

# 4A13

## Combustion and Engines

### Lent. 2022

Combustion:

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Hopkinson Lab – ISG-17

Engines:

Prof. S. Hochgreb (sh372)  
Hopkinson Lab

$8 = 7L + 1Ex.$

Quantitative/qualitative questions

1. Basics – multcomp. Mixt.  $X_i$ ,  $Y_i$ , stoichio. Govern. Eqs.  $T_f$
2. Chemical equilibrium and kinetics – combustion chemistry
3. Limit reactors – Autoignition & Extinction
4. Laminar Premixed
5. Laminar Non-premixed
6. Pollutants
7. Turbulent flames – Introd. (not examinable)
8. Example Class

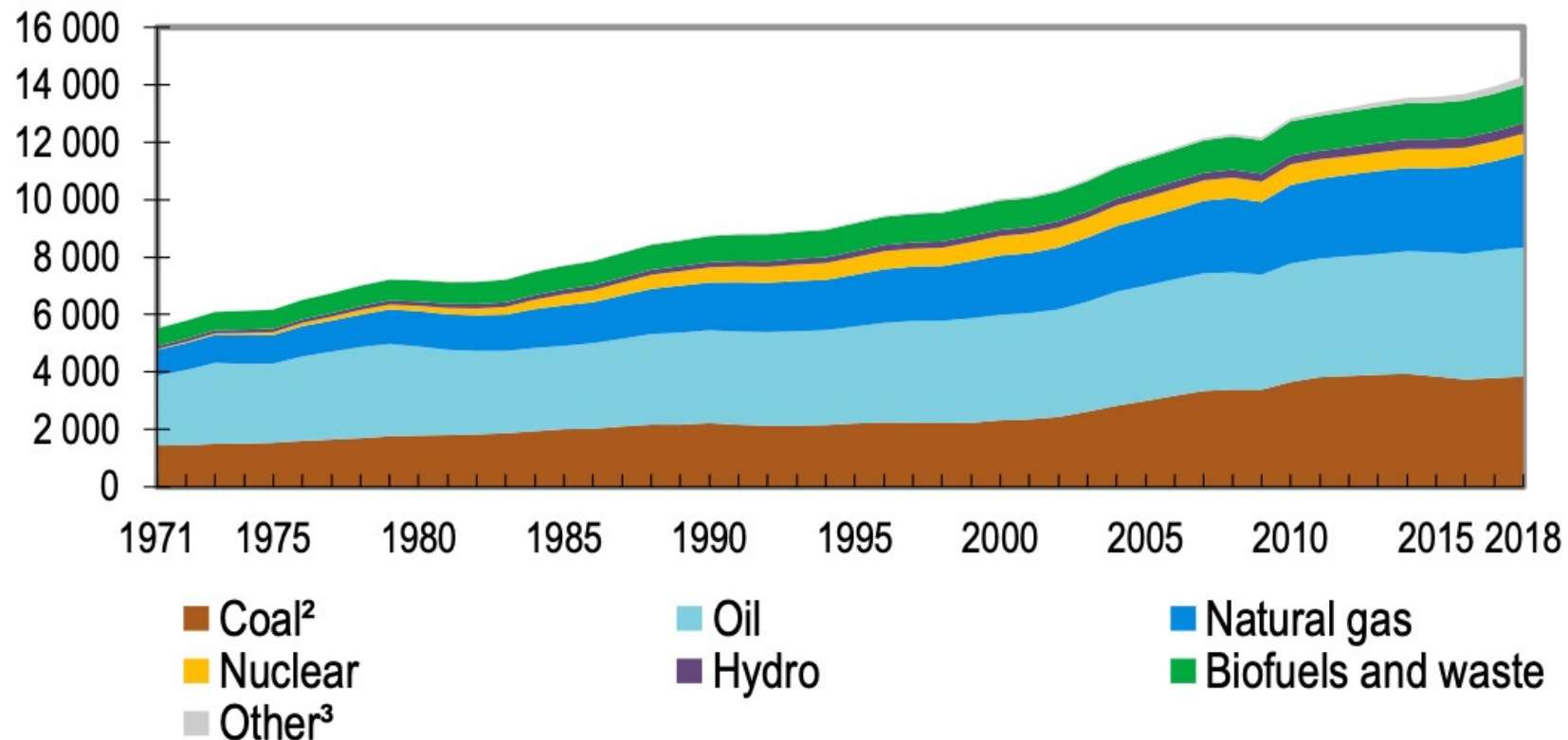
- I. Glassman, *Combustion*, 1996
- Spalding *Combustion & Mass transfer*, 1978
- S.Turns, *Introduction to Combustion*, 2000
  
