

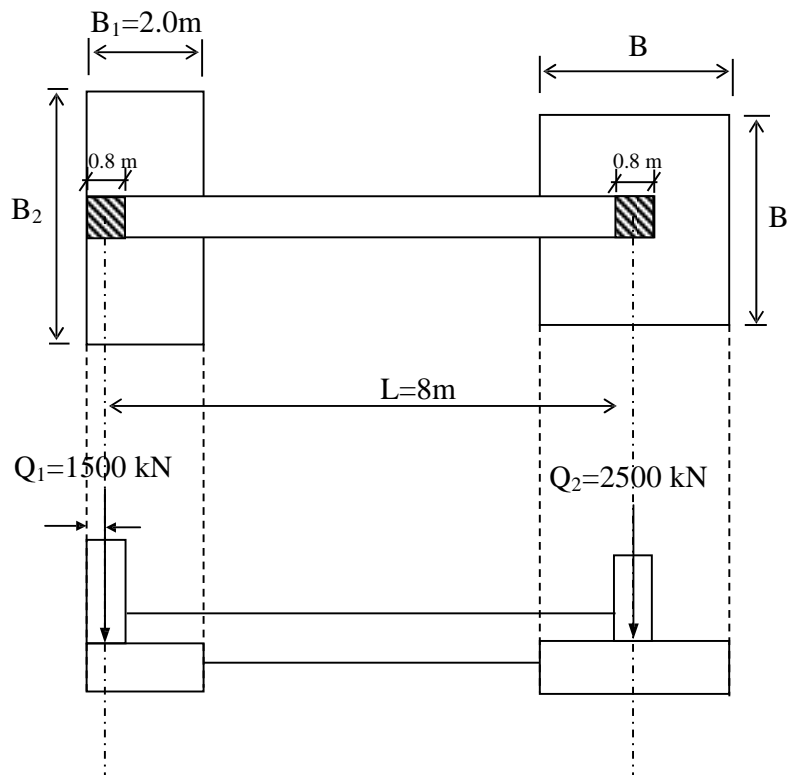
CE 366 – SHALLOW FOUNDATIONS

P.1) CANTILEVER FOOTING

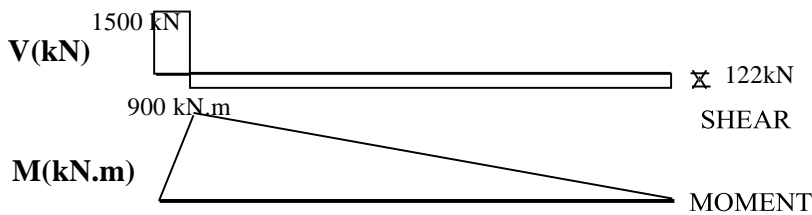
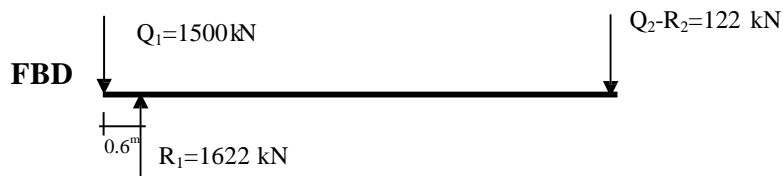
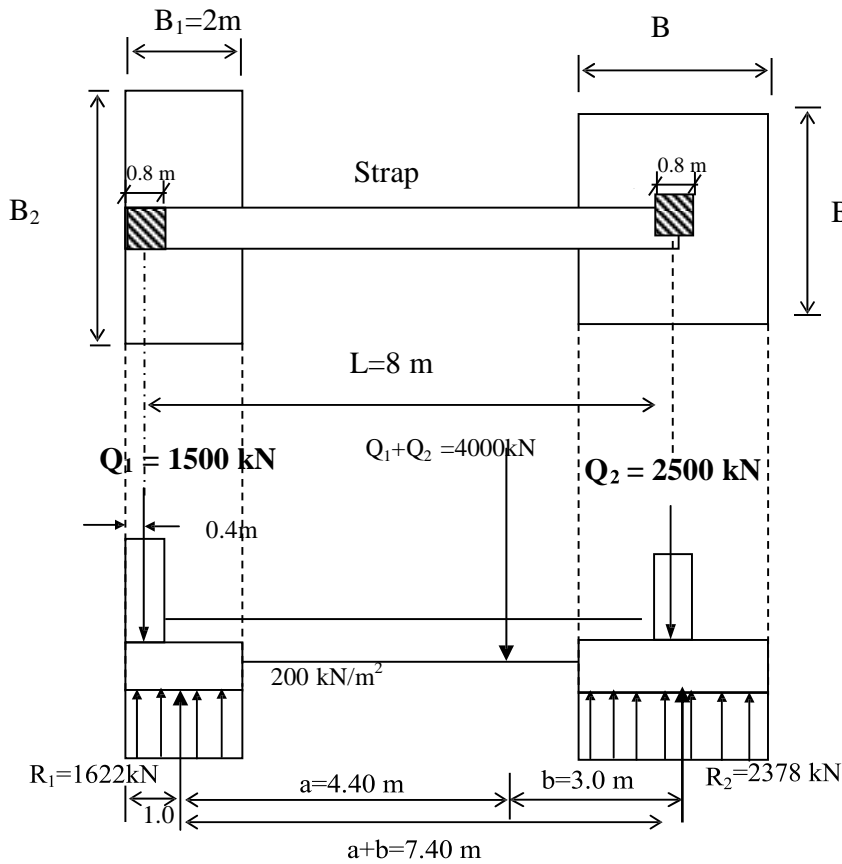
Question:

