

# Lecture 2

# Recap – Lecture 1

- Introduced quantities to characterise multi-component mixture and defined equivalence ratio, AFR
- Introduced stoichiometry relation
- Discussed methods to estimate adiabatic flame temperature
- Simple derivation of conservation equations for species
- Advective flux,  $\rho Y_i U$ , diffusive flux (Fick's Law)
- Discussed significance of energy equation

$$\frac{\partial \rho Y_i}{\partial t} + \frac{\partial \rho U Y_i}{\partial x} = \frac{\partial}{\partial x} \left( \rho \mathcal{D} \frac{\partial Y_i}{\partial x} \right) + \underline{w_i}$$

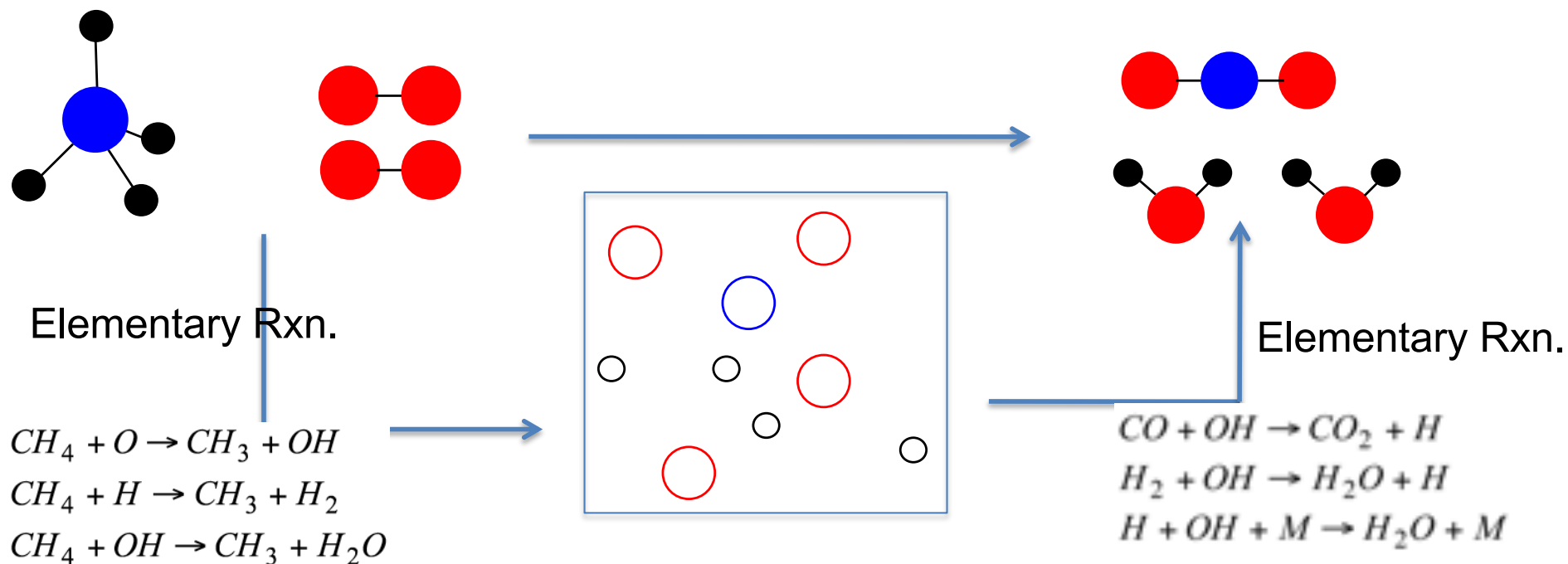
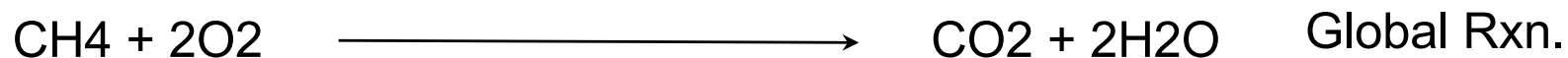
Today: Chemical Kinetics & Equilibrium

# Objectives – Chemical kinetics

- Introduce chemical kinetics concept
- Simple model for fuel consumption rate
  - Use NO formation as an example
- Qualitative description for hydrocarbon combustion

# Global & Elementary Rxn.

- How do we go from reactants to products?



