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# Overview of the course



### Mechanical Engineering Department

Course coordinator

Dr. Vishal Gupta

**Assistant Professor** 

Mechanical Engineering Department

Course Co-coordinator

Dr. Sachin Singh

**Assistant Professor** 

Mechanical Engineering Department

### Electronics and Communication Engineering Department

**Course Coordinator** 

Dr. Poonam Verma

**Assistant Professor** 

Electronics and Communication Engineering Department



## ENGINEERING DESIGN PROJECT-I UTA016

## Lecture - 2

# Instructional objective



- Study of the dynamics for the Mangonal
- ➤ No DRAG Condition (Part 1)
- ➤ With DRAG









# No DRAG Condition

# Objective





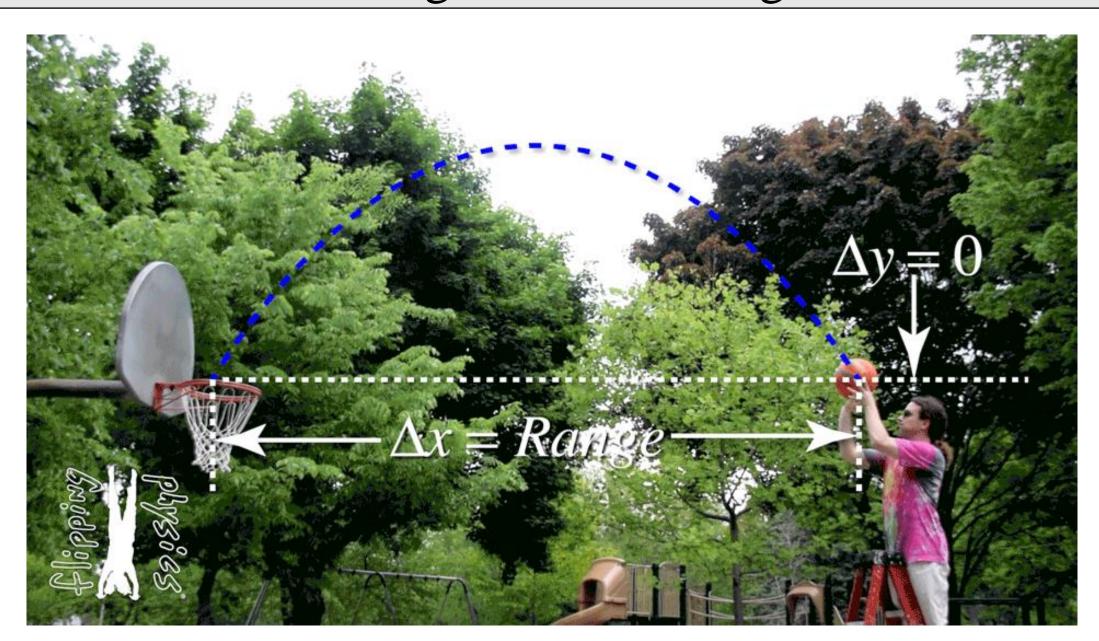
A Smaller version!



A larger version!

# Challenges in Modelling



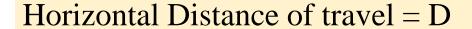


# Challenges in Modelling



- For a given "size", can we maximise the distance?
- What are the key parameters that control the distance?
- Can we formulate a model that will help us design our Mangonel?

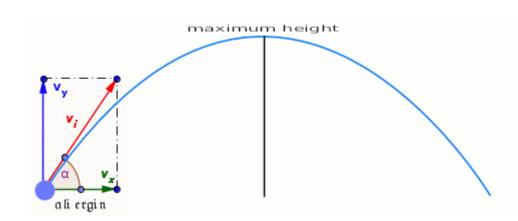
$$D = \frac{v^2 \sin 2\theta}{g}$$

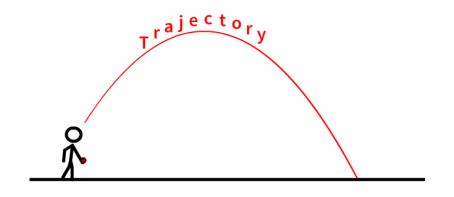


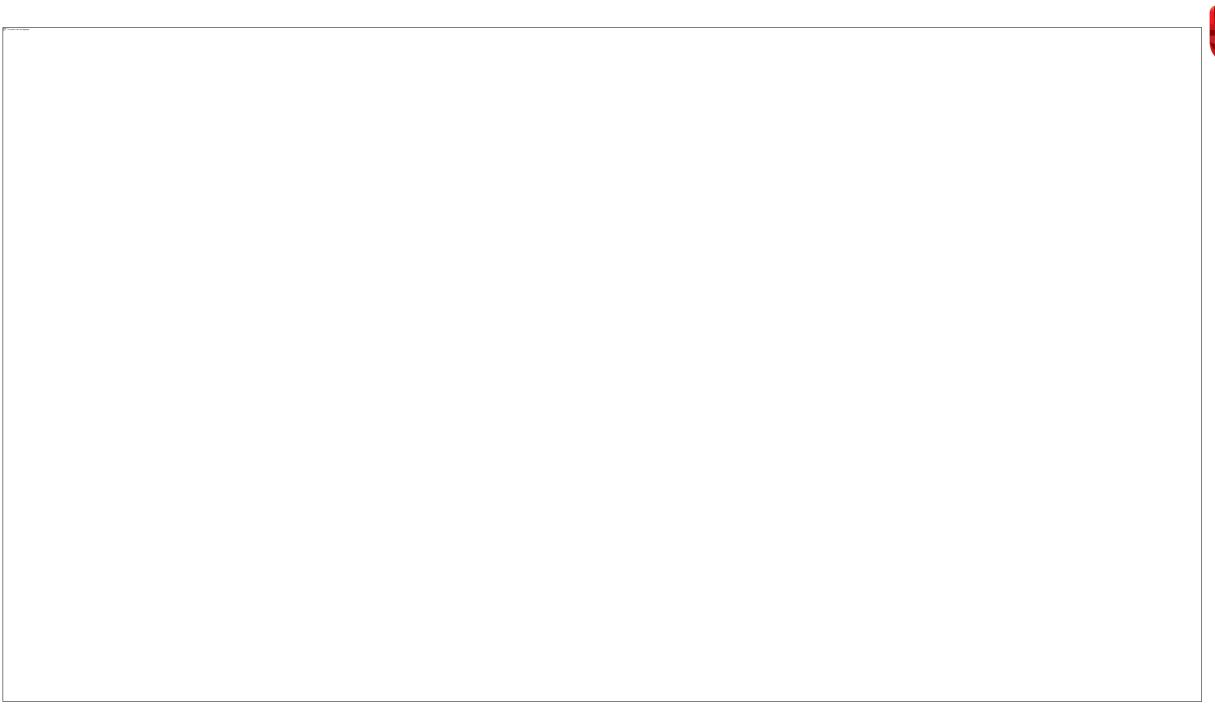
Launch Velocity = v

Angle of launch =  $\theta$ 

Acceleration due to gravity = g









## Equation of Motion



**Speed=distance/time** 

**Acceleration=velocity/time** 

$$s=ut+1/2at^2$$

$$v^2 = u^2 + 2as$$

u=initial velocity

v=final velocity

t=time duration

a=acceleration

s=distance travelled

### One Dimensional Motion

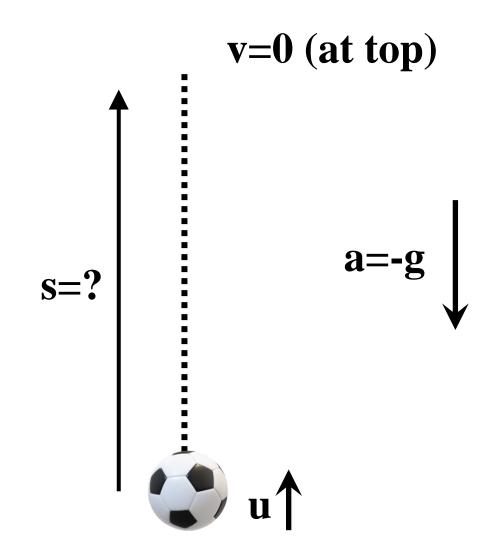


Example 1: (1-D)