Given: $Q_1 = 1500 \text{ kN}$, $Q_2 = 2500 \text{ kN}$, $q_{\text{all}} = 200 \text{ kN/m}^2$

Ignore the weight of footings and find dimensions B and B_2 of a cantilever footing for a uniform soil pressure distribution. Draw shear and bending moment distributions.



Solution:



Locate $\Sigma Q = Q_1 + Q_2$

$$b = 1500 \times 8 / 4000 = 3$$

For $B_1 = 2\text{m}$

$$a = 8.0 + 0.4 - 1.0 - 3.0$$

$$\rightarrow a = 4.40\text{m}$$

$$R_1 = (4000 \times 3) / 7.4 = 1622\text{kN}$$

$$R_2 = 4000 - 1622 = 2378\text{ kN}$$

Determine B_2 ,

$$q_{\text{all}} = Q / (2 \times B_2)$$

$$200 = 1620 / (2 \times B_2) \rightarrow B_2 = 4\text{ m}$$

OR

Without considering resultant ($Q_1 + Q_2$)

Moment w.r.t Q_2 or (R_2);

$$Q_1 \times 8 - R_1 \times 7.4 = 0 \rightarrow R_1 = 1622\text{ kN}$$

From force equilibrium;

$$\Sigma F_{\text{vertical}} = 0$$

$$1500 + 2500 - 1622 - R_2 = 0$$

$$\rightarrow R_2 = 2378\text{ kN}$$

Determine B_2 ,

$$q_{\text{all}} = Q / (2 \times B_2)$$

$$200 = 1622 / (2 \times B_2) \rightarrow B_2 \approx 4\text{ m}$$

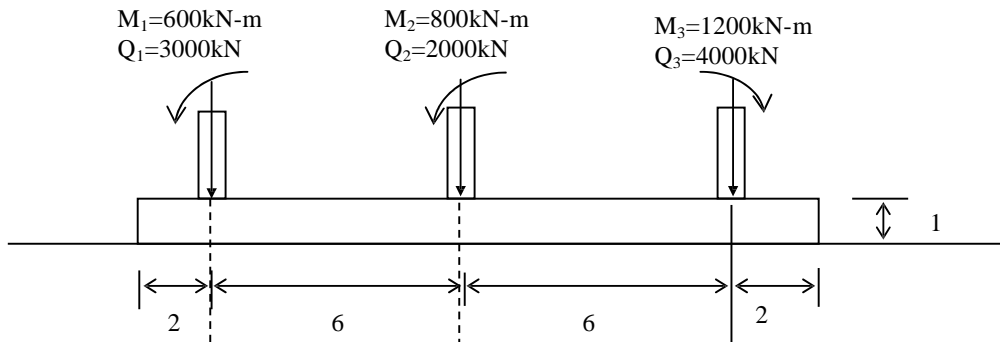
Similarly,

$$200 = 2378 / B^2 \rightarrow B \approx 3.45\text{ m}$$

P.2) TRAPEZOIDAL FOOTING

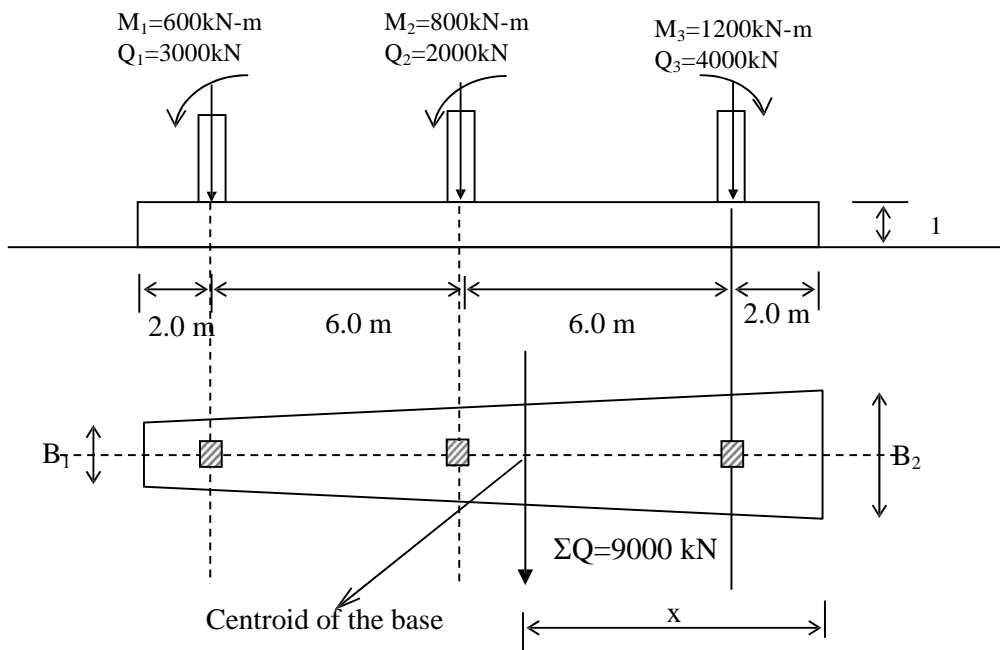
