

$$1) f_c = 50 \text{ MPa}$$

$$E_c = 12680 + 460 \cdot (50) = \underline{35680 \text{ MPa}}$$

$$\epsilon_{co} = 2.50 / 35680 = \underline{2.8 \cdot 10^{-3}}$$

$$\text{for } \sigma_c = 40 \text{ MPa}$$

$$\sigma_c = f_c \left[\frac{2\epsilon_c}{\epsilon_{co}} - \left(\frac{\epsilon_c}{\epsilon_{co}} \right)^2 \right] \quad 40 = 50 \left[\frac{2\epsilon_c}{2.8 \cdot 10^{-3}} - \frac{\epsilon_c^2}{7.86 \cdot 10^{-6}} \right]$$

$$\Rightarrow \epsilon_c^2 - 5.6 \cdot 10^{-3} \epsilon_c + 6.272 \cdot 10^{-6} = 0$$

2 Solutions:

$$\left. \begin{array}{l} \epsilon_c = 4.05 \cdot 10^{-3} \\ \underline{\epsilon_c = 1.55 \cdot 10^{-3}} \end{array} \right\} \text{ We choose the smaller one due to } \underline{\sigma_c < f_c}$$

for 40 MPa to 15 MPa

$$\sigma = E \cdot \epsilon \quad (\text{Hooke's Law})$$

$$(40 - 15) = E \cdot (35680) \quad \epsilon_r = 7.00 \cdot 10^{-4}$$

$$\epsilon = \epsilon_c - \epsilon_r = \underline{8.49 \cdot 10^{-4}}$$

2) for 45 MPa:

$$45 = 50 \left[\frac{2 \epsilon_c}{\epsilon_{co}} - \left(\frac{\epsilon_c}{\epsilon_{co}} \right)^2 \right]$$

$$\epsilon_c^2 - 5.6 \cdot 10^{-3} \epsilon_c + 7.056 \cdot 10^{-6} = 0$$

2 solutions:

$$\left. \begin{array}{l} \epsilon_c = 1.91 \cdot 10^{-3} \\ \epsilon_c = 3.68 \cdot 10^{-3} \end{array} \right\} \begin{array}{l} \text{We choose the smaller } \epsilon \text{ due to the strain should be} \\ \text{lower than } 2.8 \cdot 10^{-3} \text{ (} \underline{\epsilon < \epsilon_{co}} \text{)} \end{array}$$

3) Concrete should relax on an elastic curve so that:

$$\sigma = E \cdot \epsilon_r$$

$$(45 - 0) = 35690 \cdot \epsilon$$

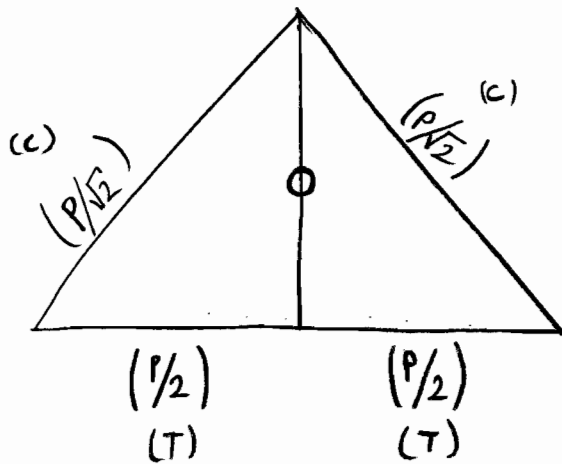
$$\underline{\underline{\epsilon_r = 1.26 \cdot 10^{-3}}}$$

Remaining ϵ will be;

$$\epsilon = \epsilon_c - \epsilon_r$$

$$\underline{\underline{\epsilon = 6.5 \cdot 10^{-4}}}$$

1,2) a)



