

Combustion

Summarized from B. Fiorina, D. Veynante, R. Vicquelin lectures, and
Veynante & Poinso's Theoretical & Numerical Combustion

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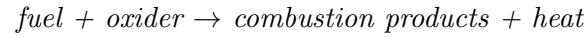
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1 Introduction

Combustion is one of the main means for energy conversion (85% of total energy conversion). It is used in many practical systems for heat production (industrial or home furnaces and heaters), electricity production (thermal power plants), and mobility (aeronautics, aerospace, automotive).

Combustion is an irreversible, largely exothermic reaction between a fuel and an oxidizer:



Some properties of combustion reactions:

- **Heat release:** High heat release in a relatively thin zone (in typical flames, $\delta_L \sim 0.1$ to 1 mm) which induces:
 - high temperature gradients (burnt vs. unburnt gases, of the order of 5 to 7).
 - large density ρ variations.
- **Reaction rate:** Steep and strongly non-linear (follows Arrhenius law).

Combustion combines four major phenomena:

- **Chemistry:** Chemical reactions between fuel and oxidizer. These should be well described and the conditions under which they happen as well (initiation, ignition, extinction...).
- **Heat transfer:** Temperature gradients induce heat transfer (convection, diffusion, radiation).
- **Mass transfer:** Reactants transport (convection, molecular diffusion, turbulent mixing).
- **Fluid mechanics:** Species transport.

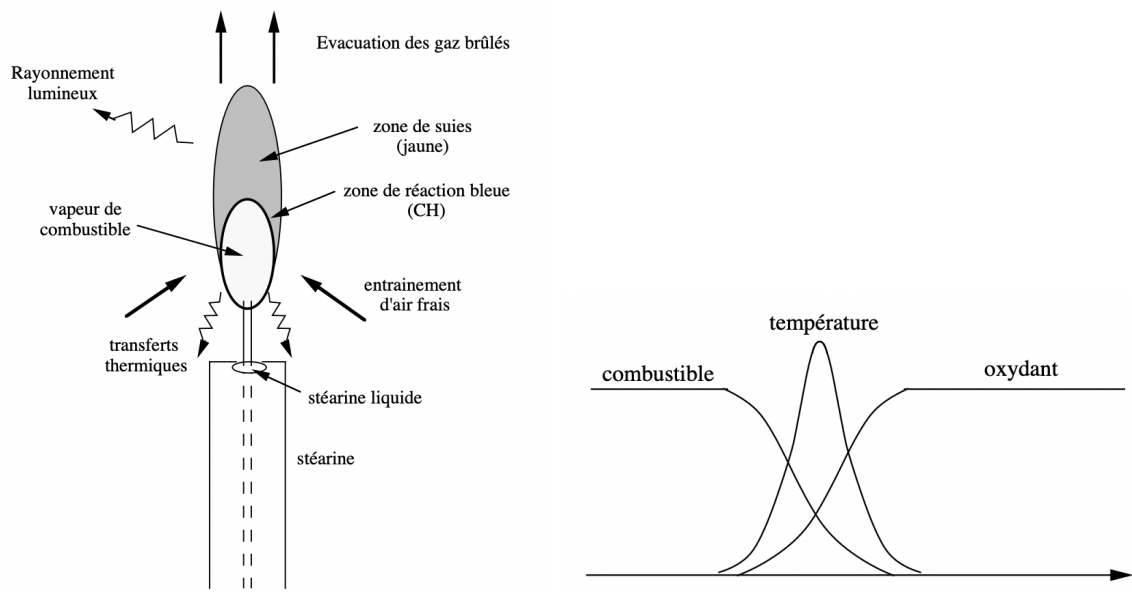


Figure 1: Four major combustion phenomena summarized in the example of a candle

Candles can be used as an example to illustrate these four phenomena:

- *Chemistry*: Blue reaction zone (CH^* radiation, intermediary chemical reaction).
- *Heat transfer*: Soot (unburnt carbon particles) radiation. Liquefaction of stearin at the top of the candle due to conductive heat transfer in the wick and radiation.
- *Fluid mechanics*: Natural convection carries fresh air towards the base of the flame and ensures the evacuation of burnt gases.

Remark: In microgravity, the candle can go out due to the accumulation of burnt gases near the flame.

2 Basics

2.1 Some definitions

2.1.1 Combustion reactions

Air composition:

$$\text{Air} = \text{O}_2 + \beta_1 \text{N}_2 + \beta_2 \text{Ar}$$

(with $\beta_1 = 3.717$ and $\beta_2 = 0.047$)

Argon presence is usually ignored, we therefore say that:

$$\mathbf{Air} = \mathbf{O}_2 + 3.764 \mathbf{N}_2$$

which is equivalent to 21% oxygen and 79% nitrogen.

Combustion reactions often involve hydrocarbon fuels ($C_n H_m$ where n and m are not necessarily *integers*, especially in mixtures of hydrocarbons, i.e: natural gas). In stoichiometric conditions (enough oxygen to convert all carbon to CO_2 and hydrogen to H_2O), the balanced chemical equation takes the form:

$$C_n H_m + (n + \frac{m}{4})(O_2 + 3.76 N_2) \rightarrow n CO_2 + \frac{m}{2} H_2O + 3.76(n + \frac{m}{4}) N_2$$

2.1.2 State variables, intensivity, and extensivity

State variables are used to describe combustion processes. Temperature and composition describe the state of a mixture at any point in time. Pressure is an additional state variable that is necessary to fully characterize a reacting mixture, but most combustion applications happen in isobaric conditions so pressure variations are neglected in the textbook. At the initial state (ambient temperature and no external energy input), the mixture is in *metastable state*. The initial and final state of a reactive mixture is defined by the **temperature** and **chemical composition**.