Question:

Determine B_1 and B_2 of a trapezoidal footing for a uniform soil pressure of 300 kN/m^2 . ($\gamma_{\text{conc}} = 24 \text{ kN/m}^3$)



Solution:

After finding the location of resultant force, you can decide whether the wider side of the trapezoid will be at the left or right side.



General formulation for finding coordinates of a centroid;

$$\bar{x} = \frac{\bar{x}_1 A_1 + \bar{x}_2 A_2}{A_1 + A_2} \quad \bar{y} = \frac{\bar{y}_1 A_1 + \bar{y}_2 A_2}{A_1 + A_2}$$

$$\Sigma Q = 9000 \text{ kN}$$

$$\text{Weight of footing} = 16 \times 24 \times (B_1 + B_2) / 2 = 192(B_1 + B_2)$$

$$\text{Area of footing} = 8(B_1 + B_2)$$

$$\underline{\Sigma F_y = 0} \quad 9000 + 192(B_1 + B_2) = 8(B_1 + B_2) \times 300$$

$$B_1 + B_2 = 4.07 \text{ m} \dots\dots\dots(1)$$

$$\underline{\Sigma M = 0} \text{ (moment about centroid of the base)}$$

$$3000(14-x) + 600 + 2000(8-x) + 800 - 4000(x-2) - 1200 + (\text{wght of ftg})x = (\text{base pressure})x$$

$$x = 7.36 \text{ m}$$

$$x = 7.36 = \frac{1}{3} \times 16 \times \frac{2B_1 + B_2}{B_1 + B_2} \quad B_2 = 1.63B_1 \dots\dots\dots(2)$$

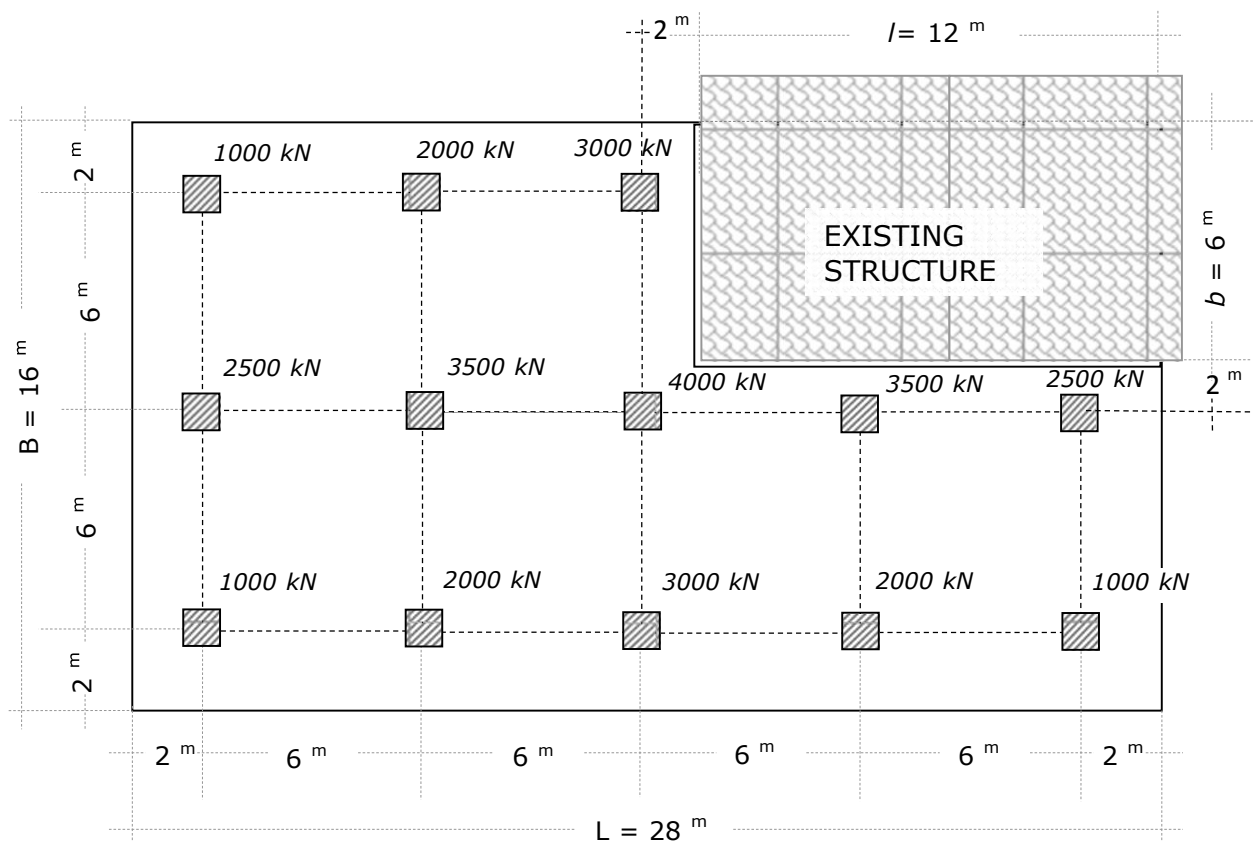
$$\text{From (1) and (2) } B_1 = 1.55 \text{ m ; } B_2 = 2.52 \text{ m}$$

