



Tutorial C T-pipe junction Steady State Thermomechanical FEM model

By Ofentse Kgoa kgoaot@eskom.co.za

Introduction



Background:

It is assumed that Tutorial A is completed.

Objectives:

- Open an existing FreeCAD project
- Prepare CAD geometry for FEM modeling
- Perform a longitudinal load calculation
- Run a steady state thermomechanical FEM model
- Evaluate and analyze the thermomechanical FEM results
- Save the FreeCAD project

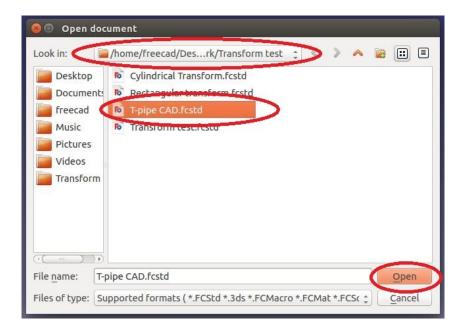
Project start Up



Open an existing project:

- To open an existing project, click on <Open a document or import files>
- A task dialogue appears, choose the directory the file directory, select the project to be opened and then click on <Open>

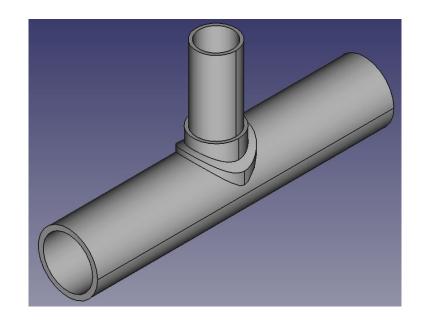






Notes and assumptions:

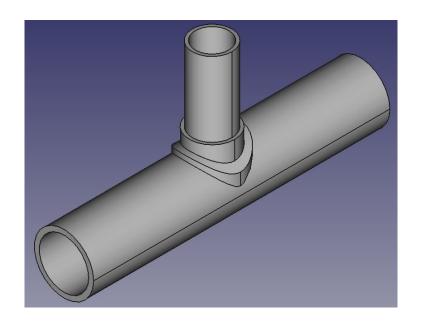
- The thermomechanical model will use the same geometry, material specification and mesh as that used in the static FEM model. Refer to Tutorial B to obtain the Mesh, Material and Boundary constraints information.
- The thermomechanical model will have the same boundary conditions as that of the static model with the addition of thermal boundary conditions.
- The external surfaces of the branch and shell pipe are insulated, whilst the reinforcement is not insulated. The induced stresses due to this are to be investigated.





Notes and assumptions:

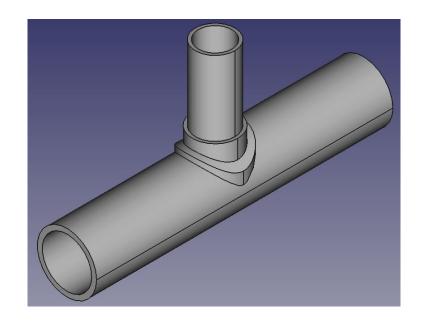
- Air is the fluid surrounding the Tpipe with a heat transfer coefficient
 of 10 W/m²K and at ambient
 temperature of 300 K. Steam at 725
 K flows through the pipe and loses
 heat to air. The heat transfer
 coefficient for water is 1000 W/m²K
- Heat transfer in the longitudinal and circumferential direction is assumed to be negligible.
- A steady state analysis is performed. In a steady state analysis, all variables are independent of time.





Notes and assumptions:

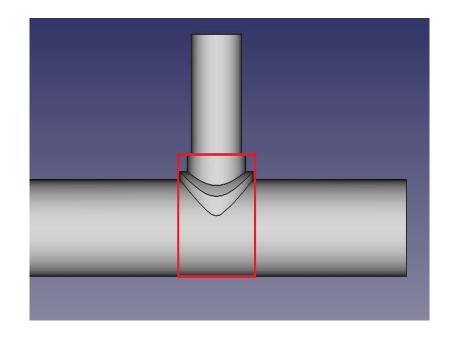
- An end cap is not placed on one of the end faces of the shell pipe this is due to the fact that the end cap will not heat up at the same rate as the rest of the T-pipe.
- This causes a thermal gradient that induces thermal stresses on the Tpipe. Because the end cap is just an artificial way of applying a longitudinal load on one of the end faces, these induced thermal stresses are not real and affect the accuracy of the results.
- The problem can simply be avoided by just calculating and applying the longitudinal load on the end face of the T-pipe.