Remark: Temperature is however an *intensive* physical quantity from a thermodynamic point-of-view (punctual in space, doesn't take into consideration the dimensions of the system) which is not very convenient. Enthalpy or internal energy are used instead, which are both *intensive properties* (proportional to a characteristic quantity of the system, usually mass or volume). The same can be applied to chemical composition. Mass (Y_k) and molar (X_k) fractions are used instead:

- Mass fraction:

$$Y_k = \frac{m_k}{m} = \frac{\rho_k}{\rho}$$

- For balanced combustion reactions:

$$Y_k = \frac{m_k}{m_{tot}} = \frac{\overbrace{n_k}^{\text{Stoichiometric factor in balanced equation}} \cdot \overbrace{M_k}^{\text{Molar mass of molecule}}}{\sum_k n_k M_k}$$

- Molar fraction:

$$X_k = \frac{n_k}{n}$$

- For balanced combustion reactions:

$$X_k = \frac{n_k}{n_{tot}} = \frac{\overbrace{n_k}^{\text{Stoichiometric factor in balanced equation}}}{\sum_k n_k}$$

- *Another very useful equation:*

– Molar mass of the mixture:

$$W = \frac{1}{n} \sum n_k W_k = \sum X_k W_k = \frac{1}{\sum \frac{Y_k}{W_k}}$$

(with $\rho_k = W_k C_k$, more details on Ronan's cheat sheet if needed)

2.1.3 Global variables, equivalence ratio

In addition to state variables, **global variables** can also help describe a system (i.e: burner or combustion chamber).

One of the most used ones is the equivalence ratio ϕ :

$$\phi = \frac{Y_{fuel}/Y_{oxidizer}}{Y_{fuel}/Y_{oxidizer_{st}}}$$

(can also be written in terms of molar fractions X_k)

It can also be calculated using mixture fractions (α):

$$\phi = \frac{\alpha}{\alpha_s}$$

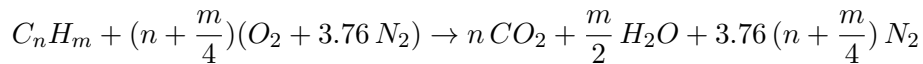
with:

$$\alpha = \frac{\dot{m}_{fuel}}{\dot{m}_{oxidizer}}$$

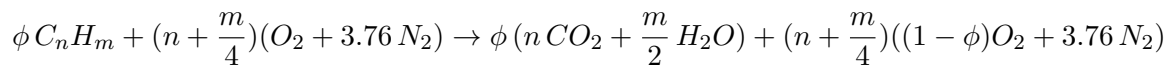
$$\alpha_s = \frac{nW_C + mW_H}{(n + \frac{m}{4})(W_{O_2} + 3.76W_{N_2})}$$

Example:

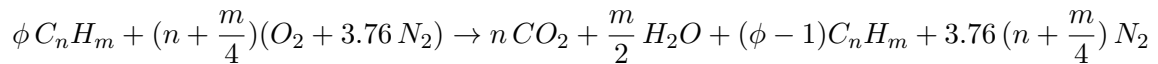
– **Stoichiometry** ($\phi = 1$):



– **Lean** ($\phi < 1$):



– **Rich** ($\phi > 1$):



(can contain traces of CO if rich, writing a balance equation can in this case be delicate)

2.2 Thermodynamics and flame temperatures

2.2.1 Local thermodynamic equilibrium, thermodynamic systems

Thermodynamics of reactive flows typically rely on the local thermodynamic equilibrium hypothesis (LTE) – hypothesis of continuous media (validity criterion: $Kn \ll 1$). In this case, the intensive and extensive properties are continuous in an arbitrarily small volume dV .

Reminder: From Jean Taine's heat transfer book:

Toute la physique des transferts dans les milieux continus repose sur l'hypothèse de l'équilibre thermodynamique local (E.T.L. ou L.T.E. dans la bibliographie anglo-saxonne) qui correspond à une situation de déséquilibre faible : pendant un intervalle de temps dt et dans un élément de volume dV arbitrairement petits, mais à l'échelle macroscopique, le système matériel est infiniment voisin d'un état d'équilibre tangent, caractérisé par un ensemble de valeurs des grandeurs physiques intensives et extensives.

Concrètement l'hypothèse de l'E.T.L. signifie qu'il est possible de définir, à chaque instant t , en tout point r , les variables physiques usuelles en particulier la température $T(\mathbf{r}, t)$. Elle revient à admettre que les degrés internes du système matériel sont thermalisés (distribution de Maxwell-Boltzmann des populations sur les niveaux d'énergie). Un critère simple de validité des conditions de l'E.T.L. dans un élément de volume dV macroscopiquement petit est que le libre parcours moyen (l.p.m.) des porteurs responsables de la thermalisation soit petit par rapport à une dimension L de cet élément ($Kn = \text{l.p.m.}/L$, nombre de Knudsen, petit devant 1.)

2.2.2 Some important definitions

Thermodynamic systems – Some types of thermodynamic systems are described in the following table:

Interactions of thermodynamic systems			
Type of system	Mass flow	Work	Heat
Open	✓	✓	✓
Closed	✗	✓	✓
Thermally isolated	✗	✓	✗
Mechanically isolated	✗	✗	✓
Isolated	✗	✗	✗

Open system – Can exchange mass, work, heat with the exterior.

Closed system – Fixed mass, no exchange of mass with the exterior.

Isolated system – No exchange of mass, heat, or work with the exterior.

Adiabatic process – No exchange of heat or mass with the exterior (only work).

Enthalpy (H) (J) – Enthalpy is a **state function** (def: a function that quantitatively describes an equilibrium state of a thermodynamic system, independently of the path / a function of **state variables** at a certain thermodynamic equilibrium state.)

