

HOMEWORK 4 – SOLUTION

- 1) At the mid-depth of N.C. Clay
(at 2.5 m below ground surface):

Before the fill is placed:

$$\sigma = 1 \times 19 + 1.5 \times 18 = 46 \text{ kPa}$$

$$u = 1.5 \times 10 = 15 \text{ kPa}$$

$$\sigma' = \sigma - u = 46 - 15 = 31 \text{ kPa}$$

Immediately after the fill is placed:

$$\sigma = 46 + 4 \times 17 = 114 \text{ kPa}$$

$$u = 1.5 \times 10 + 4 \times 17 = 83 \text{ kPa}$$

$$\sigma' = \sigma - u = 114 - 83 = 31 \text{ kPa}$$

OR

σ' remains the same (31 kPa)

$$u = 114 - 31 = 83 \text{ kPa}$$

After the clay is consolidated:

$$\sigma = 46 + 4 \times 17 = 114 \text{ kPa}$$

$$u = 15 \text{ kPa}$$

$$\sigma' = \sigma - u = 114 - 15 = 99 \text{ kPa}$$

- At the mid-depth of O.C. Clay
(at 8.5 m below ground surface):

Before the fill is placed:

$$\sigma = 1 \times 19 + 3 \times 18 + 2 \times 20 + 2.5 \times 19 = 160.5 \text{ kPa}$$

$$u = 7.5 \times 10 = 75 \text{ kPa}$$

$$\sigma' = \sigma - u = 160.5 - 75 = 85.5 \text{ kPa}$$

Immediately after the fill is placed:

$$\sigma = 160.5 + 4 \times 17 = 228.5 \text{ kPa}$$

$$u = 7.5 \times 10 + 4 \times 17 = 143 \text{ kPa}$$

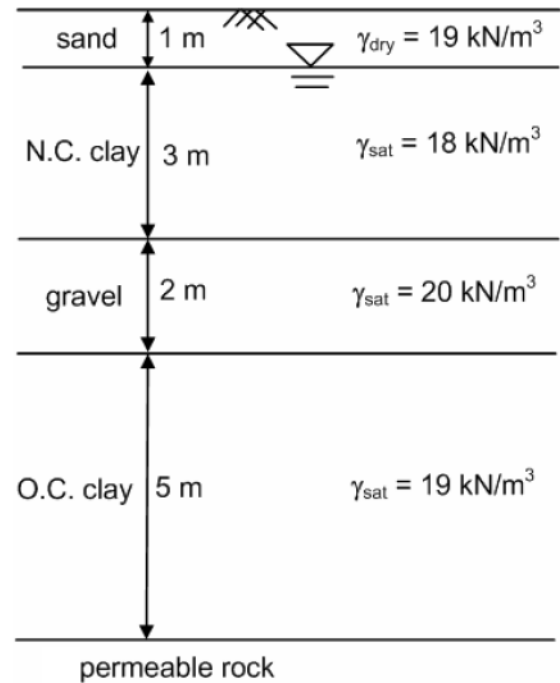
$$\sigma' = \sigma - u = 228.5 - 143 = 85.5 \text{ kPa}$$

After the clay is consolidated:

