




hashin_shtrikman_mp: a package for the optimal design and discovery of multi-phase composite materials

Carla J. Becker ¹, Hrushikesh Sahasrabudhe ^{2,3}, Max C. Gallant^{2,4}, Anubhav Jain ³, Kristin A. Persson ^{2,4}, and Tarek I. Zohdi ¹

¹ Department of Mechanical Engineering, University of California, Berkeley, California, United States of America  ² Department of Materials Science and Engineering, University of California, Berkeley, California, United States of America ³ Energy Technologies Area, Lawrence Berkeley National Laboratory, Berkeley, CA 94720, USA ⁴ Materials Sciences Division, Lawrence Berkeley National Laboratory, Berkeley, California, United States of America  Corresponding author

DOI: [10.21105/joss.08412](https://doi.org/10.21105/joss.08412)

Software

- [Review](#) 
- [Repository](#) 
- [Archive](#) 

Editor: [Prashant Jha](#)  

Reviewers:

- [@pastewka](#)
- [@Extraweich](#)

Submitted: 11 April 2025

Published: 01 October 2025

License

Authors of papers retain copyright and release the work under a Creative Commons Attribution 4.0 International License ([CC BY 4.0](https://creativecommons.org/licenses/by/4.0/)).

Summary

hashin_shtrikman_mp is a tool for composites designers who have desired composite properties in mind, but who do not yet have an underlying formulation. The library utilizes the tightest theoretical bounds on the effective properties of composite materials with unspecified microstructure – the Hashin-Shtrikman bounds – to identify candidate theoretical materials, find real materials that are close to the candidates, and determine the optimal volume fractions for each of the constituents in the resulting composite. Its features include (i) leveraging of materials in the [Materials Project](#) database, (ii) integration with the [Materials Project API](#), (iii) use of genetic machine-learning, (iv) agnosticism to underlying microstructure, and (v) ultimate engineering application, make it a tool with much broader applications than its predecessors.

Statement of need

Composites are ubiquitous in engineering due to their tunability and enhanced material properties as compared to their individual constituents. As such, composite design is an active field, but the pursuit of new materials through experimentation is expensive. Today, computational tools for materials design are integral to reducing the cost and increasing the pace of innovation in sectors like energy, electronics, aviation and beyond.

Several Python packages already exist for specific areas in composites modeling, such as [HomoPy](#), [CompositesLib](#), [Compysite](#), [FeCLAP](#), and [material-mechanics](#), all of which perform stress analysis on laminates and/or fiber-reinforced composites using either classical laminate theory or the finite element method. Others exist which, like hashin_shtrikman_mp, utilize the Hashin-Shtrikman bounds on effective composite properties, such as [BurnMan](#) for thermal analysis of composite rocks/assemblages, [rockphypy](#) for mechanical modeling of sand-shale systems, ([Zare & Rhee, 2017](#))'s modeling of clay nanocomposites, [mechmean](#), and ([Zerhouni et al., 2019](#))'s modeling of 3D printed microstructures. All of these tools, however, are highly specific to composite microstructure, macro-geometry, and composition. More notably, they focus on analysis of already well-defined composites, rather than discovery of new materials.

hashin_shtrikman_mp is intended for composites designers who are much earlier in their design process – designers who are seeking out new composite formulations and who are not yet tied to a specific underlying microstructure. hashin_shtrikman_mp defines an inverse problem wherein composite formulations which achieve a desired behavior are found by minimizing a

cost function (Zohdi, 2012). Accounting for both absolute error from the desired properties and targeting even load distribution across constituent phases, `hashin_shtrikman_mp` returns candidate theoretical materials, then searches for real materials in the Materials Project database with properties close to the recommended constituents.

Underlying theory

Governing equations and applicability of the Hashin-Shtrikman bounds

The Hashin–Shtrikman (HS) variational bounds apply to homogenization problems governed by linear, self-adjoint, elliptic partial differential equations of the form

$$-\nabla \cdot (\mathbf{A}(\mathbf{x}) : \nabla u(\mathbf{x})) = f(\mathbf{x}), \quad (1)$$

where $\mathbf{A}(\mathbf{x})$ is a symmetric positive-definite local property tensor. This general formulation covers a wide class of physical phenomena including steady-state heat conduction ($\mathbf{A} = \mathbf{k}(\mathbf{x})$, thermal conductivity), electrostatics ($\mathbf{A} = \boldsymbol{\sigma}_e(\mathbf{x})$, electrical conductivity), and linear elasticity ($\mathbf{A} = \mathbb{E}(\mathbf{x})$, stiffness). Under these assumptions, the effective local property tensor \mathbf{A}^* of the composite is uniquely defined, and the Hashin–Shtrikman bounds give the tightest possible estimates on \mathbf{A}^* given only the phase properties and volume fractions.