- C. K. Law, *Combustion Physics*, 2006
- Kuo *Principles of Combustion*, 1984
- T. Poinso & T. Veynante, *Theoretical and Numerical Combustion*

# Outline – for Today

- Why study combustion?
- Stoichiometry and thermochemistry
- Flame temperature
- Conservation equations

# Why study Combustion?

World<sup>1</sup> TES from 1971 to 2018 by source (Mtoe)



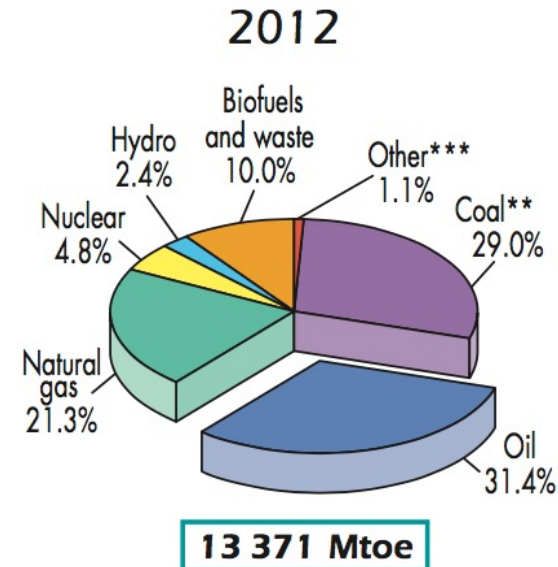
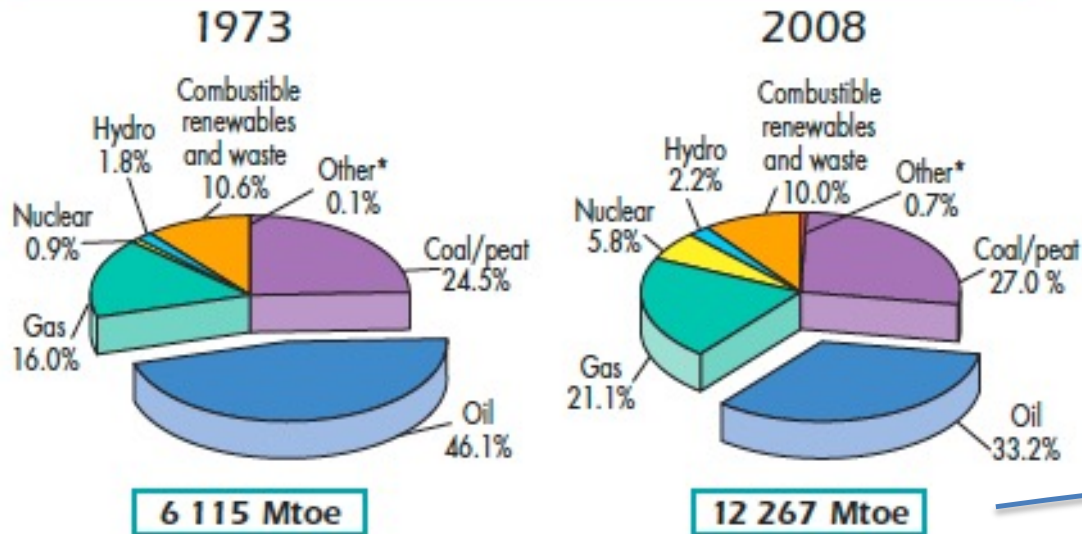
IEA Key stats, 2020