# Rxn. Mechanism – an example

	Reaction	A	n	Ea
1	$\text{H} + \text{O}_2 = \text{O} + \text{OH}$	2.650E+16	-0.6707	17041.0
2	$\text{O} + \text{H}_2 = \text{H} + \text{OH}$	3.870E+04	2.7	6260.0
3	$\text{OH} + \text{H}_2 = \text{H} + \text{H}_2\text{O}$	2.160E+08	1.51	3430.0
4	$2\text{OH} = \text{O} + \text{H}_2\text{O}$	3.570E+04	2.4	-2110.0
5 <sup>a</sup>	$\text{H} + \text{O}_2 + \text{M} = \text{HO}_2 + \text{M}$	2.800E+18	-0.86	0.0
6	$\text{H} + \text{O}_2 + \text{H}_2\text{O} = \text{HO}_2 + \text{H}_2\text{O}$	1.126E+19	-0.76	0.0
7	$\text{H} + \text{O}_2 + \text{N}_2 = \text{HO}_2 + \text{N}_2$	2.535E+19	-1.3392	0.0
8	$\text{H} + \text{O}_2 + \text{He} = \text{HO}_2 + \text{He}$	7.000E+17	-0.8	0.0
9	$\text{H} + \text{O}_2 + \text{Ar} = \text{HO}_2 + \text{Ar}$	7.000E+17	-0.8	0.0
10	$\text{H} + 2\text{O}_2 = \text{HO}_2 + \text{O}_2$	2.080E+19	-1.24	0.0
11	$\text{H} + \text{HO}_2 = 2\text{OH}$	8.316E+13	0	635.0
12	$\text{H} + \text{HO}_2 = \text{O}_2 + \text{H}_2$	4.480E+13	0	1068.0
13(D)	$\text{OH} + \text{HO}_2 = \text{O}_2 + \text{H}_2\text{O}$	1.450E+13	0	-500.0
14(D)	$\text{OH} + \text{HO}_2 = \text{O}_2 + \text{H}_2\text{O}$	5.000E+15	0	17330.0
15	$\text{H} + \text{HO}_2 = \text{O} + \text{H}_2\text{O}$	3.970E+12	0	671.0
16	$\text{O} + \text{HO}_2 = \text{OH} + \text{O}_2$	2.000E+13	0	0.0
17(D)	$2\text{HO}_2 = \text{O}_2 + \text{H}_2\text{O}_2$	1.300E+11	0	-1630.0
18(D)	$2\text{HO}_2 = \text{O}_2 + \text{H}_2\text{O}_2$	4.200E+14	0	12000.0
19 <sup>b</sup>	$2\text{OH}(+\text{M}) = \text{H}_2\text{O}_2(+\text{M})$	7.400E+13	-0.37	0.0
20	$\text{H} + \text{H}_2\text{O}_2 = \text{OH} + \text{H}_2\text{O}$	1.000E+13	0	3600.0
21(D)	$\text{OH} + \text{H}_2\text{O}_2 = \text{HO}_2 + \text{H}_2\text{O}$	1.700E+18	0	29410.0
22(D)	$\text{OH} + \text{H}_2\text{O}_2 = \text{HO}_2 + \text{H}_2\text{O}$	2.000E+12	0	427.0
23	$\text{H} + \text{H}_2\text{O}_2 = \text{HO}_2 + \text{H}_2$	1.210E+07	2	5200.0