Use equation:

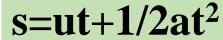
$$v^2 = u^2 + 2as$$

$$s=u^2/2g$$



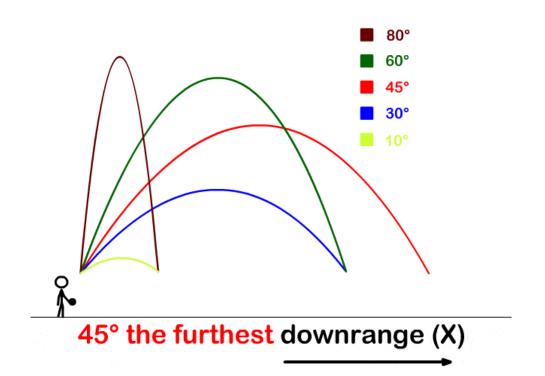
### Two Dimensional Motion: Dynamics

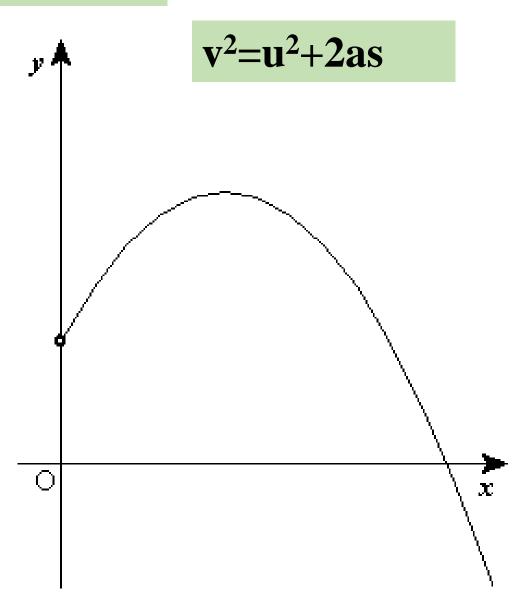




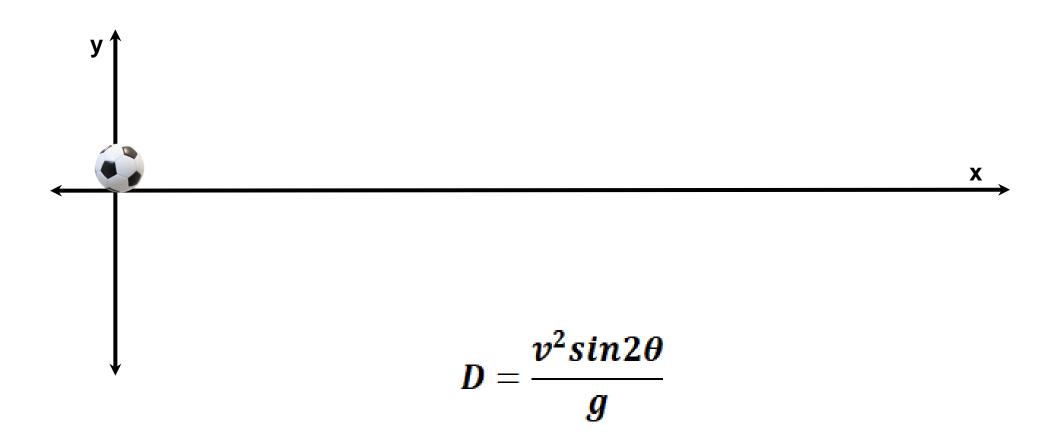


- Can we use the three equations to model the trajectory of the missile?
- Can we predict the distance?

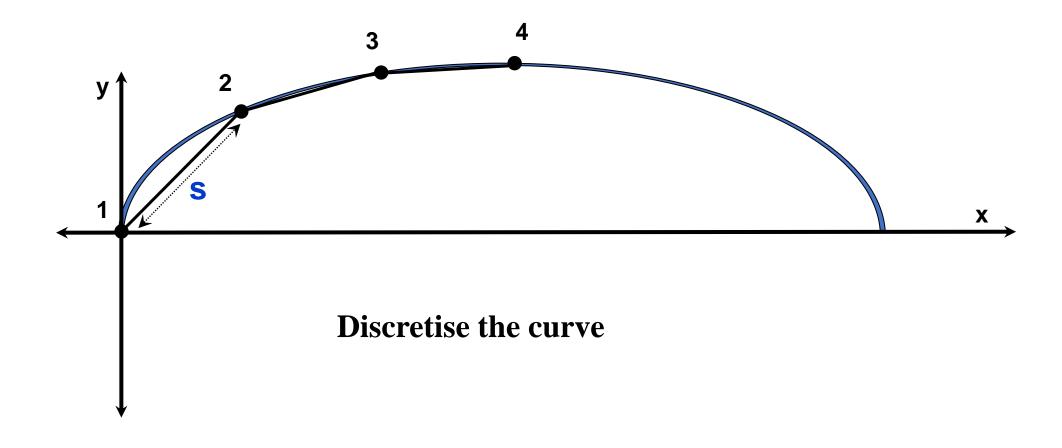




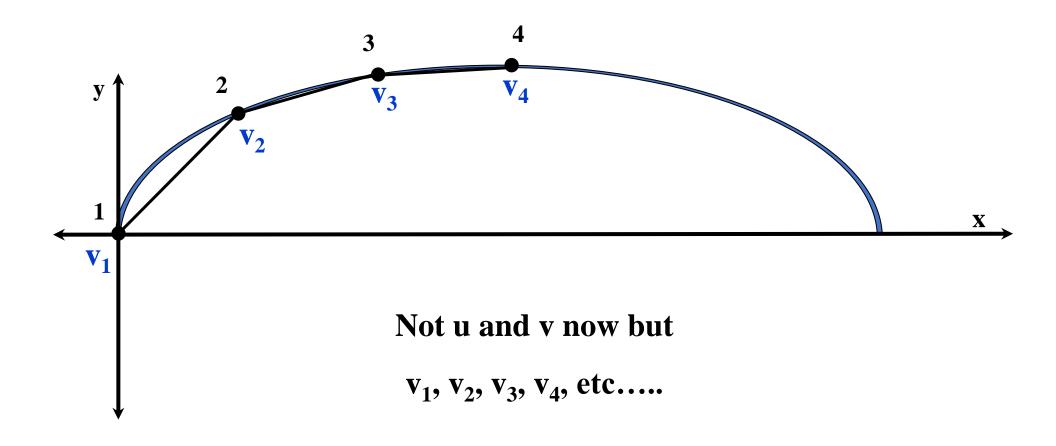




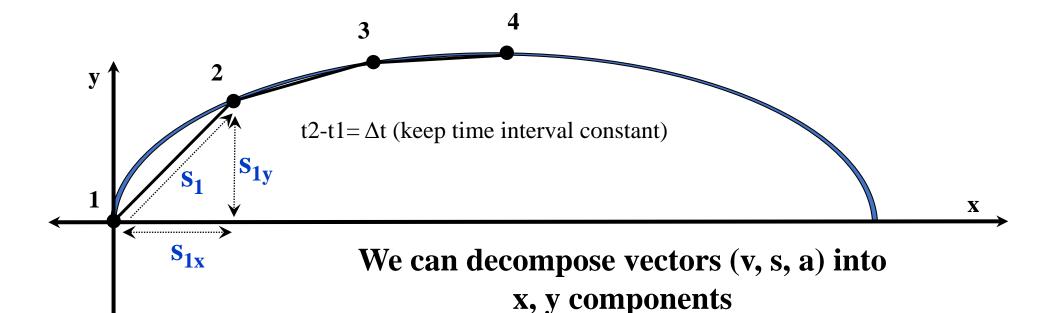












#### v=u+at becomes:

$$\bullet V_{x2} = V_{x1} + a_{x1} \Delta t$$

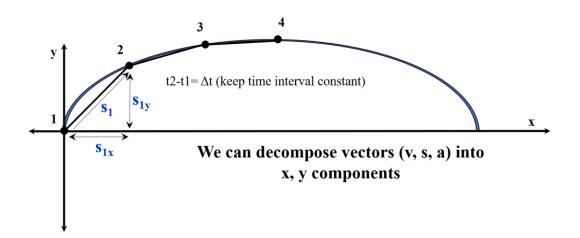
$$\bullet \mathbf{V}_{y2} = \mathbf{v}_{y1} + \mathbf{a}_{y1} \Delta \mathbf{t}$$