Note: You can also take moment about the left or right side but keep in mind that weight and base pressure will also have moment about left or right side.

P.3) MAT FOUNDATION

Question:

A mat foundation rests on a sand deposit whose allowable bearing value is 150 kN/m^2 . Column loads are given in the figure. The thickness of the mat is 2.0 m ($\gamma_{\text{concrete}} = 24 \text{ kN/m}^3$). Calculate base pressures assuming that the lines passing through the centroid of the mat and parallel to the sides are principal axes. Find the base pressure distribution beneath the base and check whether the mat foundation given is safe?



Solution:

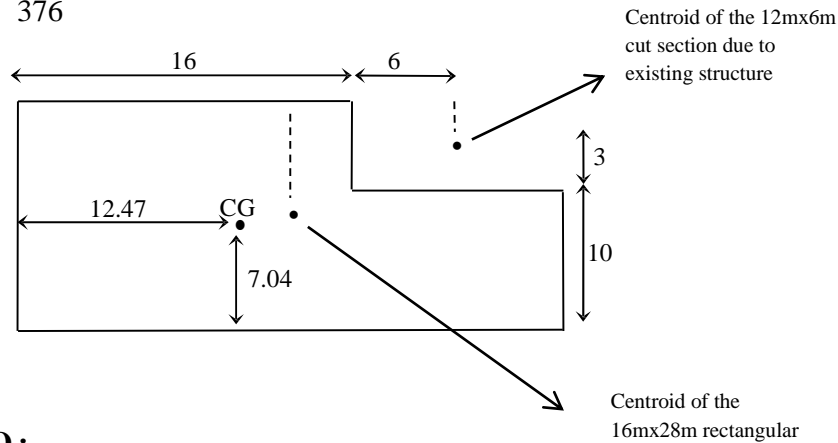
$$\text{Area of foundation} = 28 \times 16 - 12 \times 6 = 376 \text{ m}^2$$

$$\text{Total vertical load} = \Sigma V = \text{Column loads} + \text{Weight of mat} = 31000 + (376) \times 24 \times 2 = 49048 \text{ kN}$$

* **Center of gravity (CG) of mat:**

$$\frac{28 \times 16 \times 14 - 6 \times 12 \times (16 + 6)}{376} = 12.47 \text{ m from left}$$

$$\frac{28 \times 16 \times 8 - 6 \times 12 \times (3 + 10)}{376} = 7.04 \text{ m from bottom}$$



* **Location of ΣO :**

→ Take moment about the left side:

$$\begin{aligned} &= (1 / 49048) \cdot [2 \times (1000 + 2500 + 1000) + 8 \times (2000 + 3500 + 2000) + 14 \times (3000 + \\ &\quad + 4000 + 3000) + 20 \times (3500 + 2000) + 26 \times (2500 + 1000) + 376 \times 2 \times 24 \times 12.47] \\ &= 12.95 \text{ m from left} \end{aligned}$$

