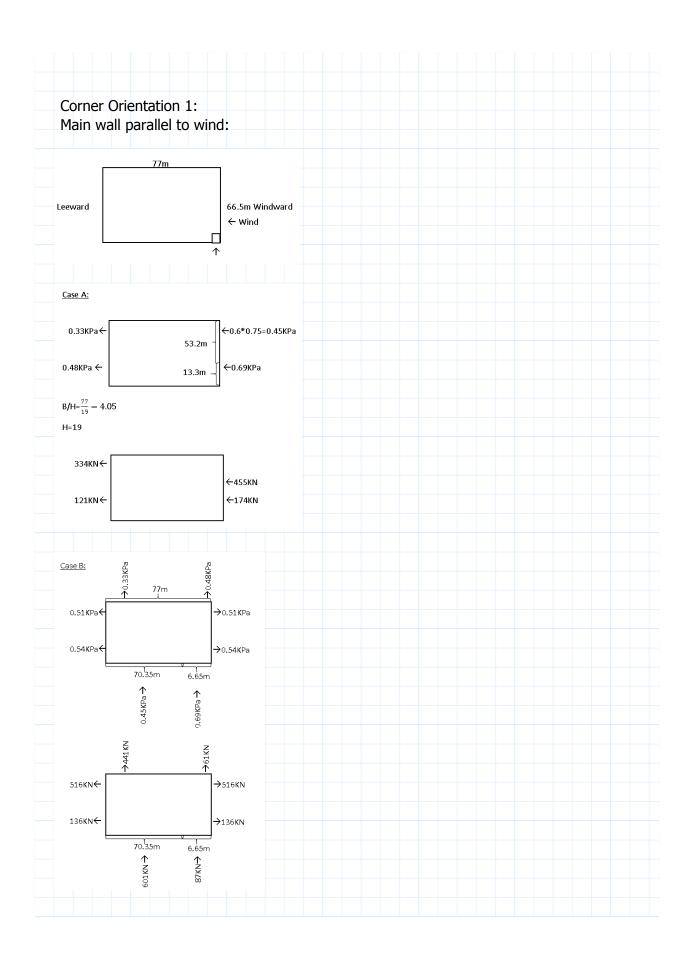
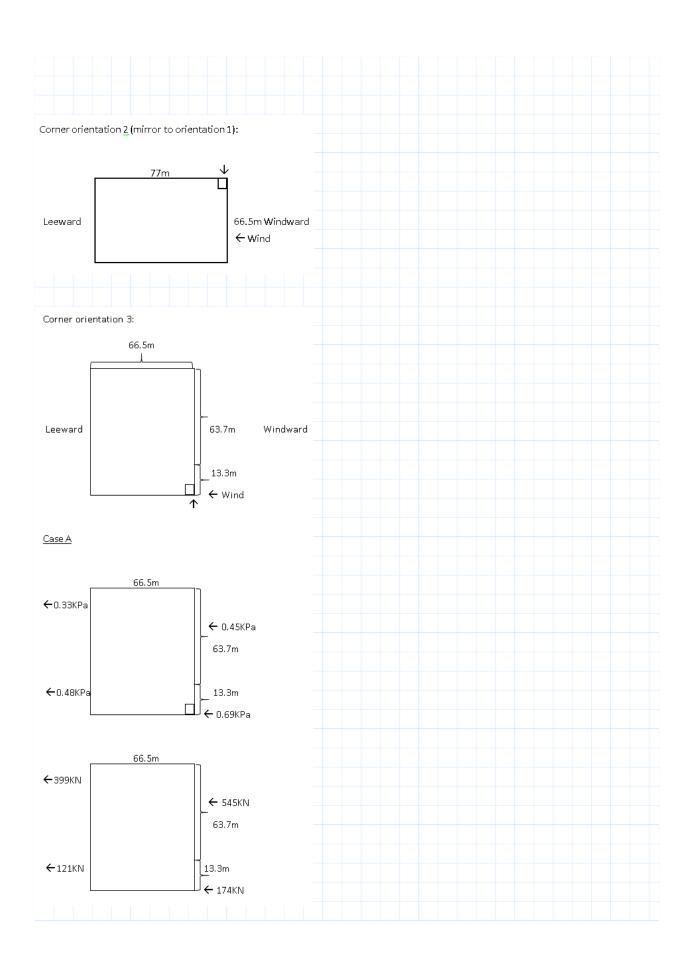
OMAR SHEMY PORTFOLIO