Estimate effective composite properties with the HS bounds

When designing composites, simple volume-weighted linear combinations of constituent material properties do not yield accurate approximations of the resulting effective composite properties. Instead, for laminates, materials designers often bound the resulting composite properties using equations from constitutive elastic theory, such as the Hill-Reuss-Voight-Weiner bounds, where the lower bound is the harmonic mean of the constituent material properties and the upper bound is the arithmetic mean (Brown, 2015). For quasi-isotropic and quasi-homogeneous multi-phase composites with arbitrary phase geometry (a more general case), a better option is to use the HS bounds, which provide even tighter ranges on the resulting effective properties (Hashin & Shtrikman, 1962). Equation 2 summarizes the HS bounds on a generalized effective material property y^* of an n -phase composite. The generalized material properties for the n -phases are ordered from least to greatest where $y_1 \leq y_2 \leq \dots \leq y_n$ with corresponding volume fractions that sum to unity $v_1 + v_2 + \dots + v_n = 1$, and are given by

$$y_1 + \frac{A_1}{1 - \alpha_1 A_1} = y^{*, -} \leq y^* \leq y^{*, +} = y_n + \frac{A_n}{1 - \alpha_n A_n} \quad (2)$$

where

$$\alpha_1 = \frac{1}{3y_1} \quad \text{and} \quad \alpha_n = \frac{1}{3y_n}, \quad (3)$$

and

$$A_1 = \sum_{i=2}^n \frac{v_i}{\frac{1}{y_i - y_1} + \alpha_1} \quad \text{and} \quad A_n = \sum_{i=1}^{n-1} \frac{v_i}{\frac{1}{y_i - y_n} + \alpha_n}. \quad (4)$$

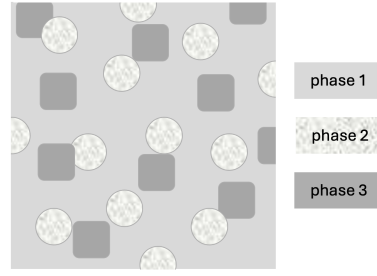


Figure 1: An example of a quasi-isotropic, quasi-homogeneous 3-phase composite.

Equation 5 and Equation 6 summarize the results of the HS derivations on the bounds on effective bulk modulus κ^* and effective shear modulus μ^* , where it is simultaneously required that $\kappa_1 \leq \kappa_2 \leq \dots \leq \kappa_n$ and $\mu_1 \leq \mu_2 \leq \dots \leq \mu_n$:

$$\kappa_1 + \frac{A_1^\kappa}{1 - \alpha_1^\kappa A_1^\kappa} = \kappa^{*, -} \leq \kappa^* \leq \kappa^{*, +} = \kappa_n + \frac{A_n^\kappa}{1 - \alpha_n^\kappa A_n^\kappa} \quad (5)$$

$$\mu_1 + \frac{A_1^\mu}{1 - \alpha_1^\mu A_1^\mu} = \mu^{*, -} \leq \mu^* \leq \mu^{*, +} = \mu_n + \frac{A_n^\mu}{1 - \alpha_n^\mu A_n^\mu} \quad (6)$$

with

$$\alpha_1^\kappa = \frac{3}{3\kappa_1 + 4\mu_1} \quad \text{and} \quad \alpha_n^\kappa = \frac{3}{3\kappa_n + 4\mu_n}, \quad (7)$$

and

$$\alpha_1^\mu = \frac{3(\kappa_1 + \mu_1)}{5\mu_1(3\kappa_1 + 4\mu_1)} \quad \text{and} \quad \alpha_n^\mu = \frac{3(\kappa_n + \mu_n)}{5\mu_n(3\kappa_n + 4\mu_n)}, \quad (8)$$

and

$$A_1^\kappa = \sum_{i=2}^n \frac{v_i}{\frac{1}{\kappa_i - \kappa_1} + \alpha_1^\kappa} \quad \text{and} \quad A_n^\kappa = \sum_{i=1}^{n-1} \frac{v_i}{\frac{1}{\kappa_i - \kappa_n} + \alpha_n^\kappa}, \quad (9)$$

and

$$A_1^\mu = \sum_{i=2}^n \frac{v_i}{\frac{1}{\mu_i - \mu_1} + \alpha_1^\mu} \quad \text{and} \quad A_n^\mu = \sum_{i=1}^{n-1} \frac{v_i}{\frac{1}{\mu_i - \mu_n} + \alpha_n^\mu}. \quad (10)$$

