

## Class 2

Lecture 3

Properties of Systems

Impulse Response of a Linear System

Lecture 4

Impulse Response of a LTI System

Transfer Function

Equivalent Systems

Concept: state space  $\longleftrightarrow$  transfer function

Outline

## Basic Properties of LTI Systems

- Memoryless
- Causal
- Time-invariant
- Linear

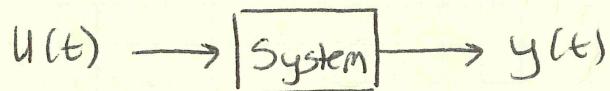
Impulse Response

Transfer Function

## Lecture 3

Basic Properties of LTI & LTV Systems① Memoryless

A system is memoryless if the output at time  $t$  depends only on the input at time  $t$ .

Examples:

$$y(t) = 4u(t) \quad \text{memoryless}$$

$$y(t) = u(t-3) \quad \text{not memoryless - needs past value}$$

$$y(t) = u(3t) \quad \text{not mem. - speed up}$$

$$y(t) = (t+5)u(t) \quad \text{mem.}$$

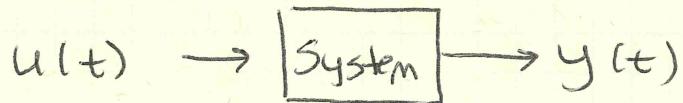
$$y(t) = u(-t) \quad \text{not mem. - time reversal}$$

$y(-1) = u(1)$  needs future time

$$y(t) = \cos(t^2 + u(t)^2) \quad \text{mem.}$$

## ② Causal

A system is causal if the output at time  $t$  depends only on the input at time  $t$  plus past values of the input.



$y(t+a)$  depends only on  $u(t+b)$  for  $b \leq a$

The system doesn't anticipate the input  
"non-anticipatory" system

### Examples:

$$y(t) = 4u(t) \quad \text{causal - amplification}$$

$$y(t) = u(t-3) \quad \text{causal - delay}$$

$$y(t) = u(t+5) \quad \text{noncausal - time shift forward}$$

$$y(t) = u(3t) \quad \text{noncausal - speed up}$$

$$y(t) = (t+5)u(t) \quad \text{causal - ramp times input}$$

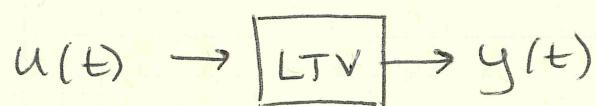
$$y(t) = u(-t) \quad \text{noncausal - time reversal}$$

$$y(t) = u(t+t_0) \quad \text{causal for } t \leq 0$$

$$y(t) = \int_{-\infty}^t u(\tau+a) d\tau \quad \text{causal for } a \leq 0$$

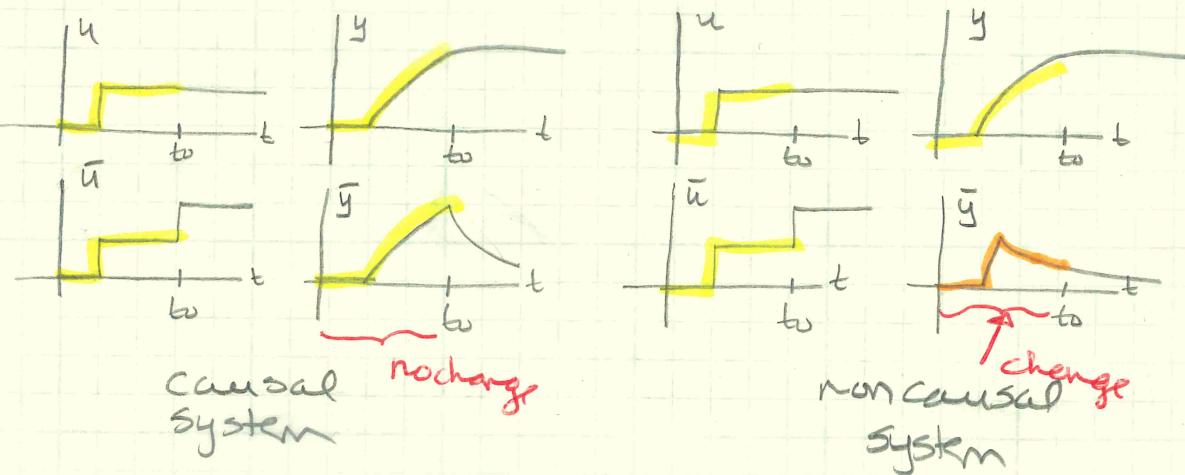
\* All memoryless systems are causal

Formal definition of causality for continuous LTV System:



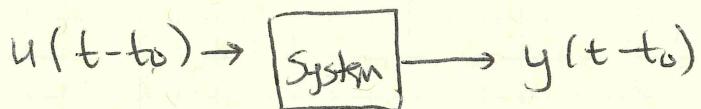
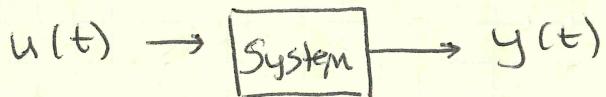
The system is causal if for other input  $\bar{u}(t)$  for which  $\bar{u}(t) = u(t) + 0 \leq t < T, T > 0$  the system exhibits at least one output  $\bar{y}(t)$  that satisfies  $\bar{y}(t) = y(t) + 0 \leq t < T$ .