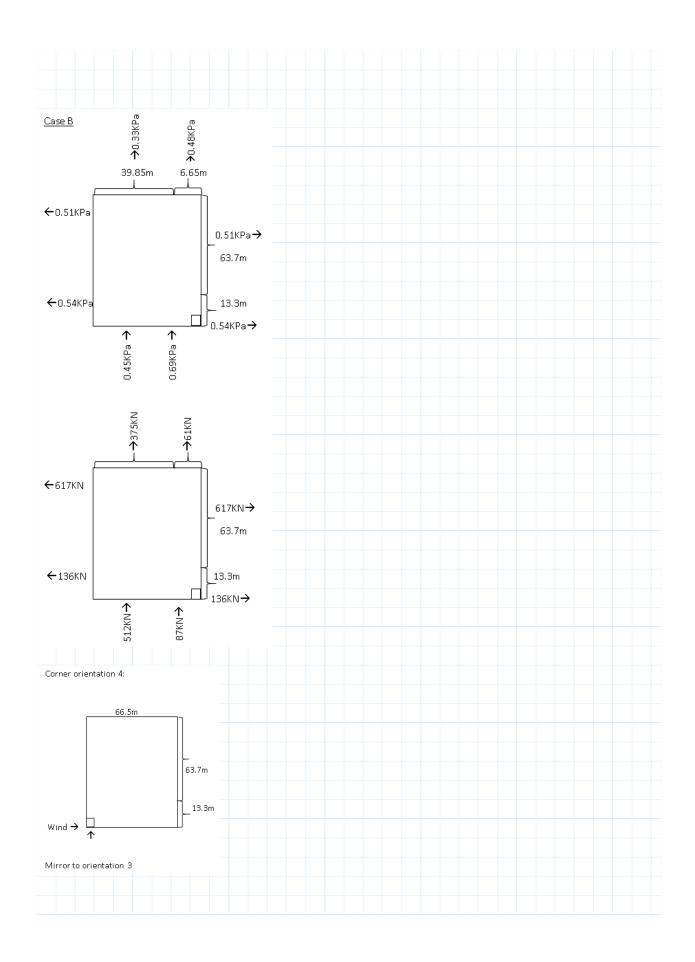
SUBJECT: Wind Load Calculation

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	References(from NBCC 2015)
$I_w = 1.0$	Table 4.1.7.3.
q = 0.6 for 1/50 year exceedence	1.1.3 Appendix C
$h = 19 \le 20$ an $h < 66.5$ (smaller planar dimension)	4.1.7.3 sentence b)
$h = \frac{19}{2} = 9.5$ 9.5 > 6 : OK	
$\begin{array}{c} \text{d} \\ h \coloneqq \frac{19}{2} = 9.5 & 9.5 > 6 \therefore \text{OK} \\ C_e \coloneqq \left(\frac{9.5}{10}\right)^{0.2} = 0.99 \qquad C_e \ge 0.9 \qquad \therefore \text{OK} \end{array}$	
$C_t = 1.0$ For no hills and escarpments	4.1.7.4
Load case a	
Main Wall	4.1.7.6
$C_p C_{q1} = 0.75$	
$C_p^P C_{g2}^{g1} = -0.55$	
$P_{windward\ mainwall} = 1.0 \cdot 0.6 \cdot 0.99 \cdot 1.0 \cdot 0.75 = 0.446$	
$P_{leeward_mainwall} \coloneqq 1.0 \cdot 0.6 \cdot 0.99 \cdot 1.0 \cdot 0.55 = 0.327$ Edge(High zone)	
$C_p C_{g3} \coloneqq 1.15$ $C_p C_{q4} \coloneqq -0.8$	
$P_{windward_edge}^{r} = 1.0 \cdot 0.6 \cdot 0.99 \cdot 1.0 \cdot 1.15 = 0.683$	
$P_{leeward_edge} \coloneqq 1.0 \cdot 0.6 \cdot 0.99 \cdot 1.0 \cdot 0.8 = 0.475$	
Load case b	
Main wall parallel to wind	
Notes checking:	4.1.7.6-A
(3) Positive coefficients denote forces toward the surfactories away from the surface	ce, negative coefficient denote
(5) The eave height, H=19m for roof slope<7 deg(6) End zone:	
$y = 2 \cdot 6.65 = 13.3$ $y > 6$ \therefore 0	
$(7)z := min(0.1 \cdot 66.5, 0.4 \cdot 19) = 6.6 $ \tag{7}	
$0.04 \cdot 66.5 = 2.66$	
6.65>2.66 ∴ OK	
(8) B/H<5 checked	