The elastic forms for $\{A_i^\kappa\}$ and $\{A_i^\mu\}$ differ from the general forms $\{A_i\}$ because of their coupling via the Kirchoff-St. Venant constitutive law.

Once upper and lower bounds on the effective composite properties have been obtained, what remains is to find a final estimate of the resulting material properties. By the definition of bounds, we can write an expression for the effective property as

$$y^* = \gamma y^{*, -} + (1 - \gamma) y^{*, +}. \quad (11)$$

Given experimental data, one could fit γ and extrapolate for a range of volume fractions, but, in the absence of experimental data, the authors select $\gamma = 0.5$. For more information, the reader is referred to (Zohdi & Wriggers, 2008).

Quantifying distributed loads with concentration tensors

In addition to finding effective properties of potential composites, hashin_shtrikman_mp recommends composites that are less prone to failure under extreme loading. When loads are not efficiently shared between constituents of the composite, stress concentrations, hot spots, and electrical shorts can develop, eventually leading to material failure. By introducing the concept of “concentration tensors”, we can quantify a constituent’s contribution to load response and then use constitutive laws to determine how the composite will respond to loads.

The general constitutive law given in Equation 1 can also be written more conveniently as

$$\xi(x) = A(x) : \nabla u(x), \quad (12)$$

where $\nabla u(x)$ is a tensor-valued load (a field gradient like strain, electric field, or temperature gradient), $\xi(x)$ is a tensor-valued response (a flux like stress, current, or heat flux), and $A(x)$ is a local property tensor (stiffness, conductivity).

Over the domain Ω , we note that, by the definition of volume fraction, the tensor-valued load will abide by:

$$\langle \nabla u(x) \rangle_{\Omega} = \sum_{i=1}^n v_i \langle \nabla u(x) \rangle_{\Omega_i} \quad (13)$$

and the tensor-valued response will abide by

$$\langle \xi(x) \rangle_{\Omega} = \sum_{i=1}^n v_i \langle \xi(x) \rangle_{\Omega_i}, \quad (14)$$

where $\langle \cdot \rangle_{\Omega} = \frac{1}{|\Omega|} \int_{\Omega} (\cdot) d\Omega$ is the average of (\cdot) over the domain, v_i is the volume fraction of phase i , and n is the number of phases. From there, we define the concentration tensors for the applied loads $\nabla u(x)$ and responses $\xi(x)$ for phases $i \in [1, \dots, n]$, respectively, as

$$\langle \nabla u(x) \rangle_{\Omega_i} \equiv C_{i,\text{load}} \langle \nabla u(x) \rangle_{\Omega} \quad (15)$$

and

$$\langle \xi(x) \rangle_{\Omega_i} \equiv C_{i,\text{response}} \langle \xi(x) \rangle_{\Omega}. \quad (16)$$

It follows from these definitions, and *the assumption that the composite is isotropic and homogeneous*, that the concentration tensors can be written only in terms of local property tensors $A(x)$. The concentration tensors for the applied loads for phases $i \in [2, \dots, n]$ are subsequently given by

$$C_{i,\text{load}} = \frac{1}{n-1} \frac{1}{v_i} [A^* - A_i] : [A_i - A_1]^{-1} \quad (17)$$

and for phase 1 as

$$C_{1,\text{load}} = \frac{1}{v_1} \left(1 - \sum_{i=2}^n v_i C_{i,\text{load}} \right). \quad (18)$$

The concentration tensors for the responses for phases $i \in [2, \dots, n]$ are given by

$$C_{i,\text{response}} = A_i : C_{i,\text{load}} : (A^*)^{-1} \quad (19)$$

and for phase 1 as

$$C_{1,\text{response}} = \frac{1}{v_1} \left(1 - \sum_{i=2}^n v_i C_{i,\text{response}} \right). \quad (20)$$