It is defined as the sum of the internal energy and the product of pressure and volume:

$$H = \underbrace{U}_{\text{Internal energy}} + \underbrace{pV}_{\text{Work}}$$

2.1: First Law of Thermodynamics

- Variant of the energy balance ("*energy can't be created or destroyed, it can only be transformed*").
- For a **closed** system:

$$\underbrace{\delta Q}_{\text{infinitesimal amount of heat}} = \underbrace{dU}_{\text{internal state energy}} + \underbrace{\delta W}_{\text{infinitesimal amount of work}}$$

The work term is sometimes neglected since it's small compared to internal energy. Usually, pressure variations can be neglected: $\delta W = pdV$

Entropy (S) ($J.K^{-1}$) – Entropy is a state function commonly referred to as the degree of disorder in a system. It is also the measurement of the probability of each energy configuration, the number of possibilities (Boltzman's equation), spread of energy (low spread = low entropy, high spread = high entropy).

It does not depend on the size of the system, it depends on the probability of spread. Higher entropy is *almost always* more likely, and the chances of entropy decreasing are extremely low especially at the scale of the objects we use. For a thermodynamic process:

$$adiabatic + reversible \rightarrow isentropic$$

The opposite, however, is not always true.

2.2: Second Law of Thermodynamics

- Multiple statements (Carnot, Clausius, Kelvin...)
- For a **closed** system:
There exists a quantity S, called the entropy, which has the property that for an infinitesimal process in a **closed** system, the following inequality always holds (only equal if the process is reversible).

$$dS \geq \frac{\delta Q}{T}$$

*The equality holds if the process is reversible.
If the process is adiabatic, $\delta Q = 0$ which gives $dS \geq 0$.*

Some interesting relations:

- Enthalpy differential using Maxwell equations:

$$dH = dU + d(pV) = dU + pdV + Vdp$$

- For a **closed** system, and neglecting pressure variations: (*Combustion reactions*)

$$dH = \delta Q$$

– For a **closed** system, reversible process, and neglecting pressure variations: (Not valid for combustion // irreversible)

$$dH = TdS + pdV$$

– For a **closed** system, adiabatic, involving ideal gases, and neglecting pressure variations:

$$dH = C_p dT$$

with C_p the heat capacity at constant pressure.

Heat of reaction (H_r) ($J.mol^{-1}$) – Also referred to as the **enthalpy of reaction**. It is the change of energy or heat content associated with a reaction at a specified temperature, where each of the reactants and products is in an appropriate **standard state** (def: for each state, a reference state exists – for gases, it's the ideal gas state at atmospheric pressure).

– *Important:* The heats of reaction should be at the same temperature.

Heat of reaction is a **state function**. The total enthalpy of a system cannot be measured directly, we measure the **enthalpy change** (ΔH) instead.

The heat of reaction can be calculated using three different methods (more details in Appendix A):

1. **Enthalpy of formation** (ΔH_f).
2. **Bond enthalpies** (ΔH , ΔH_B).
3. **Hess's law:** adding up enthalpies of reactions of different chemical reactions to obtain the enthalpy of reaction of the desired reaction (pretty much like summing a bunch of algebraic equations to cancel out some parameters and only keep the final equation – valid since it's a state function).

For the rest, we will stick to the first definition (**enthalpy of formation**). In general, it can be calculated using the following equation:

$$\Delta H = \sum_{i \text{ prod}} n_i [(H_{T_2}^\circ - H_0^\circ) - (H_{T_0}^\circ - H_0^\circ) + (\Delta H_f^\circ)_{T_0}]_i - \sum_{j \text{ react}} n_j [(H_{T_1}^\circ - H_0^\circ) - (H_{T_0}^\circ - H_0^\circ) + (\Delta H_f^\circ)_{T_0}]_j$$

By simplifying (T'_0 can be different for each reactor):

$$\Delta H = \sum_{i \text{ prod}} n_i [H_{T_2}^\circ - H_{T_0}^\circ + (\Delta H_f^\circ)_{T_0}]_i - \sum_{j \text{ react}} n_j [H_{T_1}^\circ - H_{T_0}^\circ + (\Delta H_f^\circ)_{T_0}]_j$$

Another definition (Centrale textbook), this time for specific enthalpy:

$$\underbrace{h_k(T, P)}_{\text{Specific enthalpy of species 'k'}} = \underbrace{\Delta h_{f,k}^0(T_0, P_0)}_{\text{Standard state/ reference enthalpy}} + \underbrace{\int_{T_0}^T C_{p,k}(T') dT}_{\text{Sensible enthalpy}}$$

$$\underbrace{h(T, P)}_{\text{Total specific enthalpy}} = \sum_{k=1}^K h_k(T, P) = \sum_{k=1}^K [Y_k \Delta h_{f,k}^0(T_0, P_0) + \int_{T_0}^T Y_k C_{p,k}(T') dT']$$

with T_0 standard reference temperature (298K), T_1 initial temperature of reactants (sometimes $T_1 = T_0$), T_2 final temperature of products.

2.2.3 Adiabatic flame temperature

In adiabatic conditions, the enthalpy is conserved in combustion reactions. We can write the following equations to estimate the adiabatic flame temperature T_2 :

$$\Delta h = 0$$

$$h_{reactants} = h_{products}$$

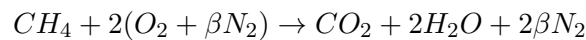
$$\sum_{k=1}^K [Y_k \Delta h_{f,k}^0(T_0, P_0) + \int_{T_0}^{T_1} Y_k C_{p,k}(T') dT']_{reactants} = \sum_{k=1}^K [Y_k \Delta h_{f,k}^0(T_0, P_0) + \int_{T_0}^{T_2} Y_k C_{p,k}(T') dT']_{products}$$

Quick hacks:

- Standard enthalpy of formation (Δh_f^0) of O_2 , N_2 , H_2 , solid C is equal to zero.
- Initial temperature $T_1 = T_0 = 298\text{ K}$: the integral term in the LHS disappears.
- Three simplifications for the **heat capacity at constant pressure** (C_p):
 1. C_p independent of temperature.
 2. C_p same for all species.
 3. (1) and (2) combined.

