v</sub>	$f_r(t) = 0 \text{ for } t < t_V$
	Time constant $\tau$	$f_r(t) = \ln(1 + (t-t_v)/\tau)$ for $t \ge t_v$
hyperbolic tangent	Event epoch t <sub>v</sub>	$f_r(t) = (1 + tanh((t - t_v)/\tau))/2$
	Time constant $\tau$	where $tanh(x) = (e^{x} - e^{-x})/(e^{x} + e^{-x})$
cyclic	Frequency f (cycles per year)	$f_r(t) = \sin(f(t - t_0)/2\pi)$
	Function reference epoch t <sub>0</sub>	

Each base time function is computed using the reference formula  $f_r(t)$  as in table Table 2 above. The result can be modified by three epoch parameters, start epoch  $t_s$ , end epoch  $t_e$ , and function reference epoch  $t_0$ , and a scale factor s. (Note that the ramp function explicitly uses the start and end epoch, and the velocity, acceleration, and cyclic functions explicitly use the function reference epoch.)

The base time function f(t) is evaluated from the reference function  $f_r(t)$  using these epochs as follows:

• If the start epoch is defined then the function is evaluated at the start epoch for all times before the start epoch. If the end epoch is defined then the function is evaluated at the end epoch for all times after the end epoch. That is:

$$f_1(t) = f_r(t_s)$$
 if  $t_s$  is defined and  $t < t_s$   
 $f_1(t) = f_r(t_e)$  if  $t_e$  is defined and  $t > t_e$   
 $f_1(t) = f_r(t)$  otherwise

• If the function reference epoch  $t_0$  is defined then a constant is added to  $f_1$  so that it evaluates to zero at the function reference epoch. That is:

$$f_2(t) = f_1(t) - f_1(t_0)$$
 if  $t_0$  is defined  $f_2(t) = f_1(t)$  otherwise

• If the scale factor s is defined then the function is multiplied by it:

$$f(t) = s.f_2(t)$$
 if s is defined  $f(t) = f_2(t)$  otherwise.

In these formulae all epochs t are defined as a decimal year.

A date/time yyyy-mm-ddTHH:MM:SS is converted to a decimal year as follows. The year number yyyy of the UTC epoch forms the integer part of the decimal year. The fractional part of the decimal year is determined by dividing the number of seconds between the beginning of the year yyyy-01-01T00:00:00Z and the date/time by the total number of seconds in the year (i.e.

the number of seconds between yyyy-01-01T00:00:00Z and yyy1-01-01T00:00Z, where yyy1 is yyyy+1).

Note that there is a small ambiguity in this formulation due to the occasional introduction of leap seconds. This impacts calculations because 1) it is not known at the beginning of the year whether a leap second will be added, and 2) standard software libraries used to implement the time functions may not include leap seconds, and if they do there will often be a delay before updates including leap seconds are distributed to users. In all realistic usages, apart from the step function at the event epoch, the difference in deformation from one second to the next is insignificant.

Since leap seconds impart no practical difference to the deformation model calculations the decimal year is considered compliant whether or not it accounts for leap seconds — there are two nominally correct answers.

Future versions of this specification may add new base time functions.

#### 6.3. COMBINATION OF ELEMENTS

To calculate the total displacement at a time and location, the displacement due to each element is calculated independently and summed. The total displacement is then applied to the coordinate. Displacement uncertainty is calculated similarly using the formula below. The same input position coordinate is used for each element. Deformation components are not applied sequentially, that is the input coordinate is not updated by the first element before being used to calculate the deformation of the second element.

At a given time and location the values obtained from each element are combined to determine the overall displacement. For example, if there are n components for which the spatial model calculates de as  $de_1$ ,  $de_2$ , ... to  $de_n$ , and the time function evaluates to  $f_1$ ,  $f_2$ , ... to  $f_n$  then the total displacement de is

$$de = f_1.de_1 + f_2.de_2 + ... + f_n.de_n$$

The uncertainty eh or ev is the root sum of squares (RSS) of the uncertainty values determined for each element. For example,

$$eh = \sqrt{(f_1^2.eh_1^2 + f_2^2.eh_2^2 + ... + f_n^2.eh_n^2)}$$

# 6.4. APPLYING THE TOTAL DISPLACEMENT TO A COORDINATE

The algorithm for applying a displacement to a coordinate depends on the units of the displacement and the type of the source and target coordinate systems.