24	$\text{O} + \text{H}_2\text{O}_2 = \text{OH} + \text{HO}_2$	9.630E+06	2	4000.0
25 <sup>c</sup>	$2\text{H} + \text{M} = \text{H}_2 + \text{M}$	1.000E+18	-1	0.0
26	$2\text{H} + \text{H}_2 = 2\text{H}_2$	9.000E+16	-0.6	0.0
27	$2\text{H} + \text{CO}_2 = \text{H}_2 + \text{CO}_2$	5.500E+20	-2	0.0
28	$2\text{H} + \text{H}_2\text{O} = \text{H}_2 + \text{H}_2\text{O}$	6.000E+19	-1.25	0.0
29 <sup>d</sup>	$\text{H} + \text{OH} + \text{M} = \text{H}_2\text{O} + \text{M}$	2.200E+22	-2	0.0
30 <sup>e</sup>	$2\text{O} + \text{M} = \text{O}_2 + \text{M}$	1.200E+17	-1	0.0
31 <sup>f</sup>	$\text{O} + \text{H} + \text{M} = \text{OH} + \text{M}$	5.000E+17	-1	0.0
32	$\text{OH} + \text{CO} = \text{H} + \text{CO}_2$	4.689E+07	1.228	70.0
33	$\text{HO}_2 + \text{CO} = \text{OH} + \text{CO}_2$	1.500E+14	0	24544.0
34 <sup>g</sup>	$\text{O} + \text{CO}(+\text{M}) = \text{CO}_2(+\text{M})$	1.800E+10	0	2385.0
35	$\text{H} + \text{HCO} = \text{H}_2 + \text{CO}$	7.340E+13	0	0.0
36	$\text{OH} + \text{HCO} = \text{H}_2\text{O} + \text{CO}$	5.000E+13	0	0.0
37	$\text{HCO} + \text{O}_2 = \text{HO}_2 + \text{CO}$	1.345E+13	0	400.0
38 <sup>h</sup>	$\text{HCO} + \text{M} = \text{H} + \text{CO} + \text{M}$	1.870E+17	-1	17000.0
39	$\text{HCO} + \text{H}_2\text{O} = \text{H} + \text{CO} + \text{H}_2\text{O}$	1.500E+18	-1	17000.0
40	$\text{O} + \text{HCO} = \text{H} + \text{CO}_2$	3.000E+13	0	0.0
41	$\text{O} + \text{CH}_4 = \text{OH} + \text{CH}_3$	1.020E+09	1.5	8600.0
42	$\text{OH} + \text{CH}_4 = \text{CH}_3 + \text{H}_2\text{O}$	1.000E+08	1.6	3120.0
43	$\text{O} + \text{CH}_3 = \text{H} + \text{CH}_2\text{O}$	5.060E+13	0	0.0
44	$\text{O} + \text{CH}_3 = \text{H} + \text{CH}_2 + \text{CO}$	3.370E+13	0	0.0
45	$\text{O} + \text{CH}_2\text{O} = \text{OH} + \text{HCO}$	3.900E+13	0	3540.0
46 <sup>i</sup>	$\text{H} + \text{CH}_3(+\text{M}) = \text{CH}_4(+\text{M})$	1.390E+16	-0.534	536.0