**1 ton of oil has 42 GJ**

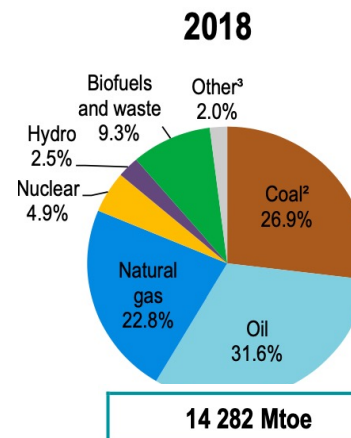
# World Primary Energy Supply

IEA Key stats, 2020

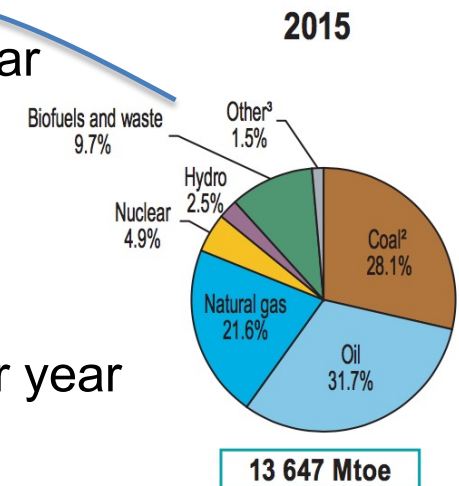
## 1973 and 2008 fuel shares of TPES



~2% increase per year

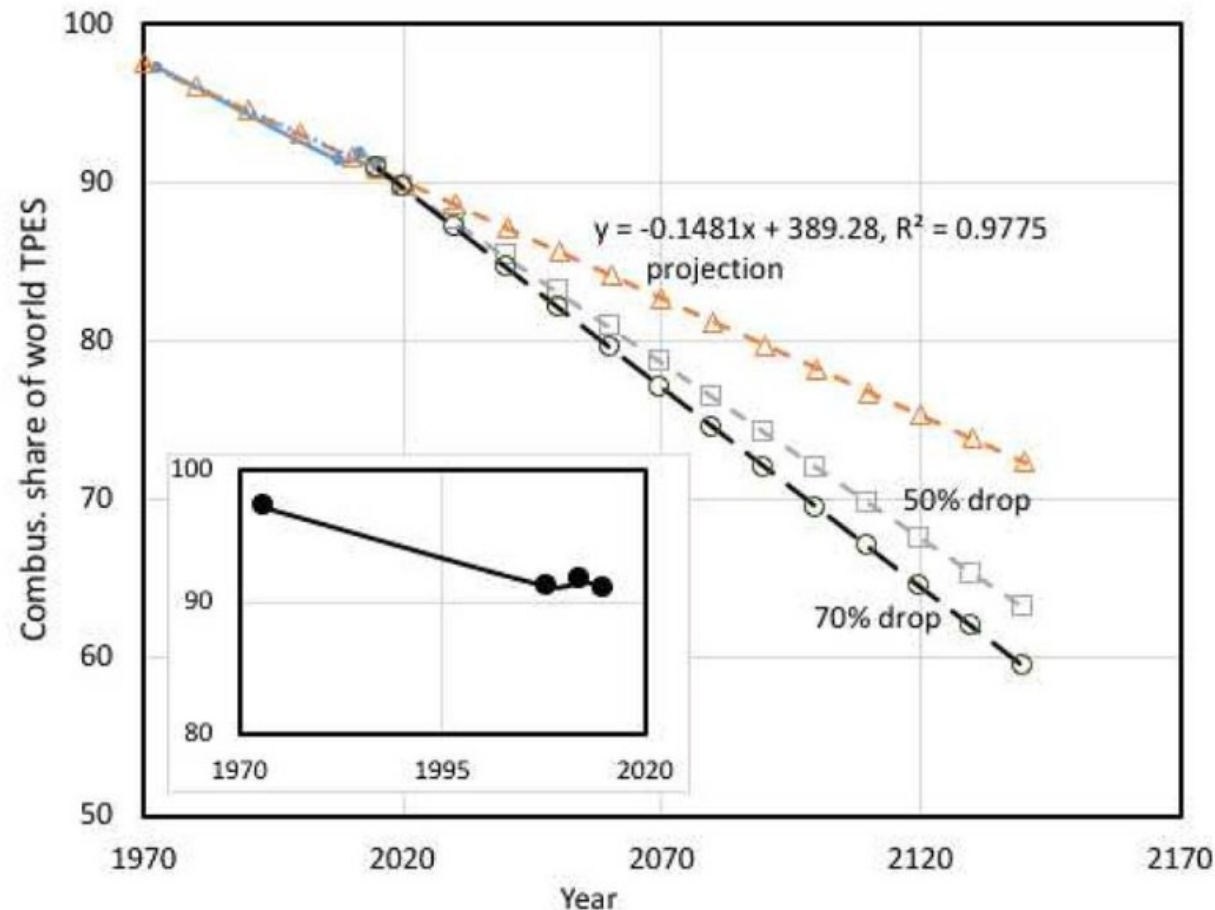


~1.5% per year



Combustion: ~ 90%

# Some projections



- Still lot to do in combustion research to make combustion systems better (“greener”)
- Unless a radical paradigm shift happens – “nuclear fusion”
- Non-combustion technology – the message is gloomy or invest more to explore new avenues!!

*Ref: Front. Mech. Eng. 5:59. 2019 doi: 10.3389/fmech.2019.00059*

# Why study combustion?

- Combustion provides about 85-90% of all the energy we use
- Advantages of fossil fuels regarding energy and power density make them very difficult to replace in the short (50 year) term
- Burning fossil fuels is responsible for the main problems we currently face:
  - Global warming
  - Energy security
- Pollutant emissions, including CO<sub>2</sub>, can still be made much smaller, with engineering advances