As a concrete example, consider Ohm's law

$$\mathbf{J}(\mathbf{x}) = \boldsymbol{\sigma}_e(\mathbf{x}) : \nabla \phi(\mathbf{x}), \quad (21)$$

which relates the applied electric field (gradient of the electric potential $\mathbf{E} = \nabla \phi(\mathbf{x})$) to the resulting current density \mathbf{J} via the electrical conductivity $\boldsymbol{\sigma}_e$, governing a 3-phase composite. The concentration tensors for current density would be

$$\begin{aligned} \mathbf{C}_{1,J} &= \frac{1}{v_1} (1 - v_2 \mathbf{C}_{2,J} - v_3 \mathbf{C}_{3,J}), \\ \mathbf{C}_{2,J} &= \boldsymbol{\sigma}_{2,e} : \mathbf{C}_{2,E} : (\boldsymbol{\sigma}_e^*)^{-1}, \\ \mathbf{C}_{3,J} &= \boldsymbol{\sigma}_{3,e} : \mathbf{C}_{3,E} : (\boldsymbol{\sigma}_e^*)^{-1}, \end{aligned} \quad (22)$$

where $\boldsymbol{\sigma}_e^*$ would be found according to the previous section. The concentration tensors for electric field would be

$$\begin{aligned} \mathbf{C}_{1,E} &= \frac{1}{v_1} (1 - v_2 \mathbf{C}_{2,E} - v_3 \mathbf{C}_{3,E}), \\ \mathbf{C}_{2,E} &= \frac{1}{2} \frac{1}{v_2} (\boldsymbol{\sigma}_e^* - \boldsymbol{\sigma}_{1,e}) : (\boldsymbol{\sigma}_{2,e}^* - \boldsymbol{\sigma}_{1,e})^{-1}, \\ \mathbf{C}_{3,E} &= \frac{1}{2} \frac{1}{v_3} (\boldsymbol{\sigma}_e^* - \boldsymbol{\sigma}_{1,e}) : (\boldsymbol{\sigma}_{3,e}^* - \boldsymbol{\sigma}_{1,e})^{-1}. \end{aligned} \quad (23)$$

In the case where the constitutive law governing concentration tensors is the Kirchhoff-St. Venant law, which relates the tensor-valued strain to the tensor-valued stress via the tensor-valued stiffness, we can additionally define scalar-valued concentration factors $C_{i,\kappa}$ and $C_{i,\mu}$, which respectively are the concentration factors for hydrostatic and deviatoric stress. For phases $i \in [2, \dots, n]$ They are defined as

$$C_{i,\kappa} = \frac{1}{v_i} \frac{\kappa_i}{\kappa^*} (\kappa^* - \kappa_1)(\kappa_i - \kappa_1)^{-1} \quad (24)$$

and

$$C_{i,\mu} = \frac{1}{v_i} \frac{\mu_i}{\mu^*} (\mu^* - \mu_1)(\mu_i - \mu_1)^{-1}, \quad (25)$$

where

$$\left\langle \frac{1}{3} \text{tr} \boldsymbol{\sigma} \right\rangle_{\Omega_i} \equiv C_{i,\kappa} \left\langle \frac{1}{3} \text{tr} \boldsymbol{\sigma} \right\rangle_{\Omega} \quad (26)$$

and

$$\langle \boldsymbol{\sigma}' \rangle_{\Omega_i} \equiv C_{i,\mu} \langle \boldsymbol{\sigma}' \rangle_{\Omega}. \quad (27)$$

For phase 1, the concentration tensors are defined as

$$\mathbf{C}_{1,\kappa} = \frac{1}{v_1} \left(1 - \sum_{i=2}^n v_i C_{i,\kappa} \right) \quad (28)$$

and

$$\mathbf{C}_{1,\mu} = \frac{1}{v_1} \left(1 - \sum_{i=2}^n v_i C_{i,\mu} \right). \quad (29)$$

For more information, the reader is referred to (Zohdi & Wriggers, 2008).

