

CE382 - REINFORCED CONCRETE FUNDAMENTALS

$$f_{cd} = 13 \text{ MPa}$$

$$f_{yd} = 365 \text{ MPa}$$

Interior

$$N_d = 1.4 \times 200 + 1.6 \times 150 = 520 \text{ kN}$$

$$V_d = 1.4 \times 10 + 1.6 \times 16 = 33.6 \text{ kN}$$

$$M_2 = 1.4 \times 0 + 1.6 \times 8 = 12.8 \text{ kN.m}$$

Exterior

$$N_d = 1.4 \times 100 + 1.6 \times 50 = 220 \text{ kN}$$

$$V_d = 1.4 \times 15 + 1.6 \times 18 = 43.8 \text{ kN}$$

$$M_2 = 1.4 \times 15 + 1.6 \times 10 = 37 \text{ kN.m}$$

$$\text{For 3m (Interior columns): } I_{3/L} = \frac{1}{12} \times 500^4 / 3000 = 1436 \times 10^3 \text{ mm}^4$$

$$\text{For 3m (Exterior columns): } I_{3/L} = \frac{1}{12} \times 600^4 / 3000 = 711 \times 10^3 \text{ mm}^4$$

$$\text{For 4m (Interior columns): } I_{3/L} = \frac{1}{12} \times 500^4 / 4000 = 1302 \times 10^3 \text{ mm}^4$$

$$\text{For 4m (Exterior columns): } I_{3/L} = \frac{1}{12} \times 600^4 / 4000 = 533 \times 10^3 \text{ mm}^4$$

$$\text{For 6m beam: } I_{cr/L} = \frac{1}{12} \times 250 \times 500^3 / 6000 = 651 \times 10^3 \text{ mm}^4$$

$$\text{For 5m beam: } I_{cr/L} = \frac{1}{12} \times 250 \times 500^3 / 5000 = 521 \times 10^3 \text{ mm}^4$$

$$\text{Check sway frame; } \Psi = 1.5 \times 5 \times \frac{(4 \times 520 + 2 \times 220)}{3000 \times [4 \times 33.6 + 2 \times 43.8]} = 0.024 < 0.05$$

Non-sway frame. ✓
Sidesway is prevented.

Interior

$$e = \frac{M_2}{N_d} = \frac{12800}{520} = 24.6 < e_{min} = 0.03 \times 500 + 15 = 30 \text{ mm}$$

$$M_2 = e_{min} \times N_d = 30 \times 520 = 15.6 \text{ kN.m}$$

$$\alpha_1 = \frac{1436 + 1302}{651 + 521} = 2.6, \quad \alpha_2 = \frac{2 \times 1436}{651 + 521} = 3 \rightarrow \alpha_n = 2.8$$

$$k = 0.7 + 0.1 \alpha_n = 0.98$$

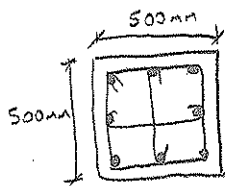
$$l_n = 3000 - 500 = 2500 \text{ mm} \rightarrow l_k = 2500 \times 0.98 = 2450 \text{ mm}$$

$$\frac{l_k}{i} = \frac{2450}{0.3 \times 500} = 16.3 \leq 34 - 12 \left(\frac{M_1}{M_2} \right) \quad \text{short column!}$$

$$M_d = M_2 = 15.6 \text{ kN.m}$$

$$\frac{N_d}{b h f_{cd}} = 0.16, \quad \frac{M_d}{b h^2 f_{cd}} = 0.0036 \rightarrow \rho_t = 0.025$$

$$m = \frac{f_{td}}{f_{cd}} = \frac{365}{13} = 28.08 \rightarrow \rho_t \approx \rho_{min}$$



$$A_{st} = 0.28 \times \frac{13}{365} \times 500^2 = 2494 \text{ mm}^2 \quad \text{Use } 8\phi 20 : 8 \times 315 = 2520 \text{ mm}^2 > A_{s,req.}$$

Exterior

$$e = \frac{M_2}{N_d} = \frac{37000}{220} = 168.2 > e_{\min} \checkmark$$

$$\alpha_1 = \frac{711+533}{651} = 1.3, \quad \alpha_2 = \frac{2 \times 711}{651} = 2.18 \quad \text{---} \quad \alpha_m = 2.04$$

$$k = 0.7 + 0.1 \alpha_m = 0.904$$

$$l_n = 2500 \text{ mm} \quad l_k = 2500 \times 0.904 = 2260 \text{ mm}$$

$$\frac{l_k}{i} = \frac{2260}{0.3 \times 400} = 18.3 \leq 34 - 12 \left(\frac{M_1}{M_2} \right) \quad \text{short column!}$$

$$M_d = M_d = 37 \text{ kN.m}$$

$$\frac{N_d}{b h f_{cd}} = 0.11, \quad \frac{M_d}{b h f_{cd}} = 0.045 \quad \text{---} \quad \rho_{tm} = 0.28 \quad \rho = \frac{365}{13}$$

$$\rho_t = 0.28 / \frac{365}{13} = 0.00937 \approx \rho_{\min}$$

$$A_{st} = 0.28 \times \frac{13}{365} \times 400^2 = 1535 \text{ mm}^2$$

$$\text{Use } 6 \varnothing 20: 6 \times 315 = 1890 \text{ mm}^2 > A_{s, \text{req}}$$