If the source and target coordinate systems are projected coordinate systems then the units must be meters and the east and north displacements are simply added to the easting, northing coordinates.

If the source and target coordinate systems are geographic coordinate systems and the east and north displacement units are degrees, then the displacements are added to the longitude and latitude coordinates.

If the source and target coordinate systems are geographic and the east and north displacement units are meters then the displacement components must be converted to degrees before being added to the longitude and latitude coordinates. The conversion from meters to degrees requires the ellipsoid parameters of the geographic coordinate system.

If a is the ellipsoid semi-major axis (e.g. 6378137.0), f is the flattening (e.g. 1.0/298.25722210),  $\lambda$  is the longitude, and  $\phi$  is the latitude then corrections to longitude d $\lambda$  and latitude d $\phi$  (in radians) are given by:

b = a.(1-f)  
dλ = de.
$$\sqrt{(b^2 \sin^2(\phi) + a^2 \cos^2(\phi))/a^2 \cos(\phi)}$$
  
dφ = dn. $(b^2 \sin^2(\phi) + a^2 \cos^2(\phi))^{3/2}/a^2b^2$ 

Note that this formula does not account for the height of a calculation point above the ellipsoidal surface. The deformation model is assumed to represent deformation on the ellipsoidal surface, so the actual east and north offset of a point above or below this surface will be slightly different to that defined in the model.

The vertical displacement is always simply added to the height coordinate.

# 6.5. ITERATIVE CALCULATION OF INVERSE TRANSFORMATION

If the interpolation coordinate system is directly related to the source or target coordinate systems then applying the displacement to a point may change its coordinate in the interpolation coordinate system, which in turn may change the calculated value of displacement. In this case the calculation and application of displacement to an input coordinate may require iteration, as described in Clause 6.5.

Calculating the inverse of the model requires an iterative solution if the interpolation coordinate system is dependent on the output coordinate system. The coordinate in the interpolation coordinate reference system is required to evaluate the displacement, but that coordinate is not known until the displacement has been calculated and applied to the input coordinate to derive the output coordinate.

This will apply in a forward transformation if the interpolation coordinate system is dependent on the target coordinate system, and in a reverse transformation if it is dependent on the source coordinate system.

The iterative calculation uses the following steps:

- use the input coordinate as an initial estimate for the output coordinate
- at each iteration:
  - use the current estimate of the output coordinate to determine the displacement that applies
  - apply this displacement to the input coordinate to obtain a new estimate for the output coordinate
  - calculate the difference between the current and new estimates of the output coordinate
  - if this difference is greater than the precision required for the inverse operation then iterate again, otherwise finish

Note that at the edge of the model it may not be possible to calculate the inverse transformation. The model is undefined outside its spatial extent in the interpolation coordinate system. If the transformation of a point near the edge of the model moves it to a location outside that extent, then the first step of the iterative calculation will fail. This step uses the transformed coordinate as a first estimate for the untransformed coordinate. However that will be a point outside the model, so calculating the transformation at that point is not possible. A more sophisticated algorithm could address this, for example using the nearest point within the spatial extent of the model at the first iteration.

# 6.6. CALCULATION OF DEFORMATION BETWEEN TWO EPOCHS

The displacement de, dn and du to transform a coordinate between two epochs is calculated in a similar way to above except that the time functions are evaluated by taking the difference between the values at each epoch.

To calculate the displacement from epoch  $t_0$  to epoch  $t_1$  the time factors in Clause 6.3 are calculated for the i<sup>th</sup> element as:

$$f_{i,t1-t0} = f_i(t_1) - f_i(t_0)$$

Note that for calculating displacement components this gives the same result as taking the difference between the displacement components calculated individually for each epoch. However, this method must be used to give the correct value of the uncertainty of the displacement between two epochs.