$$S = ut + 1/2at^2$$
 becomes:

$$\bullet \Delta s_x = v_{x1} \Delta t + 1/2 a_{x1} \Delta t^2$$

$$\bullet \Delta s_y = v_{y1} \Delta t + 1/2 a_{y1} \Delta t^2$$





v=u+at becomes:

$$\bullet v_{x2} = v_{x1} + a_{x1} \Delta t$$

$$\bullet v_{x2} = v_{x1} + a_{x1} \Delta t$$

$$\bullet v_{y2} = v_{y1} + a_{y1} \Delta t$$

s=ut+1/2at<sup>2</sup> becomes:

$$\bullet \Delta s_x = v_{x1} \Delta t + 1/2 a_{x1} \Delta t^2$$

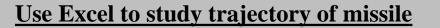
$$\bullet \Delta s_y = v_{y1} \Delta t + 1/2 a_{y1} \Delta t^2$$

Acceleration is constant (for no drag of lift – we'll return to this point later)

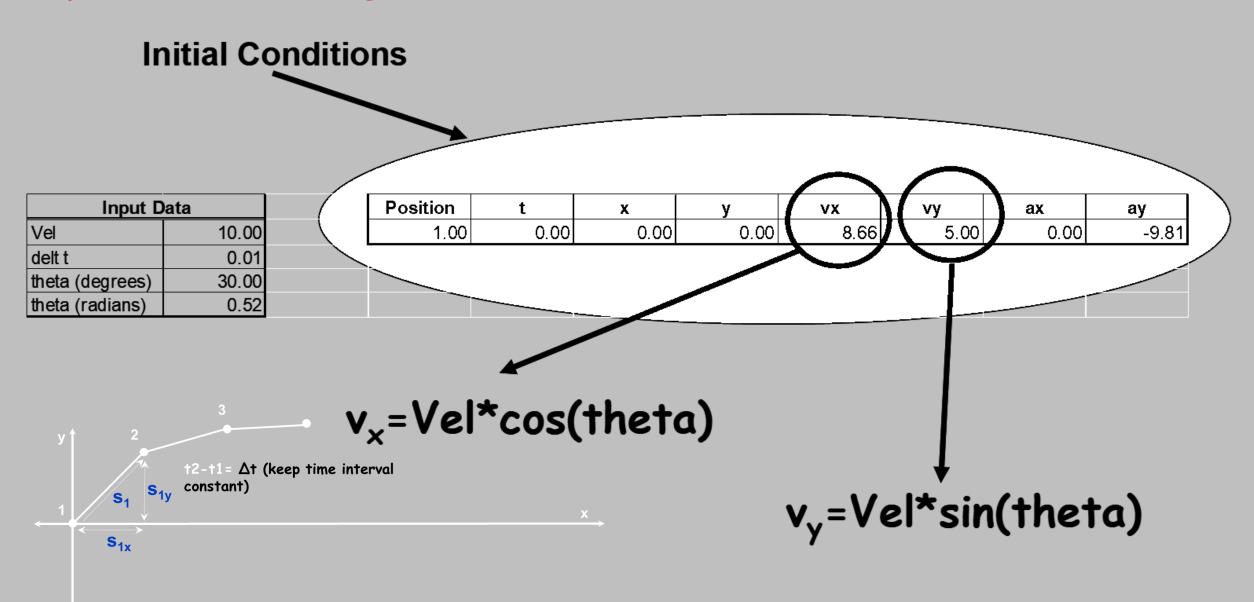
$$ax=0!$$

t2-t1=  $\Delta t$  (keep time interval constant)

## Dynamics - Assignment1

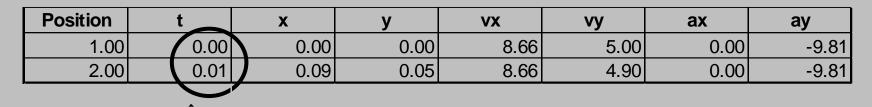


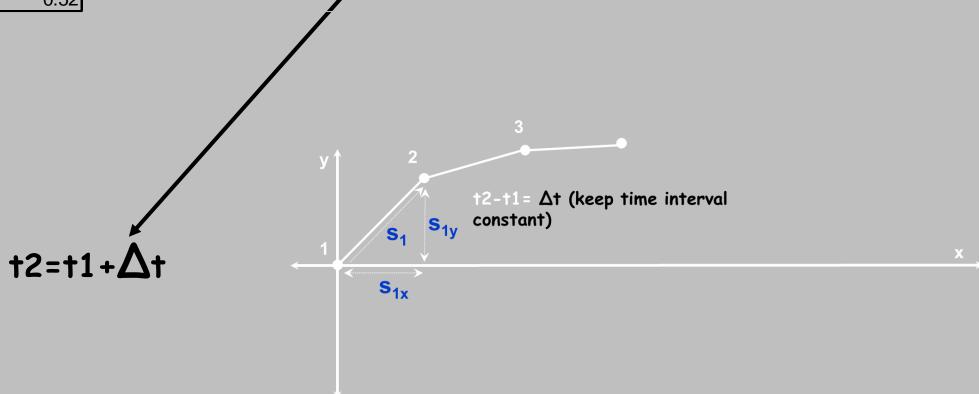






Input Data					
Vel	10.00				
delt t	0.01				
theta (degrees)	30.00				
theta (radians)	0.52				

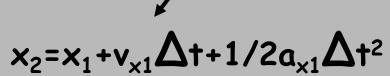


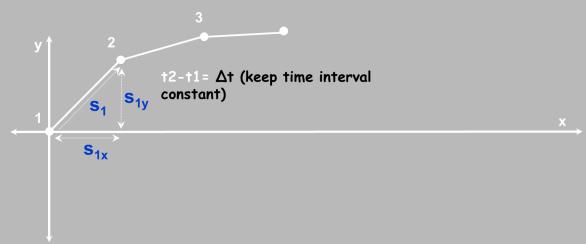




Input Data						
Vel	10.00					
delt t	0.01					
theta (degrees)	30.00					
theta (radians)	0.52					

Position	t	Х	у	VX	vy	ax	ay
1.00	0.00	0.0	0.00	8.66	5.00	0.00	-9.81
2.00	0.01	0.0	0.05	8.66	4.90	0.00	-9.81



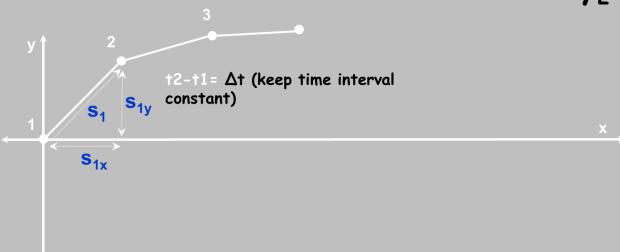




Input Data						
Vel	10.00					
delt t	0.01					
theta (degrees)	30.00					
theta (radians)	0.52					

Position	t	Х	у	VX	vy	ax	ay
1.00	0.00	0.00	0.00	8.66	5.00	0.00	-9.81
2.00	0.01	0.09	0.05	8.66	4.90	0.00	-9.81