Example: Case 3 – C_p independent of temperature and same for all species.

For the following stoichiometric chemical reaction:



$$T_2 = \frac{Y_{CH_4} \cdot \Delta h_f^0(CH_4) - Y_{CO_2} \cdot \Delta h_f^0(CO_2) - Y_{H_2O} \cdot \Delta h_f^0(H_2O)}{C_p} + T_0$$

3 Chemical kinetics

3.1 Introduction

Combustion reactions are characterized by the rates at which they happen and reaction conditions. Some of the most important conditions are temperature, pressure, species concentrations (reactants) and the presence (or absence) of catalysts or inhibitors. Understanding the chemical mechanisms of combustion reactions is therefore of utmost importance, and so is the analysis of the production or destruction of pollutants, as well as some important phenomena such as ignition or extinction.

Combustion reactions can be modelled using **global reactions**. A general form is:



Such models are commonly used in complex systems where the calculation of the aerodynamic field takes up most of the computation power and where accounting for all detailed chemical mechanisms is virtually impossible. In reality, combustion reactions are the sum of many elementary reactions.

3.1.1 Molecular collisions, reaction frequency

Combustion reactions are initiated at high temperatures where the probability of molecular collisions increases. The **frequency of molecular collisions** (by volume unit) Z_{AB} is defined as:

$$Z_{AB} = N_a^2 [A][B] \sigma_{AB} v_{AB}$$

with the **motion molecular velocity** v_{AB} defined as:

$$v_{AB} = \sqrt{\frac{8k_B T}{\pi \mu_{AB}}}$$

with: N_a : Avogadro's constant ($6.022 \cdot 10^{23}$ particles), $[A]$: molar concentration (moles per volume unit) of species A, σ_{AB} : cross section of possible collisions ($\Pi r_{AB}^2 = (r_A + r_B)^2$), k_B : Boltzmann's constant (gas constant/ N_a , $1.381 \cdot 10^{-23}$, in $J.K^{-1}$), μ_{AB} : reduced mass ($\frac{1}{\mu_{AB}} = \frac{1}{m_A} + \frac{1}{m_B}$), T: Temperature.

But since not all collisions lead to reactions, two other correcting factors are added to the above stated equation to model the frequency of collisions **leading to reactions**.

- **Steric factor** (p): probability that colliding molecules are "properly oriented".
- **Energetic factor** (f): probability that the energy content of colliding molecules is higher than a certain activation energy (E_a in $J.mol^{-1}$). This term corresponds to the exponential factor in the Arrhenius equation:

$$f = e^{\frac{E_a}{RT}}$$

The frequency of molecular collisions *leading to reactions* (by unit volume) is therefore defined as:

$$v = p.f.Z_{AB}$$

or

$$v = k[A][B]$$

where k is a constant that depends on temperature and can easily be determined by identification.

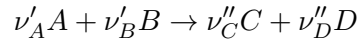
3.1.2 Rate of reactions, Arrhenius' law

Arrhenius' postulate defines the **rate of reaction constant** as:

$$k(T) = \underbrace{A.T^\beta}_{\text{pre-exponential factor}} \cdot \underbrace{e^{\frac{-E_a}{RT}}}_{\text{exponential(energetic) factor}}$$

where A , β , and E_a are empirical and vary from an author to another.

The **reaction rate** can then be calculated using the constant k . For a simple direct (one-way) reaction of the form:



the reaction rate of species A is:

$$\frac{d[A]}{dt} = -k\nu'_A [A]^{\nu'_A} [B]^{\nu'_B}$$

similarity:

$$\frac{d[C]}{dt} = +k\nu'_C [A]^{\nu'_A} [B]^{\nu'_B}$$

The order of reaction is defined as:

$$m = \sum_{i=1}^N \nu'_i$$

The molar reaction rate is defined as:

$$\dot{\omega}_k = \frac{d[A]_k}{dt}$$

Other interesting types of reactions (can be found on B. Fiorina's kinetics slides): opposing reactions, competitive reactions, consecutive reactions.

4 Spontaneous combustion

4.1 Introduction

In ambient temperature, a fuel-oxidizer mixture is in a metastable state where reaction speeds are practically null. By increasing the temperature gradually, the exothermic slow oxidation reactions are initiated and temperature increases (as long as heat losses to the walls are not important). The slow reactions will therefore be accelerated. We may end up with one of the two following situations:

- If $T < T_i$: The reactants are fully consumed and the reaction speed decreases.
- If $T \geq T_i$: The reaction turns into a combustion when the temperature reaches the ignition temperature.

In the second case ($T \geq T_i$), there is a certain delay before ignition happens (a certain concentration of radicals is necessary to initiate the combustion). This delay is referred to as the **ignition delay** (τ_i).

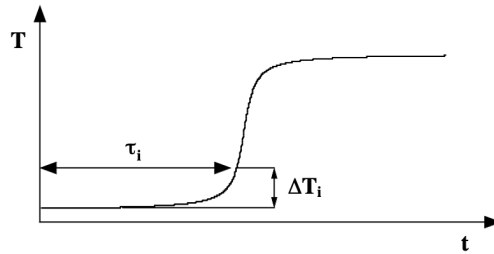


Figure 2: Ignition delay illustrated

Both T_i and τ_i depend on: equivalence ratio, pressure, the presence of inert dilutants in the mixture, the presence of additives favoring or limiting chain reactions, wall temperatures, and the dimensions of the system containing the mixture.

4.2 Semenov's theory

To be continued later on, not sure if it's the most interesting part to cover for the moment.