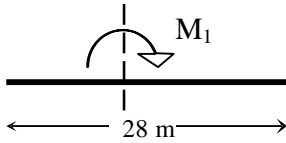
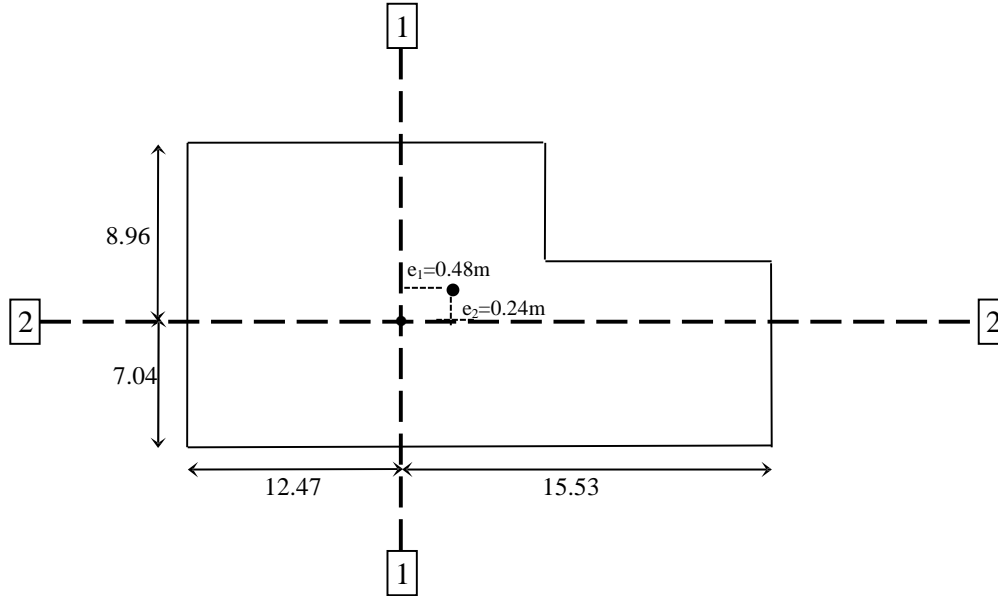
→ Take moment about bottom side :

$$\begin{aligned} &= (1 / 49048) \cdot [2 \times (1000 + 2000 + 3000 + 2000 + 1000) + 8 \times (2500 + 3500 + 4000 + \\ &\quad + 3500 + 2500) + 14 \times (1000 + 2000 + 3000) + 376 \times 2 \times 24 \times 7.04] \\ &= 7.28 \text{ m from bottom} \end{aligned}$$

Eccentricity :

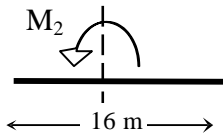
$$e_1 = 12.95 - 12.47 = 0.48 \text{ m}$$

$$e_2 = 7.28 - 7.04 = 0.24 \text{ m}$$



M_1 about 1-1 axis:

$$M_1 = \Sigma Q \cdot e_1 = 49048 \cdot (0.48) = 23543 \text{ kN.m}$$



M_2 about 2-2 axis:

$$M_2 = \Sigma Q \cdot e_2 = 49048 \cdot (0.24) = 11772 \text{ kN.m}$$

$$I_{1-1} = \left[\frac{B \cdot L^3}{12} + B \cdot L \cdot (D_1)^2 \right] - \left[\frac{b \cdot l^3}{12} + b \cdot l \cdot (d_1)^2 \right] =$$

$$= \left[\frac{16 \times 28^3}{12} + 16 \times 28 \times (14 - 12.47)^2 \right] - \left[\frac{6 \times 12^3}{12} + 6 \times 12 \times (22 - 12.47)^2 \right] = 22915 \text{ m}^4$$

$$I_{2-2} = \left[\frac{L \cdot B^3}{12} + B \cdot L \cdot (D_2)^2 \right] - \left[\frac{l \cdot b^3}{12} + b \cdot l \cdot (d_2)^2 \right] =$$

$$= \left[\frac{28 \times 16^3}{12} + 16 \times 28 \times (8 - 7.04)^2 \right] - \left[\frac{12 \times 6^3}{12} + 12 \times 6 \times (13 - 7.04)^2 \right] = 7197 \text{ m}^4$$

Note: In soil mechanics compression is taken as positive (+)

$$q = \frac{\Sigma Q}{Area} \pm \frac{M_1 \cdot y_1}{I_{1-1}} \pm \frac{M_2 \cdot y_2}{I_{2-2}}$$

$$q = \frac{49048}{376} \pm \frac{23543 \cdot y_1}{22915} \pm \frac{11772 \cdot y_2}{7197} = 130.4 \pm 1.03y_1 \pm 1.64y_2$$

$$q_A = 130.4 \pm 1.03y_1 \pm 1.64y_2 = 130.4 + 1.03 \cdot (3.53) + 1.64 \cdot (2.96) = 138.9 \quad \text{kN/m}^2$$