$$\sigma = 160.5 + 4 \times 17 = 228.5 \text{ kPa}$$

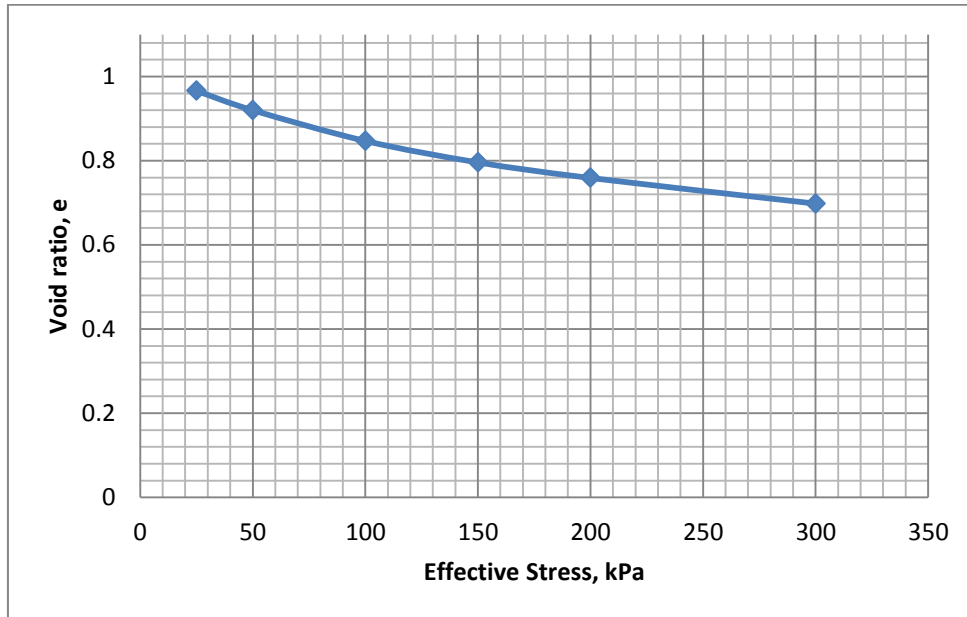
$$u = 75 \text{ kPa}$$

$$\sigma' = \sigma - u = 228.5 - 75 = 153.5 \text{ kPa}$$



- 2) From question 1, $\sigma_0' = 31$ kPa and $\sigma_f' = 99$ kPa. By linear interpolation, from the given data, void ratio values corresponding to effective stress values can be found:

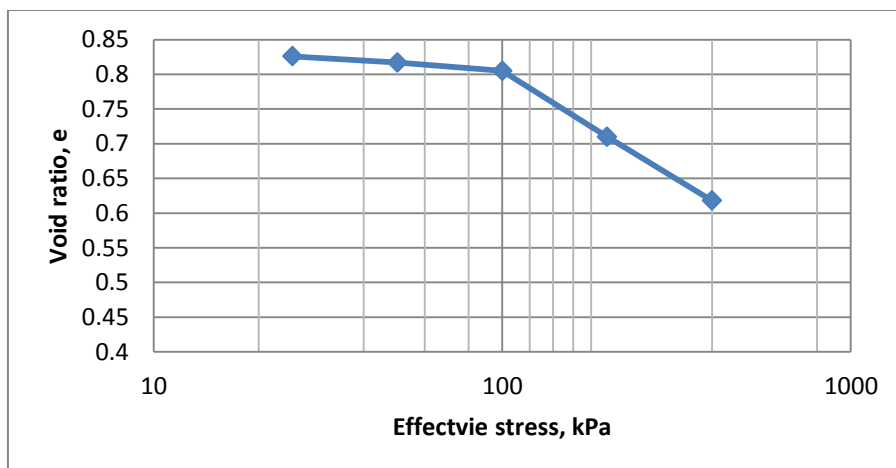
$$(e_0, \sigma_0') = (0.9549, 31) \text{ and } (e_f, \sigma_f') = (0.8485, 99)$$



Using these values, m_v can be calculated for the effective stress range of 31 to 115 kPa:

$$m_v = \frac{\Delta e}{\Delta \sigma'} \cdot \frac{1}{1 + e_0} = \frac{(0.9549 - 0.8485)}{(99 - 31)} \cdot \frac{1}{1 + 0.9549} = 8 \times 10^{-4} \text{ m}^2/\text{kN}$$

- 3) Plotting the given data:



From the plot, $\sigma_p' = 100$ kPa

Using two effective stress values, that are on the linear portion of the curve before the preconsolidation pressure, for example 25 and 50 kPa:

$$C_r = \frac{\Delta e}{\Delta \log \sigma'} = \frac{(0.826 - 0.817)}{\log 50 - \log 25} = 0.02989$$

Using two effective stress values, that are on the linear portion of the curve after the preconsolidation pressure, for example 200 and 400 kPa:

$$C_c = \frac{\Delta e}{\Delta \log \sigma'} = \frac{(0.710 - 0.618)}{\log 400 - \log 200} = 0.30562$$

$$\sigma_v' = 1 \times 19 + 3 \times 18 + 2 \times 20 - 5 \times 10 = 63 \text{ kPa}$$

$$\text{OCR} = \sigma_p' / \sigma_v' = 100/63 = 1.59$$

4) N.C. clay layer:

$$(e_0, \sigma_0') = (0.9549, 31) \text{ and } \sigma_1' = 99 \text{ kPa, } \Delta \sigma' = 4 \times 17 = 68 \text{ kPa}$$

$$S_{\text{N.C. clay}} = m_v \times H \times \Delta \sigma' = 8 \times 10^{-4} \times 3 \times 68 = 0.1632 \text{ m}$$