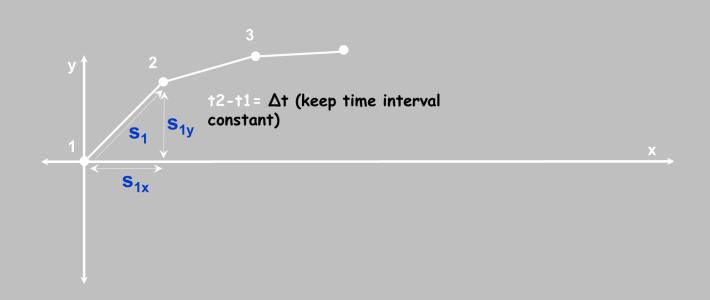
$$y_2 = y_1 + v_{y1} \Delta t + 1/2 \alpha_{y1} \Delta t^2$$





Input Data						
Vel	10.00					
delt t	0.01					
theta (degrees)	30.00					
theta (radians)	0.52					

Position	t	X	у	VX	vy	ax	ay
1.00	0.00	0.00	0.00	8.66	5.00	0.00	-9.81
2.00	0.01	0.09	0.05	8.66	4.90	0.00	-9.81
		V <sub>×2</sub>	<sub>2</sub> =ν <sub>×1</sub> +α,	×1Δt			

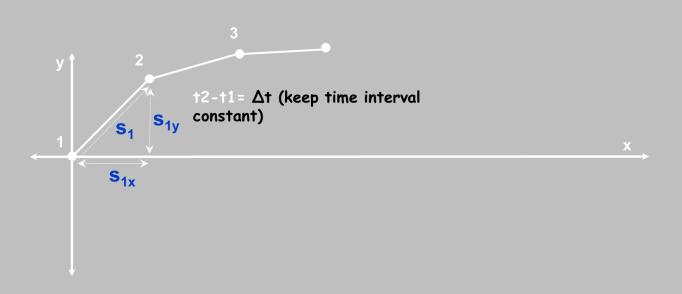




Input Data						
Vel	10.00					
delt t	0.01					
theta (degrees)	30.00					
theta (radians)	0.52					

Position	t	X	у	VX	vy	ax	ay
1.00	0.00	0.00	0.00	8.66	5.00	0.00	-9.81
2.00	0.01	0.09	0.05	8.66	4.90	0.00	-9.81
					·		

 $v_{y2}=v_{y1}+a_{y1}\Delta t$ 

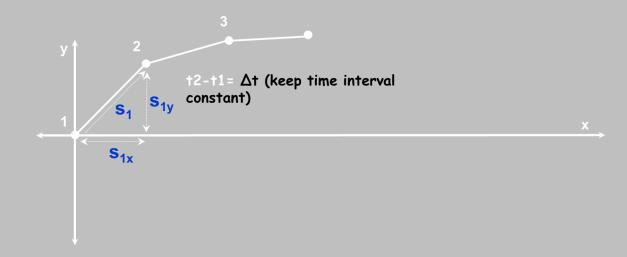




Input Data						
Vel	10.00					
delt t	0.01					
theta (degrees)	30.00					
theta (radians)	0.52					

Position	t	X	у	VX	vy	ax	ay
1.00	0.00	0.00	0.00	8.66	5.00	0.00	-9.81
2.00	0.01	0.09	0.05	8.66	4.90	0.00	-9.81
						$\sim$	



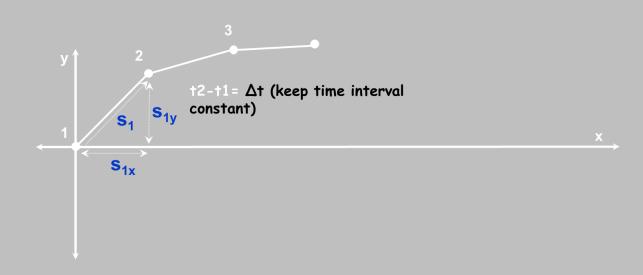




Input Data					
Vel	10.00				
delt t	0.01				
theta (degrees)	30.00				
theta (radians)	0.52				

Positio	n	t	X	у	VX	vy	ax	ay
1.	00	0.00	0.00	0.00	8.66	5.00	0.00	-9.81
2.	00	0.01	0.09	0.05	8.66	4.90	0.00	-9.81
								$\overline{}$







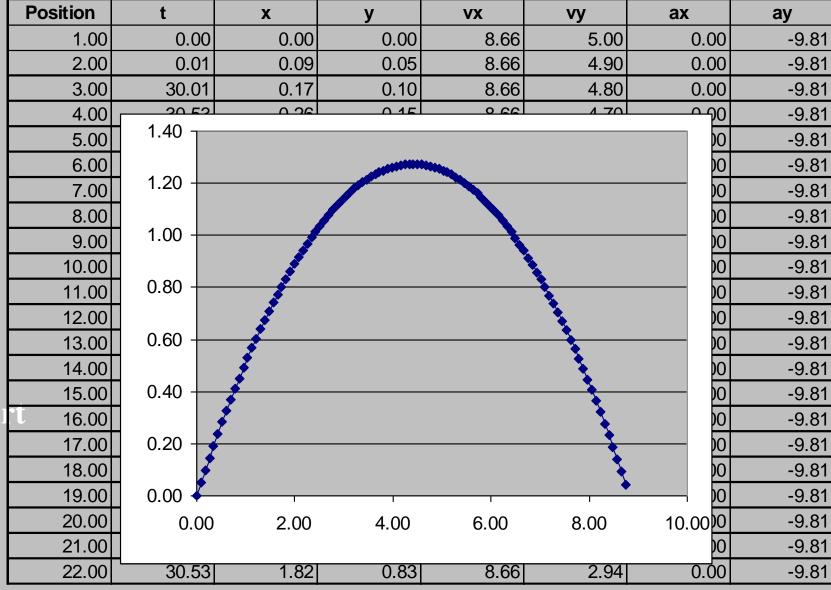
Input Data					
Vel	10.00				
delt t	0.01				
theta (degrees)	30.00				
theta (radians)	0.52				

Position	t	Х	у	VX	vy	ax	ay
1.00	0.00	0.00	0.00	8 66	5.00	0.00	-9.81
2.00	0.01	0.09	0.05	8.66	4.90	0.00	-9.81
3.00	0.02	0.17	0.10	8.66	4.80	0.00	-9.81
4.00	0.03	0.26	0.15	8.66	4.70	0.00	-9.81
5.00	0.04	0.35	0.19	8.66	4.61	0.00	-9.81
6.00	0.05	0.43	0.24	8.66	4.51	0.00	-9.81
7.00	0.06	0.52	0.28	8.66	4.41	0.00	-9.81
8.00	0.07	0.61	0.33	8.66	4.31	0.00	-9.81
9.00	0.08	0.69	0.37	8.66	4.21	0.00	-9.81
10.00	0.09	0.78	0.41	8.66	4.11	0.00	-9.81
11.00	0.10	0.87	0.45	8.66	4.02	0.00	-9.81
12.00	0.11	0.95	0.49	8.66	3.92	0.00	-9.81
13.00	0.12	1.04	0.53	8.66	3.82	0.00	-9.81
14.00	0.13	1.13	0.57	8.66	3.72	0.00	-9.81
15.00	0.14	1.21	0.60	8.66	3.62	0.00	-9.81
16.00	0.15	1.30	0.64	8.66	3.53	0.00	-9.81
17.00	0.16	1.39	0.67	8.66	3.43	0.00	-9.81
18.00	0.17	1.47	0.71	8.66	3.33	0.00	-9.81
19.00	0.18	1.56	0.74	8.66	3.23	0.00	-9.81

Copy formula down



Input Data				
Vel	10.00			
delt t	0.01			
theta (degrees)	30.00			
theta (radians)	0.52			



Plot x versus y using chart wizard

## Assignment1



#### Mangonel Dynamics Design Tool using Excel

Work in groups and/or individually in computer rooms today and during week to

- 1.Create excel spreadsheet as demonstrated
- 2.Plot x versus y
- 3. Study effect of changing velocity
- 4. Study effect of changing angle

An assignment will be set based on this work. Assignment to be submitted individually – no copying!