5 Premixed flames

5.1 Introduction

Premixed flames are often encountered in many applications. The simplest one is perhaps the bunsen burner (laminar flame). Premixed flames are also used in more complex systems, particularly Otto engines and gas turbines (turbulent regime). Premixed flames can be divided to two main regions:

1. **Preheating region:** Where the main phenomena are species transport (mass transfer) and heat transfer.
2. **Reaction zone:** Where all essential chemical reactions happen. They can usually be described using a simple reaction model (one-step). By following a streamline, the evolution of temperature can be described as in the figures below.

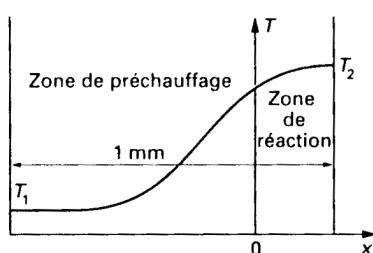


Figure VI.2: Profil de température dans une flamme laminaire prémélangée

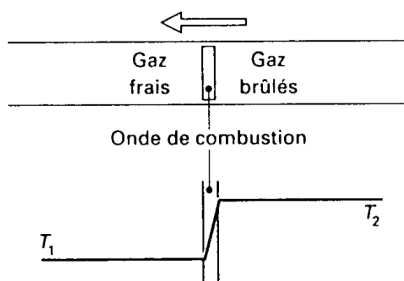


Figure VI.3: Onde de combustion

Figure 3: Temperature profile and combustion wave propagation in a premixed system

A similar phenomenon to combustion in a bunsen burner can be observed if we use a tube containing a reactive mixture where both extremities are initially covered. If the latter are instantly uncovered and the mixture is ignited in one of them, a flame front will appear and propagate towards the other side at a velocity of around 5 m.s^{-1} . This flame front has the same properties of the reaction zone of a bunsen burner flame (and can be treated like such, like a **planar wave**). We are in this case in presence of a subsonic combustion wave (**deflagration**). If the same experiment is repeated while the other extremity is this time covered, the flame front will propagate at a much higher speed (a few km.s^{-1}). We are in this case in presence of a supersonic combustion wave (**detonation**).

5.2 Combustion wave equation

Here, we detail the conservation equations on each side of the combustion wave (with 1: fresh gases, and 2: burnt gases):

- Continuity equation:

$$\frac{\dot{m}}{A} = \rho_1 u_1 = \rho_2 u_2$$

- Momentum conservation:

$$p_1 + \rho_1 u_1^2 = p_2 + \rho_2 u_2^2$$

- Energy conservation:

$$h_1 + \frac{u_1^2}{2} = h_2 + \frac{u_2^2}{2}$$

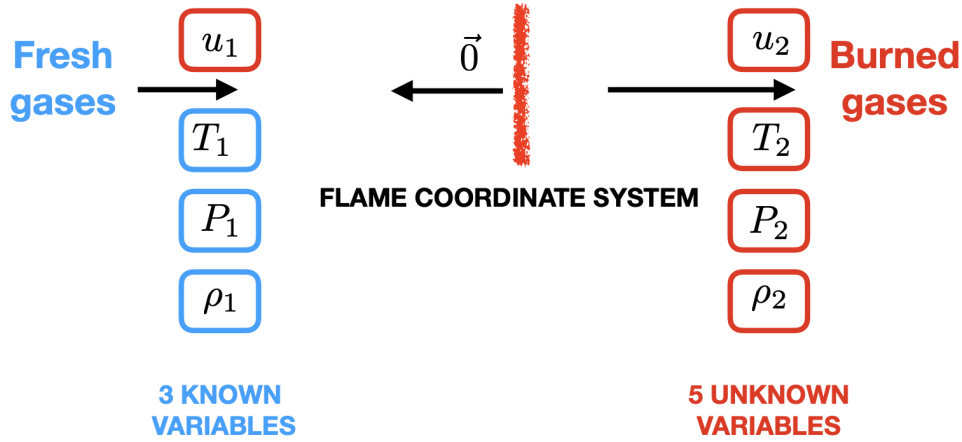
$$C_p T_1 + \frac{u_1^2}{2} + \Delta h_0 = C_p T_2 + \frac{u_2^2}{2}$$

with: $\Delta h_0 = h_1^0 - h_2^0$ (where h^0 is the standard enthalpy of formation).

- State equations (ideal gas):

$$p_1 = \rho_1 r T_1$$

$$p_2 = \rho_2 r T_2$$



By combining mass continuity and momentum equations, we define the **Rayleigh line** such that:

$$p = -\left(\frac{\dot{m}}{A}\right)^2 \frac{1}{\rho} + cst$$

Using the previous result and the energy conservation equation, we define p_2 as:

$$p_2 = \frac{\Delta h_0 + \frac{\gamma+1}{2(\gamma-1)} - \frac{p_1}{2} \frac{1}{\rho_2}}{-\frac{1}{2\rho_1} + \frac{\gamma+1}{2(\gamma-1)} \frac{1}{\rho_2}}$$

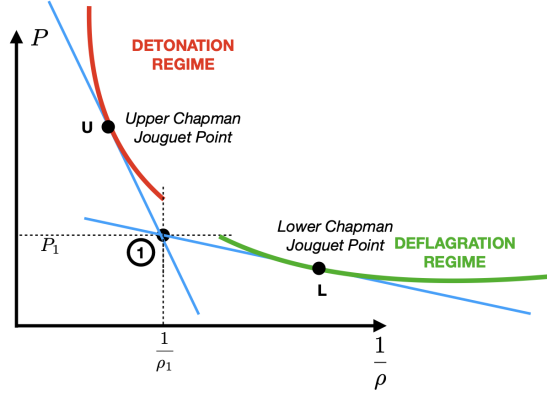


Figure 4: Clapeyron's diagram

Reminder: $M = u/c$ and $c = \sqrt{\gamma r T}$

The function $p = f(\frac{1}{\rho})$ is therefore a hyperbola (Hugoniot's curve or Hugoniot's hyperbola). In absence of chemical reactions, the specific reference enthalpy is null ($\Delta h^0 = 0$) and the curve crosses the point of coordinates $(p_1, 1/\rho_1)$. This function separates three different regions which correspond to all possible solutions (intersection of Rayleigh's line with Hugoniot's curve).

