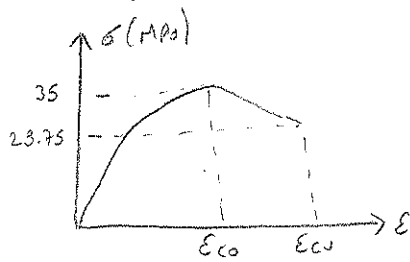


CE382 - Homework I

1) By using Hognested mathematical model:



$$E_{co} = \frac{2f_c}{\epsilon_c} \rightarrow E_c = 12680 + 460f_c$$

$$f_c = 35 \text{ MPa} \rightarrow E_c = 28780 \text{ MPa}$$

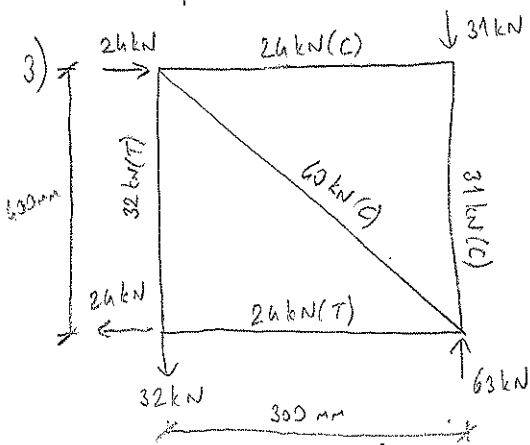
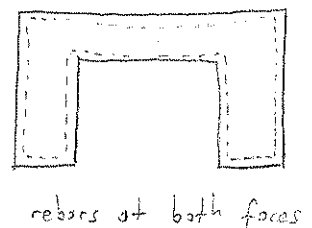
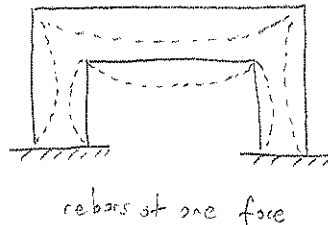
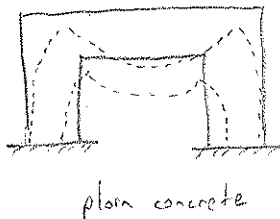
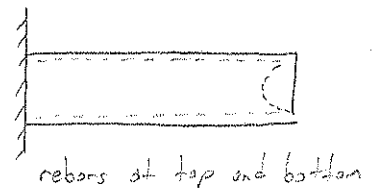
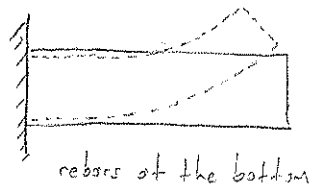
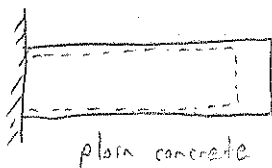
$$E_{co} = 0.00243$$

$$\sigma_c = f_c \left[\frac{2\epsilon_c}{E_{co}} - \left(\frac{\epsilon_c}{E_{co}} \right)^2 \right] = 35 \left[\frac{2\epsilon_c}{0.00243} - \left(\frac{\epsilon_c}{0.00243} \right)^2 \right]$$

$$\sigma = 30 \text{ MPa} \rightarrow E_c = 0.001511$$

$$\sigma = 15 \text{ MPa} \rightarrow E_c = 0.000533$$

2)



$$f_c = 30 \text{ MPa}$$

60x60 mm members are in compression, also two 120x120 mm members are in tension.

$$\text{direct tensile: } f_{ct} = 0.35\sqrt{f_c}$$

$$f_{ct} = 0.35\sqrt{30} \text{ MPa} = 1.92 \text{ MPa}$$

checking compression members:

$$\sigma_c = \frac{60000 \text{ N}}{60 \times 60 \text{ mm}^2} \approx 25 \text{ MPa} < f_c \text{ it is OK.}$$