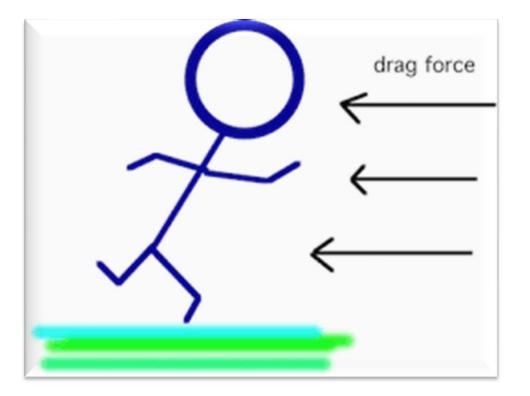
# With DRAG Condition

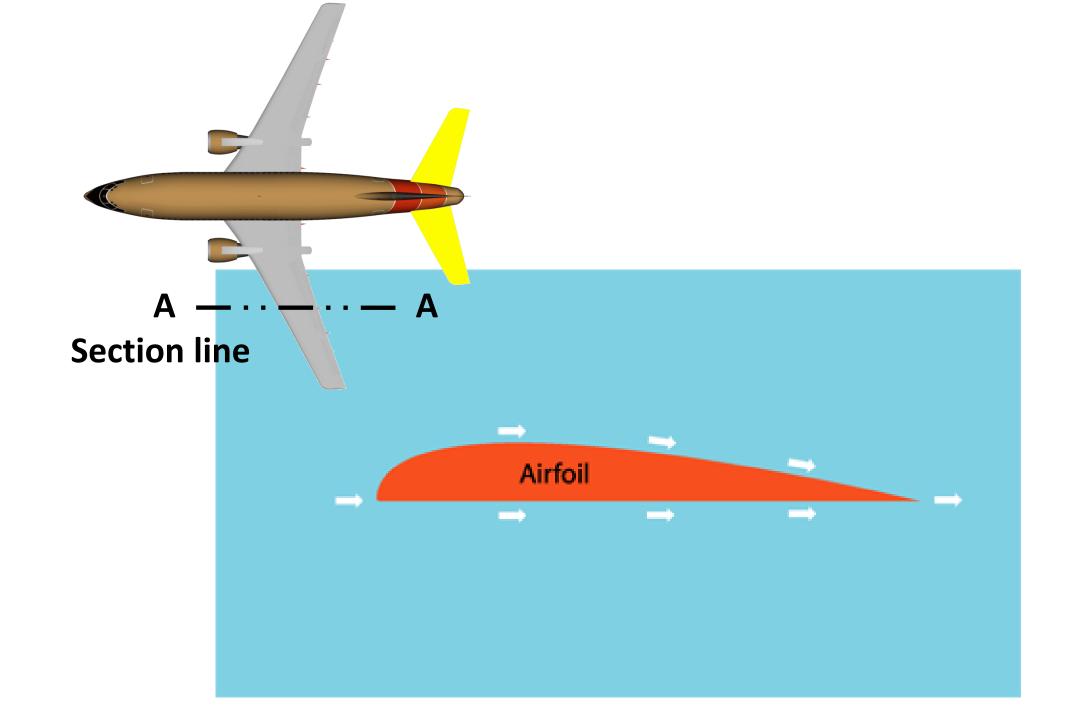
# Drag force



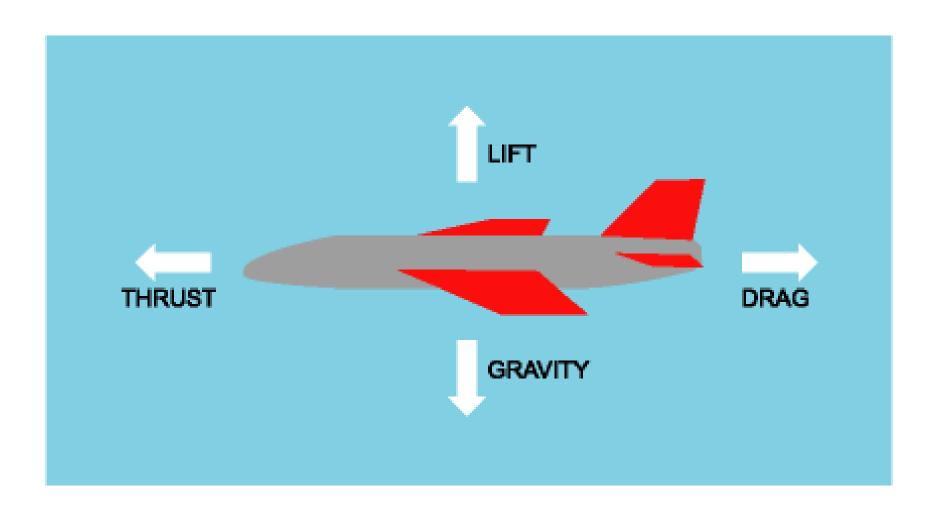
A drag force is the resistance force caused by the motion of a body through a fluid, such as water or air. A drag force acts opposite to the direction of the oncoming flow velocity







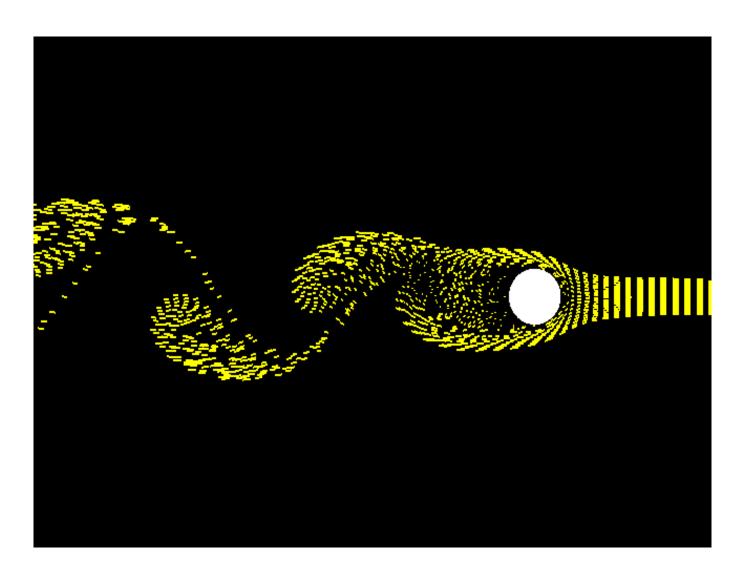








**Golf ball** 



## Drag on a Smooth ball





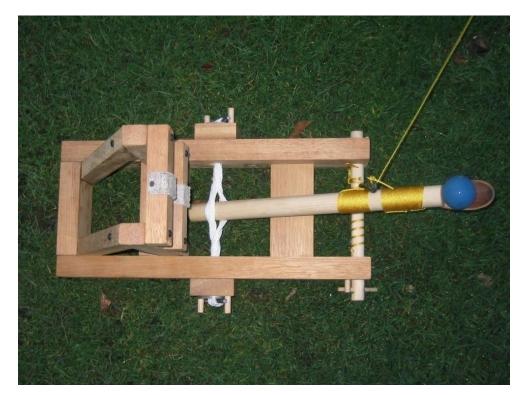


Drag on a ball with dimple



The "projectile" which our Mangonel will fire will be a squash-ball which is spherical See fig 1.





<u>a.</u>

<u>b.</u>

Fig 1. Prototype of our Mangonel!