- **Detonation regime:** When $p_2 \gg p_1$ and $M_1 > 1$. The combustion wave is supersonic. The velocity of at which fresh gases approach the planar combustion wave from its point of view is higher than that of burnt gases $u_1 > u_2$.
- **Deflagration regime:** When $p_2 \approx p_1$ and $M_1 < 1$. The combustion wave is subsonic. It's the case for flames encountered in Bunsen burners. The intersection of Rayleigh's line and Hugoniot's curve in this case corresponds to $M = 1$ which reduces the range of possible solutions to $p = f(1/\rho)$ with $1/\rho < 1/\rho_{M=1}$. In order to fully solve the problem, an additional equation is necessary (flame thickness δ_l).
- There is no solution for the equation when $p > p_1$ and $1/\rho > 1/\rho_1$.

5.3 Laminar flame speed

There are many definitions of the laminar flame speed and most definitions have changed or evolved along the years. Historically, two major approaches have been suggested to calculate the laminar flame speed:

- **Thermal approach:** (Mallard, Le Châtelier 1885) Related to transport phenomena (mostly heat transfer). This approach defines the laminar flame speed as:

$$S_l = \sqrt{D_T \bar{\omega}}$$

where $\bar{\omega}$ is the average reaction rate.

- **Diffusion approach:** (Zeldovich, Frank-Kamenetskii, Semenov 1938) Relies on mass transfer or diffusion of species and free radicals. This approach defines the laminar flame speed as:

$$S_l = C \sqrt{\frac{\lambda}{\rho_1^2 C_p (Y_{F1} - Y_{F2})}} \bar{\omega}$$

where C is a constant and λ the thermal conductivity.

- Current approaches rely on numerical simulation to combine both the thermal approach and molecular diffusion.

Both approaches make use of simplifications and assumptions to estimate the laminar flame speed, more detail on the combustion textbook (poly Centrale).

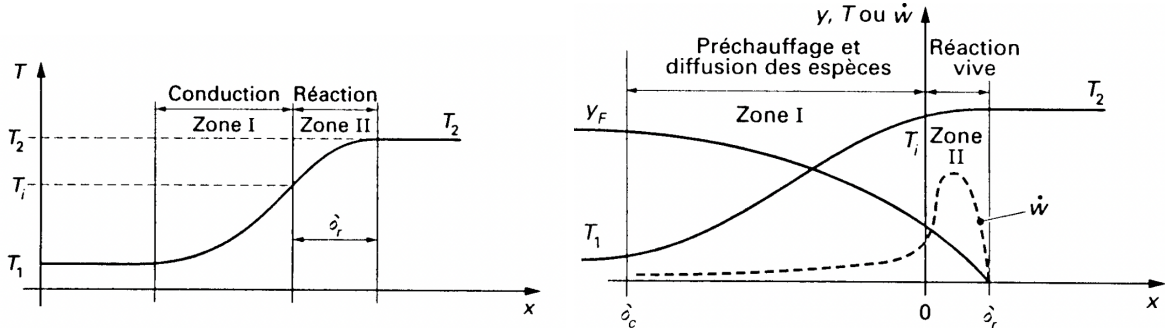


Figure 5: Thermal approach (left) and diffusive approach (right) in calculating the laminar flame speed

5.3.1 Some important dimensionless numbers

We define hereby the following dimensionless numbers:

- **Prandtl's number:** (with D_T : thermal diffusivity).

$$Pr = \frac{\nu}{D_T} = \frac{\text{momentum transport}}{\text{thermal transport}}$$

- **Schmidt's number:**

$$Sc = \frac{\nu}{D_J} = \frac{\text{momentum transport}}{\text{species or mass transport}}$$

- **Lewis' number:** Thermo-diffusive effects.

$$Le = \frac{D_T}{D_J} = \frac{Sc}{Pr} = \frac{\text{diffusive mass transfer}}{\text{heat transfer}}$$

- **Progress variable:** (with $c=0$ in unburnt gases and $c=1$ in burnt gases)

$$c = \frac{T - T_1}{T_2 - T_1} = \frac{Y_F - Y_{F_1}}{Y_{F_2} - Y_{F_1}}$$

6 Premixed turbulent combustion

6.1 Damköhler, Karlovitz numbers, and flame thickness

From Veynante's & Poinso's books and lectures

Turbulence is characterized by the RMS turbulent velocity u' and its integral length scale l_t . Derivations of turbulent combustion models also use a second assumption: turbulence is isotropic and homogeneous. The local dissipation rate of turbulent kinetic energy ϵ :

$$\epsilon = \frac{u'(r)^3}{r}$$

We can then define the **turbulent time scale**:

$$\tau_m(r) = \frac{r}{u'(r)} = \frac{r^{2/3}}{\epsilon^{1/3}}$$

and the **chemical time scale** (or flame, combustion, diffusion time scale):

$$\tau_c = \frac{\delta}{s_L^0} = \frac{\text{flame thickness}}{\text{flame speed}}$$

with the **flame thickness** δ_L defined as:

$$\delta_L = \frac{\alpha}{(s_L^0)^2} = \frac{T_b - T_u}{(\frac{\partial T}{\partial x})_{max}}$$

where α is the thermal diffusivity.

We can combine both into the **Damköhler number**:

$$Da(r) = \frac{\tau_m(r)}{\tau_c} = \frac{\text{turbulent time scale}}{\text{chemical time scale}}$$

- $Da \gg 1$ ($\tau_c \ll \tau_t$): Turbulence effect on inner flame structure is limited/ not significant.
- $Da \ll 1$ ($\tau_c \gg \tau_t$): Flame strongly modified by turbulent eddies.