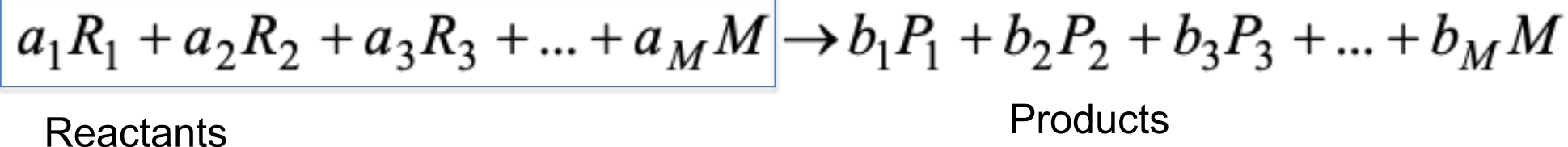
Detailed chemical mechanism:  
involves 100s of elementary reactions,  
10s of species

even for a simplest hydrocarbon, CH<sub>4</sub>

(Combust. Flame, 160, p.56-75, 2013,  
Nikolaou, Chen, Swaminathan)

# Law of Mass Action

Elementary reaction:



$$\frac{d[R_1]}{dt} = -a_1 \omega, \quad \frac{d[R_2]}{dt} = -a_2 \omega, \quad \frac{d[R_3]}{dt} = -a_3 \omega, \dots$$

$$\frac{d[P_1]}{dt} = b_1 \omega, \quad \frac{d[P_2]}{dt} = b_2 \omega, \quad \frac{d[P_3]}{dt} = b_3 \omega, \dots$$

$$\frac{d[M]}{dt} = b_M \omega - a_M \omega$$

$$\omega = k[R_1]^{a_1} [R_2]^{a_2} [R_3]^{a_3} \dots$$

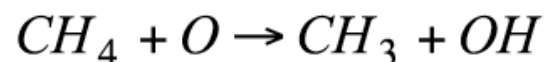
# Arrhenius Rate & Rate Constant

$$\omega = k[R_1]^{a_1} [R_2]^{a_2} [R_3]^{a_3} \dots \quad (\text{kmol/m}^3\text{-s})$$

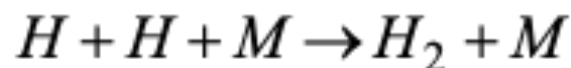
$$k = A \exp\left(-\frac{E_{act}}{R^0 T}\right)$$

Proportions of successful collisions with enough energy to break bonds

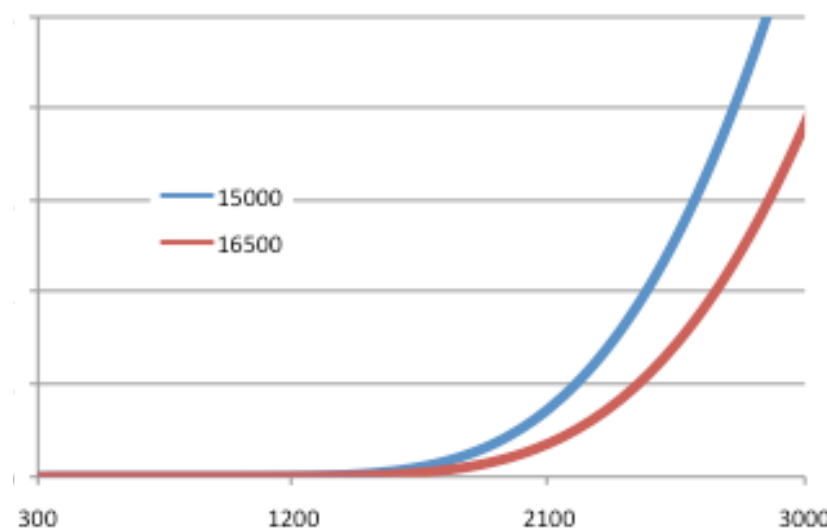
Number of collisions per unit time



$$\frac{d[\text{CH}_4]}{dt} = -k_1[\text{CH}_4][\text{O}]$$



$$\frac{d[\text{H}]}{dt} = -2k_5[\text{H}]^2[\text{M}] \quad \frac{d[\text{H}_2]}{dt} = k_5[\text{H}]^2[\text{M}] \quad \frac{d[\text{M}]}{dt} = 0$$