Preparing the geometry:

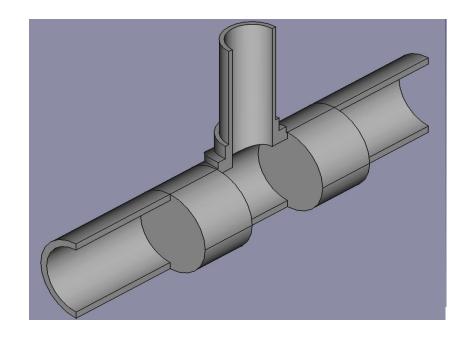
- Pipes are insulated using insulation blankets/cladding that is wrapped around the pipe.
- Due to this the external surface area depicted in the picture is the area that is not insulated and it is therefore exposed to the surrounding air.
- The branch pipe needs to be cut in order to create selectable surfaces on which a heat flux will be applied to.





Preparing the geometry:

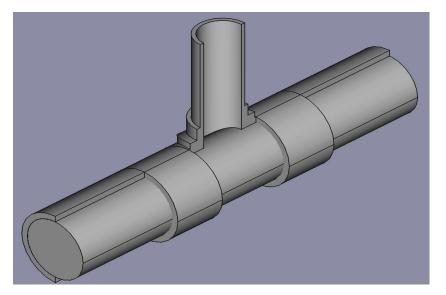
- Create a cylinder of radius 150 mm and a length of 200 mm. Translate this cylinder -150 mm in the Y direction. Rotate this cylinders 90° about the X-axis as indicated in the picture.
- Create another cylinder with a radius of 150 mm and a length of 200 mm. Translate this cylinder 350 mm in the Y direction. Rotate this cylinders 90° about the X-axis as indicated in the picture.
- Join the two cylinders together using the <Make union of several shapes>.

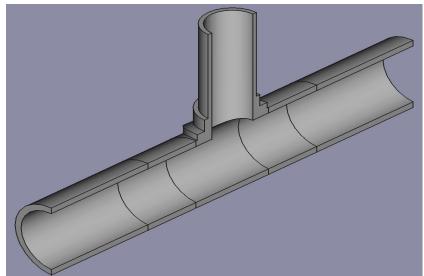




Preparing the geometry:

- Create another cylinder of length 1500 mm and radius 125 mm. Rotate and translate the cylinder so that it is similar to that depicted in the picture.
- Cut the two cylinders in half so that they are similar to that depicted in the picture.
- Join all the parts together with <Make union of several shapes>.

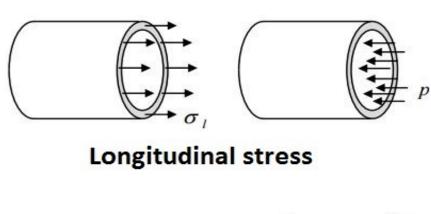


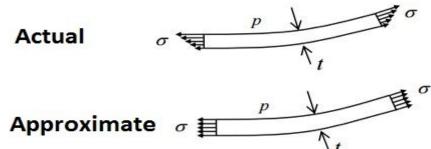




Determining the longitudinal load:

- The longitudinal stress on the shell pipe has already been calculated in Tutorial B under "Verification". This stress will used as a pressure applied to the end face of the shell pipe.
- As depicted, the downside of the calculation is loss of accuracy as it assumes that the stress distribution along the thickness of the pipe is uniform.
- The longitudinal pressure to be applied to the shell pipe end face is 24.75 MPa (from Tutorial B).





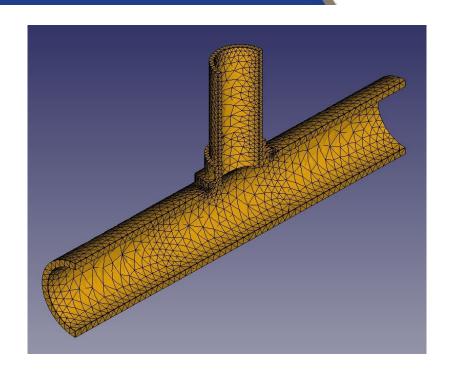


Creating the Mesh:

- For all FEM models, a mesh needs to be created.
- Refer to Tutorial B which shows how to create a mesh.