Package overview

Implementation notes

The library has been designed to handle the design of 2- to 10-phase isotropic and homogeneous composites. All materials in the Materials Project database are available for search through `hashin_shtrikman_mp`, but it is recommended that users restrict the search bounds for universal anisotropy to be between 0.5 and 1.5 for results closer to theory. Additionally, at the time of this writing, because of the assumption that the composite and its constituents are isotropic and homogeneous, the full tensor forms for the effective properties and concentration tensors are collapsed to scalar forms. This is simpler computationally and allows the same code to be used for all properties (aside from bulk and shear moduli, which cannot be decoupled). For material properties in the Materials Project database with full tensor values available, `hashin_shtrikman_mp` uses the largest eigenvalue. [Figure 2](#) is a flow chart demonstrating the most common usage of `hashin_shtrikman_mp`.

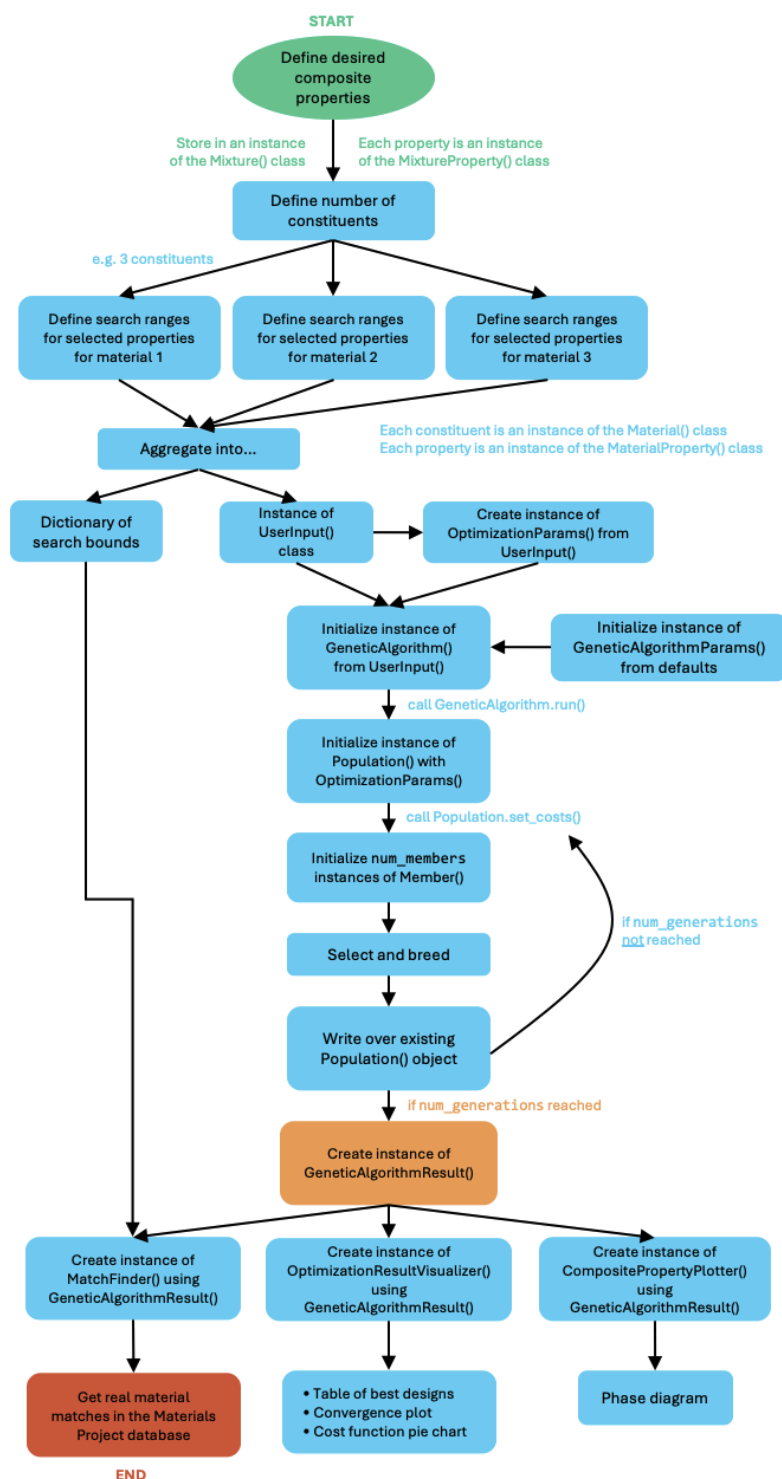


Figure 2: A flow chart demonstrating the most common usage of hashin_shtrikman_mp.