### Example



### ③ Time - Invariant

A system is time-invariant if a time shift in the input results in the same time shift in the output.



Examples:

$$y(t) = 2u(t) \quad \text{T.I.} - \text{amplification}$$

$$y(t) = (u(t))^2 \quad \text{T.I.} \quad y(t-t_0) = (u(t-t_0))^2$$

$$y(t) = t u(t) \quad \text{Time-varying} \quad y(t-t_0) = (t-t_0)u(t-t_0)$$

but  $u(t-t_0) \sim t u(t-t_0)$

$$y(t) = 3u(t-5) \quad \text{T.I.} \quad y(t-t_0) = 3u(t-t_0-5)$$

$u(t-t_0) \sim 3u(t-t_0-5)$

$$y(t) = \int_{-\infty}^t u(\tau) d\tau \quad \text{T.I.} \quad y(t-t_0) = \int_{-\infty}^{t-t_0} u(\tau) d\tau$$

$u(t-t_0) \sim \int_{-\infty}^t u(t-t_0-\tau) d\tau$

$$= \int_{-\infty}^{t-t_0} u(v) dv$$

$$y(t) = u(5t) \quad \text{Time-varying} \quad y(t-t_0) = u(5(t-t_0)) = u(5t-5t_0)$$

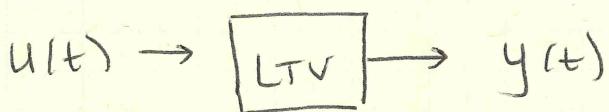
$u(t-t_0) \sim u(5t-5t_0)$

$$y(t) = u(-t) \quad \text{Time-varying} \quad y(t-t_0) = u(-(t-t_0)) = u(-t+t_0)$$

$u(t-t_0) \sim u(-t+t_0)$

$$y(t) = \sin(u(t)) \quad \text{T.I.}$$

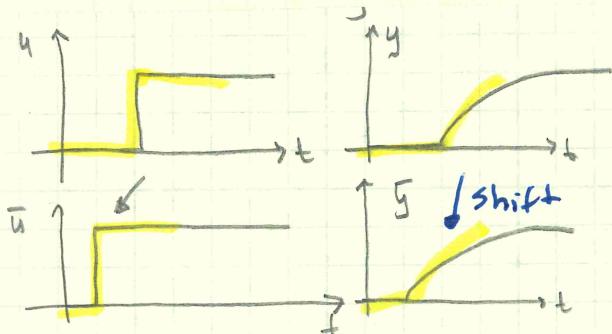
Formal definition of time-invariance for continuous LTV System:



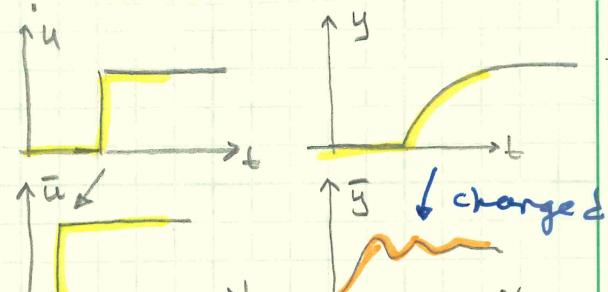
The system is time-invariant if

$$u \rightsquigarrow y \Rightarrow u(t+T) \rightsquigarrow y(t+T) \quad \forall T > 0 \\ \forall t \geq 0$$

Example:



Time-invariant system



Time-varying system

Comment on Initial Condition

$$\left. \begin{array}{l} x(t_0) \\ u(t), t \geq t_0 \end{array} \right\} \rightsquigarrow y(t), t \geq t_0$$



$$\left. \begin{array}{l} x(t_0+T) \\ u(t-T), t \geq t_0+T \end{array} \right\} \rightsquigarrow y(t-T), t \geq t_0+T$$

initial state shifted to  $t_0 + T$   
same input waveform applied at  $t_0 + T$  (vs  $t_0$ )

⇒ output waveform is the same except it starts to appear at time  $t_0 + T$

(4)

Linear

A system is linear if it has the following three properties:

1) Additivity

$$\left. \begin{array}{l} x_i(t_0) \\ u_i(t), t \geq t_0 \end{array} \right\} \rightarrow y_i(t), t \geq t_0$$

$$\Rightarrow \left. \begin{array}{l} \sum_i x_i(t_0) \\ \sum_i u_i(t), t \geq t_0 \end{array} \right\} \rightarrow \sum_i y_i(t), t \geq t_0$$

2) Scale / Homogeneity

$$\left. \begin{array}{l} x(t_0) \\ u(t), t \geq t_0 \end{array} \right\} \rightarrow y(t), t \geq t_0 \Rightarrow \left. \begin{array}{l} \alpha x(t_0) \\ \alpha u(t), t \geq t_0 \end{array} \right\} \rightarrow \alpha y(t), t \geq t_0$$

$$\alpha \in \mathbb{R}$$

3) Superposition

$$\left. \begin{array}{l} x_i(t_0) \\ u_i(t), t \geq t_0 \end{array} \right\} \rightarrow y_i(t), t \geq t_0$$

$$\Rightarrow \left. \begin{array}{l} \sum_i \alpha_i x_i(t_0) \\ \sum_i \alpha_i u_i(t) \quad t \geq t_0 \end{array} \right\} \rightarrow \sum_i \alpha_i y_i(t), t \geq t_0$$

