## Chapter 4 — Differential Relationship

- 4.1 Linear and Rotational Velocity
- 4.2 Motion of the Links of a Robot
- 4.3 dx = Jdq
- $4.4 \Delta$  and  $^{T}\Delta$
- 4.5 Manipulator Jacobian
- 4.6 Inverse Jacobian
- 4.7 Singularity

Analyze the relationship of

$$dx = Jdq$$
$$J^{-1}dx = dq$$

- □ Linear velocity:
  - Let Q be a vector, to specify its linear velocity, we need to select the reference frame. If a frame {B} is chosen, then:

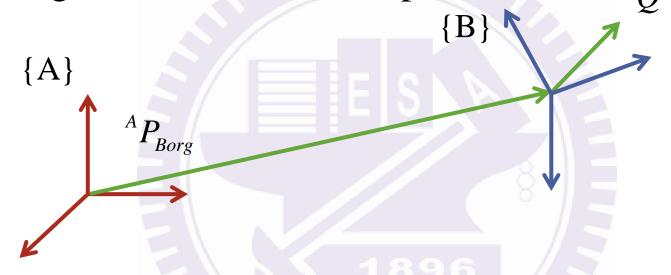
$$\frac{d^{B}Q}{dt} = \lim_{\Delta t \to 0} \frac{{}^{B}Q(t + \Delta t) - {}^{B}Q(t)}{\Delta t} = {}^{B}V_{Q}$$

 $\square$  When expressed in the frame  $\{A\}$ , then:

$${}^{A}({}^{B}V_{Q}) = \frac{{}^{A}d^{B}Q}{dt} = {}^{A}_{B}R^{B}V_{Q}$$

□ Where  ${}_{B}^{A}R$  is the transformation from {A} to {B}

□ Note: that  ${}^BV_Q$  is significant only in direction and magnitude, but not in the point.



□ Consider the movement of the origin of frame {B}

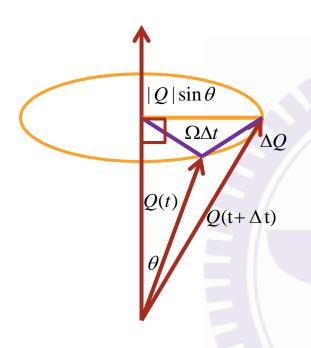
$$^{A}V_{Q} = ^{A}V_{Borg} + ^{A}_{B}R^{B}V_{Q}$$

#### Rotational velocity:

Describe the rotational motion of a frame. Let  ${}^A\Omega_B$  denote the rotation of frame {B} relative to {A}.  ${}^A\Omega_B$  can be expressed in terms of different coordinates frames.

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- □ The question: How does a vector change with time as viewed from {A} when it is fixed in {B} and the systems are rotating?
- Now the orientation of frame  $\{B\}$  with respect to frame  $\{A\}$  is changing in time, let the rotational velocity of  $\{B\}$  related to  $\{A\}$  is described by a vector called  ${}^A\Omega_B$  when  ${}^BQ$  is fixed in  $\{B\}$  and viewed from frame  $\{B\}$  ( ${}^BV_Q=0$ ). However Q will have a velocity viewed from  $\{A\}$  due to  ${}^A\Omega_B$ .



$$\left|\Delta Q\right| = \left(\left|^{A}Q\right|\sin\theta\right)\left|^{A}\Omega_{B}\Delta t\right|\right)$$

$$^{A}V_{Q} = ^{A}\Omega_{B} \times ^{A}Q$$

$$|v| = |r\omega|$$

Q may be changing with respect to frame {B}

$${}^{A}V_{Q} = {}^{A}({}^{B}V_{Q}) + {}^{A}\Omega_{B} \times {}^{A}Q$$
$$= {}^{A}R_{B}{}^{B}V_{Q} + {}^{A}\Omega_{B} \times ({}^{A}R_{B}{}^{B}Q)$$

Both linear and rotational

$${}^{A}V_{O} = {}^{A}V_{Borg} + {}^{A}R_{B}{}^{B}V_{O} + {}^{A}\Omega_{B} \times ({}^{A}R_{B}{}^{B}Q) - (*)$$