Cost function design and optimization with genetic algorithm

To find optimal composite mixtures, `hashin_shtrikman_mp` simultaneously seeks composite compositions with effective properties close to the desired properties and seeks to ensure even load sharing among the composite constituent phases. Accordingly, the cost function is constructed in the following way.

Each property category selected by a user contributes its own term to the total cost function. At the time of this writing, the possible property categories are elastic, dielectric, carrier-transport, magnetic, and piezoelectric. Combining the individual cost functions to optimize across all design goals simultaneously yields

$$\Pi^{\text{total}} = W_{\text{domains}} [\Pi^{\text{elastic}} + \Pi^{\text{dielectric}} + \Pi^{\text{carrier-transport}} + \Pi^{\text{magnetic}} + \Pi^{\text{piezoelectric}}] \quad (30)$$

where W_{domains} normalizes for the number of active property categories. Each property category contribution is composed of two weighted sums: 1) one with terms for absolute error between the effective and desired properties and 2) another for the absolute error between the concentration factors and a tolerance TOL that quantifies “well-distributed” load sharing. That is,

$$\Pi^{\text{general}} = \begin{cases} w_{\text{eff}} \sum_{i=1}^{n_{\text{props}}} \left| \frac{y_i^{*,D} - y_i^*}{y^{*,D}} \right| + \sum_{i=1}^{n_{\text{cfs}}} \hat{w}_{\text{cf}}^i \left| \frac{C_i - \text{TOL}}{\text{TOL}} \right|, & \text{if property category active,} \\ 0, & \text{else,} \end{cases} \quad (31)$$

where the superscript D denotes the desired value, n_{props} is the number of properties in that property category, n_{cfs} is the number of concentration factors in that category (typically two \times the number of properties), and C_i is a general scalar-valued concentration factor from section “Quantifying distributed loads with concentration tensors”. Note also that $w_{\text{eff}} = 1/n_{\text{props}}$ and

$$\hat{w}_{\text{cf}}^i = \begin{cases} w_{\text{cf}}, & C_i > \text{TOL}, \\ 0, & \text{otherwise,} \end{cases}$$

where $w_{\text{cfs}} = 1/(2n_{\text{props}}n_{\text{materials}})$, except in the elastic case where $w_{\text{cfs}} = 1/n_{\text{props}}n_{\text{materials}}$.

As a concrete example, the dielectric contribution to the cost function would take the form

$$\Pi^{\text{dielectric}} = \begin{cases} w_{\text{eff}} \left| \frac{\epsilon^{*,D} - \epsilon^*}{\epsilon_{ij}^{*,D}} \right| + \hat{w}_{\text{cf}}^{i,E} \left| \frac{C_{i,E} - \text{TOL}}{\text{TOL}} \right| + \hat{w}_{\text{cf}}^{i,E_0} \left| \frac{C_{i,E_0} - \text{TOL}}{\text{TOL}} \right|, & \text{if dielectric property category active,} \\ 0, & \text{else,} \end{cases} \quad (32)$$

where the constitutive law, in the scalar case, relates applied field E_0 to resulting field E via the dielectric constant ϵ according to $E = \epsilon E_0$ and the same rules for the weights apply as above.

With the cost function defined, `hashin_shtrikman_mp` converges to an optimal solution with a genetic algorithm. Each member of a population in the genetic algorithm is composed of candidate material property values. After successive selection and breeding over many generations, the genetic algorithm will converge. The default genetic algorithm parameters are 10 parents, 10 children, 200 members per population, and 100 generations, but a user can change them. Given the cost function design, the cost value can be thought of as the fractional error from the desired outcome, plus penalties for “bad” load sharing (should contribute 0 in the case of “good” load sharing). A user can monitor the results of the genetic algorithm with the convergence plot, an example of which is included in [Figure 3](#).

Notes on genetic algorithms: Genetic algorithms are great for exploring promising parts of the design space, and since the end goal is to choose composite constituents from a set of discrete choices (materials in the MP database), no further refinement with a gradient-based optimization method is needed. The nature of genetic algorithms is to produce several offspring with the same properties and costs after many generations. Thus, `hashin_shtrikman_mp` presents the user with only the *unique* top performing designs in a table. For the singular lowest-cost performer, users are presented with a breakdown of the cost, as in Figure 4.

Visualization and analysis

`hashin_shtrikman_mp` provides visualization tools for the genetic algorithm results and for matches with 2-, 3-, or 4- phases.