Examples:

$$y(t) = c u(t)$$

linear - amplification

$$\alpha_1 y_1(t) + \alpha_2 y_2(t) = c (\alpha_1 u_1(t) + \alpha_2 u_2(t))$$

$$\alpha_1 u_1(t) + \alpha_2 u_2(t) \rightsquigarrow c (\alpha_1 u_1(t) + \alpha_2 u_2(t))$$

$$y(t) = (u(t))^2$$

nonlinear  $\alpha_1 y_1(t) + \alpha_2 y_2(t)$ 

$$\neq (\alpha_1 u_1(t) + \alpha_2 u_2(t))^2$$

$$y(t) = u(t) + 5$$

nonlinear  $\alpha y(t) = \alpha u(t) + 5\alpha$ 

$$\neq \alpha u(t) \rightsquigarrow \alpha u(t) + 5$$

$$y(t) = \int_{-2}^2 u(t+\tau) d\tau \quad \text{linear}$$

$$y(t) = \int_{t-1/2}^{t+1/2} u(\tau) d\tau \quad \text{linear}$$

$$y(t) = \frac{du(t)}{dt} \quad \text{linear}$$

$$y(t) = \frac{(u(t))^2}{u(t-1)} \quad \text{nonlinear}$$

$$\alpha_1 u_1(t) + \alpha_2 u_2(t) \not\rightsquigarrow \alpha_1 y_1(t) + \alpha_2 y_2(t)$$

## Complete Response to a Given Input

For every linear system:

Response = zero-input response + zero-state response

⇒ can study two responses separately  
then sum for complete response

### zero - input Response

$$\left. \begin{array}{l} x(t_0) \\ u(t) = 0 \end{array} \right\} \rightarrow y_{zi}(t) \quad t \geq t_0$$

### zero - state Response

$$\left. \begin{array}{l} x(t_0) = 0 \\ u(t) \quad t \geq t_0 \end{array} \right\} \rightarrow y_{zs}(t) \quad t \geq t_0$$

Additivity property ⇒

$$\text{Response to } \left. \begin{array}{l} x(t_0) \\ u(t) \quad t \geq t_0 \end{array} \right\} = \text{Response to } \left. \begin{array}{l} x(t_0) \\ u(t) = 0 \quad t \geq t_0 \end{array} \right\} + \text{Response to } \left. \begin{array}{l} x(t_0) = 0 \\ u(t) \quad t \geq t_0 \end{array} \right\}$$

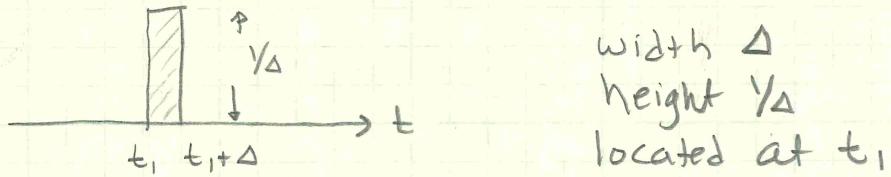
## Impulse Response

Fundamental Result: Any LTI system can be completely characterized by its impulse response.

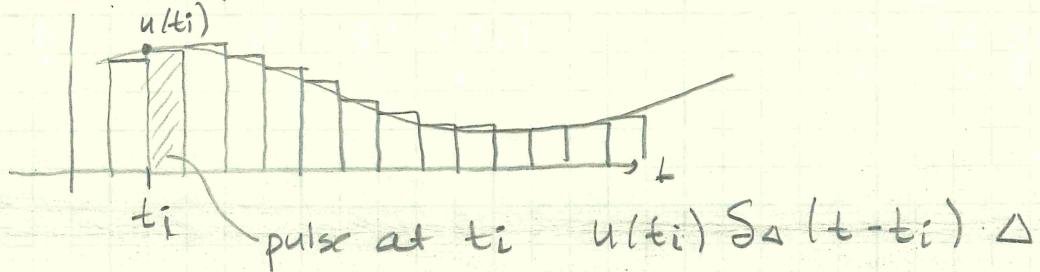
Consider a SISO system first.

Consider the zero-state response - output is excited exclusively by the input.

Let  $s_\Delta(t-t_i)$  be the unit pulse



Then, every input  $u(t)$  can be approximated by a series of pulses



$$\Rightarrow u(t) \approx \sum u(t_i) s_\Delta(t-t_i) \Delta$$

Let  $g_\Delta(t, t_i)$  be the output at time  $t$  with impulse at  $t_i$  from input  $u(t) = s_\Delta(t-t_i)$  applied at  $t_i$

$$\Rightarrow s_\Delta(t-t_i) \rightarrow g_\Delta(t, t_i)$$

$$s_\Delta(t-t_i) u(t_i) \Delta \rightarrow g_\Delta(t, t_i) u(t_i) \Delta \quad \text{homogeneity}$$

$$\sum_i s_\Delta(t-t_i) u(t_i) \Delta \rightarrow \sum_i g_\Delta(t, t_i) u(t_i) \Delta \quad \text{additivity}$$

$\Rightarrow$  The output  $y(t)$  excited by the input  $u(t)$  can be approximated by

$$y(t) \approx \sum_i g_\Delta(t, t_i) u(t_i) \Delta \quad \star$$

## Impulse Response (continued)

Let  $\Delta \rightarrow 0$

$\Rightarrow S_\Delta(t-t_i)$  pulse  $\rightarrow$  impulse  $S(t-t_i)$  at  $t_i$