## 4.2 Motion of the Links of a Robot

□ Angular velocity of link i + 1 with respect to coordinate of link i is about the  $Z_i$  axis  $(\theta_i + 1)$ 

$$W_s = \begin{cases} \vec{Z}_i \dot{q}_{i+1} & \text{If link i+1 is rotational} \\ 0 & \text{If link i+1 is translational} \end{cases}$$

$$W_{i+1} = W_i + W_s = \begin{cases} W_i + \vec{Z}_i \dot{q}_{i+1} & \text{If link i+1 is rotational} \\ W_i & \text{If link i+1 is translational} \end{cases}$$

□ Linear velocity

□ Define: 
$$P_{i+1}^* = P_{i+1} - P_i$$

$$V_{i+1} = \begin{cases} W_s \times P_{i+1}^* + W_i \times P_{i+1}^* + V_i, & i+1, & R \\ \vec{Z}_i \cdot \dot{q}_{i+1} + W_i \times P_{i+1}^* + V_i, & i+1, & P \end{cases}$$

$$= \begin{cases} W_{i+1} \times P_{i+1}^* + V_i, & i+1, & R \\ \vec{Z}_i \cdot \dot{q}_{i+1} + W_{i+1} \times P_{i+1}^* + V_i, & i+1, & P \end{cases}$$

# 4.3 dx = Jdq

$$dX = \begin{bmatrix} dx \\ dy \\ dz \\ \delta x \\ \delta y \\ \delta z \end{bmatrix} \quad dq = \begin{bmatrix} d\theta_1 \\ d\theta_2 \\ \dots \\ d\theta_N \end{bmatrix}$$

$$\frac{dX}{dt} = \frac{df(q)}{dt} = \frac{df(q)}{dq} \times \frac{dq}{dt}$$

X = f(q)

$$\dot{X} = J * \dot{q}$$
  $POS = BASE * T_N * TOOL$ 

# 4.3 dx = Jdq

#### □ Differential Translation and Rotation

With respect to base:

$$T + dT = Trans(dx, dy, dz) * Rot(k, d\theta) * T$$
$$dT = [Trans(dx, dy, dz) * Rot(k, d\theta) - I] * T = \Delta * T$$

For 
$$Rot(k, d\theta)$$

When  $d\theta \to 0$ 

$$\begin{cases}
\cos d\theta \approx 1 \\
\sin d\theta \approx d\theta \\
Vers(d\theta) \approx 0
\end{cases}$$

# 4.3 dx = Jdq

$$Rot(k, d\theta) = \begin{pmatrix} 1 & -k_z d\theta & k_y d\theta & 0 \\ k_z d\theta & 1 & -k_x d\theta & 0 \\ -k_y d\theta & k_x d\theta & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\Delta = \begin{pmatrix} 1 & 0 & 0 & dx \\ 0 & 1 & 0 & dy \\ 0 & 0 & 1 & dz \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & -k_z d\theta & k_y d\theta & 0 \\ k_z d\theta & 1 & -k_x d\theta & 0 \\ -k_y d\theta & k_x d\theta & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} - \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\Delta = \begin{pmatrix} 0 & -k_z d\theta & k_y d\theta & dx \\ k_z d\theta & 0 & -k_x d\theta & dy \\ -k_y d\theta & k_x d\theta & 0 & dz \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

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### With respect to T

 $4.3 \ dx = Idq$ 

$$T + dT = T * Trans(dx, dy, dz) * Rot(k, d\theta)$$
$$dT = T * [Trans(dx, dy, dz) * Rot(k, d\theta) - I] = T * ^T \Delta$$

 $Rot(k, d\theta)$  can also be formulated as differential rotations  $\delta_x$ ,  $\delta_y$ ,  $\delta_z$  around x, y, z axes

$$Rot(x,\delta x) \cong \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & -\delta x & 0 \\ 0 & \delta x & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}, Rot(y,\delta y) \cong \begin{pmatrix} 1 & 0 & \delta y & 0 \\ 0 & 1 & 0 & 0 \\ -\delta y & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}, Rot(z,\delta z) \cong \begin{bmatrix} 1 & -\delta z & 0 & 0 \\ \delta z & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$Rot(x,\delta x) * Rot(y,\delta y) * Rot(z,\delta z) = \begin{pmatrix} 1 & -\delta z & \delta y & 0 \\ \delta z & 1 & -\delta x & 0 \\ -\delta y & \delta x & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$Rot(x, \delta x) * Rot(y, \delta y) * Rot(z, \delta z) = \begin{pmatrix} 1 & -\delta z & \delta y & 0 \\ \delta z & 1 & -\delta x & 0 \\ -\delta y & \delta x & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^{T}\Delta = \begin{pmatrix} 0 & -\delta z & \delta y & dx \\ \delta z & 0 & -\delta x & dy \\ -\delta y & \delta x & 0 & dz \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