# Common combustion modes



Premixed flame

Ex. Spark ignition engines  
Stationary GT  
a variant for future Aero-GT

F, O

Product

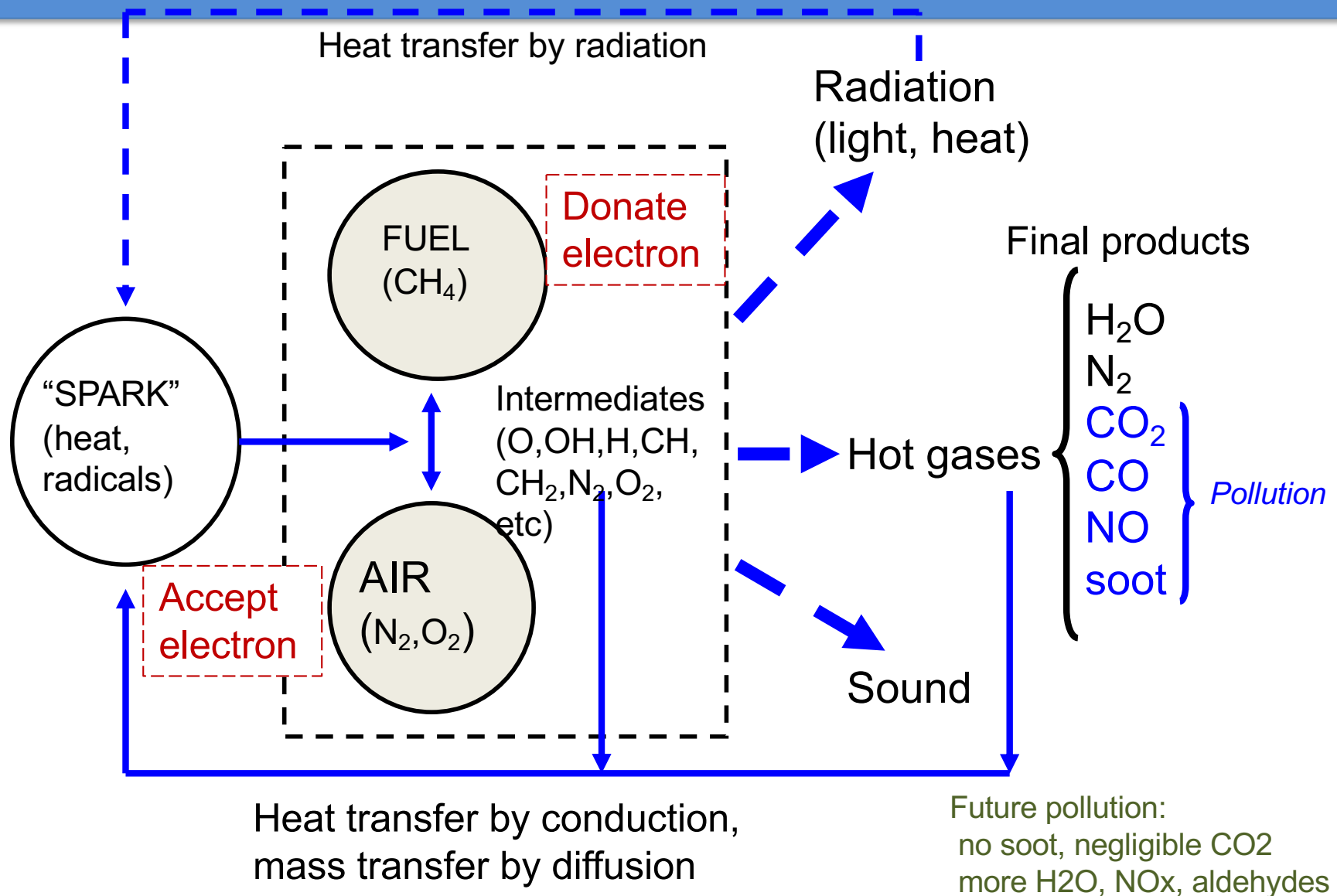


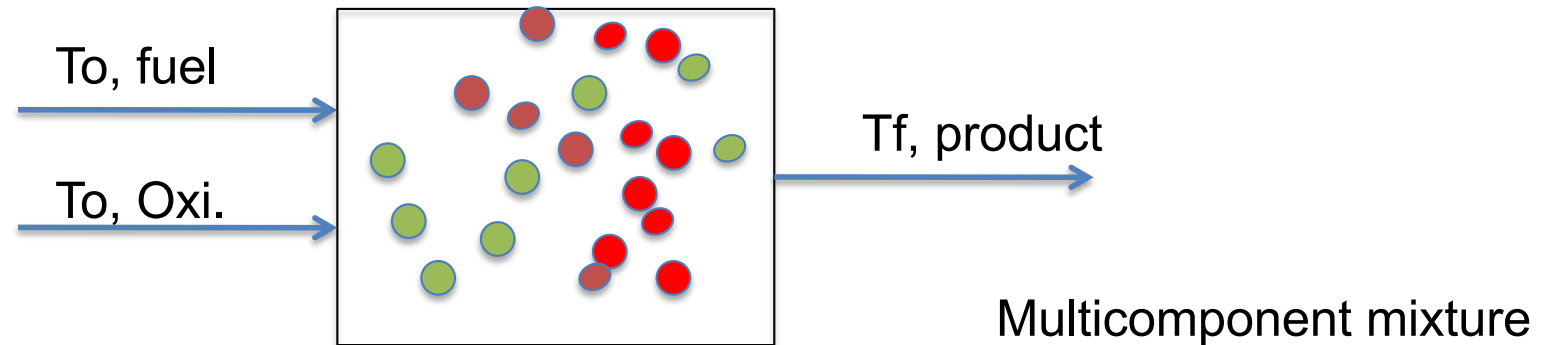
Diffusion flame

Ex. CI engines  
Furnaces, Old GTs  
Current Aero-GT, after burners  
In modern terms – a “dirty flame”

F O

# Combustion in a nutshell – relation to other subjects





- Introduce concepts to help us to estimate
  - T, composition of products
  - Rate of heat release
  - Ignition energy/T, chemical/thermal explosions
  - Pollutants formation rate
  - Other quantities of interest

# Some definitions - Stoichiometry

Equivalence ratio:

$$\phi = \frac{(m_{fuel} / m_{air})}{(m_{fuel} / m_{air})_{st}} = \frac{(V_{fuel} / V_{air})}{(V_{fuel} / V_{air})_{st}}$$