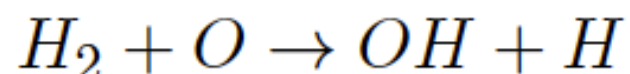




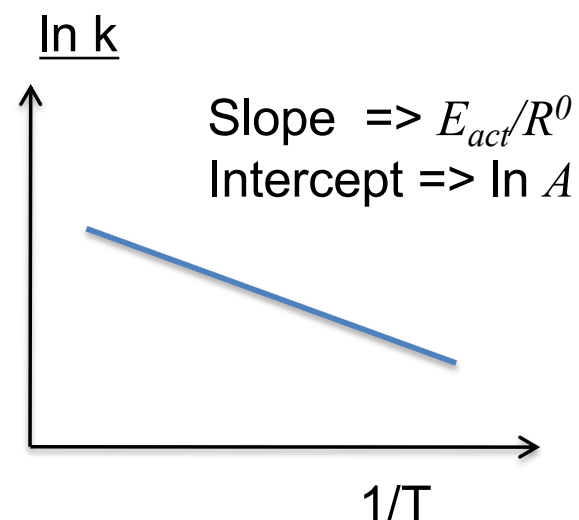
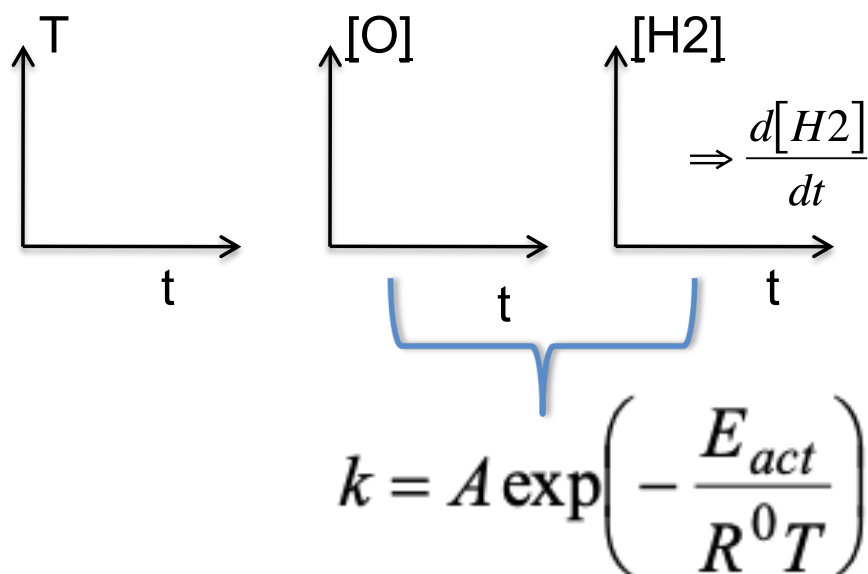
# How to get rate constant?