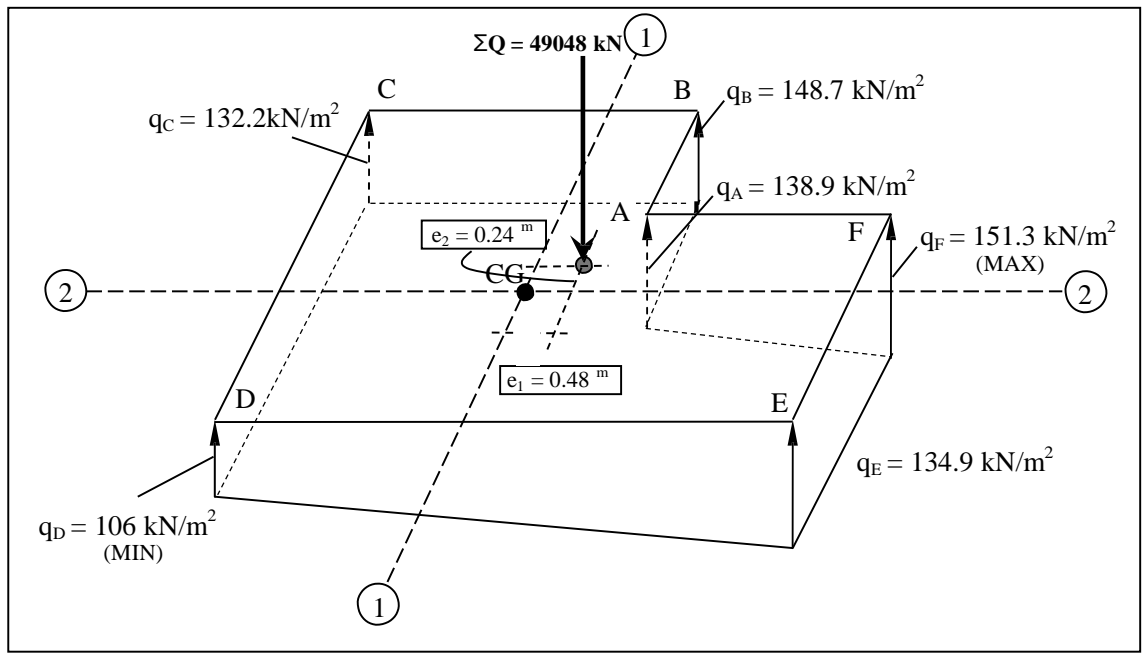
$$q_B = 130.4 + 1.03 \cdot (3.53) + 1.64 \cdot (8.96) = 148.7 \quad \text{kN/m}^2$$

$$q_C = 130.4 - 1.03 \cdot (12.47) + 1.64 \cdot (8.96) = 132.2 \quad \text{kN/m}^2$$

$$q_D = 130.4 - 1.03 \cdot (12.47) - 1.64 \cdot (7.04) = 106 \quad \text{kN/m}^2$$

$$q_E = 134.9 \text{ kN/m}^2$$

$$q_F = 151.3 \text{ kN/m}^2$$

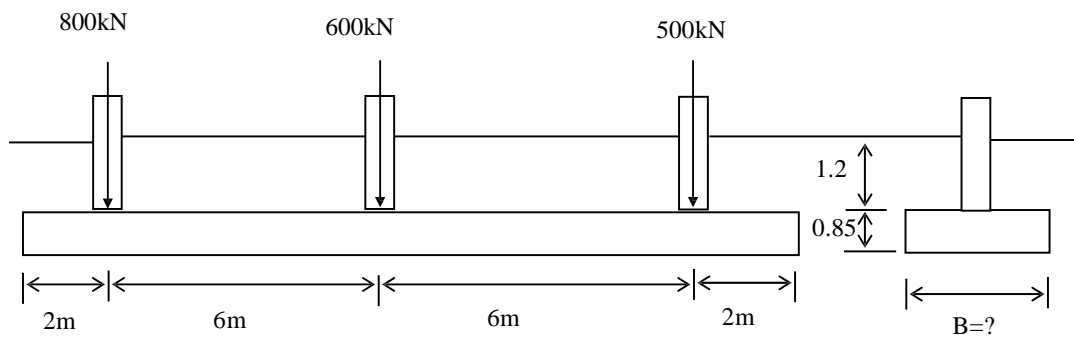


Since at all critical points stress values are almost $\approx < q_{all} = 150 \text{ kN/m}^2$ given mat foundation is safe.