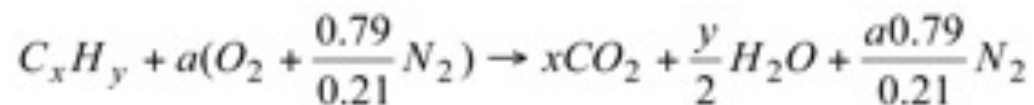
$\phi = 1$  – Stoichiometric  
 $> 1$  – Fuel rich  
 $< 1$  – Fuel lean

Air to Fuel ratio:

$$AFR = \frac{1}{\phi} AFR_{st}$$

$AFR$  and  $\phi$  are used commonly  
in combustion analysis

How to get  $AFR_{st}$ ?



Balance of O gives

$$a = x + y/4$$

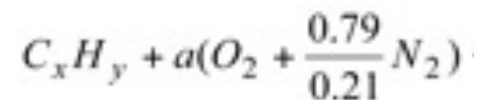
$$AFR_{st} = \frac{a(MW_{O_2} + 0.79/0.21 MW_{N_2})}{MW_{fuel}}$$

$$AFR_{st, vol} = \frac{a(1 + 0.79/0.21)}{1}$$

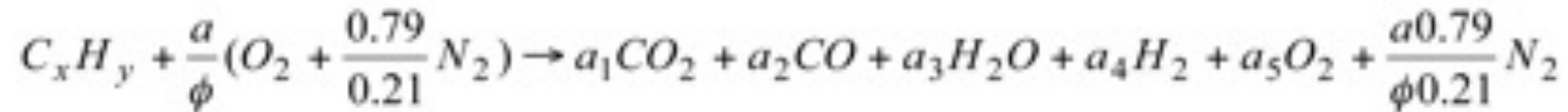
# Example

Fuel	CH <sub>4</sub>	C <sub>7</sub> H <sub>16</sub>	H <sub>2</sub>
$c$	1	7	0
$h$	4	16	2
$\nu_s$	2	11	0.5
$n_r$	10.52	53.4	3.38

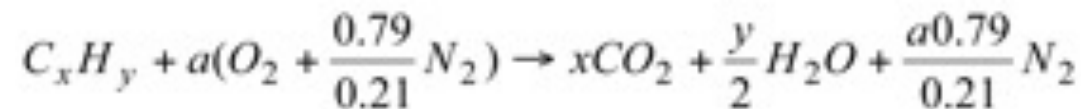
total number of moles



# Products of Combustion



$\phi = 1$  – Stoichiometric: complete combustion



$\phi < 1$  – Fuel lean – complete combustion

$$a_2 = a_4 = 0$$

$$a_1 = x, a_3 = y/2, \text{ and } a_5 = a(1-\phi)/\phi$$

Excess air

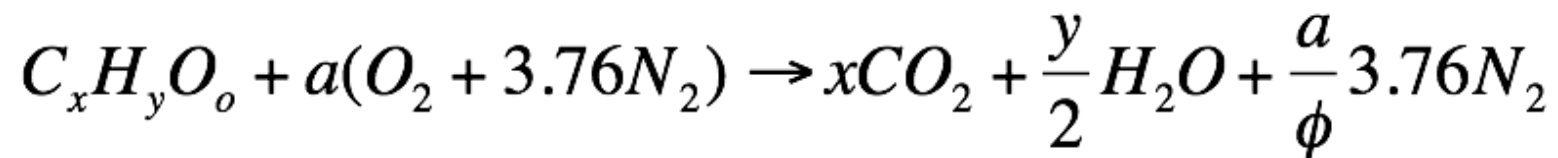
$\phi > 1$  – Fuel rich

atom conservation is not enough! (more unknown, intermediates, radicals involved)  
equilibrium relations are required

# Examples

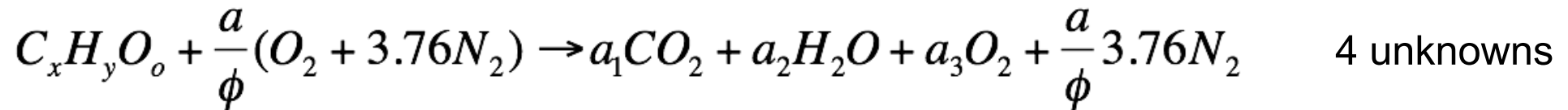
Example 1 – 1: Calculate the mole and mass fractions in the reactants and products of complete gasoline (taken as 100% octane) combustion at  $\phi=0.6$  - worked out in Lect. notes (in page 10 of Lect. notes, Ch. 1)