Material specification:

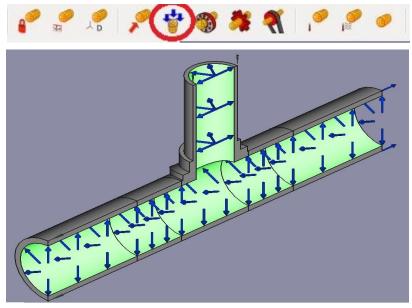
- The material to be used in the analysis is "Steel-Generic".
- Refer to Tutorial B on how to specify a material.

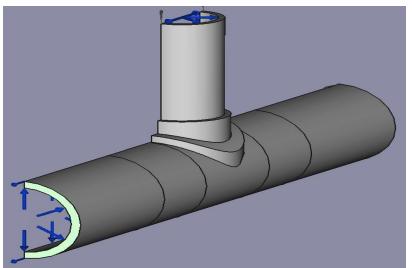




Boundary Conditions:

- The T-pipe needs to fixed in the X, Y and Z directions. To do this use the displacement constraint. Refer to Tutorial B for more information.
- Add a pressure of 9 MPa to the internal surface of the T-pipe as indicated in the picture.
- Add a pressure of 24.75 MPa to the end face of the T-pipe. The direction should be the same as that indicated in the picture.



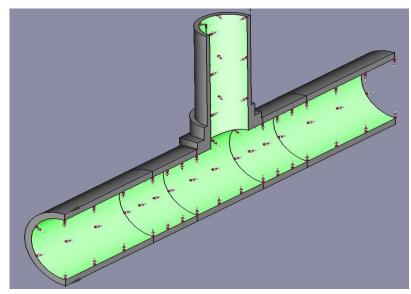




Boundary Conditions:

- The initial temperature of the body needs to be specified for all thermomechanical analysis. Click on <Create FEM constraint for initial temperature acting on the body> and enter an initial temperature of 300 K. Note that temperature is always specified in Kelvin [K].
- Add a heat flux constraint on the internal surface of the T-pipe with <Create FEM constraint for Heat flux acting on a face>. The ambient temperature should be 725 K and the Film coefficient should be 1000 W/m²K.



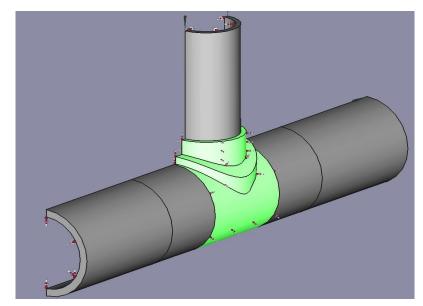




Boundary Conditions:

- Add a heat flux constraint on the reinforcement of the T-pipe as indicated in the picture with <Create FEM constraint for Heat flux acting on a face>.
- The ambient temperature should be 300 K and the Film coefficient should be 10 W/m²K.
- A face with no thermal boundary condition implies that the face is insulated.
- A picture showing all the boundary conditions for the model is displayed for reference





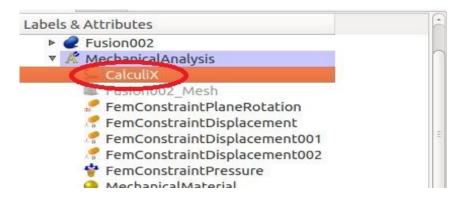


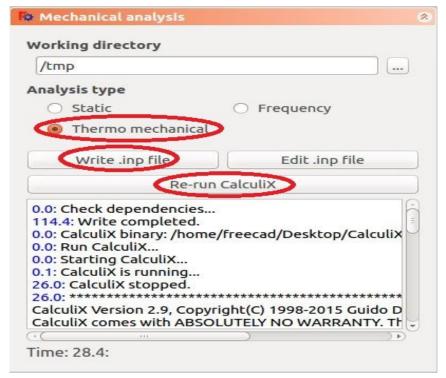
Thermomechanical FEM model (Steady state) Running the solver



Running the analysis:

- Double click on <CalculiX> in the object tree view.
- Select a Thermomechanical analysis
- Write the input file
- Run CalculiX