P.4) COMBINED FOOTING ANALYZED BY RIGID METHOD

Question:

A rectangular combined footing which supports three columns is to be constructed on a sandy clay layer whose allowable bearing value (base pressure) is 84 kN/m^2 . The thickness of the concrete footing is 0.85m. There is a 1.20m thick soil fill having same unit weight with sandy clay on the footing. Unit weight of the sandy clay and the concrete are 20 kN/m^3 and 24 kN/m^3 respectively. Analyze the footing by rigid method and plot shear and moment diagrams.



Solution:

Neglecting column weights;

$$\Sigma Q_{\text{net}} = 800 + 600 + 500 + (24 - 20) \times 16 \times B \times 0.85 = 1900 + 54.4B$$

$$e = \frac{\Sigma M}{\Sigma V} = \frac{800 \times 6 - 500 \times 6}{1900 + 54.4B} = \frac{1800}{1900 + 54.4B}$$

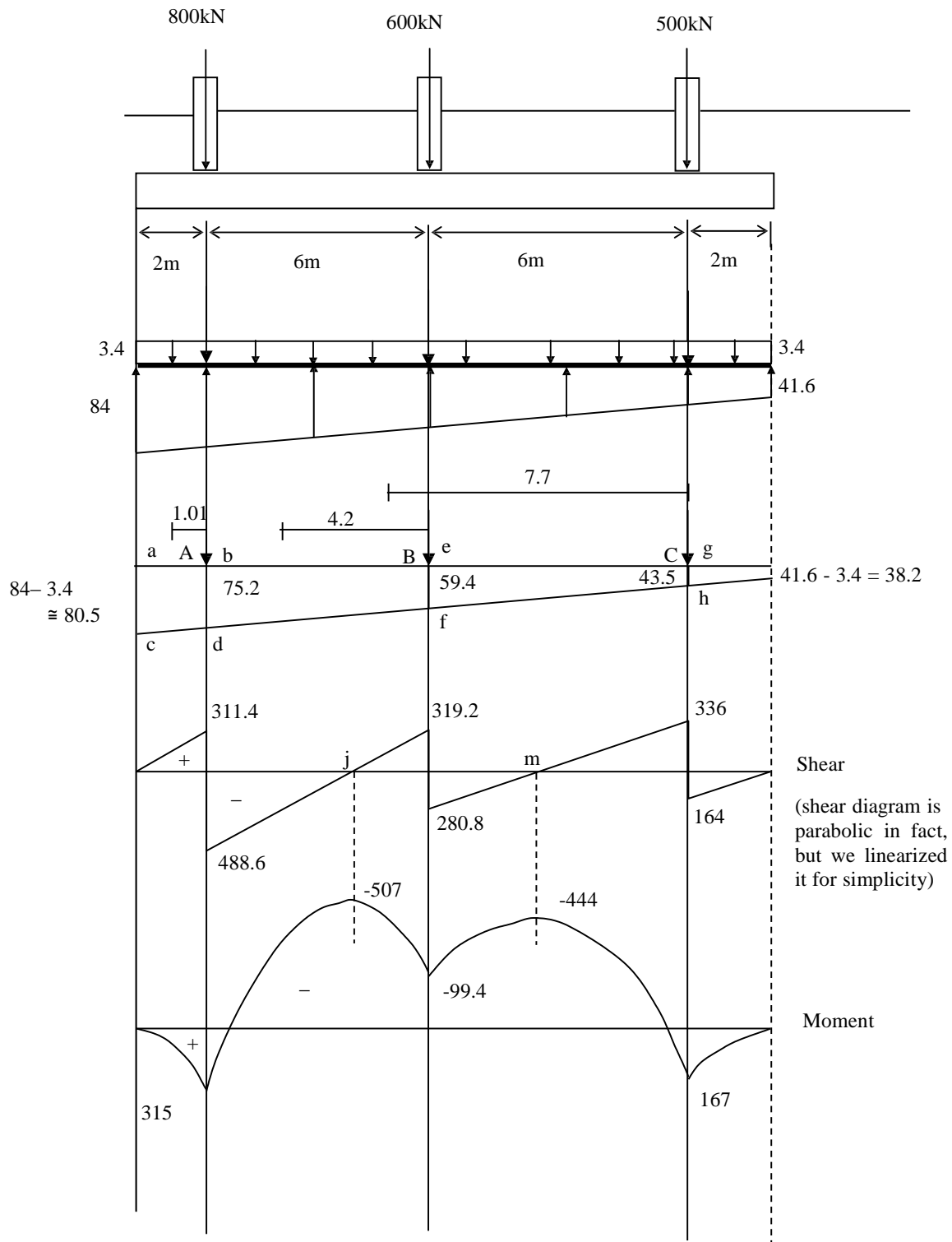
$$q_{\text{max}} = \frac{\Sigma V}{B \times L} \left(1 + \frac{6e}{L} \right) = 84 \text{ kN/m}^2$$

$$84 = \frac{1900 + 54.4B}{B \times 16} \left(1 + \frac{6 \times 1800}{(1900 + 54.4B) \times 16} \right) \Rightarrow B = 2.0 \text{ m}$$

$$\text{Use } B = 2.0 \text{ m} \quad q_{\text{max}} = 84 \text{ kN/m}^2 ; q_{\text{min}} = 41.6 \text{ kN/m}^2$$

$$\text{Downward uniform pressure} = 0.85 \times (24 - 20) = 3.4 \text{ kN/m}^2$$

