

## Spring'14 Soil Mechanics Homework 6 Solution

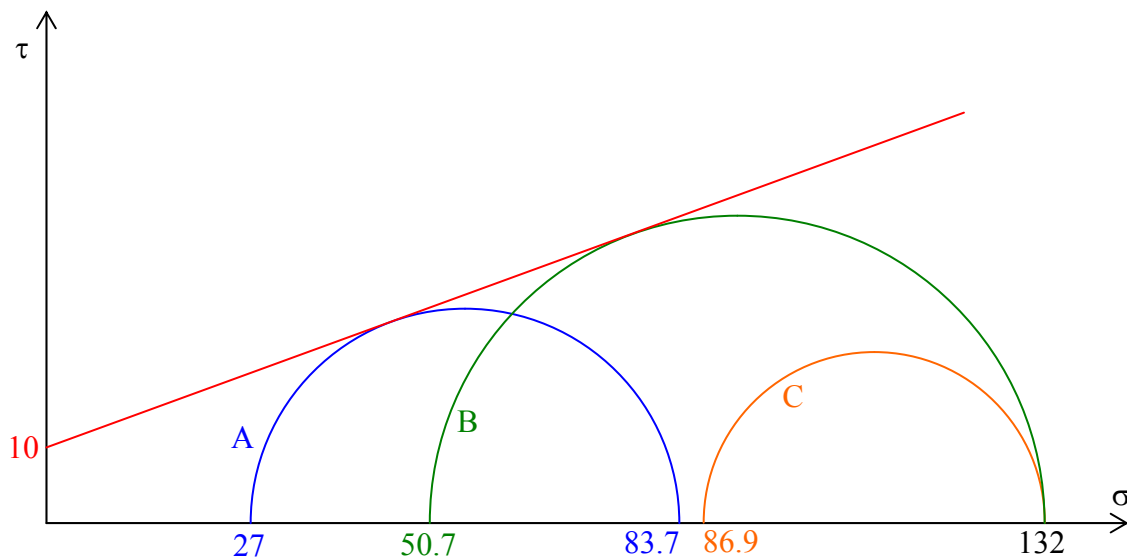
1. If the wall moves into the excavation, it moves towards A, and away from B. This means if the wall movement is large enough to yield the soil, A has passive failure and B has active failure. Point C is not affected by the excavation, therefore the soil there does not have lateral strain, indicating  $K_0$  condition.

$$K_a = \frac{1 - \sin \phi'}{1 + \sin \phi'} = \frac{1 - \sin 20^\circ}{1 + \sin 20^\circ} = 0.49 \quad K_p = 1/K_a = 2.04 \quad K_0 = (1 - \sin \phi') \sqrt{OCR} = 0.658$$

At point A;  $\sigma_v' = \sigma_v - u = (1 \times 17 + 1 \times 20) - 10 = 27 \text{ kPa}$   
 $\sigma_{hp}' = \sigma_v' \cdot K_p + 2c'\sqrt{K_p} = 27 \times 2.04 + 2 \times 10 \times \sqrt{2.04} = 55.1 + 28.6 = 83.7 \text{ kPa}$

At point B;  $\sigma_v' = \sigma_v - u = (20 + 6 \times 17 + 1 \times 20) - 10 = 132 \text{ kPa}$   
 $\sigma_{ha}' = \sigma_v' \cdot K_a - 2c'\sqrt{K_a} = 132 \times 0.49 - 2 \times 10 \times \sqrt{0.49} = 64.7 - 14 = 50.7 \text{ kPa}$

At point C;  $\sigma_v' = 132 \text{ kPa}$   
 $\sigma_h' = \sigma_v' \cdot K_0 = 132 \times 0.658 = 86.9 \text{ kPa}$  (assuming normally consolidated)



2. Tension crack occurs on the active (right) side. At the bottom of a tension crack horizontal (effective for drained analysis, total for undrained analysis) stress shall be zero.,

$$\sigma_{ha}' = \sigma_v' \cdot K_a - 2c'\sqrt{K_a}$$

$$0 = (20 + 17 \cdot z) \cdot 0.49 - 2 \times 10 \times \sqrt{0.49} = 9.8 + 8.33 z - 14 = 8.33 z - 4.2$$