Figure 3 is a convergence plot showing the value of the genetic algorithm cost function decreasing over generations. The monotonically decreasing staircase nature is characteristic of genetic algorithm convergence, where the best performer may remain the best for several generations and where several genetic strings may converge to the same value (e.g. when the average cost of top ten performers equals the best cost). As the cost function has been designed to represent absolute error from the desired properties, a cost of 1.0 represents 100% error.

Figure 4 contains a breakdown of the non-zero cost at the end of optimization for a 3-phase material where the properties of interest were electrical conductivity, thermal conductivity, bulk modulus, shear modulus, and universal anisotropy. We expect the cost function to have 31 terms in this case, as there is one effective property term per property and there are two concentration factor terms per property per material, except in the coupled case of bulk and shear moduli, where there are two concentration factors per material instead of the expected four i.e.

- 5 effective properties: one for each of the properties of interest,
- 18 non-modulus concentration factors: one load and one response concentration factor for each of the 3 non-elastic properties (electrical conductivity, thermal conductivity, and universal anisotropy), and for each of the 3 phases, and
- 6 modulus concentration factors: one hydrostatic and one deviatoric concentration factor for each of the 3 phases.

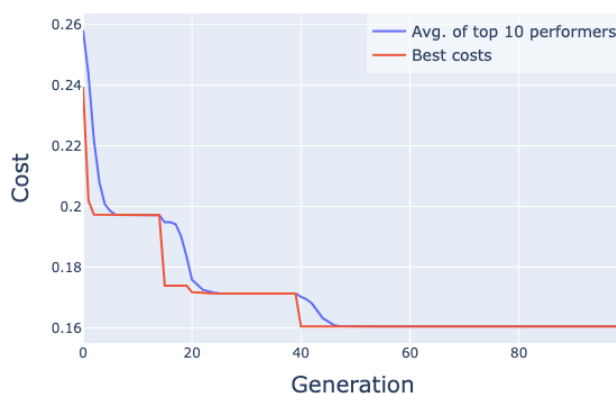


Figure 3: An example of the convergence plot for the genetic algorithm.

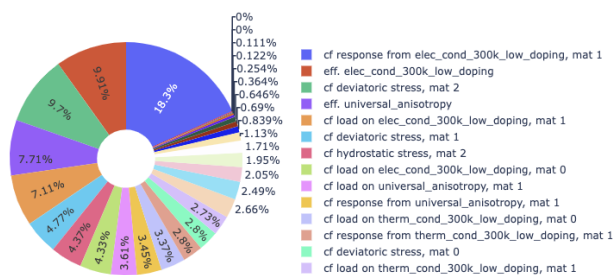


Figure 4: A breakdown of the contributions to the non-zero cost at the end of optimization. Due to the scrollable nature of the legend, only a subset of the 31 entries is visible.

Once matches have been identified for a desired composite, along with recommended volume fractions, a user can still explore how varying the volume fractions of the constituents affect the resulting effective properties through interactive phase diagrams. Examples of these phase diagrams are included in [Figure 5](#), [Figure 6](#), and [Figure 7](#).

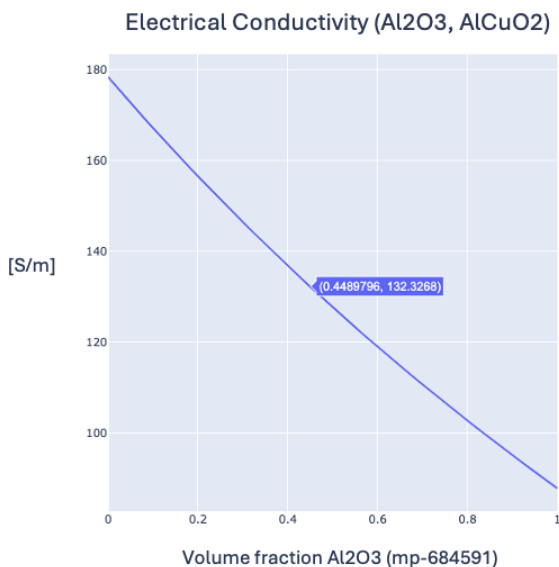


Figure 5: Example phase diagram for a 2-phase mixture of Al_2O_3 and AlCuO_2 . The “mp” numbers are the Materials Project IDs for the materials.