$g_\Delta(t, t_i) \rightarrow g(t, t_i)$  output

$$y(t) \approx \sum_i g_\Delta(t, t_i) u(t_i) \Delta \rightarrow y(t) = \int_{-\infty}^{\infty} g(t, \tau) u(\tau) d\tau$$

↑                      ↑                      ↑  
 summation    time becomes continuum    written  
 becomes integral                                  as                       $d\tau$

Note -  $g(t, \tau)$  is function of 2 variables

$\tau$  = time at which impulse input applied

$t$  = time at which output is observed

& is called the impulse response

If causal system,  $g(t, \tau) = 0$  for  $t < \tau$   
(output doesn't appear before input applied)

If  $x(t_0) = 0$ , output excited by  $u(t), t \geq t_0$  only

Then  $y(t) = \int_{t_0}^t g(t, \tau) u(\tau) d\tau$   
 ↑ limits changed

Define Impulse Response Matrix

$P$  inputs,  $Q$  outputs (MIMO)

$$y(t) = \int_{t_0}^t G(t, \tau) u(\tau) d\tau$$

$$G(t, \tau) = \begin{bmatrix} g_{11}(t, \tau) & g_{12}(t, \tau) & \dots & g_{1P}(t, \tau) \\ \vdots & & & \\ g_{Q1}(t, \tau) & g_{Q2}(t, \tau) & \dots & g_{QP}(t, \tau) \end{bmatrix}$$

Where  $g_{ij}(t, \tau)$  = response at time  $t$  at  $i^{th}$  output terminal due to impulse applied at time  $\tau$  at  $j^{th}$  input terminal.

If time-invariant,

$$G(t+T, \tau+T) = G(t, \tau) \quad \forall t, \tau, T \geq 0$$

Then for  $T=0$ ,  $t_1=T$ ,  $t_2=t+T$

$$G(t_2, t_1) = G(t_2 - t_1, 0) \quad \forall t_2 \geq t_1 \geq 0$$

$\Rightarrow G(t_2, t_1)$  is a function of  $t_2 - t_1$ .

If causal & time-invariant

Then

$$y(t) = \int_0^t G(t-\tau) u(\tau) d\tau$$

$$= (G * u)(t) \quad \forall t \geq 0$$

Convolution Operator

### Transfer Function

Recall Laplace Transform

- $\mathcal{L}[x(t)] = \hat{x}(s) = \int_0^\infty e^{-st} x(t) dt \quad s \in \mathbb{C}$  complex number
- $\mathcal{L}[\dot{x}(t)] = s \hat{x}(s) - x(0)$
- $\mathcal{L}[(x * y)(t)] = \hat{x}(s) \hat{y}(s)$

Thus

$$\hat{y}(s) = \hat{G}(s) \hat{u}(s)$$

Define Transfer Function of a continuous time,

causal, LTI system is

$$\hat{G}(s) = \mathcal{L}[G(t)] = \int_0^\infty e^{-st} G(t) dt$$

Transfer function = Laplace transform of the impulse response

Easier to use transform is convolution

Recall: circuit analogy

Outline

Impulse Response for LTI System

Transfer function for LTI System

Converting State Space  $\leftrightarrow$  Transfer function

Equivalent Systems

## Lecture 4

LTI State Space equation

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases} \quad \begin{matrix} x \in \mathbb{R}^n \\ u \in \mathbb{R}^m \\ y \in \mathbb{R}^m \end{matrix}$$

Apply Laplace transform

$$s\hat{x}(s) - x(0) = A\hat{x}(s) + B\hat{u}(s)$$

$$\hat{y}(s) = C\hat{x}(s) + D\hat{u}(s)$$

Combining terms

$$s\hat{x}(s) - A\hat{x}(s) = x(0) + B\hat{u}(s)$$

$$(sI - A)\hat{x}(s) = x(0) + B\hat{u}(s)$$

$$\hat{x}(s) = (sI - A)^{-1}x(0) + (sI - A)^{-1}B\hat{u}(s)$$

$$\hat{y}(s) = C(sI - A)^{-1}x(0) + C(sI - A)^{-1}B\hat{u}(s) + D\hat{u}(s)$$

$$= \underbrace{C(sI - A)^{-1}x(0)}_{\text{zero-input response}} + \underbrace{(C(sI - A)^{-1}B + D)\hat{u}(s)}_{\text{zero-state response}}$$

Define  $\hat{y}(s) = \hat{\Phi}(s)x(0) + \hat{G}(s)\hat{u}(s)$ 

$$\hat{\Phi}(s) = C(sI - A)^{-1}$$

frequency domain

$$\hat{G}(s) = C(sI - A)^{-1}B + D$$

Transfer Function

time domain

$$G(s) = \mathcal{L}^{-1}[G(s)]$$

unique

Impulse Response

Example (p.89 Ch4)

$$A = \begin{bmatrix} 0 & -1 \\ 1 & -2 \end{bmatrix} \quad \text{Recall } A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}, A^{-1} = \frac{1}{a_{11}a_{22} - a_{12}a_{21}} \begin{bmatrix} a_{22} & -a_{12} \\ -a_{21} & a_{11} \end{bmatrix}$$

$$(sI - A)^{-1} = \begin{bmatrix} s & 1 \\ -1 & s+2 \end{bmatrix}^{-1} = \frac{1}{s^2 + 2s + 1} \begin{bmatrix} s+2 & -1 \\ 1 & s \end{bmatrix} = \begin{bmatrix} \frac{s+2}{(s+1)^2} & \frac{-1}{(s+1)^2} \\ -\frac{1}{(s+1)^2} & \frac{s}{(s+1)^2} \end{bmatrix}$$

## Motivation

Given  $y(t) = \int_{t_0}^t G(t-\tau) u(\tau) d\tau$

No simple way to compute convolution

Easiest way would be numerically on computer  
on discretized equation

But - least accurate result because of  
step size

For LTI Systems, we can use

$$\hat{y}(s) = \hat{G}(s) \hat{u}(s)$$

to compute the solution via  $\mathcal{L}^{-1}(\hat{y}(s))$

But - complicated due to sensitivity  
in data, round-off errors etc.