# ANNEX A (INFORMATIVE) NOTES FOR DEFORMATION MODEL PRODUCERS



# ANNEX A (INFORMATIVE) NOTES FOR DEFORMATION MODEL PRODUCERS

### A.1. DECOMPOSITION INTO ELEMENTS

This deformation model specification assumes that the deformation can be partitioned into one or more elements each of which is characterized by a time function. There are many other ways deformation can be modeled. For example in geophysical research it is often modeled using uniform dislocation on a rectangular fault surfaces in a uniform elastic half space. While such models may be used to research and develop deformation models, the common practice in publishing them for coordinate transformations is to convert the model to a grid describing the resultant surface displacement.

Deformation is caused by a number of geophysical phenomena, each of which may be represented by one or more elements in a deformation model.

Typically, there is a secular velocity element representing the long term tectonic deformation — this is a single element with a velocity time function.

Overlaid on this there may be deformation due to earthquakes. The coseismic deformation will be represented by an element with a step time function. Postseismic deformation from the earthquake may be represented by several elements depending on the complexity of the deformation and the quality of information about it. Several versions of a deformation model may be published after an earthquake as the ongoing postseismic deformation evolves and as the measurements and modeling of deformation are refined.

Alternatively, the deformation model may be based more directly on observations. For example, in Japan the dense network of CORS stations provides a continuous record of deformation. Each year a new version of the deformation model is generated based on these measurements. Each of these could be represented by an element with a step time function.

# A.2. REQUIREMENT FOR THE MODEL TO BE CONTINUOUS AND INVERTIBLE

Deformation models described by this specification are used for coordinate operations — either to define time dependent transformations between different coordinate systems or to track the motion of objects between different epochs within a single coordinate system.

Generally, the user expectation of these functions is that they are invertible. That is, data can be transformed between any two epochs, and transforming data from one epoch to another and then back again leaves it unchanged.

To support this expectation the deformation model should be spatially continuous and invertible for any valid epoch. This is specified above as a compliance requirement of a deformation model.

Within a single grid the use of bilinear interpolation ensures that the deformation is spatially continuous. It also ensures the deformation is invertible provided the displacements calculated in the grid are not greater than the grid spacing, which is generally very unlikely.

The only opportunity for discontinuity in a deformation model is at the edges of grids.

This places two constraints on deformation model producers.

- where an element does not cover the full extent of the deformation model then the deformation at the edge of the element must be zero. For example, an element might represent coseismic deformation from an earthquake. The deformation caused by the earthquake may not be significant over the full extent of the model so the element would only cover a subset of that area. To ensure continuity the displacements at the edge element should be set to zero, even though the actual displacements will be slightly different from zero.
- where an element is represented by multiple overlapping or nested grids there will be transitions between one preferred grid and another. At these transitions the values interpolated from each grid must be exactly the same. For example, the displacement at the edge of a child grid will generally have exactly match that of its parent grid. However if the edge abuts the edge of another child grid, then its displacement only needs to match that of the abutting grid.

In practice the second of these constraints means that parent and child grids must be aligned — any node of a parent grid that lies within the child grid must also be a node of the child grid. Where grids are abutting, then along the common edge at least one of the grids should include all the nodes of the other.

These constraints, and indeed the use of a gridded model, mean that the model cannot represent the true deformation exactly. For example, where there is surface faulting the actual deformation may not be continuous across a fault line. The deformation also may not be invertible (at least as a function of horizontal position) in areas of thrust faulting where points

originally on opposite sides of the fault may be moved to the same horizontal position (though at different heights).

For model producers, this can create a tension between the scientific desire to represent deformation as accurately as possible, and the practical constraints of a deformation model suitable for coordinate operations. This specification is framed within the context of coordinate operations — it is not purporting to model deformation for scientific use.

The challenge for model producers is to decide the extent to which the deformation can be usefully modeled to best support the geospatial community.

### A.3. NO DATA AND ZERO VALUES

There may be areas within the extent of the deformation model grids where the deformation is either not known or is not within the model producer's jurisdiction. In these areas the model producer may prefer to not specify an unreliable or unauthoritative displacement.