4.3 dx = Idq

$$\begin{cases} \delta x = k_x d\theta \\ \delta y = k_y d\theta \\ \delta z = k_z d\theta \end{cases}$$

## $4.4 \Delta and ^T \Delta$

$$dT = \Delta * T = T * {}^{T}\Delta$$

$${}^{T}\Delta = T^{-1} * \Delta * T$$

$$= \begin{pmatrix} n \cdot (\delta \times n) & n \cdot (\delta \times o) & n \cdot (\delta \times a) & n \cdot [(\delta \times P) + d] \\ o \cdot (\delta \times n) & o \cdot (\delta \times o) & o \cdot (\delta \times a) & o \cdot [(\delta \times P) + d] \\ a \cdot (\delta \times n) & a \cdot (\delta \times o) & a \cdot (\delta \times a) & a \cdot [(\delta \times P) + d] \\ 0 & 0 & 1 \end{pmatrix}$$

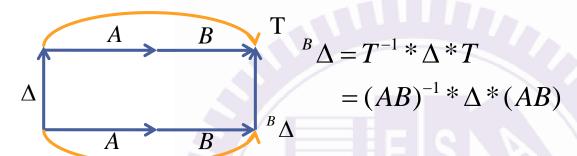
From  $a \cdot (b \times c) = -b \cdot (a \times c) = b \cdot (c \times a)$ 

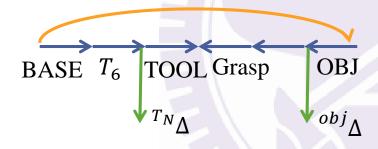
$$\Rightarrow \begin{pmatrix} 0 & -\delta \cdot a & \delta \cdot o & (\delta \times P) \cdot n + d \cdot n \\ \delta \cdot a & 0 & -\delta \cdot n & (\delta \times P) \cdot o + d \cdot o \\ -\delta \cdot o & \delta \cdot n & 0 & (\delta \times P) \cdot a + d \cdot a \\ 0 & 0 & 0 & 1 \end{pmatrix}, T_d = \begin{pmatrix} (\delta \times P + d) \cdot n \\ (\delta \times P + d) \cdot o \\ (\delta \times P + d) \cdot a \end{pmatrix}, T_{\delta} = \begin{pmatrix} \delta \cdot n \\ \delta \cdot o \\ \delta \cdot a \end{pmatrix}$$

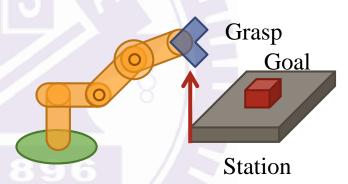
## $4.4 \Delta$ and $^{T}\Delta$

#### **NCTU-Human and Machine lab**

#### □ Assume T=A\*B







Know 
$$^{Obj}\Delta$$
 find  $^{T6}\Delta$ 

$$T = Grasp * TOOL^{-1}$$

$$T = OBJ^{-1} * BASE * T_6$$

$$^{T_N}\!\Delta = T^{-1} \cdot ^{obj} \Delta \cdot T$$

# $T_{N} = A_{1} * A_{2} * ... * A_{N}$ $q_{i} = \begin{cases} \theta_{i}, revolute \\ d_{i}, prismatic \end{cases}$

$$A_{i} = \begin{pmatrix} C\theta_{i} & -S\theta_{i}C\alpha_{i} & S\theta_{i}S\alpha_{i} & a_{i}C\theta_{i} \\ S\theta_{i} & C\theta_{i}C\alpha_{i} & -C\theta_{i}S\alpha_{i} & a_{i}S\theta_{i} \\ 0 & S\alpha_{i} & C\alpha_{i} & d_{i} \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