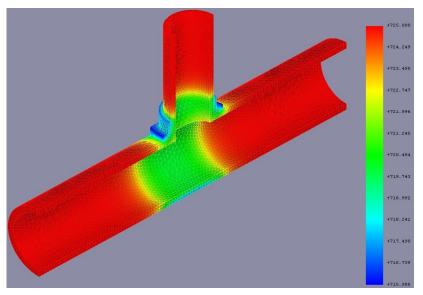


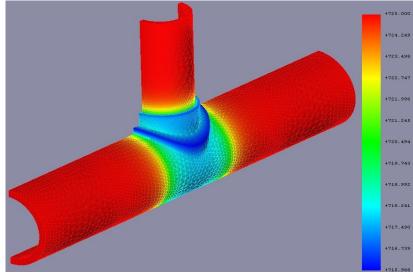




Viewing the results:

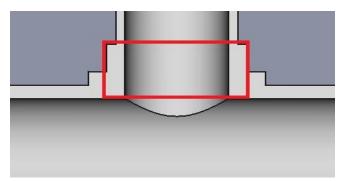
- Create a new pipeline that displays the temperature distribution across the T-pipe section. Remember to hide all other objects that are displayed in the document window.
- The temperature distribution (in Kelvin) across the T-pipe is displayed in the pictures.
- Other result sets(stress or displacement) can also be viewed with the pipeline.

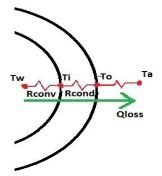






Verification:





Im thirs in istatacre, eyeviéric action is used sted check her blether to the notation of the office who is solver to also solved this is the distance of the contract of the

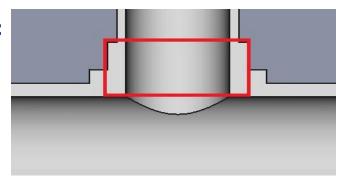
Thermal resistance analysis(for pipes):

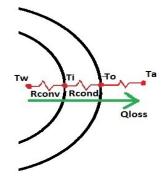
- 11. (Pleat-Heax, filtern perature perature mal-resistance, ii = immer wall, o = outer wall, a = ambient (air), w = water cond = heat conduction through the wall, conv = heat convection by fluid
- 2. $\Delta T_{total} = T_a T_w$, $R_{total} = R_{conv,w} + R_{cond} + R_{conv,a}$
- 23. [@nergy Qalance, Qwith, Q as the at flux]

4.
$$Q_{loss} = \frac{\Delta T_{total}}{R_{total}}$$



Verification:





- $R_{conv} = \lim_{\pi r Lh} h^{-1}$, pipe = $\frac{1}{\pi} e^{-\frac{1}{2} i \frac{\pi}{2} h}$, pipe = $\frac{1}{\pi} e^{-\frac{1}{2} i \frac{\pi}{2} h}$
- 7. , $k = \lim_{n \to \infty} 1$ conductivity
- 7. $R_{cond} = \frac{r_i}{\pi kL}$, k = thermal conductivity
- 8. $T_a = 300 \text{ K}, \quad T_w = 725 \text{ K}$

Klength vof/reagion that conducts here, see shide=9).000 W/m²K

 $L_{b} + e_{as} = 0.103 m$ (length of region that conducts heat, see slide 9)

$$r_o = 0.115 \text{ mm}, r_o = 0.085 \text{ mm}$$

8.
$$R_{conv,w} = 0.0.036 \frac{K}{W}$$
, $R_{cond} = 0.0.019 \frac{K}{W}$, $R_{conv,a} = 2.69 \frac{K}{W}$

9.
$$Q_{loss} = -155.0 \text{ W}$$

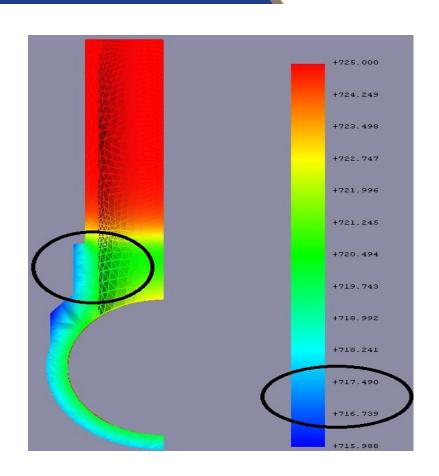
10.
$$T_o = T_a - Q_{loss} R_{cond} = 716.47 \text{ K}$$



Verification:

- The clipping plane result pipeline is used for verification.
- The outer wall of branch pipe has a temperature in the range of 716.7