Statistical mechanics calculations

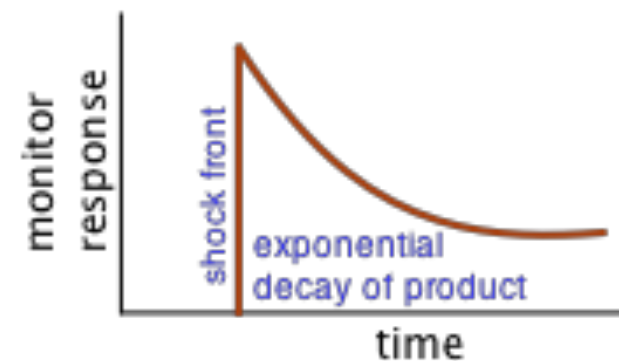
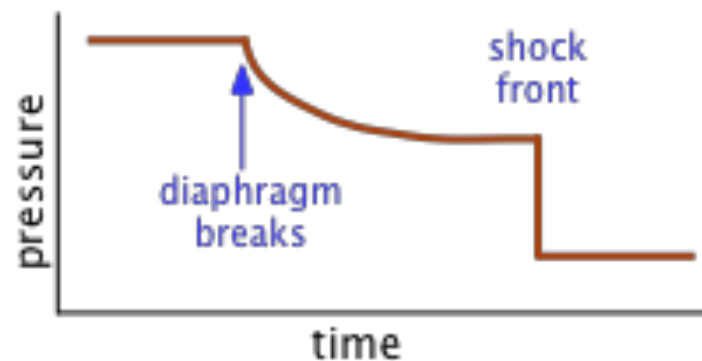
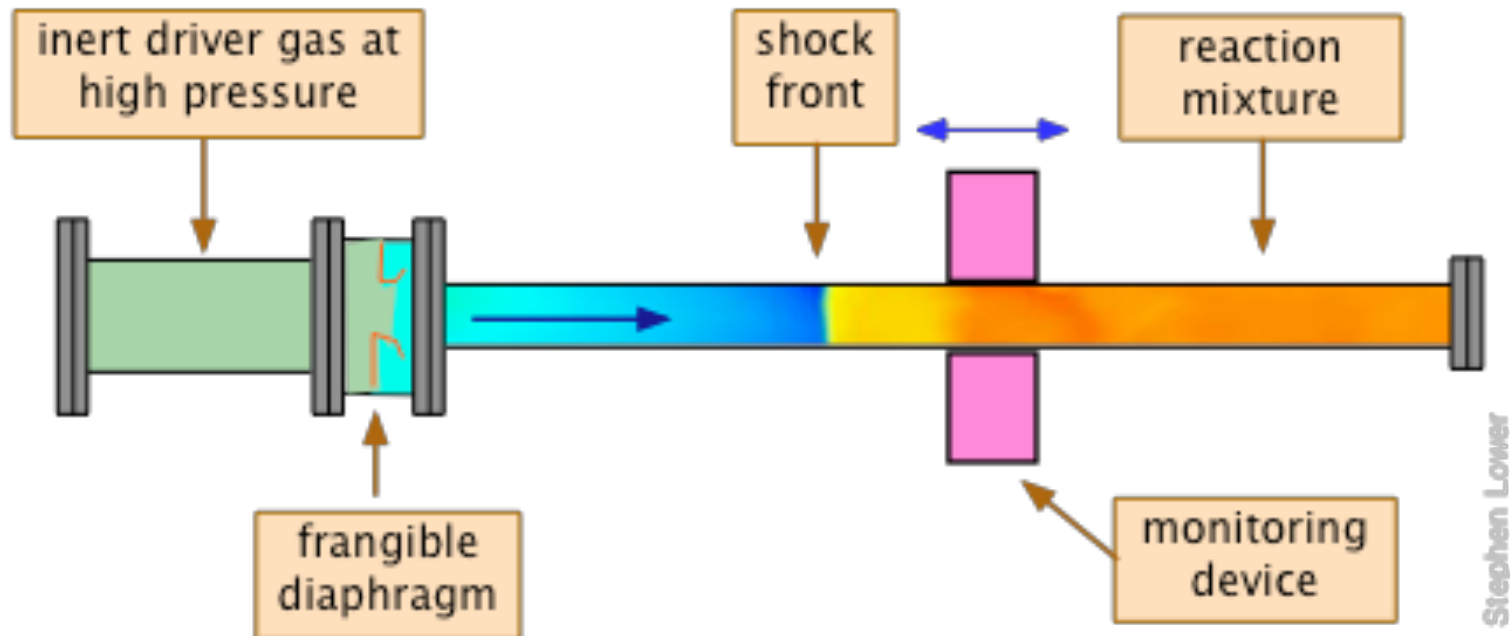
shock tube experiments are used to measure the followings



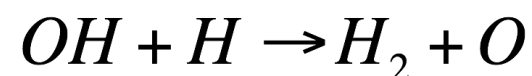
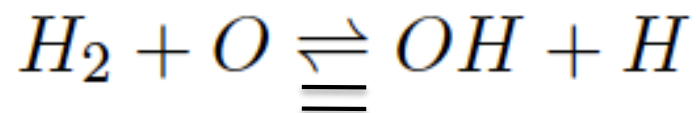
$$\frac{d[H_2]}{dt} = -k[O][H_2]$$



# Shock Tube



# Reverse (forward & backward) reactions

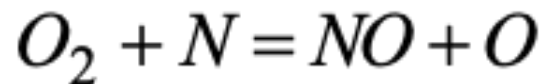
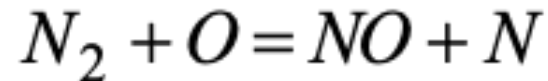


$$\frac{d[H]}{dt} = \underbrace{k_f [H_2] [O]}_{\text{forward}} - \underbrace{k_b [OH] [H]}_{\text{backward}}$$

$$\frac{d[H]}{dt} = 0 \quad \longrightarrow \quad \frac{k_f}{k_b} = \frac{[OH] [H]}{[H_2] [O]}$$