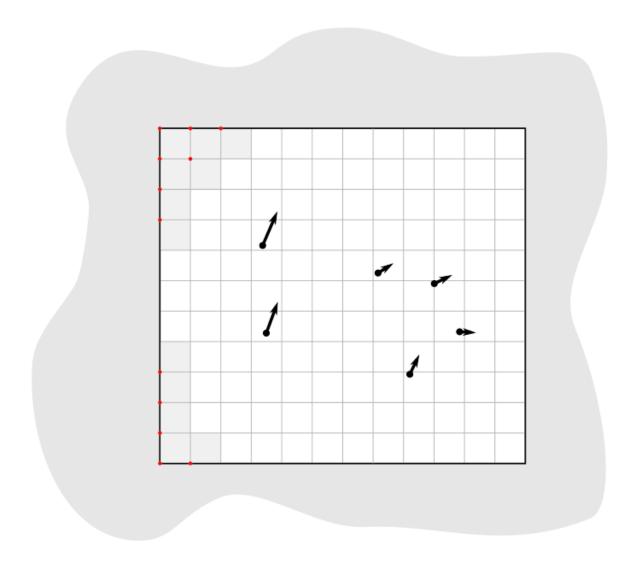
Grids must be defined by rectangular regions, which are unlikely to match the extent of the known deformation. To avoid grids being used in areas where the deformation is undefined, it is desirable that special "no-data" values can be used for displacements at nodes where this applies. The implementation of "no-data" will be dictated by the format used to carry the deformation model.

The "no data" value for a displacement is different from a zero displacement. A value of zero is used where there is no significant displacement. A "no-data" value is used where the displacement is unknown.

Instead of using "no data" values, a producer may choose to specify a value with a large uncertainty. This may be preferable to ensure a continuous and invertible model, as discussed in Annex A.2. However not all software will use uncertainty information.

If any element of the model evaluates to "no-data" at a given location and time then the displacement (or uncertainty) at that location is undefined. Figure A.1 illustrates the use of "no-data" values in the model. In this figure the gray area shows the region where displacement is undefined and the square marks the total extent of the model. Outside this area the model cannot be evaluated. Within the gridded spatial function there are a number of nodes at which the displacement is not defined — these are identified with a "no-data" value. Where these nodes are required to interpolate a displacement, which is any grid cell they are on the boundary of, the displacement cannot be calculated..

Figure A.1 — Influence of "no data" values



The gray area, where displacement is undefined, might include coastal regions where the deformation of the seabed is not measured, or it may cross a jurisdictional boundary. Since the grid is rectangular, it may include regions where the deformation is not known, which are represented in the model by a "no data" value.

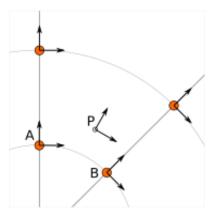
## A.4. DEFORMATION MODELS NEAR POLES

Representing deformation in near polar regions using this specification may not give the desired results if the interpolation coordinate system or source and target coordinate systems are geographic. Both the means of interpolating across a grid cell, and the formulae for applying the displacment to a coordinate, may not be suitable. The simplest way to represent deformation in

such cases is to use a suitable projection coordinate system. Future versions of this specification may add support for geographic coordinate systems in polar regions.

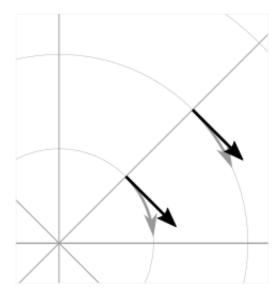
Near the poles grid cells may span a large longitude range. Consequently the east and north components of a vector at adjacent grid nodes may be in quite different directions, as illustrated in Figure A.2. Interpolating east and north components independently as described in Clause 6.1.2 fails to account for this. For example, if the grid cell spans 1° of longitude and the displacement is 1m then bilinear interpolation may give rise to an error of up to about 2cm (the length of the displacement vector multiplied by the cosine of the longitude range of the grid cell). This can be mitigated by using a finer longitude grid spacing.