Most critical:	
Orientation 3,4: load case A dominates:	
$399 \ kN + 545 \ kN = 944 \ kN$	
$121 \ kN + 174 \ kN = 295 \ kN$	
Comparing to:	
$512 \ kN + 375 \ kN = 887 \ kN$	
$87 \ kN + 61 \ kN = 148 \ kN$	
oad case 1,2: load case B dominates:	
$441 \; kN + 601 \; kN = (1.042 \cdot 10^3) \; kN$	
$87 \ kN + 61 \ kN = 148 \ kN$	
Comparing to :	
$445 \ kN + 334 \ kN = 779 \ kN$	
$121 \ kN + 174 \ kN = 295 \ kN$	
	References
Hangar walls:	(NBCC 2015)
$Z = min(0.1 \cdot 54, 0.4 \cdot 19) = 5.4$	4.1.7.6-B
$5.4 > 1$ $\therefore OK$	
e: Area := 5.4 • 19 = 102.6	
$N: Area_w1 := (54 - Z \cdot 2) \cdot 19 = 820.8$	
$Area_{w2} := (77 - Z \cdot 2) \cdot 19 = 1.258 \cdot 10^{3}$	
$C_p C_q coefficients$:	
e: +1.3 -1.5	
w: +1.3 -1.5	
Hangar roof:	
$C: Z^2 = 29.16$	
5: $Area_S1 := (54 - Z \cdot 2) \cdot Z = 233.28$	
$Area_S2 := (77 - Z \cdot 2) \cdot Z = 357.48$	
$Area_r := (54 - Z \cdot 2) \cdot (77 - Z \cdot 2) = 2.86 \cdot 10^3$	
$C_p C_q$ coefficient	
C: 0.3 -2.0 S: 0.3 -2.0	
∵ 0.3 −1.5	
$\cdot (0.6) \ 1 \cdot 1 \cdot 0.3 = 0.18$	
$\bullet 0.6 \bullet 1 \bullet 1 \bullet -2 = -1.2$	
$\cdot 0.6 \cdot 1 \cdot 1 \cdot -1.5 = -0.9$	
Interior pressure:	4.1.7.3-7
interior pressurer	
a = 9.5	

$= \left(\frac{9.5}{10}\right)^{0.2} = 0.99 \qquad 0.99 > 0.9 \therefore OK$					4.1.7.3-5			
=1.0					4.1.7.4-	1		
:=2.0					4.1.7.3-	10		
	0.45 to 0.3				4.1.7.7-	1 Table 4	1.7.7	
C_{pi} ranges from $P_{int_positive} \coloneqq 1.0$			0.356					
$P_{int_negative}^{int_positive} \coloneqq -$.0 0.00 0.0	0.000					
-								
Summary		ext		int		Netpres	sure	
Surface	+ 0.78	- -0.9	+ 0.36	- -0.54		+ 1.14	- -1.44	
e w	0.78	-0.9	0.36	-0.54		1.14		
С	0.18	-1.2	0.36	-0.54		0.54		
S	0.18	-1.2	0.36	-0.54 -0.54		0.54	-1.74 -1.44	
r	0.18	-0.9	0.36	-0.54		0.54	-1.44	
					Referen	ces		
Office walls:					(NBCC 2			
Z = min(0.1		9.91) = 1.25			4.1.7.6-	В		
1.25 > 1	:.OK	0.0						
e: $Area = 1.25$								
$W: Area_w1 := ($ $Area_w2 := ($	$(34-2\cdot 2)\cdot 8$	9.91 = 510.305						
$C_p C_q coefficien$	ats:	• 9.91 = 99.1						
e: +1.4								
w: +1.3								
$C_p C_g$ coe	efficient				4.1.7.6	C		
Area = 1	2.5*55=687.	.5						
r: 0.3 -	-1.5							
Interior pressu	re:				4.1.7	.3-7		
$h \coloneqq 6$								

$C_{ei} := \left(\frac{6}{10}\right)^{0.2} = 0.9$	0.90	3>0.9 ∴ <i>OK</i>	-	4.1	.7.3-5	
$C_t = 1.0$				4.1	.7.4-1	
$C_{gi} \coloneqq 2.0$				4.1	.7.3-10	
C_{pi} ranges from	n -0.45 to 0.3	0.0002.03	2-0.225		4.1.7.7-1 Tal	ole 4.1.7
$P_{int_positive}^{F} \coloneqq 1.$ $P_{int_negative} \coloneqq -$	-0.49		5=0.325			
Summary Surface	+ P	ext -	P.	int -	Netpre	essure -
e W	0.76	-0.92 -0.81 -0.81	0.33	-0.49 -0.49 -0.49	1.25 1.19 0.65	-1.24 -1.13 -1.13
	0.10	0.01	0.55	0.15	0.03	1.13