4.5 Manipulator Jacobian

For revolute joint

## 4.5 Manipulator Jacobian

For prismatic joint

For revolute joint, only (rotational error) around  $Z_{i-1}$  axis

$$d_i = 0, i^{-1}\delta_i = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

For prismatic joint, only (translational error) along  $Z_{i-1}$  axis

$$^{i-1}\delta_i=0,\,^{i-1}d_i=\begin{bmatrix}0\\0\\1\end{bmatrix}$$

## 4.5 Manipulator Jacobian

Due to errors in  $dA_i$ , i = 1, 2, ..., N

## 4.5 Manipulator Jacobian

For revolute joint

$$d_{i} = 0, i^{-1} \delta_{i} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

Where n, o, a, p are of  $U_{i-1}$ 

$$T_N \delta_i = \begin{pmatrix} n \cdot i^{-1} & \delta_i \\ o \cdot i^{-1} & \delta_i \\ a \cdot i^{-1} & \delta_i \end{pmatrix} = \begin{pmatrix} n_Z \\ o_Z \\ a_Z \end{pmatrix}$$

#### For prismatic joint

$$^{i-1}d_{i} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}, ^{i-1}\delta_{i} = 0 \quad ^{T_{N}}d_{i} = \begin{pmatrix} n_{Z} \\ o_{Z} \\ a_{Z} \end{pmatrix}, ^{T_{N}}\delta_{i} = 0$$

4.5 Manipulator Jacobian

In total 
$$T_N \Delta = \sum_{i=1}^N (U_{i-1}^{-1} *^{i-1} \Delta_i * U_{i-1})$$

$$\begin{bmatrix} T_N d \\ T_N \delta \end{bmatrix} = \begin{pmatrix} \vdots & \vdots & \vdots & \vdots \\ T_N \Delta_1 & T_N \Delta_2 & \cdots & T_N \Delta_N \\ \vdots & \vdots & \vdots & \vdots \\ \vdots & \vdots & \vdots & \vdots \end{pmatrix} \begin{pmatrix} dq_1 \\ dq_2 \\ \vdots \end{pmatrix}$$

## 4.6 Inverse Jacobian

- Using  $dq = J^{-1}dx$  to invert the J matrix directly is very inefficient. We need to consider the case when  $J^{-1}$  doesn't exist (det J = 0, not full rank)
  - R. Paul's method
    - a) From  $^{T6}d$ ,  $^{T6}q$  compute  $dT_6 = T_6 * ^{T6}\Delta$

$$= \begin{pmatrix} dn_6 & do_6 & da_6 & dp_6 \\ 0 & 0 & 0 & 0 \end{pmatrix}$$

## 4.6 Inverse Jacobian

- b) Kinematic solution.
  - Differentiate the solution given a value of  $T_6$ , the expressions for each differential changes are functions of  $dT_6$  and those  $d\theta's$  that are already obtained.
- Example: PUMA 560

$$-S_1 P_x + C_1 P_y = d_3$$

$$(-C_1P_x - S_1P_y)d\theta_1 - (S_1dP_x - C_1dP_y) = 0$$

$$d\theta_{1} = -\frac{S_{1}dP_{x} - C_{1}dP_{y}}{C_{1}P_{x} + S_{1}P_{y}}$$

 $\square$  Similarly  $d\theta_2 \dots d\theta_6$  can be obtained

#### Mochine lab

- Method frequently used in the industries in the past
  - a) Compute  $dT_6$
  - Compute  $T_6^N = T_6 + dT_6 \Rightarrow T^T \Delta = \frac{\partial T \Delta}{\partial q} \partial q$
  - Compute new joint solution from  $T_6^N$

4.6 Inverse Jacobian

- d)  $dq = q^N q$
- Neural Network Approach
- Fuzzy Approach
- "An efficient Solution of Differential Inverse Kinematics Problem for Wrist-Partitioned Robots" IEEE Trans. Rob. & Auto. Vol. 6(1) PP. 117-123, 1990

$$J^{wrist} = \begin{pmatrix} J_1 & 0 \\ J_2 & J_3 \end{pmatrix} \quad J^{-1} = [J_1]^{-1}[J_3]^{-1}$$

- $\Box J = 0 \Rightarrow dq = J^{-1}dx$  can not be obtained
- □ 3 cases for PUNA560:

4.7 Singularity

- Unks 2 and 3 are fully extended.
- 2 Joint 5 at its zero position.
- 3 The end of link 3 aligns with the axis of robot trunk.