Figure A.2 — Different directions of east and north components at grid nodes and a calculation point



Where the source and target coordinate systems are geographic, then adding east and north offsets to the the latitude and longitude coordinates may not be appropriate. This is illustrated in Figure A.3 where the gray vector shows the result of adding an east displacement to the longitude coordinate, and the black vector shows the result applying the same east displacement in the direction of the east vector component. Close to the pole, offsetting the longitude coordinate can give a significantly different result to applying a displacement in the direction of the east vector. At the pole itself, offsetting the longitude coordinate makes no difference to the location at all and the formula described in Clause 6.4 cannot be used.

Figure A.3 — Comparison of vector and angular displacement near a pole

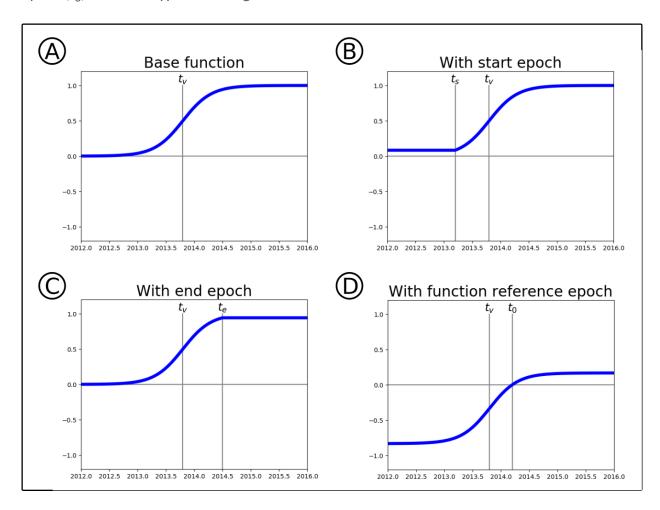


This is only a significant issue very close to a geographic pole. It diminishes rapidly moving away from the pole. For displacement d at a point at distance R from the pole, the difference is approximately  $d^*(1-\cos(d/R))$ , or approximately  $d^3/2R^2$ . For example, applying 1 m east displacement 1 km from the pole by offsetting the longitude would incur an error of only  $5.10^{-7}$  m.

### A.5. TIME FUNCTION EPOCHS

The time functions used for deformation model elements can be modified by specifying a function reference epoch  $t_0$ , a start epoch  $t_s$ , and an end epoch  $t_e$ . The effect of these is illustrated in Figure A.4 showing a base hyperbolic tangent function without these parameters (graph A) and the same function with each parameter applied in turn. The base function has an event epoch  $t_v$  = 2013.8 and a time constant  $\tau$  = 0.5 years.

Figure A.4 — The effects of adding a start epoch ( $t_s$ ), end epoch ( $t_e$ ), and function reference epoch ( $t_0$ ) to a base hyperbolic tangent function



The base function shows an event building in magnitude from 0.0 to 1.0. This might represent, for example, a slow slip event. However it is never exactly 0 or 1, even though it appears to be in the graph. It approaches 0 exponentially as the epoch moves further into the past, and approaches 1 asymptotically as the epoch moves further into the future. The rate of change becomes infinitesimally small more than a few years from the event date.

The start and end epochs can be used to remove any change before the start epoch or after the end epoch. Setting a start epoch (graph B) applies the base function value at that epoch to any time before the start epoch. Similarly, setting an end epoch (graph C) applies the base function value at that epoch to any time after the end epoch. A consequence of this is that the start and end values are no longer 0 and 1. Generally a deformation model producer would use a function reference epoch as well as a start epoch, as described below, so that the time function is zero before the start date.

Using start and end epochs has practical value for deformation model producers managing a coordinate system. In particular using the start epoch means that displacements calculated before that epoch do not change. This may be more realistic geophysically. Although the

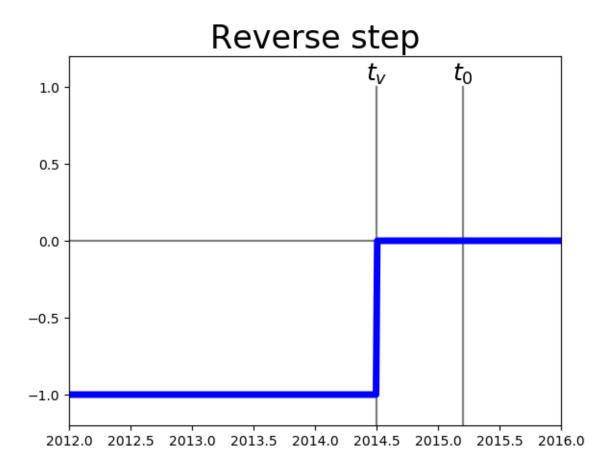
mathematical model does not define it, there is a time at which the slow slip event starts, and before which it is causing no deformation.