Better Method: Transform transfer function  
into state-space equations & compute  
solution

Today - See connection between  
steady-state & transfer function



1<sup>st</sup> order  
differential  
equations

higher-order  
differential  
equations

RealizationState Space  $\leftrightarrow$  Transfer Function

$$\begin{array}{l} \text{LTI System} \\ \left\{ \begin{array}{l} \dot{x} = Ax + Bu \\ y = Cx + Du \end{array} \right. \end{array}$$

is a realization of  $\hat{G}(s)$  if

$$\hat{G}(s) = C(sI - A)^{-1}B + D$$

Equivalent Systems: Zero-State Equivalent

Two state-space systems are zero-state equivalent if they realize the same transfer function i.e., they have the same I/O pairs.

Equivalent Systems: Algebraically Equivalent

Two LTI systems

$$\begin{array}{l} \left\{ \begin{array}{l} \dot{x} = Ax + Bu \\ y = Cx + Du \end{array} \right. \\ \quad \quad \quad \left\{ \begin{array}{l} \dot{\bar{x}} = \bar{A}\bar{x} + \bar{B}\bar{u} \\ \bar{y} = \bar{C}\bar{x} + \bar{D}\bar{u} \end{array} \right. \end{array}$$

are algebraically equivalent if  $\exists$  nonsingular matrix  $P$  st.

$$\bar{x} = P x$$

$$\bar{A} = P A P^{-1}$$

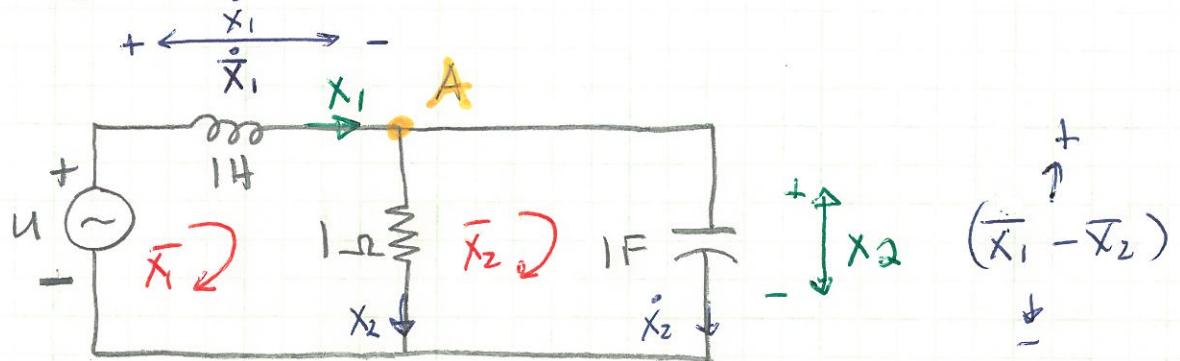
$$\bar{B} = P B$$

$$\bar{C} = C P^{-1}$$

$$\bar{D} = D$$

$\star$  Algebraic Equivalence  $\Rightarrow$  Zero-State Equivalence  
but not vice versa

Example (p. 93 Chen)



$\leftarrow \rightarrow \downarrow \uparrow$

State Variable Set #1

$x_1$  = inductor current

$x_2$  = capacitor voltage

Note

$$\dot{i} = C \frac{dv}{dt} = C \dot{x}_2 = \dot{x}_2$$

$$v = L \frac{di}{dt} = L \dot{x}_1 = \dot{x}_1$$

$$\dot{i} = \frac{v}{R} = \frac{x_2}{R} = x_2$$

KCL @ A

$$x_1 = x_2 + \dot{x}_2 \quad \text{or} \quad \dot{x}_2 = x_1 - x_2$$

KVL @ LHS

$$\dot{x}_1 + x_2 - u = 0 \quad \text{or} \quad \dot{x}_1 = -x_2 + u$$

$$\Rightarrow \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & -1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u$$

$$y = [0 \ 1] x$$

State Variable Set #2

$\bar{x}_1$  = loop current LHS

$\bar{x}_2$  = loop current RHS

Note

$$v = L \frac{di}{dt} = L \dot{\bar{x}}_1 = \dot{\bar{x}}$$

$$v = \dot{i} R = (\bar{x}_1 - \bar{x}_2) R = (\bar{x}_1 - \bar{x}_2)$$

KVL @ LHS

$$u = \bar{x}_1 + (\bar{x}_1 - \bar{x}_2)$$

$$\text{or} \quad \dot{\bar{x}}_1 = -\bar{x}_1 + \bar{x}_2 + u$$

$$\dot{i} = C \frac{dv}{dt} = C (\dot{\bar{x}}_1 - \dot{\bar{x}}_2) = \bar{x}_2$$

$$\text{or} \quad \dot{\bar{x}}_2 = \bar{x}_1 - \bar{x}_2 = -\bar{x}_1 + u$$

$$\Rightarrow \begin{bmatrix} \dot{\bar{x}}_1 \\ \dot{\bar{x}}_2 \end{bmatrix} = \begin{bmatrix} -1 & 1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} \bar{x}_1 \\ \bar{x}_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u$$

$$y = [1 \ -1] \bar{x}$$

Two different equations for same network

Are they equivalent?