## Factors that control drag

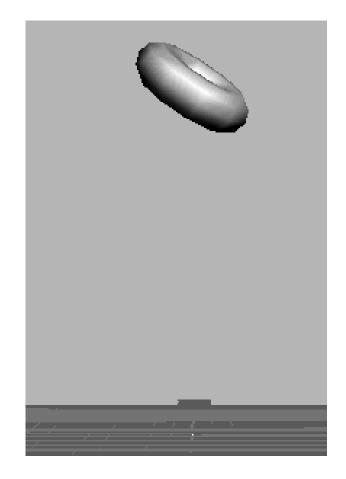


Drag reduces the distance travelled by the ball before it hits the ground.

- What are the factors that control drag? and
- How can you reduce it?

If you can reduce drag then your object will travel further!



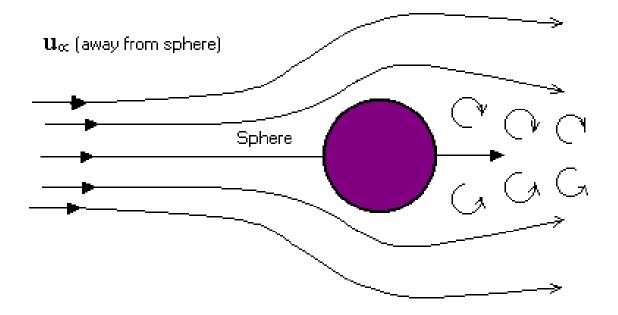


## Empirical formula of drag



The equation that expresses the drag force  $(F_d)$  experienced by an object moving in air is:

 $F_d=1/2 \rho A V^2 C_d$ 

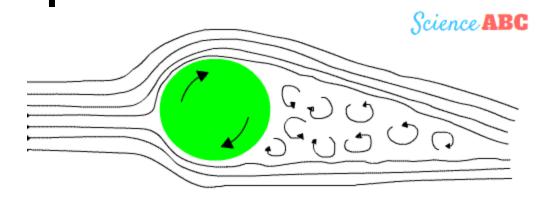


 $\rho$  =Density of air

A =Projected area of the body

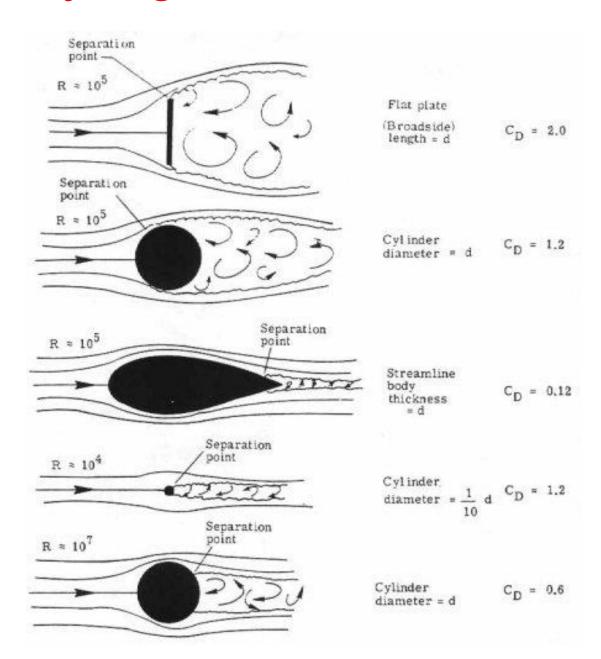
V = Velocity of the body

C<sub>d</sub> =Drag Coefficient



### Empirical formula of drag







$$F_d=1/2 \rho A V^2 Cd$$

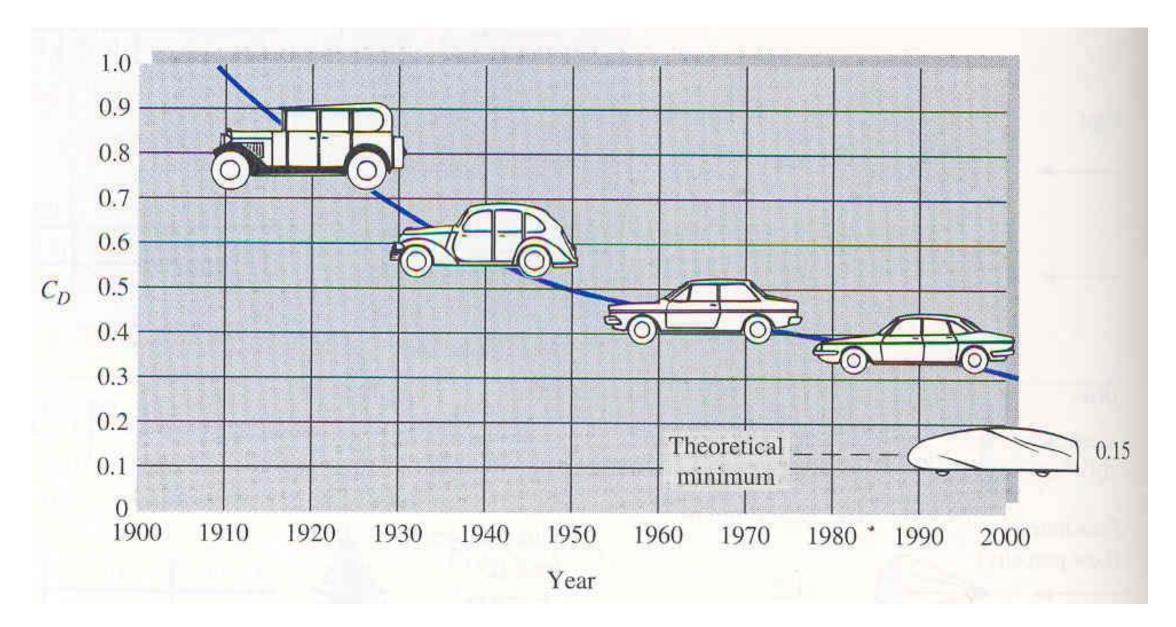
So, we see the drag force increases with size (A) and velocity  $(V^2)$ .

It makes sense to reduce the size but what about the velocity?

If we reduce the velocity the drag force reduces but the missile wont go as far!

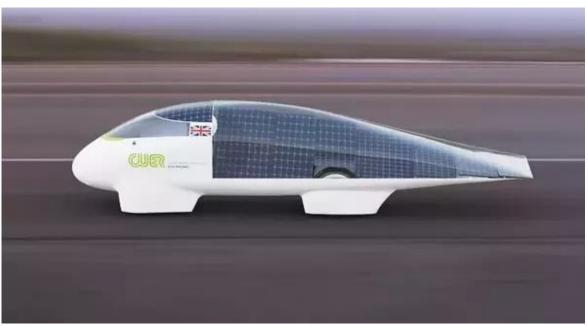
# Concept of darg











### Acceleration due to drag



Newton's 2<sup>nd</sup> Law

$$F_d=1/2 \rho A V^2 C_d=ma_d$$

$$a_d = 1/(2m) C_d \rho A V^2$$

#### The magnitude of the acceleration is thus expressed

$$\begin{vmatrix} a_d \end{vmatrix} = \frac{1}{(2m)} C_d \rho A (v_x^2 + v_y^2)$$
Constant (k)