The function reference epoch  $t_0$  is an epoch at which the function is forced to be zero, and therefore when the calculated displacement for the event will be zero. A constant offset is added to the function to force it to be zero at this epoch. In graph D the value -0.8 is added to the time functions so that it is zero at the function reference epoch 2014.2.

In a more realistic example the start epoch and function reference epoch would both be used. In graph B, for example, the producer could set the function reference epoch to the same value as the start epoch - 2013.2. This would ensure that the time function is exactly zero for any epoch before this.

One usage of the function reference epoch is to describe deformation that occurred before the reference epoch of a datum. For example an earthquake occurring before the datum epoch may be modeled by a step function with a function reference epoch set to the datum epoch. This is illustrated in Figure A.5 which shows the modified step time function where the event epoch is 2014.5 and the datum epoch is 2015.2. As the datum is referenced to 2015.2 the earthquake has no effect on coordinates observed at or after that date. However, to calculate the location of an object before the earthquake, the displacements caused by the earthquake must be subtracted from the object coordinates. By setting the function reference epoch to 2015.2, the step function becomes -1.0 for dates before the earthquake, and 0.0 for dates after it — a "reverse step" function.

Figure A.5 - A " reverse step" function modeling an earthquake occurring before the datum reference epoch (defined by the function reference epoch  $t_0$ )



В

# ANNEX B (INFORMATIVE) FUTURE DEVELOPMENT

В

# ANNEX B (INFORMATIVE) FUTURE DEVELOPMENT

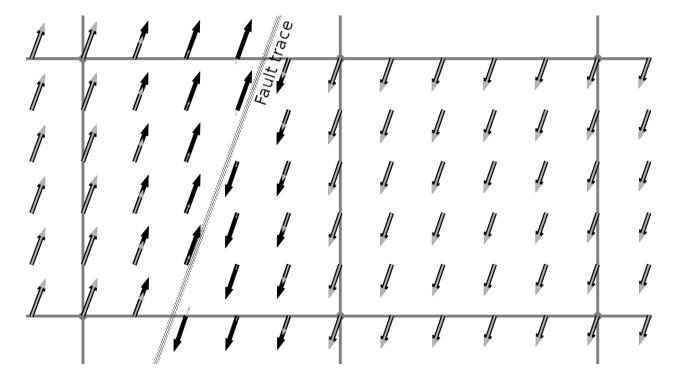
In the terminology of agile development this specification is a "minimal viable product". It is intended to be suitable for the majority of deformation models current and proposed deformation models. However during the course of its development a number of potential future enhancements were identified. Some of these are discussed below.

# B.1. DISCONTINUITIES IN THE DISPLACEMENT FIFLD

One difficulty with representing deformation using gridded deformation models is that they cannot represent discontinuity in the displacement field such as occurs where there is surface faulting. There may be metres of relative coseismic movement across a fault trace which may traverse one or more grids in the model. There may be breaks between segments of a fault trace between which the ground is distorted in unpredictable and often unmeasureable ways.

These displacements cannot be represented in a gridded displacement model in which the displacements are interpolated smoothly across each grid cell. This is illustrated in Figure B.1 showing a modelled displacement field. In the left hand grid cell, containing the fault trace, the interpolated displacement (gray arrows) is very different from the actual displacement (black arrows). By contrast in the adjacent cell, which does not contain a fault trace, the interpolated and actual displacements are visually indistinguishable.

Figure B.1 — Ground displacement (black arrows) and interpolated displacement (gray arrows) in a grid cell containing a fault trace (hashed) line.