But in reality, $Da(r)$ depends on r with $\eta_k < r < l_t$ (with η_k : Kolmogorov length scale, and l_t : Integral length scale). So, instead, we define the following dimensionless number:

- **Damköhler number** (Da): Defined for the largest scales l_t :

$$Da = \frac{\tau_m(l_t)}{\tau_c} = \frac{\tau_t}{\tau_c} = \frac{\frac{l_t}{u_t}}{\frac{\delta}{s_L^0}}$$

- **Karlovitz number** (Ka): Inverse of Da but only for the smallest Kolmogorov scales:

$$Ka = \frac{1}{Da(\eta_k)} = \frac{\tau_c}{\tau_k} = \frac{\frac{\delta}{s_L^0}}{\frac{\eta_k}{u'(\eta_k)}}$$

(Other forms of this equation available on p. 208 of V & P's book)

In Kolmogorov's cascade, kinetic energy is transferred from the larger scales to the smaller scales. The dissipation rate of kinetic energy remains constant:

$$\epsilon \approx \frac{u_t^3}{l_t} \approx \frac{u_k^3}{l\eta_k} \approx \nu \left(\frac{u_k}{\eta_k} \right)^2$$

This yields the following interesting equation:

$$Re_t = \frac{u_t l_t}{\nu}$$

$$Re_t^{1/2} = Da.Ka$$

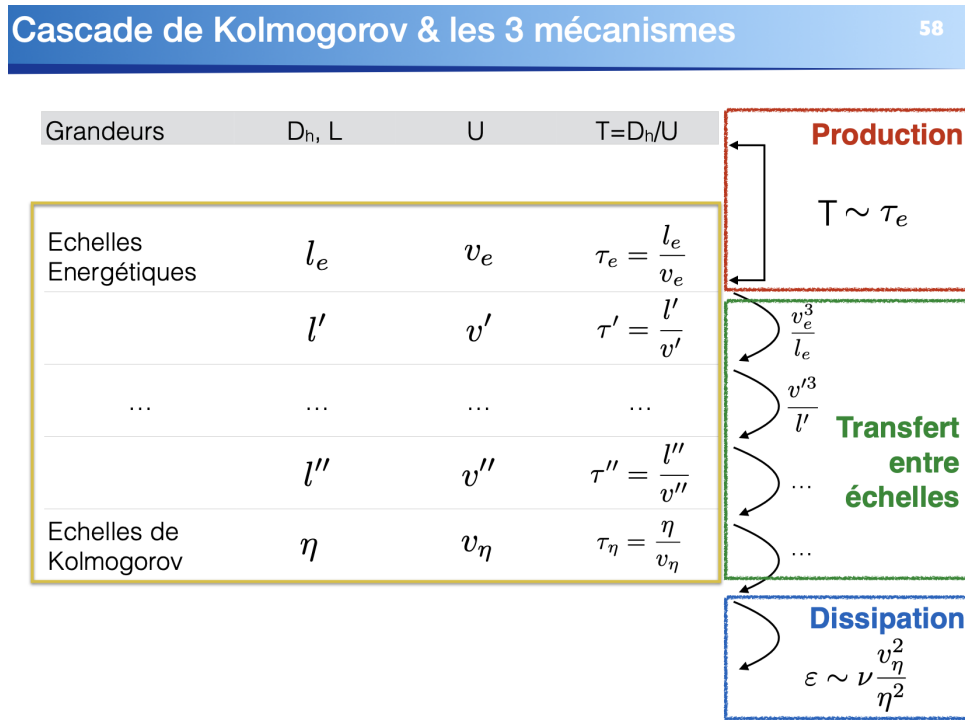


Figure 6: (a) Kolmogorov cascade and the three energy transfer mechanisms (Turbulence_E2_01 Ronan)

6.2 Turbulent flame regimes

Using the quantities introduced previously, we can define a turbulent combustion diagram comprised of different zones.

1. **Flamelet regime** or **thin flame regime** ($Da > 1$ and $Ka < 1$): In this region, the chemical time scale is shorter than any turbulent time scale, even the Kolmogorov scale (*region "dominated" by turbulence but to an extent*).
Features – Thin reaction zone, flame thickness smaller than any turbulent scale, the flame has an inner structure similar to that of a laminar flame and is wrinkled by turbulent motion.
 - (a) **Wrinkled flamelets** ($u' < s_L^0$): the speed of turbulent motion is too low to wrinkle the flame front to the extent of causing flame interactions.

Rapport des tailles caractéristiques	$\frac{\eta}{\ell_e} \approx \frac{1}{(\text{Re}_{\ell_e})^{3/4}}$	
Rapport des vitesses caractéristiques	$\frac{v_\eta}{v_e} \approx \frac{1}{(\text{Re}_{\ell_e})^{1/4}}$	avec $\text{Re}_{\ell_e} = \frac{v_e \ell_e}{\nu}$
Rapport des temps caractéristiques	$\frac{\tau_\eta}{\tau_e} \approx \frac{1}{(\text{Re}_{\ell_e})^{1/2}}$	

Figure 7: (b) Some basic equations relating the different scales (Turbulence_E2_01 Ronan)

- (b) **Corrugated flamelets** ($u' < s_L^0$): the speed of turbulent motion is enough to wrinkle the flame front to the extent of causing flame interactions leading to the formation of pockets of burnt and unburnt gases.
2. **Thickened-wrinkled flame** ($1 < Ka < 100$): In this region, turbulent structures increase the thickness of the preheating zone but do not penetrate the reaction zone which remains thin and *close* to a laminar flame.
 3. **Thickened flame** ($Ka > 100$, $Da \ll 1$): In this region, the mixing is fast and the overall reaction rate is mainly limited by chemistry (*region "dominated" by **chemistry***). Both the preheating and reaction zones are perturbed by turbulence and *no laminar flame structure can be indentified*.