Thus

$$\mathbf{a}_{xd} = \mathbf{a}_{d} \operatorname{Cos}(\beta)$$

$$a_{yd} = a_d \operatorname{Sin}(\beta)$$

$$a_{xd} = k (v_x^2 + v_y^2) Cos(\beta)$$

$$a_{yd} = k (v_x^2 + v_y^2) Sin(B)$$

$$a_x$$
=0-k  $(v_x^2+v_y^2)$  Cos(ß) and  $a_y$ =-9.81-k  $(v_x^2+v_y^2)$  Sin(ß) where 
$$\beta = tan^{-1}(v_y/v_x)$$





ta		Position	t	X	у	VX	vy	beta [rads]	cos(beta)	sin(beta)	ax	ay
	Change to see											
15.00	impact!!!!	1.00	0.00	0.00	0.00	7.51	12.99	1.04667	0.50046	0.86576	-0.85919	-11.29633
0.01		2.00	0.01	0.08	0.13	7.50	12.87	1.04337	0.50331	0.86411	-0.85237	-11.27338
	Change to see											
60.00	impact!!!!	3.00	0.02	0.15	0.26	7.49	12.76	1.04003	0.50619	0.86242	-0.84559	-11.25067
1.05		4.00	0.03	0.22	0.38	7.48	12.65	1.03666	0.50910	0.86071	-0.83886	-11.22820
		5.00	0.04	0.30	0.51	7.47	12.54	1.03323	0.51204	0.85896	-0.83217	-11.20597
		6.00	0.05	0.37	0.64	7.46	12.42	1.02977	0.51502	0.85718	-0.82552	-11.18397
		7.00	0.06	0.45	0.76	7.46	12.31	1.02626	0.51802	0.85537	-0.81892	-11.16220
		8.00	0.07	0.52	0.88	7.45	12.20	1.02270	0.52106	0.85352	-0.81236	-11.14067
		9.00	0.08	0.60	1.00	7.44	12.09	1.01910	0.52413	0.85164	-0.80584	-11.11937
ta		10.00	0.09	0.67	1.12	7.43	11.98	1.01545	0.52723	0.84972	-0.79936	-11.09829
	The value at											
	atmospheric											
1.20	conditions	11.00	0.10	0.75	1.24	7.42	11.87	1.01176	0.53037	0.84777	-0.79292	-11.07744
	This is a typical											
	value, however											
	try and change											
0.40	it!	12.00	0.11	0.82	1.36	7.42	11.76	1.00802	0.53354	0.84577	-0.78653	-11.05682
	Change to see											
0.050	impact!!!!	13.00	0.12	0.89	1.48	7.41	11.65	1.00422	0.53674	0.84375	-0.78018	-11.03642
	Change to see											
0.045	impact!!!!	14.00	0.13	0.97	1.59	7.40	11.54	1.00038	0.53998	0.84168	-0.77387	-11.01624
0.0016		15.00	0.14	1.04	1.71	7.39	11,42	0.99649	0.54325	0.83957	-0.76760	-10.99628
0.01		16.00	0.15	1.12	1.82	7.38	11.31	0.99254	0.54656	0.83742	-0.76137	-10.97654
	15.00 0.01 60.00 1.05 ta 1.20 0.40 0.050 0.045 0.0016	Change to see impact!!!!  1.05  Change to see impact!!!!  1.05  The value at atmospheric conditions This is a typical value, however try and change it!  Change to see impact!!!!  Change to see impact!!!!  Change to see impact!!!!	Change to see   impact!!!!	Change to see impact!!!! 1.00 0.00 0.01 2.00 0.01 Change to see impact!!!! 3.00 0.02 1.05 4.00 0.03 5.00 0.04 6.00 0.05 7.00 0.06 8.00 0.07 9.00 0.08 ta 10.00 0.09 The value at atmospheric 1.20 conditions 11.00 0.10 This is a typical value, however try and change 0.40 it! 12.00 0.11 Change to see 0.055 impact!!!! 13.00 0.12 Change to see 0.045 impact!!!! 14.00 0.13 0.0016 15.00 0.14	Change to see impact!!!! 1.00 0.00 0.00 0.00 0.01 0.01 2.00 0.01 0.08 Change to see impact!!!! 3.00 0.02 0.15 1.05 4.00 0.03 0.22 5.00 0.04 0.30 6.00 0.05 0.37 7.00 0.06 0.45 8.00 0.07 0.52 8.00 0.07 0.52 9.00 0.08 0.60 impact!!! 12.00 0.10 0.75 This is a typical value, however try and change 0.40 it! 12.00 0.11 0.82 Change to see 0.050 impact!!!! 13.00 0.12 0.89 0.0016 14.00 0.13 0.97 0.0016 15.00 0.14 1.04	Change to see impact!!!!	Change to see   15.00   1.00   0.00   0.00   0.00   7.51     O.01   2.00   0.01   0.08   0.13   7.50     Change to see   60.00   impact!!!!   3.00   0.02   0.15   0.26   7.49     1.05   4.00   0.03   0.22   0.38   7.48     1.05   5.00   0.04   0.30   0.51   7.47     6.00   0.05   0.37   0.64   7.46     7.00   0.06   0.45   0.76   7.46     8.00   0.07   0.52   0.88   7.45     9.00   0.08   0.60   1.00   7.44     1a   The value at atmospheric   1.20   conditions   11.00   0.10   0.75   1.24   7.42     This is a typical value, however try and change   0.40   it   12.00   0.11   0.82   1.36   7.42     Change to see   0.050   impact!!!!   13.00   0.12   0.89   1.48   7.41     Change to see   0.045   impact!!!!   14.00   0.13   0.97   1.59   7.40     0.0016   15.00   0.14   1.04   1.71   7.39	Change to see 15.00 impact!!!  0.01  Change to see 60.00 impact!!!  1.00  0.00  0.00  0.00  0.00  7.51  12.99  0.01  Change to see 60.00 impact!!!  3.00  0.02  0.15  0.26  7.49  12.76  1.05  4.00  0.03  0.22  0.38  7.48  12.65  5.00  0.04  0.30  0.51  7.47  12.54  6.00  0.05  0.37  0.64  7.46  12.31  8.00  0.07  0.52  0.88  7.45  12.20  9.00  0.08  0.60  1.00  7.44  12.09  10.00  10.00  10.00  10.00  11.0	Change to see 15.00 impact!!!! 1.00 0.00 0.00 0.00 7.51 12.99 1.04667 0.01 2.00 0.01 0.08 0.13 7.50 12.87 1.04337  Change to see 60.00 impact!!!! 3.00 0.02 0.15 0.26 7.49 12.76 1.04003 1.05 4.00 0.03 0.22 0.38 7.48 12.65 1.03666 5.00 0.04 0.30 0.51 7.47 12.54 1.03323 6.00 0.05 0.37 0.64 7.46 12.42 1.02977 7.00 0.06 0.45 0.76 7.46 12.31 1.02626 8.00 0.07 0.52 0.88 7.45 12.20 1.02270 9.00 0.08 0.60 1.00 7.44 12.09 1.01910 ta  The value at atmospheric 1.20 conditions 11.00 0.10 0.75 1.24 7.42 11.87 1.01176 This is a typical value, however try and change 0.40 it! 12.00 0.11 0.82 1.36 7.42 11.76 1.00802 Change to see 0.050 impact!!! 13.00 0.12 0.89 1.48 7.41 11.65 1.00422 Change to see 0.045 impact!!! 14.00 0.13 0.97 1.59 7.40 11.54 1.0038 0.0016	Change to see   1.00   0.00   0.00   0.00   7.51   12.99   1.04667   0.50046	Change to see   15.00	Change to see   1.00   0.00   0.00   0.00   7.51   12.99   1.04667   0.50046   0.86576   -0.85919   0.01   0.01   0.02   0.01   0.08   0.13   7.50   12.87   1.04337   0.50331   0.86411   -0.85237   0.01   0.05