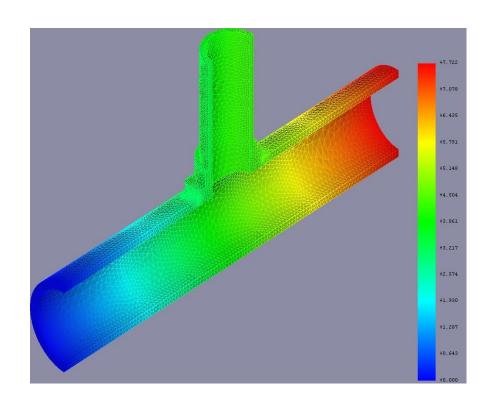
 717.5 K as can be seen in the picture. The calculated outer wall temperature of 716.45 K is fairly close to the temperature range.
- Furthermore, it can be seen that the rest of the T-pipe (areas excluding the reinforcement) go to a temperature of 725 K (steam temperature), which is to be expected because these regions are insulated on the outside and therefore heat is not lost.
- It can now be concluded that the FEM solver has correctly solved for





Analyzing the results(Displacements):

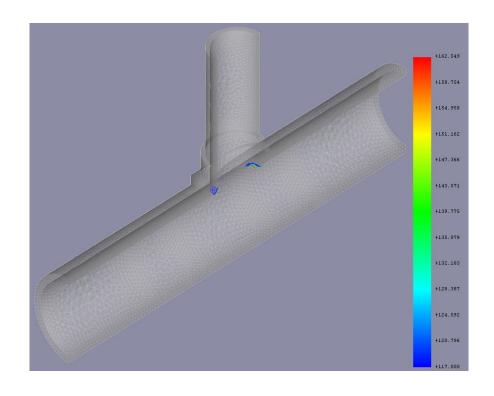
- Now that it has been verified that the temperatures were solved for correctly, we can start analyzing the displacement.
- In some cases, the T-pipe may only be allowed a certain amount of displacement due to its support.
- Create a pipeline that displays the displacement in the y-direction(axial shell pipe direction), from this it is found that the maximum displacement in the y-direction is 7.815 mm.
- If this displacement is not accounted for or beyond the maximum allowed displacement in the direction, it can induce stresses on the parts and it may lead to failure.





Analyzing the results(Stresses):

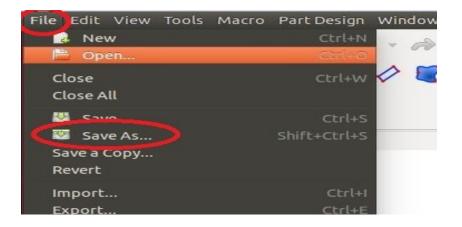
- A von mises stress scalar clip of 117
 MPa is created to investigate which
 regions in the T-pipe experience
 stresses above the design stress.
- It can be seen that the branch and shell pipe junction experiences a stress of 162 MPa which is above the design stress but below the proof strength (175 MPa).
- It can be concluded that in the steady state operation of the T-pipe junction, the pipe does not fail.

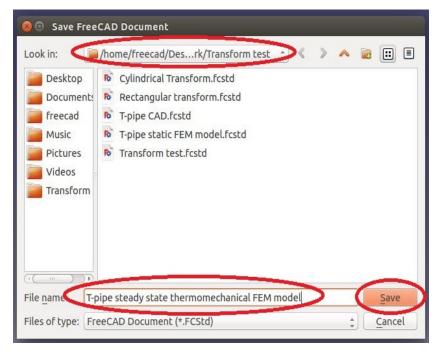


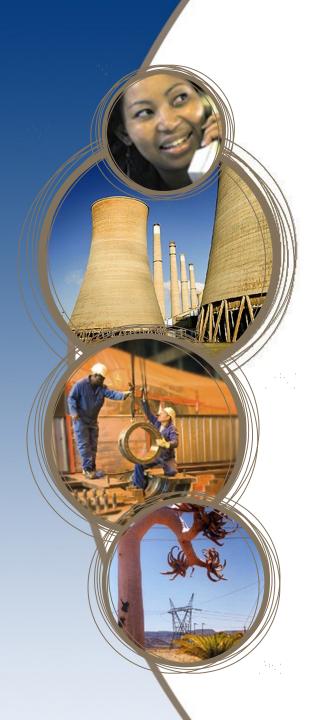


Saving the FreeCAD project:

- To save the project under a different name, go to File and then click on <Save As>.
- A task dialogue appears, choose the file directory, enter the file name and click <Save>.
- The project is going to be used for the transient thermomechanical model.









END