Example (continued)

Check if Algebraically Equivalent:

Need to find  $P$  s.t.  $\bar{x} = Px$

By definition  $\bar{x}_1 = x_1$

Voltage across resistor  $= x_2 \cdot R = x_2$

Current through resistor  $= x_2 = \bar{x}_1 - \bar{x}_2$

$$\Rightarrow \bar{x}_2 = \bar{x}_1 - x_2 = x_1 - x_2$$

$$\Rightarrow P = \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} \quad \begin{bmatrix} \bar{x}_1 \\ \bar{x}_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

*nonsingular ✓*

Check

$$\checkmark \bar{A} = PAP^{-1} = \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} 0 & -1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} = \begin{bmatrix} 0 & -1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} = \begin{bmatrix} -1 & 1 \\ 1 & 0 \end{bmatrix}$$

$$\text{where } P^{-1} = \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix}^{-1} = \frac{1}{-1} \begin{bmatrix} -1 & 0 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix}$$

$$\checkmark \bar{B} = PB = \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$\checkmark \bar{C} = CP^{-1} = \begin{bmatrix} 0 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} = \begin{bmatrix} 1 & -1 \end{bmatrix}$$

$$\checkmark \bar{D} = D = 0$$

So, Algebraically Equivalent

Example (Continued)

Check if Zero-State Equivalent

Need to see if  $\hat{G}(s) = \frac{1}{G(s)}$

$$\hat{G}(s) = C(SI - A)^{-1}B + D$$

$$= [0 \ 1] \left[ \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & -1 \\ 1 & -1 \end{bmatrix} \right]^{-1} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$\left[ \begin{bmatrix} s & 1 \\ -1 & s+1 \end{bmatrix} \right]^{-1} = \frac{1}{s(s+1)+1} \begin{bmatrix} s+1 & -1 \\ 1 & s \end{bmatrix}$$

$$= \frac{1}{s^2+s+1} \begin{bmatrix} s+1 & -1 \\ 1 & s \end{bmatrix}$$

$$= \begin{bmatrix} \frac{s+1}{s^2+s+1} & \frac{-1}{s^2+s+1} \\ \frac{1}{s^2+s+1} & \frac{s}{s^2+s+1} \end{bmatrix}$$

$$= [0 \ 1] \begin{bmatrix} \frac{s+1}{s^2+s+1} & \frac{-1}{s^2+s+1} \\ \frac{1}{s^2+s+1} & \frac{s}{s^2+s+1} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} \frac{1}{s^2+s+1} & \frac{s}{s^2+s+1} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \frac{1}{s^2+s+1}$$

$$\frac{1}{G(s)} = \bar{C} (S\bar{I} - \bar{A})^{-1} \bar{B} + \bar{D}$$

$$= [1 \ -1] \begin{bmatrix} s+1 & -1 \\ 1 & s \end{bmatrix}^{-1} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$\left[ \begin{bmatrix} s+1 & -1 \\ 1 & s \end{bmatrix} \right]^{-1} = \frac{1}{s(s+1)+1} \begin{bmatrix} s & 1 \\ -1 & s+1 \end{bmatrix} = \begin{bmatrix} \frac{s}{s^2+s+1} & \frac{1}{s^2+s+1} \\ \frac{-1}{s^2+s+1} & \frac{s+1}{s^2+s+1} \end{bmatrix}$$

$$= [1 \ -1] \begin{bmatrix} \frac{s}{s^2+s+1} & \frac{1}{s^2+s+1} \\ \frac{-1}{s^2+s+1} & \frac{s+1}{s^2+s+1} \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} \frac{s+1}{s^2+s+1} & \frac{-s}{s^2+s+1} \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$= \frac{1}{s^2+s+1}$$

So Zero-State Equivalent

Theorem A transfer function  $\hat{G}(s)$  can be realized by an LTI state-space system iff  $\hat{G}(s)$  is a proper rational function.

Concept :

$$\hat{G}(s) = \frac{\text{num}}{\text{den}} = \frac{\text{polynomial in } s}{\text{polynomial in } s}$$

If  $\deg(\text{den}) \geq \deg(\text{num})$

Then  $\hat{G}(s)$  is a proper rational function.

What does  $\hat{G}(s)$  look like in polynomial form?

$$\hat{G}(s) = C(SI - A)^{-1}B + D$$

$$M^{-1} = \frac{1}{\det M} (\text{adj } M)' \quad \begin{matrix} \text{transpose} \\ \uparrow \\ \text{Adjoint Matrix of } M \end{matrix}, \quad \text{adj } M = \left[ \begin{matrix} \text{cof}_{ij} M \end{matrix} \right]$$

$\text{cof}_{ij} M$   
 $\uparrow$   
 $i^{\text{th}}$  cofactor of  $M$   
 $= \text{determinant of } i^{\text{th}}$   
 $\text{submatrix of } M$   
 $\text{obtained by removing}$   
 $\text{row } i \text{ and column } j$   
 $\text{Multiplied by } (-1)^{i+j}$

Thus,

$$\hat{G}(s) = \frac{1}{\det(SI - A)} C \left[ \text{adj } (SI - A)' \right] B + D$$

$\uparrow$

denominator := characteristic polynomial of  $A$

roots = eigenvalues of  $A$

Note, if  $A$  diagonal,  $A = \begin{bmatrix} a_1 & 0 & 0 \\ 0 & a_2 & 0 \\ 0 & 0 & a_3 \end{bmatrix}$

then  $\det(SI - A) = (s-a_1)(s-a_2)(s-a_3)$

roots = eigenvalues for diagno.  $A$

So  $\det(sI - A)$  is a polynomial of  $A$  of degree  $n$ .