Example 1 – 2: Stoichiometric relations are used to work out molecular composition of fuel and its molecular weight (in page 11 of Lect. notes, Ch. 1)



$$O : a = x + y/4 - o/2$$

# Example I- 2



$$C : a_1 = x \quad H : a_2 = y/2 \quad O : a_3 = a(1-\phi)/\phi$$

$$X_{O_2,r} = \frac{a/\phi}{1 + 4.76 a/\phi} = 0.20807$$

$$p = n_{tot} R^0 T$$

$$\frac{n_{tot}^{dry}}{n_{tot}^{wet}} = \frac{p_2 T_1}{p_1 T_2}$$

$$X_{O_2,p}^{dry} = \frac{a_3}{x + a_3 + 3.76 a/\phi} = 0.04404$$

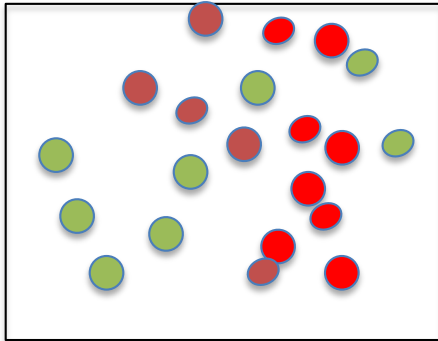
$$\frac{n_{tot}^{dry}}{n_{tot}^{wet}} = \frac{x + a_3 + 3.76 a/\phi}{x + y/2 + a_3 + 3.76 a/\phi} = \frac{0.517}{0.573}$$

$$X_{CO_2,p}^{dry} = \frac{x}{x + a_3 + 3.76 a/\phi} = 0.12788$$

$$C_{12.6} H_{21.4} O_{1.1} \quad MW = 190 \text{ kg/kmol}$$



# Some definitions



Mole fraction:

$$X_i = n_i/n_{\text{tot}} \quad n_{\text{tot}} = \sum n_i$$

$$\sum_{i=1}^N X_i = 1$$

Mass fraction:

$$Y_i = m_i/m \quad m = \sum m_i$$

$$\sum_{i=1}^N Y_i = 1$$

$$Y_i = \frac{m_i}{m} = \frac{n_i MW_i}{n_{\text{tot}} \overline{MW}} = X_i \frac{MW_i}{\overline{MW}}$$

$$\overline{MW} = \sum X_i MW_i$$

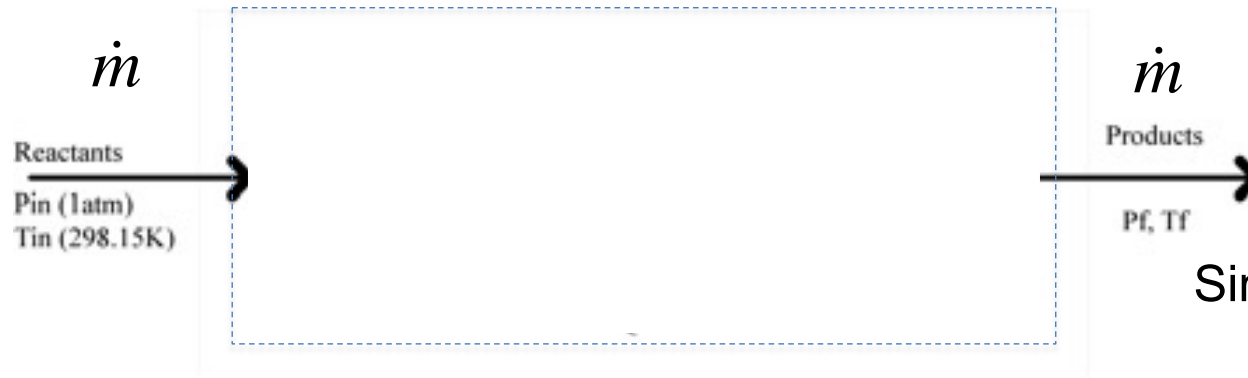
$$C_i = \frac{n_i}{V} = \frac{X_i n_{\text{tot}}}{V} = X_i \frac{P}{R^0 T} = Y_i \frac{\rho}{MW_i} \quad \rho = \sum X_i \rho_i$$