These are the diagrams related to forces and moments acting on the foundation. Explanations are at the next page;

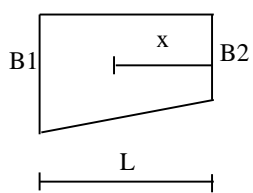


$$V_A = \frac{80.5 + 75.2}{2} \times 2 \times 2 = 311.4 \text{ kN}$$

area (abcd)
B = 2

$$V_{A'} = 311.4 - 800 = -488.6 \text{ kN}$$

To find the centroid of a trapezoid on the horizontal axis;



$$x = \frac{L}{3} \frac{2B_1 + B_2}{B_1 + B_2}$$

x: distance from shorter dimension

$$x(\text{abcd}) = \frac{2}{3} \frac{2 \times 80.5 + 75.2}{80.5 + 75.2} = 1.01 \text{ m}$$

$$M_A = 311.4 \times 1.01 = 315 \text{ kN.m}$$

$$V_{BA} = \frac{80.5 + 59.4}{2} \times 8 \times 2 - 800 = 319.2 \text{ kN}$$

$$V_{BC} = 319.2 - 600 = -280.8 \text{ kN}$$

$$x(\text{aefc}) = \frac{8}{3} \frac{2 \times 80.5 + 59.4}{80.5 + 59.4} = 4.2 \text{ m}$$

$$M_B = \left[\frac{80.5 + 59.4}{2} \times 8 \times 2 \right] \times 4.2 - 800 \times 6 = -99.4 \text{ kN.m}$$

$$V_{CB} = \frac{80.5 + 43.5}{2} \times 14 \times 2 - 800 - 600 = 336 \text{ kN}$$

$$V_C = 336 - 500 = -164 \text{ kN}$$

Check the end point; $\frac{80.5 + 38.2}{2} \times 16 \times 2 - 800 - 600 - 500 = 0 \longrightarrow \text{OK}$

$$x \text{ (aghc)} = \frac{14}{3} \frac{2 \times 80.5 + 43.5}{80.5 + 43.5} = 7.7 \text{ m}$$

$$M_C = \left[\frac{80.5 + 43.5}{2} \times 14 \times 2 \right] \times 7.7 - 800 \times 12 - 600 \times 6 = 167 \text{ kN.m}$$

Slope of V b/w $x = 2$ and $x = 8 \text{ m}$ $\Delta (488.6 + 319.2)/6 = 134.6 \text{ kN/m}$

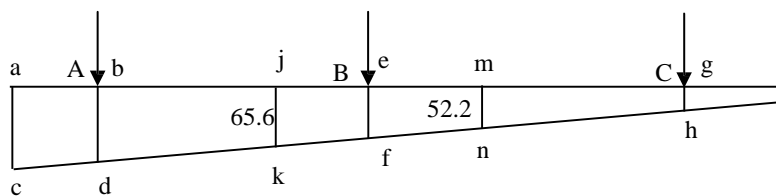
Equation of V b/w $x = 2$ and $x = 8 \text{ m}$ $\Delta V(x) = -488.6 + 134.6 (x)$ for $V(x)=0 \Delta x=3.6 \text{ m}$

Base pressure @ $x = 2 + 3.6 = 5.6 \text{ m}$ $\Delta 65.6 \text{ kN/m}^2$

Similarly @ $x = 10.7 \text{ m}$ $V = 0$

Base pressure @ $x = 10.7 \text{ m}$ $\Delta 52.2 \text{ kN/m}^2$

maximum points of the moment diagram;



j and m are the points where shear forces are equal to zero (i.e. moment is max)

the distance between point b and point j

$$x \text{ (ajkc)} = \frac{(2 + 3.6)}{3} \frac{2 \times 80.5 + 65.6}{80.5 + 65.6} = 2.9 \text{ m}$$

$$M_{AB} = \left[\frac{80.5 + 65.6}{2} \times (2 + 3.6) \times 2 \right] \times 2.9 - 800 \times 3.6 = -507 \text{ kN.m}$$

$x \text{ (amnc)} = 5.73 \text{ m}$

$M_{BC} = -444 \text{ kN.m}$