O.C. clay layer:

$\sigma_0' = 85.5$ kPa and $\sigma_1' = 153.5$ kPa. To find the initial void ratio at $\sigma_0' = 85.5$ kPa, we can use the lab data and linear interpolating between the void ratios corresponding to 50 and 100 kPa:

$$e_0 = 0.8085$$

Since the effective stress after consolidation is (153.5) kPa greater than the preconsolidation pressure (100 kPa), we should use the equation with C_r and C_c .

$$S = \frac{C_r}{1+e_0} \cdot H \cdot \log \left(\frac{\sigma_p'}{\sigma_0'} \right) + \frac{C_c}{1+e_0} \cdot H \cdot \log \left(\frac{\sigma_1'}{\sigma_p'} \right) = \frac{0.02989}{1+0.8085} \cdot 5 \cdot \log \left(\frac{100}{85.5} \right) + \frac{0.30562}{1+0.8085} \cdot 5 \cdot \log \left(\frac{153.5}{100} \right) = 0.1628 \text{ m}$$

(Note: it is just a coincidence that both N.C. and O.C. clays gave very similar settlement values.)

5) 7 months after the end of a 2-month construction period is same as $7+2/2 = 8$ months after instantaneous loading.

Calculating the average degree of consolidation of each clay layer at 8 months:

At 8 months, N.C. clay:

$$T_v = \frac{c_v \times t}{d^2} = \frac{1.8 \times (8/12)}{(1.5)^2} = 0.533 \quad \Rightarrow \quad \text{lower graph} \quad \Rightarrow \quad U_{av} = 78 \%$$

$$S_{8\text{months}} = S_{\text{final}} \times U_{\text{av}} = 0.78 \times 0.1632 = 0.127 \text{ m}$$

At 8 months, O.C. clay:

$$T_v = \frac{c_v \times t}{H_d^2} = \frac{1.2 \times (8/12)}{(2.5)^2} = 0.128 \quad \Rightarrow \quad \text{lower graph} \quad \Rightarrow \quad U_{\text{av}} = 40 \%$$

$$S_{8\text{months}} = S_{\text{final}} \times U_{\text{av}} = 0.40 \times 0.1628 = 0.0652 \text{ m}$$

Ground surface settlement at 8 months:

$$0.127 + 0.0652 = 0.16 \text{ m}$$

$$6) \quad S_t = S_{\text{final}} \times U_{\text{av}} \quad \Rightarrow \quad 0.05\text{m} = 0.1628 \times U_{\text{av}} \quad \Rightarrow \quad U_{\text{av}} = 30.7\%.$$

From lower graph, $T_v = 0.07$

$$T_v = \frac{c_v \times t}{d^2} \quad 0.07 = \frac{(1.8) \times (t)}{(1.5)^2} \quad t = 0.0875 \text{ years} \approx t_c/2 = 1 \text{ month}$$

Note that the time calculated here is from the middle of the construction period, placing the answer to the end of construction period.

- 7) For O.C. clay layer at 1 year after the end of construction ($12+2/2 = 13$ months after an equivalent instantaneous loading):

$$T_v = \frac{c_v \times t}{H_d^2} = \frac{1.2 \times (13/12)}{2.5^2} = 0.208$$

Using the upper graph, for $T_v = 0.208$ and $z/H_d = 4 \text{ m} / 2.5 \text{ m} = 1.6$, the degree of consolidation at that point at that time is about $U_z = 0.57$.

\Rightarrow 57% of $\Delta\sigma$ has been transferred to σ' \Rightarrow 43% of $\Delta\sigma$ is still on u

$$\Rightarrow u = u_o + \Delta u = 9 \times 10 + 0.43 \times 68 = 90 + 29.24 = 119.24 \text{ kPa}$$