Mean properties:

$$\eta = \sum_{i=1}^N Y_i \eta_i$$

$$\bar{\eta} = \sum_{i=1}^N X_i \bar{\eta}_i$$

# Adiabatic Flame Temperature



Simple approximation:

$$\dot{m} c_p (T_f - T_{in}) = \dot{m}_{fuel} Q$$

$$\Rightarrow Y_{fuel} Q = c_p (T_f - T_{in})$$

Heat of combustion – Reactants & products are at 298.15K

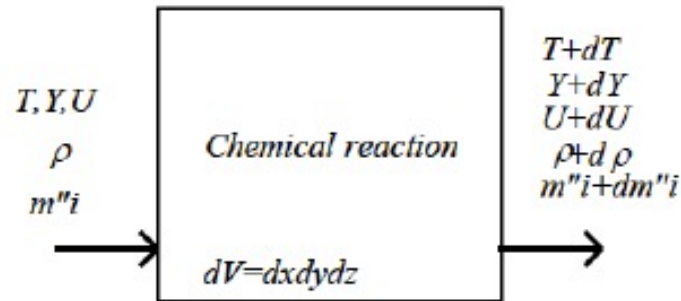
This heat is then used to heat up the products from 298.15 to  $T_f$  to satisfy the 1st Law of Thermodynamics

$$\left[ \sum_{i=1}^N n_i \bar{h}_i(T_{in}) \right]_{reac} + Q = \left[ \sum_{i=1}^N n_i \bar{h}_i(T_f) \right]_{prod}$$

$$\bar{h}_i = \int_{298.15}^T \bar{c}_{p,i} dT$$

Example 1-3

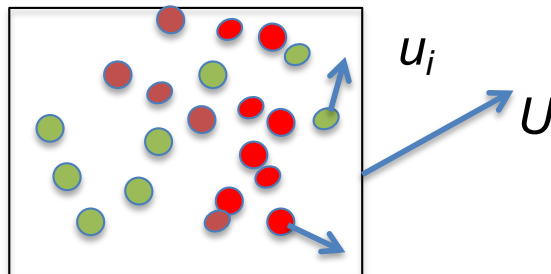
# Conservation equation - Differential



$$\frac{\partial(\rho Y_i)}{\partial t} = -\frac{\partial \dot{m}_i''}{\partial x} + \dot{w}_i$$

summing over all species

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho U}{\partial x} = 0$$



$$\dot{m}_i'' = \dot{m}_{i,ADV}'' + \dot{m}_{i,DIFF}''$$

$$\rho U Y_i \quad -\rho \mathcal{D}_i \frac{\partial Y_i}{\partial x}$$

$$\mathcal{D}_i = \mathcal{D} \quad \rho \mathcal{D} = \frac{\lambda}{c_p}$$

$$\frac{\partial \rho Y_i}{\partial t} + \frac{\partial \rho U Y_i}{\partial x} = \frac{\partial}{\partial x} \left( \rho \mathcal{D} \frac{\partial Y_i}{\partial x} \right) + w_i$$

$$\rho c_p \frac{\partial T}{\partial t} + \rho c_p U \frac{\partial T}{\partial x} = \frac{\partial p}{\partial t} + \frac{\partial}{\partial x} \left( \lambda \frac{\partial T}{\partial x} \right) - Q w_{fuel}$$

$$\frac{\partial \rho Y_i}{\partial t} + \frac{\partial \rho U Y_i}{\partial x} = \frac{\partial}{\partial x} \left( \rho \mathcal{D} \frac{\partial Y_i}{\partial x} \right) + \underline{w_i}$$

Next Lect. : Equilibrium and Chemical Kinetics