$\text{adj}(sI - A)$  will have degree  $(n-1)$  or smaller

$C [\text{adj}(sI - A)'] B$  will be a linear combination of polynomials of degree  $(n-1)$  or smaller.

$\Rightarrow \hat{G}(s)$  is a proper rational function

### Examples

$$\hat{G}(s) = \frac{1}{s^2 + 5s + 2}$$

$$\hat{G}(s) = \frac{s+2}{s^2 + 2s + 4}$$

$$\hat{G}(s) = \frac{s^2 - 2s - 10}{s^2 + 5s + 4}$$

Given  $\hat{G}(s)$ , Find State-Space Equations

SISO

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

$$\begin{aligned}\hat{G}(s) &= \frac{\hat{Y}(s)}{\hat{U}(s)} = \frac{\beta_1 s^{n-1} + \beta_2 s^{n-2} + \dots + \beta_{n-1} s + \beta_n}{s^n + \alpha_1 s^{n-1} + \alpha_2 s^{n-2} + \dots + \alpha_{n-1} s + \alpha_n}\end{aligned}$$

Controllable Canonical Form:

$$A = \begin{bmatrix} -\alpha_1 & -\alpha_2 & \cdots & -\alpha_{n-1} & -\alpha_n \\ 1 & & & & \\ 0 & 1 & \ddots & 0 & 0 \\ & 0 & \ddots & \ddots & 0 \\ & & & & \ddots \end{bmatrix} \quad B = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \\ 0 \end{bmatrix}$$

$$C = [\beta_1 \ \beta_2 \ \cdots \ \beta_{n-1} \ \beta_n]$$

Observable Canonical Form:

$$\bar{A} = \begin{bmatrix} -\alpha_1 & 1 & & & \\ -\alpha_2 & & 1 & 0 & \\ \vdots & & & \ddots & \\ -\alpha_n & 0 & \ddots & \ddots & \end{bmatrix} \quad \bar{B} = \begin{bmatrix} \beta_1 \\ \beta_2 \\ \vdots \\ \beta_{n-1} \\ \beta_n \end{bmatrix}$$

$$\bar{C} = [1 \ 0 \ \cdots \ 0]$$

$$\text{note } A = \bar{A}' \quad B = \bar{C}' \quad C = \bar{B}'$$

Create  $A, B, C, D$  by reading coefficients of  $\hat{G}(s)$

MIMOGiven  $\hat{G}(s)$ 

$$\begin{aligned} \text{Decompose } \hat{G}(s) &= C(SI - A)^{-1}B + D \\ &= \hat{G}_{sp}(s) + \lim_{s \rightarrow \infty} \hat{G}(s) \\ &\quad \text{strictly proper} \qquad \text{constant} \end{aligned}$$

Find monic least common denominator of all entries of  $\hat{G}_{sp}(s)$ .

monic lcd = monic polynomial (lead coefficient of 1) of smallest order that can be divided by all others

$$d(s) = s^n + d_1 s^{n-1} + d_2 s^{n-2} \dots + d_{n-1} s + d_n$$

$$\text{Expand } \hat{G}_{sp}(s) = \frac{1}{d(s)} [N_1 s^{n-1} + N_2 s^{n-2} + \dots + N_{n-1} s + N_n]$$

$m \times k$  matrices

Set

$$A = \begin{bmatrix} -d_1 I_{nk \times k} & -d_2 I_{nk \times k} & \dots & -d_n I_{nk \times k} \\ I_{k \times k} & & & O \\ & \ddots & & O \\ & & \ddots & \\ O & & & I_{nk \times k} \end{bmatrix}_{nk \times nk}$$

$$B = \begin{bmatrix} I_{nk \times k} \\ O_{nk \times k} \\ \vdots \\ O_{nk \times k} \end{bmatrix}_{nk \times k}$$

$$C = [N_1 \ N_2 \ \dots \ N_{n-1} \ N_n]_{m \times n_k}$$

This gives a realization of  $\hat{G}(s)$ .

Example Two zero-state Equivalent Realizations  
(but not Algebraically Equivalent)

1) Given  $\hat{G}(s) = \begin{bmatrix} \frac{4s-10}{2s+1} & \frac{3}{s+2} \\ \frac{1}{(2s+1)(s+2)} & \frac{s+1}{(s+2)^2} \end{bmatrix}$