There may not be a unique correct way to transform geographic features near a fault trace. For example, the transformation of a cadastral boundary may be define by legal considerations which override the physical movement of the ground. A road crossing a fault trace will be physically straightened to be usable. These considerations cannot be accounted for by the deformation model. In many cases data must be recaptured in such areas to restore spatial integrity.

For the users of deformation models it could be valuable to know when a transformation is likely to be affected by large errors which cannot be represented in the model. Conceptually software would generate a warning to users. For example, this would happen when transforming a feature spanning a fault trace and over a time range that includes the time of the earthquake.

Four mechanisms have been suggested that could either alert users to such a situation, or allow them to discover when it could affect their work.

- add metadata that defines the affected location and time. This could be a multipolygon definition in a standard spatial format, such as well known text, associate with a date or epoch attribute. It could be either included in the deformation model metadata, or as an online resource referenced in the metadata. This specification does not describe any standard for presenting such metadata. It would be up to the user to identify and interpret it.
- use a large uncertainty to indicate where there is likely to be a large difference between the interpolated and actual displacements. While this can be used to indicate the approximate area affected by discontinuity, it is spatially imprecise. A large uncertainty value at a node is interpolated into the four grid cells

surrounding the node. As shown in Figure B.1, the interpolation error from the discontinuity only affects the grid cells containing the fault trace — adjacent cells are not affected. This cannot be accurately represented with uncertainty. Nonetheless it is an option available producers, provided it is understood that it may overestimate the error in the vicinity of a fault trace.

- analyse the displacement vectors at the grid nodes. Grid cells likely to be affected by large interpolation errors could be identified by analysing the displacement vectors themselves. A simple measure of this uncertainty in a grid cell is the the maximum vector difference between any two of the displacement vectors at the four nodes of the cell. For a grid cell spanning the fault trace, the displacement vectors for nodes on one side of the fault are in the opposite direction to those of nodes on the other side of the fault. There is a large vector difference between these vectors. Conversely, for a grid cell to one side of the fault trace, the four displacement vectors have approximately the same direction and magnitude, so the maximum vector difference between any two of these vectors is small. This method require special purpose software to analyse the grids and determine the affected grid cells. The software would then have to alert users when these cells were used in a transformation. A benefit of this approach is that it provides an indication of the magnitude of the potential error.
- use an additional grid node attribute a "flag" value that specifically identifies affected cells. This is a boolean value, either true or false. There are several options for how this could identify the affected cell. One option is to use a convention defining which node identifies a grid cell. For example the node on row i and column j could identify the cell between grid nodes on rows i and i+1 and columns j and j+1. Another option is to set the flag as true on all nodes of an affected grid cell. A grid cell is identified as affected only if the flag value is true on all four of its nodes. Such an attribute would require special processing by software.

One difficulty with all these mechanisms is that coordinate operations are "black box" operations to most users — they often happen within GIS software as data from different coordinate systems or different epochs is combined for analysis and presentation. In many cases this will be done on remote servers presenting information to users in web browsers. Users may not even be aware that a coordinate operation is happening. The mechanisms above would need extensive implementation in the spatial software stack for a warning generated in a coordinate transformation to be presented to users in a meaningful way. In light of this practical difficulty, this specification does not explicitly define how discontinuity should be handled.

Although handling of discontinuity is not defined in this specification, the first two of these options, using metadata and using uncertainty, are available to model producers already.

The third method, analysing the displacment vectors, can be used with any deformation model. An approach like this could be developed in software for analysing deformation models independently of coordinate transformation software. This is an area that may warrant further research once more deformation models, and particularly models incorporating coseismic displacements, become available for analysis.

# B.2. VECTOR INTERPOLATION IN POLAR REGIONS

As noted in Annex A.4 this specification does not support the use of geographic coordinate reference systems (ie latitude/longitude) for deformation models close to the geographic poles. In such cases the horizontal displacement vector cannot be interpolated or applied correctly. Early versions of this specification did include an alternative interpolation method, and an alternative method of adding horizontal displacements to a geographic coordinate. In each case the method involved transforming the displacements to and from a geocentric cartesian coordinate system.

These were removed from the specification for two reasons. The primary reason is that currently there is no requirement for this capability. The second reason is that it was felt further research should be undertaken before recommending these specific methods.