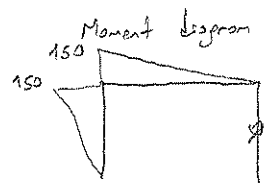
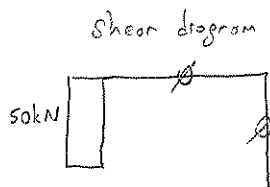
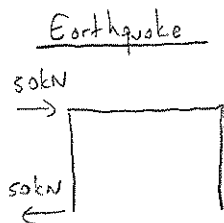
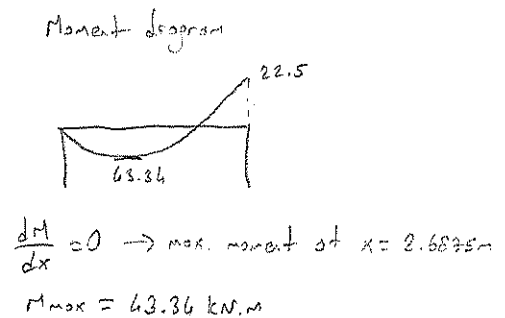
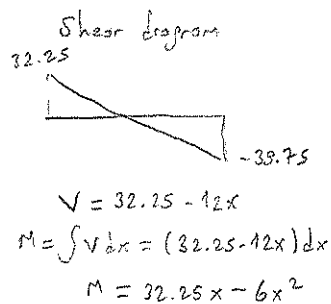
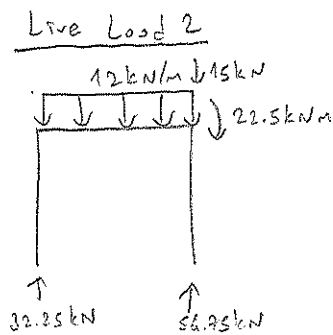
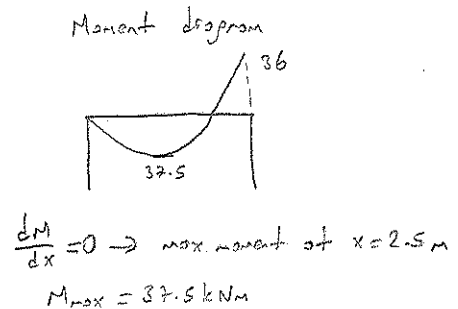
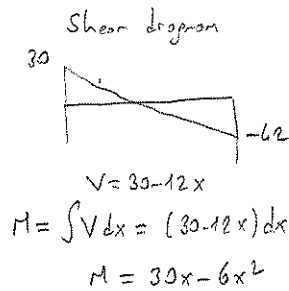
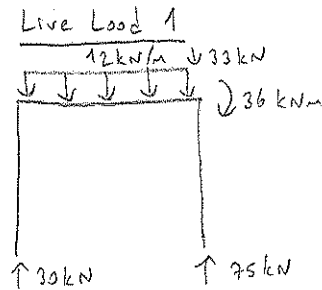
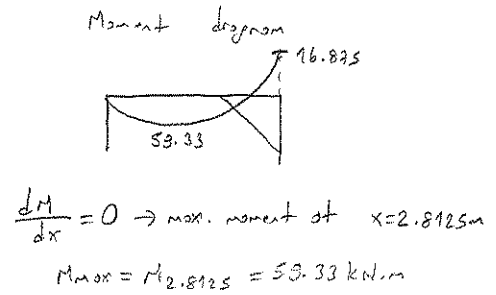
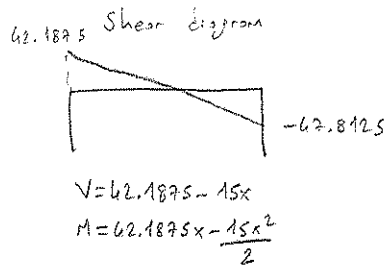
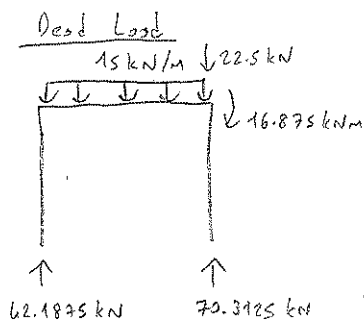
checking tension members:

$$\sigma_{ct} = \frac{32000 \text{ N}}{120 \times 120 \text{ mm}^2} = 2.22 \text{ MPa} > f_{ct} \text{ not OK!}$$

it cannot carry the applied load,
it will FAIL!

- 4) a) Since the thermal expansion coefficients of concrete and steel are same, they will not occur stress developed. (shortening with same amount)
- b) From the text book, for humid environment and adequate curing $E_{cs} = 0.00025$.