Rewrite as constant matrix + strictly proper rational matrix

$$\begin{aligned} \hat{G}(s) &= \lim_{s \rightarrow \infty} \hat{G}(s) + \hat{G}_{sp}(s) & \xrightarrow{\text{def}} & \frac{-12}{2s+1} = \frac{-b}{s+\gamma_2} \\ &= \begin{bmatrix} 2 & 0 \\ 0 & 0 \end{bmatrix} + \begin{bmatrix} \frac{-b}{s+\gamma_2} & \frac{3}{s+2} \\ \frac{\gamma_2}{(s+\gamma_2)(s+2)} & \frac{s+1}{(s+2)^2} \end{bmatrix} \end{aligned}$$

$$\lim_{s \rightarrow \infty} \left( \frac{4s-10}{2s+1} \right) = \lim_{s \rightarrow \infty} \left( \frac{4s}{2s} \right) = 2 \quad \frac{4s-10}{2s+1} = \frac{2(2s+1) - 12}{2s+1} = \frac{2s+1 - 6}{2s+1} = \frac{1}{2}$$

$$d(s) = (s+\gamma_2)(s+2)^2 = s^3 + 4.5s^2 + bs + 2$$

$$\begin{aligned} \hat{G}_{sp}(s) &= \frac{1}{s^3 + 4.5s^2 + bs + 2} \begin{bmatrix} -6(s+2)^2 & 3(s+2)(s+\gamma_2) \\ \frac{1}{2}(s+2) & (s+1)(s+\gamma_2) \end{bmatrix} \\ &= \frac{1}{d(s)} \begin{bmatrix} (-6s^2 - 24s - 24) & (3s^2 + 7.5s + 3) \\ (\frac{1}{2}s + 1) & (s^2 + 1.5s + \gamma_2) \end{bmatrix} \\ &= \frac{1}{d(s)} \left( \begin{bmatrix} -6 & 3 \\ 0 & 1 \end{bmatrix} s^2 + \begin{bmatrix} -24 & 7.5 \\ \gamma_2 & 1.5 \end{bmatrix} s + \begin{bmatrix} -24 & 3 \\ 1 & \gamma_2 \end{bmatrix} \right) \end{aligned}$$

The realization is

$$\left\{ \begin{array}{l} \dot{x} = \left[ \begin{array}{cc|cc|cc} -4.5 & 0 & -6 & 0 & -2 & 0 \\ 0 & -4.5 & 0 & -6 & 0 & -2 \\ \hline 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \end{array} \right] x + \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} u \\ y = \left[ \begin{array}{cc|cc|cc} -6 & 3 & -24 & 7.5 & -24 & 3 \\ 0 & 1 & \gamma_2 & 1.5 & 1 & \gamma_2 \end{array} \right] x + \begin{bmatrix} 2 & 0 \\ 0 & 0 \end{bmatrix} u \end{array} \right.$$

$$y = \left[ \begin{array}{cc|cc|cc} -6 & 3 & -24 & 7.5 & -24 & 3 \\ 0 & 1 & \gamma_2 & 1.5 & 1 & \gamma_2 \end{array} \right] x + \begin{bmatrix} 2 & 0 \\ 0 & 0 \end{bmatrix} u$$

## Example (Continued)

2) Look at 1<sup>st</sup> column of  $\hat{G}(s)$ :

$$\hat{G}_1(s) = \begin{bmatrix} \frac{4s-10}{2s+1} \\ \frac{1}{(2s+1)(s+2)} \end{bmatrix} = \begin{bmatrix} \frac{(4s-10)(s+2)}{(2s+1)(s+2)} \\ \frac{1}{(2s+1)(s+2)} \end{bmatrix} = \begin{bmatrix} \frac{4s^2-2s+20}{2s^2+5s+2} \\ \frac{1}{2s^2+5s+2} \end{bmatrix}$$

$$\text{Matlab} \quad n_1 = [4, -2, -20; 0, 0, 1]$$

$$d_1 = [2, 5, 2]$$

$$[A_1, B_1, C_1, D_1] = \text{tf2ss}(n_1, d_1)$$

$$\Rightarrow \begin{cases} \dot{x}_1 = A_1 x_1 + B_1 u_1 = \begin{bmatrix} -2,5 & -1 \\ 1 & 0 \end{bmatrix} x_1 + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u_1 \\ y_1 = C_1 x_1 + D_1 u_1 = \begin{bmatrix} -6 & -12 \\ 0 & 0,5 \end{bmatrix} x_1 + \begin{bmatrix} 2 \\ 0 \end{bmatrix} u_1 \end{cases}$$

Do same for 2<sup>nd</sup> column:

$$\hat{G}_2(s) = \begin{bmatrix} \frac{3}{s+2} \\ \frac{s+1}{(s+2)^2} \end{bmatrix} \quad \text{& use tf2ss}$$

$$\Rightarrow \begin{cases} \dot{x}_2 = A_2 x_2 + B_2 u_2 = \begin{bmatrix} -4 & -4 \\ 1 & 0 \end{bmatrix} x_2 + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u_2 \\ y_2 = C_2 x_2 + D_2 u_2 = \begin{bmatrix} 3 & 6 \\ 1 & 1 \end{bmatrix} x_2 + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u_2 \end{cases}$$

Combine

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} A_1 & 0 \\ 0 & A_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} B_1 & 0 \\ 0 & B_2 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$y = [C_1 \ C_2] x + [D_1 \ D_2] u$$

$$(2) \quad \begin{cases} \dot{x} = \left[ \begin{array}{cc|c} -2,5 & -1 & 0 \\ 1 & 0 & 0 \\ \hline 0 & -4 & -4 \\ 1 & 0 & 1 \end{array} \right] x + \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix} u \\ y = \begin{bmatrix} -6 & -12 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 3 & 6 \\ 1 & 1 \end{bmatrix} x + \begin{bmatrix} 2 & 0 \\ 0 & 0 \end{bmatrix} u \end{cases}$$

Why?

\* BUT not  
algebraically  
equivalent

(1) &amp; (2) zero-state Equivalent b/c same transfer function