$$\Rightarrow z = 4.2/8.33 = \underline{\underline{0.5 \text{ m}}}$$

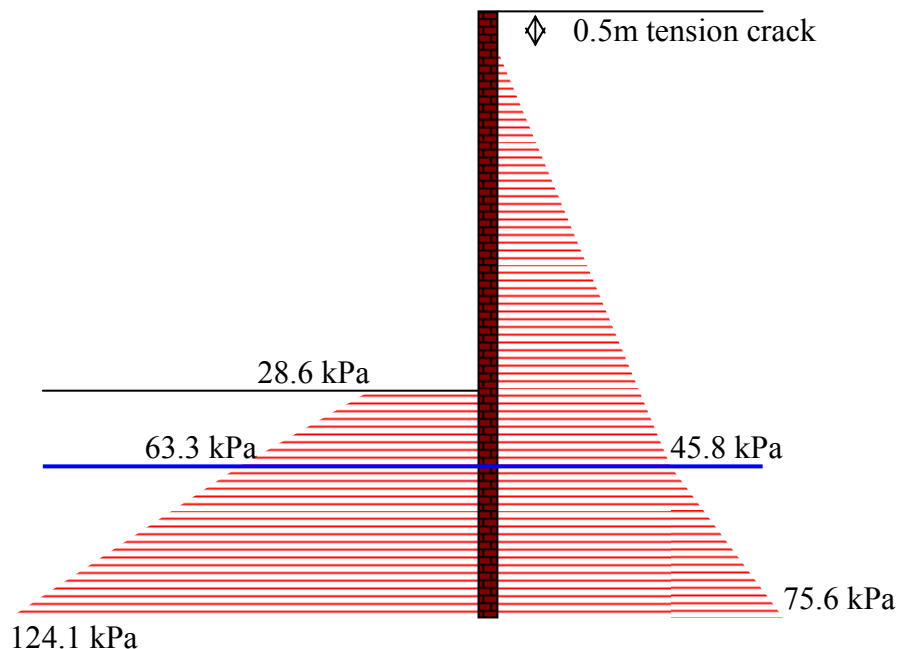
3. Active side: groundwater level:  $\sigma_v' = \sigma_v - u = (20 + 6 \times 17) - 0 = 122 \text{ kPa}$   
 $\sigma_{ha}' = \sigma_v' \cdot K_a - 2c'\sqrt{K_a} = 122 \times 0.49 - 2 \times 10 \times \sqrt{0.49} = 59.8 - 14 = 45.8 \text{ kPa}$   
 $\sigma_{ha} = \sigma_{ha}' + u = 45.8 + 0 = 45.8 \text{ kPa}$

tip of the wall:  $\sigma_v' = \sigma_v - u = (20 + 6 \times 17 + 2 \times 20) - 20 = 142 \text{ kPa}$   
 $\sigma_{ha}' = \sigma_v' \cdot K_a - 2c'\sqrt{K_a} = 142 \times 0.49 - 2 \times 10 \times \sqrt{0.49} = 69.6 - 14 = 55.6 \text{ kPa}$   
 $\sigma_{ha} = \sigma_{ha}' + u = 55.6 + 20 = 75.6 \text{ kPa}$

Passive side : ground surface :  $\sigma_v' = 0$   
 $\sigma_{hp}' = \sigma_v' \cdot K_p + 2c'\sqrt{K_p} = 0 \times 2.04 + 2 \times 10 \times \sqrt{2.04} = 28.6 \text{ kPa} = \sigma_{hp}$

groundwater level :  $\sigma_v' = \sigma_v - u = (1 \times 17) - 0 = 17 \text{ kPa}$   
 $\sigma_{hp}' = \sigma_v' \cdot K_p + 2c'\sqrt{K_p} = 17 \times 2.04 + 2 \times 10 \times \sqrt{2.04} = 34.7 + 28.6 = 63.3 \text{ kPa}$   
 $\sigma_{hp} = \sigma_{hp}' + u = 63.3 + 0 = 63.3 \text{ kPa}$

tip of the wall:  $\sigma_v' = \sigma_v - u = (1 \times 17 + 2 \times 20) - 20 = 37 \text{ kPa}$   
 $\sigma_{hp}' = \sigma_v' \cdot K_p + 2c'\sqrt{K_p} = 37 \times 2.04 + 2 \times 10 \times \sqrt{2.04} = 75.5 + 28.6 = 104.1 \text{ kPa}$   
 $\sigma_{hp} = \sigma_{hp}' + u = 104.1 + 20 = 124.1 \text{ kPa}$



4. Total Active Force =  $\frac{45.8 \times 5.5}{2} + 2 \cdot \frac{45.8 + 75.6}{2} = 247.35 \text{ kN/m}$

Total Passive Resistance =  $\frac{28.6 + 63.3}{2} + 2 \cdot \frac{63.3 + 124.1}{2} = 233.35 \text{ kN/m}$

required support force to stabilize the wall =  $247.35 - 233.35 = 14 \text{ kN/m}$   
 supports are every 4 m  $\Rightarrow$  each support carries  $4 \times 14 = \underline{56 \text{ kN}}$

5. No horizontal displacement means we want to have zero horizontal strain, which is the  $K_0$  condition. So if you make stresses on each side equal to  $K_0$  stresses, you will eliminate horizontal movement. (Note that the excavation side will be over-consolidated due to removal of soil, even though the soil was initially normally consolidated)