

## CE420 IRRIGATION AND DRAINAGE

### HOMEWORK # 1

1. Particle size analyses is the most sure method of determining the textural properties of a soil. Given the following results of soil sample retained on various size sieves, what is the soil texture of the sample?

Sieve Size (mm)	Mass (gr)
2	0
1	0
0.5	5
0.25	4
0.1	8
0.05	15
0.002	30
Not caught	40

2. A tube 5 cm diameter was used to remove one sample of soil which was trimmed to 5.0 cm length; the soil, after trimming, weighted 156.68 gr. It was dried and reweighed and found to have lost 31.33 gr. Compute (assuming no shrinkage)  
a)  $\theta_m$     b)  $\rho_b$     c)  $\theta_v$     d)  $n$     if particle density is  $2.67 \text{ g/cm}^3$
3. What is the matrix potential of a soil which has drained until pores with an equivalent diameter of 0.00020 mm remain filled?
4. What would the equivalent diameter of capillarity drained to  $-1/3$  bar matrix potential be? Assume pure water and give your answer in mm.
5. What solute concentration would yield an osmotic potential equal to  $-1/3$  bar?
6. What is the water potential in bars of a soil water at  $-1/3$  bar if the water contains an active solute concentration of  $2 \times 10^{-4} \text{ moles/cm}^3$  at a temperature of 290 K?
7. Compute a characteristic curve for the soil in example 3.4 in the lecture notes.

# HW1 SOLUTION

**1) Mass of Soil =  $5 + 4 + 8 + 15 + 30 + 40 = 102$  gr**

	SAND		SILT		CLAY	
	Mass (gr)	% (Mass/Soil Mass)	Mass (gr)	% (Mass/Soil Mass)	Mass (gr)	% (Mass/Soil Mass)
$d \geq 0.05\text{mm}$	32	31.4				
$0.002 \text{ mm} \leq d \leq 0.05\text{mm}$			30	29.4		
$d \leq 0.002 \text{ mm}$					40	39.22

From Piper Diagram (%Sand=31.4, % Silt =29.4, %Clay= 39.2)

The Sample is **CLAY LOAM**

$$2.) V_{\text{soil}} = \frac{\pi D^2}{4} \cdot L = \frac{3.14 \cdot 25}{4} \cdot 5 = 98.175 \text{ cm}^3$$

a)  $m_{\text{soil}} = 156.68\text{gr}$

$$m_{\text{water}} = 31.33 \text{ gr}$$

$$m_{\text{dry}} = m_{\text{soil}} - m_{\text{water}} = 156.8 - 31.33 = 125.35 \text{ gr}$$

$$\theta_m = \frac{m_{soil} - m_{dry}}{m_{dry}} = \frac{31.33}{125.35} \cdot 100 \quad \theta_m = 25\%$$

$$\text{b) } \rho_b = \frac{m_{\text{dry}}}{V_{\text{soil}}} = \frac{125.35}{98.175} \cong 1.28 \text{ gr/cm}^3$$

c)  $\theta_v = \theta_m \cdot \rho_b = 25\% \cdot 1.28 \cong 32\%$

$$\text{d) } n = 1 - \frac{\rho_b}{\rho_s} = 1 - \frac{1.28}{2.67} = 0.521 \Rightarrow n=52.1 \%$$

$$\mathbf{3.)} \quad \psi_m = -h = -2 \frac{\gamma}{\rho g r} \quad \gamma=0.073 \text{ N/m}, g=9.807 \text{ m/s}^2, \rho=1000 \text{ kg/m}^3$$

$$2r = 0.0002 \times 10^{-3} \Rightarrow r = 1 \times 10^{-7} \text{ meter}$$

$$\psi_m = -2 \frac{0.073 \text{ N/m}}{9.807 \text{ m/s}^2 \cdot 10^{-7} \cdot 1000 \text{ kg/m}^3} = -148.8 \text{ m} = -14.5 \text{ bar}$$