$$A_c = 150^2 = 22500 \text{ mm}^2$$

$$f_c = 20 \text{ MPa}$$

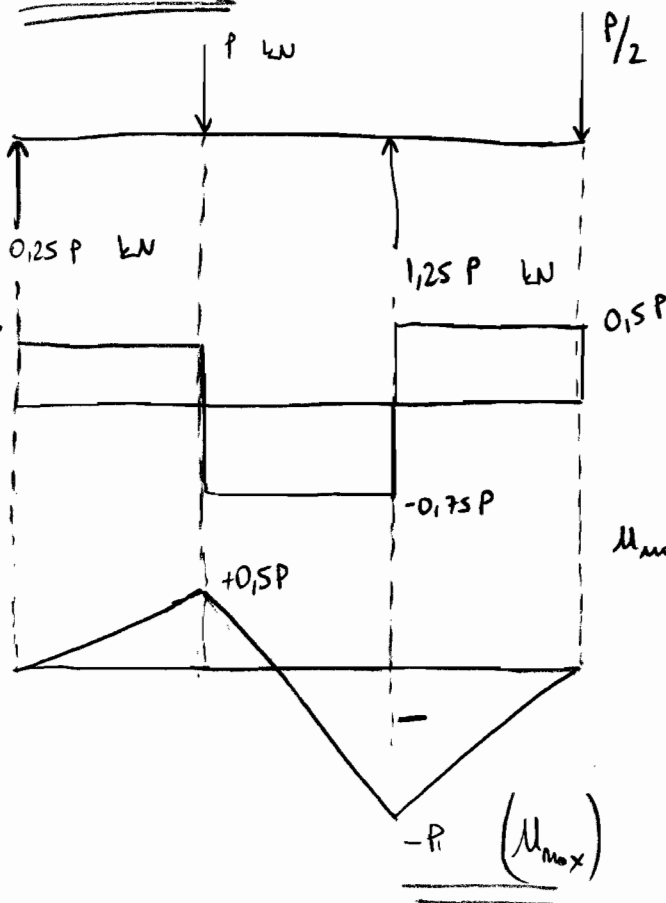
$$f_{CT} = 0,35 \cdot \sqrt{f_c} = \underline{\underline{1,6 \text{ MPa}}}$$

$$\frac{P/\sqrt{2}}{22500} \leq 20 \text{ MPa} \Rightarrow P \leq 636 \text{ kN (in Compression)}$$

$$\frac{(P/2)}{22500} \leq 1,6 \text{ MPa} \Rightarrow P \leq 72 \text{ kN (in Tension)}$$

$$P_{\max} = 72 \text{ kN}$$

b)



$$f_{CTF} \approx 0,7 \sqrt{f_c} = 3,1 \text{ MPa}$$

$$\sigma_{\max} = \frac{M_{\max} c}{I}$$

$$c = 200 \text{ mm}$$

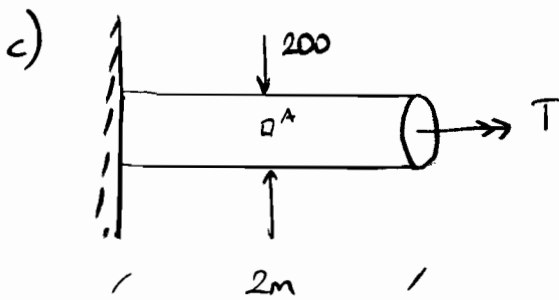
$$I = 200 \cdot (400)^3 / 12 = 1,07 \cdot 10^9 \text{ mm}^4$$

$$M_{\max} = (3,1) \cdot (1,07 \cdot 10^9) / 200$$

$$= 16,54 \text{ kN} \cdot \text{m}$$

$$M_{\max} = P = \underline{\underline{16,54 \text{ kN}}}$$

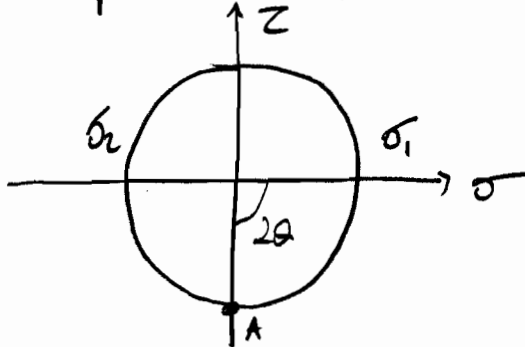
(C)



$$\tau_{max} = \frac{Tc}{J} = \frac{(P \cdot 10^6 \text{ N/mm}) (100)}{(\pi/2 \cdot 100^4 \text{ mm}^4)}$$

$$= (0,637 P \text{ MPa})$$

Principal Stresses:



At A $\sigma_x = 0$ $\tau_{xy} = -0,637 P$

$\sigma_y = 0$

$\sigma_2 = -0,637 P$

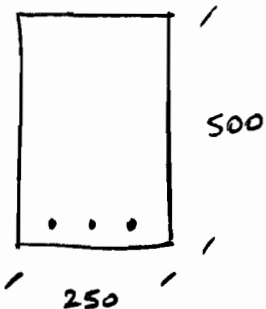
$\sigma_1 = 0,637 P$

$f_{ct5} = 0,5 \sqrt{f_c} = \underline{2,2 \text{ MPa}}$

$\sigma_1 = 0,637 P = 2,2 \Rightarrow \underline{\underline{P_{max} = 3,45 \text{ kN}}}$

14) Concrete will crack due to the excessive shear stress, so that it must be checked.