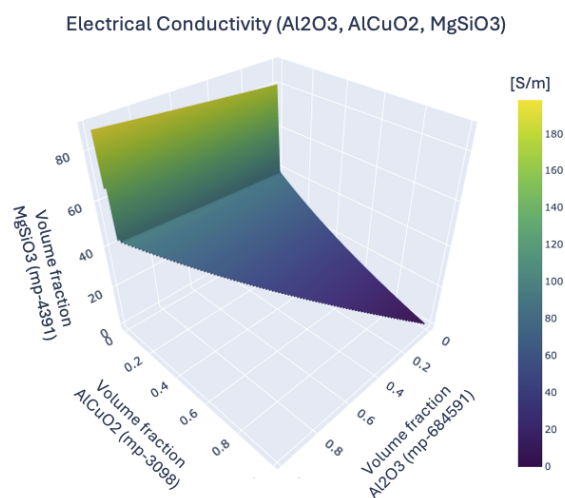


Figure 6: Example phase diagram for a 3-phase mixture of Al₂O₃, AlCuO₂, and MgSiO₃.

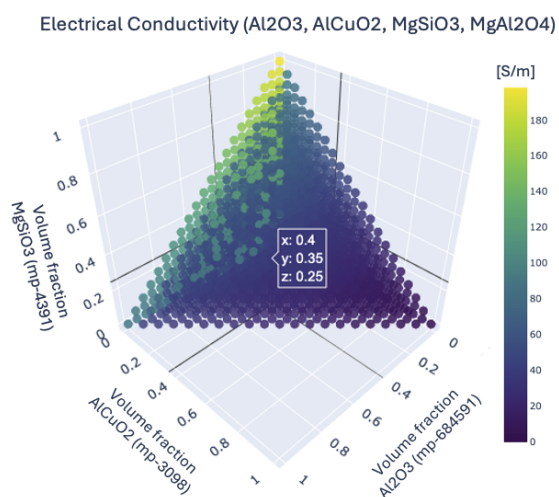


Figure 7: Example phase diagram for a 4-phase mixture of Al₂O₃, AlCuO₂, MgSiO₃ and MgAl₂O₄.

Match-finding

The genetic algorithm returns suggested material properties for each of the phases in the composite and then `hashin_shtrikman_mp` finds real materials in the Materials Project database which are similar, according to some percent error threshold, which the user can control.

Acknowledgments

This work was primarily funded by the Materials Project, which is funded by the U.S. Department of Energy, Office of Science, Office of Basic Energy Sciences, Materials Sciences and Engineering Division, under Contract no. DE-AC02-05-CH11231: Materials Project program KC23MP. The project has been intellectually led by Tarek Zohdi and Kristin Persson. We would also like to thank the software engineering team at the Materials Project – Patrick Huck, Jason Munro, and Ruoxi Yang – for their support.

References

- Brown, J. M. (2015). Determination of hashin–shtrikman bounds on the isotropic effective elastic moduli of polycrystals of any symmetry. *Computers & Geosciences*, 80, 95–99. <https://doi.org/10.1016/j.cageo.2015.03.009>
- Hashin, Z., & Shtrikman, S. (1962). A variational approach to the theory of the effective magnetic permeability of multiphase materials. *Journal of Applied Physics*, 33(10), 3125–3131. <https://doi.org/10.1063/1.1728579>
- Zare, Y., & Rhee, K. Y. (2017). Development of hashin-shtrikman model to determine the roles and properties of interphases in clay/CaCO₃/PP ternary nanocomposite. *Applied Clay Science*, 137, 176–182. <https://doi.org/10.1016/j.clay.2016.12.033>
- Zerhouni, O., Tarantino, M. G., & Danas, K. (2019). Numerically-aided 3D printed random isotropic porous materials approaching the hashin-shtrikman bounds. *Composites Part B: Engineering*, 156, 344–354. <https://doi.org/10.1016/j.compositesb.2018.08.032>
- Zohdi, T. I. (2012). *Electromagnetic properties of multiphase dielectrics: A primer on modeling, theory and computation* (Vol. 64). Springer Science & Business Media. <https://doi.org/10.1007/978-3-642-28427-4>
- Zohdi, T. I., & Wriggers, P. (2008). *Introduction to computational micromechanics*. Springer-Verlag. <https://doi.org/10.1007/978-3-540-32360-0>