$k_b$  from  $k_f$  and thermodynamic data

# Multiple reactions & $w_i$



Zeldovich Mechanism for  
thermal nitric oxide

$$\hat{w}_{NO} \equiv \frac{d[NO]}{dt} = k_{Z1f}[N_2][O] - k_{Z1b}[NO][N] + k_{Z2f}[O_2][N] - k_{Z2b}[NO][O]$$

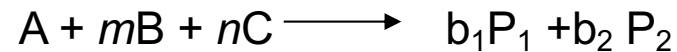
(kmol m<sup>-3</sup> s<sup>-1</sup>)

$$\dot{w}_{NO} = \hat{w}_{NO} MW_{NO}$$

(This is for the species conservation equation)

(kg m<sup>-3</sup> s<sup>-1</sup>)

# Types of Reactions

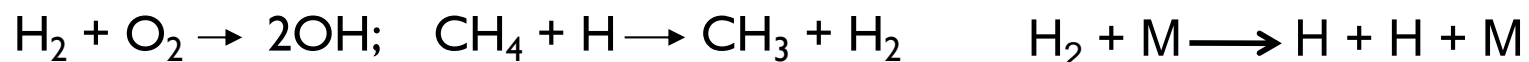


$$d[A]/dt = -k[A][B]^m[C]^n$$

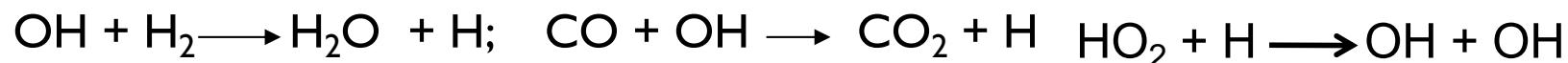
- $m^{\text{th}}$  order w.r.t. species B;  $n^{\text{th}}$  order w.r.t. species C
- overall order  $(m+n+1)$
- molecularity - # of molecules taking part in the reaction – overall order
- dissociation - first order & unimolecular  
 $A + M \rightleftharpoons A^* + M; A^* \rightarrow \text{products}$
- bimolecular and second order - most probable and common in combustion
- trimolecular - less probable but plays very important role in flames  
 $H + O_2 + M \longrightarrow HO_2 + M$  (usually process terminator)  
 $H + H + M \longrightarrow H_2 + M$
- reactions may be classified

# Classification of (chain) Reactions

- Initiation - forms an unstable/excited molecule or atom



- propagation - # of unstable species remain constant

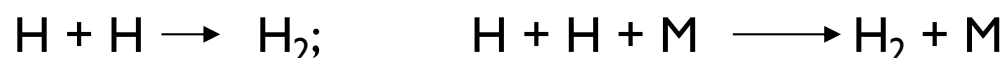


- branching - # of unstable species grow - responsible for a type explosion



- termination - # of unstable species produced is zero

– wall/gas termination

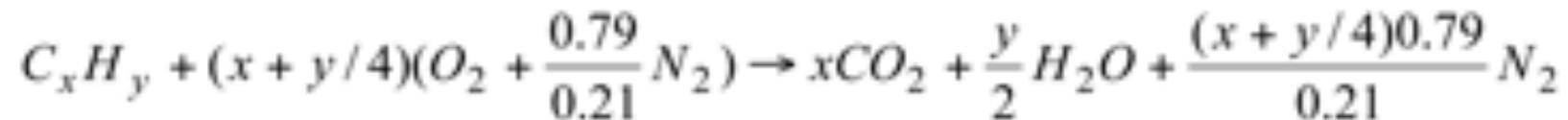


# Simplification: one step model

$$\frac{dc_i}{dt} = \sum_{r=1}^R \hat{w}_r(c_i, p, T)$$

- Coupled non-linear ODEs
- Many time scales ('stiff')
- Specialized solvers
  - ▶ ChemKin, Cosilab, Cantera