7 Diffusion flames

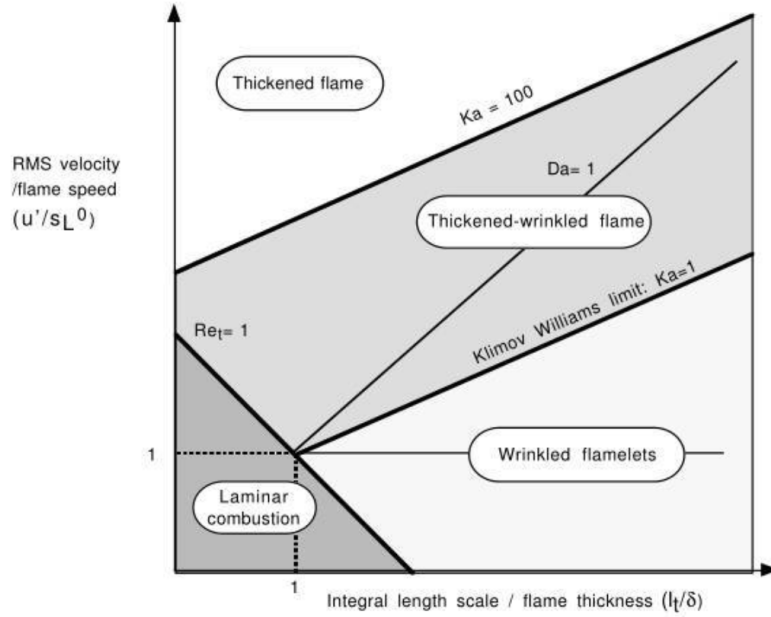


Figure 8: Premixed turbulent combustion regimes (**Remark about the Damköhler line, the slope of the line is actually $1/Da$**)

A Entropy and disorder

1. Enthalpies of chemical reactions

$$\Delta H = H_f - H_i$$

- Heat released during a chemical reaction ($\Delta H < 0$) or required ($\Delta H > 0$) to initiate it.
- $\Delta H = \Delta U$ ($p\Delta V$ term small compared to ΔU so it is often omitted).
- Enthalpy is a state function (independent of path). It depends only on the initial and final states.
- **Hess's law:** adding up enthalpies of reactions of different chemical reactions to obtain the enthalpy of reaction of the desired reaction (pretty much like summing a bunch of algebraic equations to cancel out some parameters and only keep the final equation).
- **Three way to calculate the heat of reaction:**
 - (a) **Bond enthalpies (ΔH , ΔH_B) :**

$$\Delta H_r = \sum \Delta H(\text{bonds broken}) - \Delta H(\text{bonds formed})$$

$$\Delta H_r = \sum \Delta H(\text{reactants}) - \Delta H(\text{products})$$

- (b) **Enthalpy of formation (ΔH_f):** (what we typically use in combustion)

$$\Delta H_r = \sum \Delta H_f(\text{products}) - \Delta H_f(\text{reactants})$$

- (c) **Hess's law.**

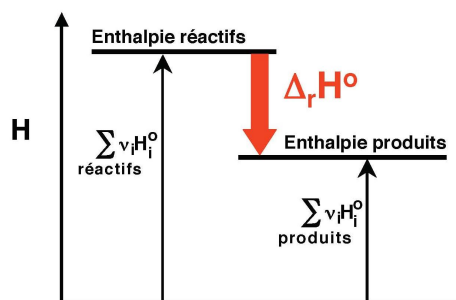


Figure 9: L'enthalpie de réaction correspond à la différence d'enthalpie entre les produits de la réaction (à droite) et les réactifs (à gauche). Pour calculer cette différence, il est capital de disposer d'une référence commune.

2. Spontaneous change and free energy

- Reaction will proceed in a direction without any external interference to force it to happen.
- Endothermic equations are **more likely** to be non-spontaneous than exothermic reactions. However, endothermic equations **can be spontaneous** (i.e: melting of a solid H_2O cube).
- However, **enthalpy isn't a measure of spontaneity**, we use instead the **Gibbs free energy** to assess whether a reaction is spontaneous or not.
- **Gibbs free energy (ΔG) :**

$$\underbrace{\Delta G}_{\text{Useful work or free energy}} = \Delta H - \underbrace{T\Delta S}_{\text{Amount of energy that gets "stuck" in molecules (i.e: vib, rot...)}}$$

for constant temperature and pressure.

- (a) $\Delta G < 0$: Spontaneous.
- (b) $\Delta G = 0$: Equilibrium (no net change).
- (c) $\Delta G > 0$: Non-spontaneous.

3. Entropy

- Measure of disorder of a system.
- Change of entropy: are we becoming more ordered or more disordered?
- Also a state function (only depends on initial and final state).
- **Entropy of reaction (ΔS_r):**

$$\Delta S_r^0 = \sum \Delta S^0(\text{products}) - \Delta S^0(\text{reactants})$$

where S^0 is the absolute standard enthalpy.

Important: Multiply S of products or reactants by corresponding stoichiometric coefficient (with S in $kJ.K^{-1}.mol^{-1}$)

- $S = 0$ for the perfect crystal at absolute zero $T = 0 K$ (**Third law of thermodynamics**).
- Don't confuse **thermodynamics** (no info on timescales) and **kinetics** (info about timescales, speed of reactions, etc.)

4. Free energy of formation

- **Free energy of formation (ΔG_f) :** Stability of a compound relative of its elements.

$$\Delta G_f^0 = \Delta H_f^0 - T\Delta S^0$$

** 0 superscript: standard thermodynamic state (arbitrary reference, typically $P = 1 \text{ bar}$ and $T = 298.15 \text{ K}$).

- (a) $\Delta G_r < 0$: Stable.
- (b) $\Delta G_r > 0$: Unstable.