5)



We take into consideration load combinations that create the most critical situation:
1.4G + 1.6Q and 1.0G + 1.0Q + 1.0E

Left column

$$V_d = 1.0G + 1.0Q + 1.0E = 50 \text{ kN}$$

$$M_d = 1.0G + 1.0Q + 1.0E = 150 \text{ kNm}$$

Beam

$$V_d = 1.4G + 1.6Q$$

$$= 1.4 \times 62.1875 + 1.6 \times 62 = 134.1375 \text{ kN}$$

$$M_d = 1.4G + 1.6Q$$

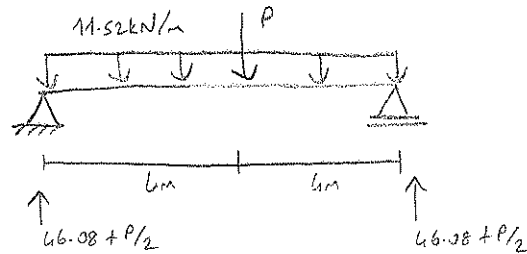
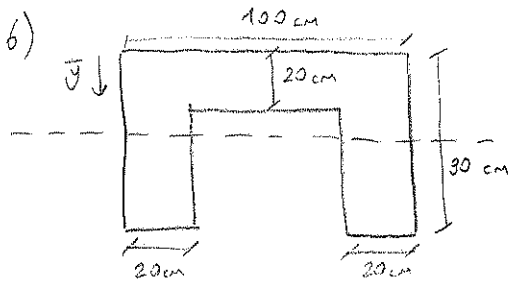
$$= 1.4 \times 53.33 + 1.6 \times 63.36 = 152.606 \text{ kNm}$$

Right column

$$V_d = 0$$

$$M_d = 1.4G + 1.6Q$$

$$= 1.4 \times 16.875 + 1.6 \times 36 = 81.225 \text{ kNm}$$



$$\left. \begin{aligned} A_{res} &= (1 \times 0.2) + (2 \times 0.7 \times 0.2) = 0.48 \text{ m}^2 \\ \gamma_{conc} &= 24 \text{ kN/m}^3 \end{aligned} \right\} \text{distributed load} = 24 \times 0.48 = 11.52 \text{ kN/m}$$

$$M_{max} = 4 \times \left(46.08 + \frac{P}{2} \right) - \frac{11.52 \times 4^2}{2} = 184.32 + 2P - 92.16 = (92.16 + 2P) \text{ kN.m}$$

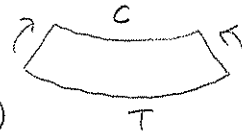
$$\bar{y} = \frac{(100 \times 20 \times 10) + (2 \times 20 \times 70 \times 55)}{4800} = 36.25 \text{ cm}$$

$$I = \frac{1}{12} (100) (20^3) + (100 \times 20) (26.25)^2 + 2 \times \left[\frac{1}{12} \times 20 \times 70^3 + 20 \times 70 \times 18.75^2 \right]$$

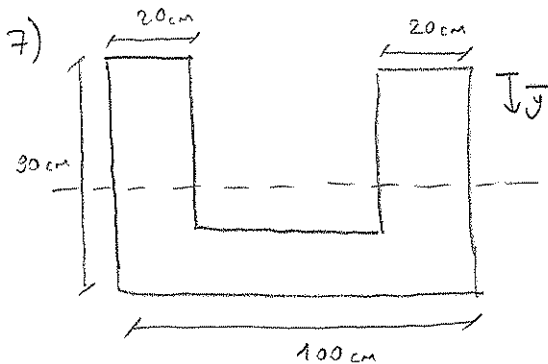
$$I = 3572500 \text{ cm}^4 = 0.035725 \text{ m}^4$$

$$\text{flexural tensile: } f_{ctf} = 0.7 \sqrt{f_c} = 4.14 \text{ MPa}$$

$$6_{ct} = \frac{My}{I} \rightarrow 4.14 \times 10^3 = \frac{(92.16 + 2P) \times (0.3 - 0.3625)}{0.035725}$$



$$P = 81.5 \text{ N}$$



$$\bar{y} = 80 - 36.25 = 52.75 \text{ cm}$$

$$\left. \begin{aligned} M_{max} &= (92.16 + 2P) \text{ kN.m} \\ I &= 0.035725 \text{ m}^4 \end{aligned} \right\} \text{they are taken from answer 6, because they are same.}$$

$$4.14 \times 10^3 = \frac{(92.16 + 2P) \times 0.3625}{0.035725} \Rightarrow P = 157.3 \text{ N}$$