For this module:



$$\frac{d[C_xH_y]}{dt} = -A_G \exp\left(-E_{act} / R^0T\right) [C_xH_y]^p [O_2]^q$$

$$p = q = 1$$

# Simplification: systematic reduction



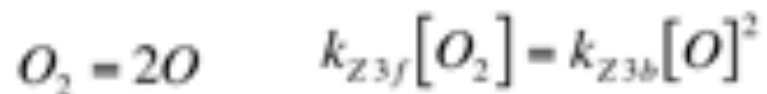
$$\frac{d[NO]}{dt} = k_{z1f}[N_2][O] + k_{z2f}[O_2][N]$$

Steady state for N:

$$\frac{d[N]}{dt} = k_{z1f}[N_2][O] - k_{z2f}[O_2][N] = 0$$

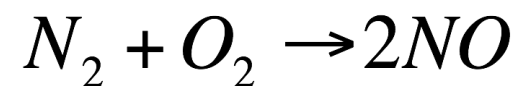
$$[N] = \frac{k_{z1f}[N_2][O]}{k_{z2f}[O_2]}$$

Partial equilibrium:



$$[O] = \left( \frac{k_{z3b}}{k_{z3f}} \right)^{1/2} [O_2]^{1/2}$$

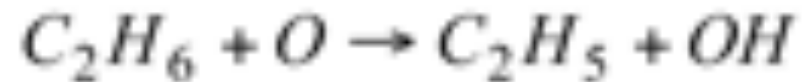
$$\frac{d[NO]}{dt} = 2k_{z1f} \left( \frac{k_{z3b}}{k_{z3f}} \right)^{1/2} [O_2]^{1/2} [N_2]$$





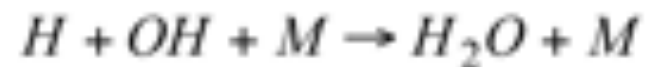
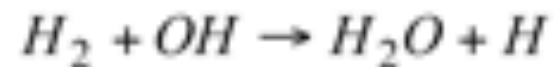
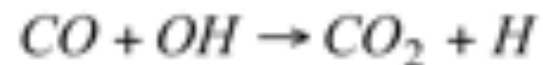
# Typical combustion sequence

1. Fuel Attack by radicals – Break down of fuel



2. Formation of CO and H<sub>2</sub>

3. Oxidation of H<sub>2</sub> to H<sub>2</sub>O and CO to CO<sub>2</sub> – large part of heat is released here



# Summary: chemical kinetics

- Global reaction rate is typically empirical
- Elementary reaction rate is given by Law of Mass action  $k \prod_{i=1}^N [R_i]^{a_i}$
- Rate constant - Arrhenius rate – energetic collisions are required
- Types of reactions
- Full mechanism is very large and complex
- Simplification possible: steady state and equilibrium approximations
  - NO formation as an example

# Example 2-I

To introduce species lifetime and how to calculate it?

$$d[C_3H_8]/dt = -A_G \exp(-T_{act}/T)[C_3H_8][O_2]$$

$$\frac{d[C_3H_8]}{[C_3H_8]} = -A_G \exp(-T_{act}/T)[O_2]dt$$

$$[C_3H_8] = [C_3H_8]_{in} \exp(-t/\tau)$$

$$\tau^{-1} = A_G \exp(-T_{act}/T)[O_2]$$

$$\tau(1200\text{ K}) = 149 \times 10^{-3}\text{ s}, \text{ and}$$
$$\tau(1500\text{ K}) = 15 \times 10^{-3}\text{ s}.$$

Why this change?

High  $T_{act}$   $\Rightarrow$  high sensitivity of Rxn rate to  $T$

How about  $P$  effects?

$$\text{As } P \uparrow [O_2] \uparrow \Rightarrow \tau \downarrow$$