(1 bar = 10.35m)

4.)  $\psi_m = -1/3 \text{ bar} = -10.33 \text{ m} / 3 = -3.44 \text{ H}_2\text{O}$

$$\psi_m = -2 \frac{\gamma}{\rho_{gr}} - 3.44m = -2 \frac{0.073N/m}{1000kg/m^3 \cdot 9.807m/s^2 \cdot r}$$

$$r = 4.33 \times 10^{-6} m \Rightarrow d = 2r = 8.655 \times 10^{-6} m \Rightarrow \mathbf{d = 0.0087 \text{ mm}}$$

$$\mathbf{5.)} \quad \psi_0 = -RTC_s \quad \psi_0 = -1/3 \text{ bar}$$

$$T = 290^0 K \text{ (assumed)}$$

$$R = 8.314 \text{ bar-cm}^3/\text{K-mole} \times 290 \text{ K} \times C_s \Rightarrow \mathbf{C_s = 1.38 \times 10^{-4} \text{ moles/cm}^3}$$

$$\mathbf{6.)} \quad \psi_m = -1/3 \text{ bar}$$

$$\psi_0 = -RTC_s \quad ; T = 290^0 K \quad ; R = 8.314 \text{ bar-cm}^3/\text{K-mole} \quad ; C_s = 2 \times 10^{-4} \text{ moles/cm}^3$$

$$\psi_0 = -8.314 \cdot 290 \cdot 2 \cdot 10^{-4} = -0.482 \text{ bar}$$

$$\psi_T = \psi_m + \psi_0 = -\frac{1}{3} + (-0.482) \quad \mathbf{\psi_T = -0.816 \text{ bar}}$$

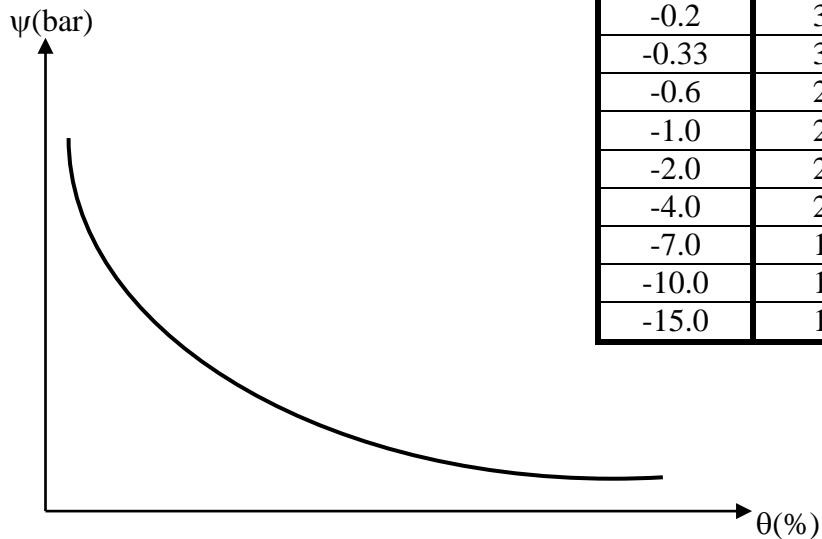
**7.)** Based on Example 3.4

$$20\% \text{ Clay} \Rightarrow C = 20 \quad ; \text{ OM} = 2.1\%$$

$$50\% \text{ Silt} \quad \rho_b = 1.33 \text{ kg/cm}^3$$

$$30\% \text{ Sand} \quad S = 30$$

$$\frac{\theta}{100} = a_0 + a_1 S + a_2 C + a_3 \text{ OM} + a_4 \rho_b$$



$\psi_m$ (bar)	$\theta_v$ (%)
-0.1	-
-0.2	36
-0.33	32
-0.6	29
-1.0	26
-2.0	23
-4.0	20
-7.0	19
-10.0	18
-15.0	16