$$\tau = \frac{VA}{It}$$



$t = 250 \text{ mm}$

$V_{max} = P/2$

$A = 250 \cdot 250 \cdot 125$

$= 7812500 \text{ mm}^3$

$I = \frac{1}{12} b h^3 = \frac{1}{12} \cdot 250 \cdot 500^3$

$= 2604166667 \text{ mm}^4$

$\tau = P \cdot 6 \cdot 10^{-6} \text{ N/mm}^2$

for max; $\theta = 45^\circ$

$f_{ctf} = \sqrt{f_c} \cdot 0,7 = 3,13 \text{ MPa}$

$3,13 = 6 \cdot 10^{-6} \cdot P$

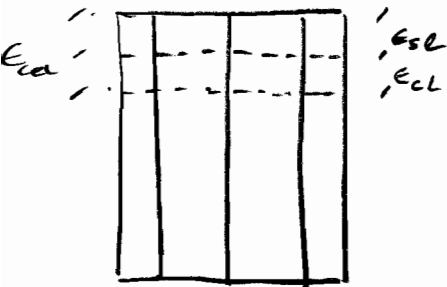
$\underline{\underline{P = 521,7 \text{ kN}}} \quad \theta = 45^\circ$

Tension crack
angle

(1)

$$1.6) \quad \epsilon_{ce} = \frac{\sigma_{co}}{E_c} \phi_{ce} = \frac{8}{20.000} (2) = 8 \cdot 10^{-4} "$$

Stresses in steel and concrete due to creep (only)



① Equilibrium, $F_s - F_c = 0$

$$\sigma_s A_s - \sigma_c A_c = 0$$

$$E_s E_s A_s - E_c E_c A_c = 0$$

$$E_s (200.000) (8.531) - E_c (20.000) (400^2 - 8.531) = 0$$

$$\underline{\underline{E_s = 3.76 E_c}}$$

② Displacement Compatibility

$$\epsilon_{sl} + \epsilon_{cl} = \epsilon_{cel}$$

$$E_s + E_c = 0.0008 \rightarrow E_s = 6.32 \cdot 10^{-4}$$

$$E_c = 1.68 \cdot 10^{-4}$$

$$\sigma_s = E_s \epsilon_s = 126.35 \text{ MPa (in Compression)}$$

$$\sigma_c = E_c \epsilon_c = 3.36 \text{ MPa (in Tension)}$$

Superposition of Creep Effect:

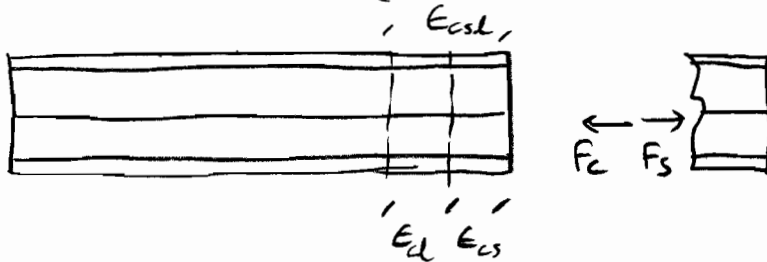
$$\sigma_c = 8 - 3.36 = 4.64 \text{ MPa Comp}$$

$$\sigma_s = 120 + 126.35 = 246.35 \text{ MPa Comp}$$

$$1.7) \quad l_e = \frac{2 A_c}{u} = \frac{2(250)(700)}{2(250)(700)} = 184 \text{ mm.}$$

from (Table 1.3) pg. 48: Assuming Dry Climate;

$$\epsilon_{cs} = 0.00059 \quad (\text{Interpolated Result})$$



① Equilibrium;

$$-F_c + F_s = 0$$

$$\Rightarrow -E_c E_c A_c + E_s E_s A_s = 0 \quad \xrightarrow{A_c} \quad \xrightarrow{E_s}$$

$$\Rightarrow +E_c (28,500) \cdot (250 \cdot 700 - 10 \cdot 201) = E_s \cdot (200,000) \cdot (10 \cdot 201)$$

\swarrow from the book

$$E_c (4.93 \cdot 10^9) = E_s (4.02 \cdot 10^9)$$

$$\Rightarrow \underline{E_c (1226) = E_s}$$

② Disp. Comp

$$\epsilon_{cl} + \epsilon_{sl} = 0.00059$$

$$\epsilon_{cl} = 4.45 \cdot 10^{-5}$$

$$\epsilon_{sl} = 5.45 \cdot 10^{-4}$$

$$\sigma_s = E_s \cdot \epsilon_s = (200,000) (5.45 \cdot 10^{-4}) = (109.07 \text{ MPa}) \quad \text{Compression}$$

$$\sigma_c = E_c \cdot \epsilon_c = (28,500) (4.45 \cdot 10^{-5}) = (1.27 \text{ MPa}) \quad \text{Tension}$$