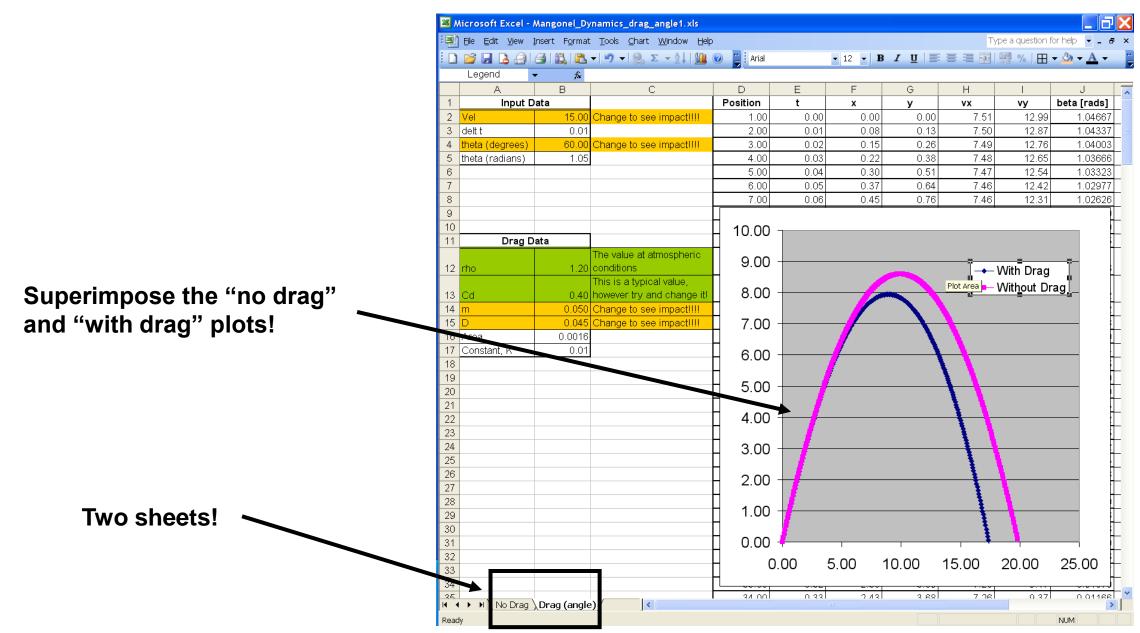




Innut Da	4-0		Dooltien	1			1.07		bata [vasl-1	/b-t-\	ein/bets	0.4	-
Input Da	ta		Position	t	Х	у	VX	vy	beta [rads]	cos(beta)	sin(beta)	ax	ay
		Change to see											
Vel		impact!!!!	1.00	0.00	0.00	0.00	7.51	12.99	1.04667	0.50046	0.86576	+	-11.29633
delt t	0.01		2.00	0.01	0.08	0.13	7.50	12.87	1.04337	0.50331	0.86411	-0.85237	-11.27338
		Change to see											
theta (degrees)		impact!!!!	3.00	0.02	0.15	0.26	7.49			0.50619			-11.25067
theta (radians)	1.05		4.00	0.03	0.22	0.38	7.48	12.65	1.03666	0.50910		-0.83886	-11.22820
			5.00	0.04	0.30	0.51	7.47	12.54	1.03323	0.51204	0.85896	-0.83217	-11.20597
			6.00	0.05	0.37	0.64	7.46	12.42	1.02977	0.51502	0.85718	-0.82552	-11.18397
			7.00	0.06	0.45	0.76	7.46	12.31	1.02626	0.51802	0.85537	-0.81892	-11.16220
			8.00	0.07	0.52	0.88	7.45	12.20	1.02270	0.52106	0.85352	-0.81236	-11.14067
			9.00	0.08	0.60	1.00	7.44	12.09	1.01910	0.52413	0.85164	-0.80584	-11.11937
Drag Da	ta		10.00	0.09	0.67	1.12	7.43	11.98	1.01545	0.52723	0.84972	-0.79936	-11.09829
		The value at											
		atmospheric											
rho	1.20	conditions	11.00	0.10	0.75	1.24	7.42	11.87	1.01176	0.53037	0.84777	-0.79292	-11.07744
		This is a typical											
		value, however											
		try and change											
Cd	0.40		12.00	0.11	0.82	1.36	7.42	11.76	1.00802	0.53354	0.84577	-0.78653	-11.05682
		Change to see											
m	0.050	impact!!!!	13.00	0.12	0.89	1.48	7.41	11.65	1.00422	0.53674	0.8437	-0.78018	-11.03642
		Change to see				_							
D	0.045	impact!!!!	14.00	0.13	0.97	1.59	7.40	11.54	1.00038	0.53998	0.84168	-0.77387	-11.01624
Area	0.0016		15.00	0.14	1.04	1.71	7.39	11.42	0.99649	0.54325	0.83957		-10.99628
Constant, K	0.01		16.00		1.12	1.82	7.38			0.54656	0.83742		-10.97654
,													









Type a question for help 🔻 💄 🗗 🗙

12.99

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beta [rads]

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5.00 0.30 12.54 0.04 0.51 7.47 1.03323 6.00 0.05 0.64 7.46 1.02977 7.00 0.76 12.31 1.02626 10 10.00 Drag Data The value at atmospheric 9.00 12 rho 1 20 conditions → With Drag This is a typical value, Plot Area - Without Drag 8.00 13 Cd 0.40 however try and change it! 0.050 Change to see impact!!!! 15 E 0.045 Change to see impact!!!! 7.00 0.0016 17 Constant, k 0.01 6.00 Adjust  $C_d$ , mass and the diameter 18 19 5.00 20 the see effect as well as the initial 21 4.00 22 velocity and launch angle! 23 24 3.00 25 26 2.00 27 28 1.00 29 30 0.00 31 32 10.00 15.00 20.00 0.00 25.00 33 34 0.27 0.01166

No Drag Drag (angle)

0.01

60.00

Legend

5 theta (radians)

3 delt t

Input Data

| **(1)** | **(1)** | **(2)** | **(3)** | **(3)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(4)** | **(** 

15.00 Change to see impact!!!!

Change to see impact!!!!

Arial

Position

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2.00

3.00

4.00

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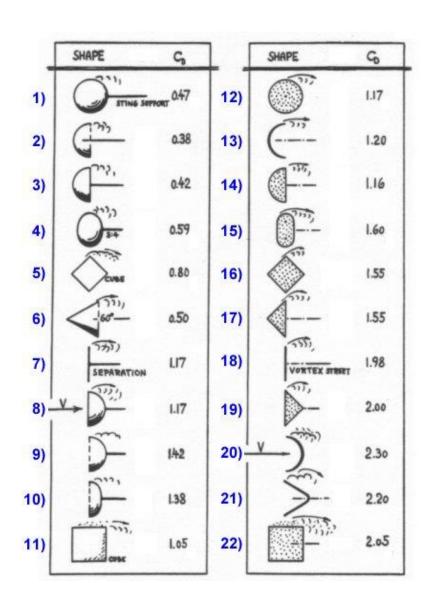
0.01

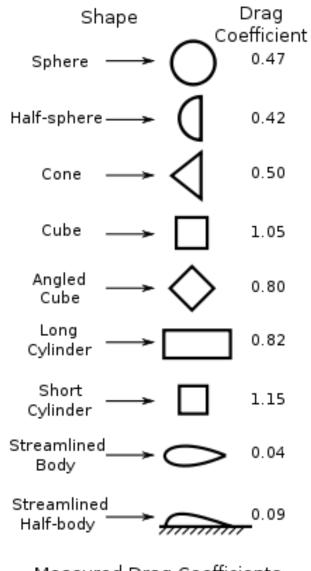
0.02

0.03



Object Air Velocity	Shape	c <sub>D</sub>	
	<b>A</b>		
Parachute		1.35	
Flat plate ———— (Square)		1.17	
Flat top tractor → #	00 00	0.99*	
High roof sleeper (van trailer at 18" gap)		0.60**	
Cone (60°)	$\langle \!                                   $	0.51	
Hemisphere		0.41	
Thunderbird (1984 Ford)		0.35	
Cone (30°) —	307	0.34	
Sphere —	$\bigcirc$	0.10	
Airfoil — (	$\rightarrow$	0.05	





Measured Drag Coefficients





		Cr	m kg	C.	A m²	km/h	V <sub>750</sub> km/h
Traditionele fiets	\$	0,006	90	1,1	0,51	18	44
Racefiets	A.	0,003	81	0,88	0,36	24	55
Tandem	_TTO	0,0045	163	1,0	0,48	25	59
Superfiets HPV		0,006	90	0,10	0,44	40	102
Perfect streamliner	0.0	-		0,05	0,13	94	203
"Motor Pacing"	50	0,006	91			47	470
"Moon Bike"	<b>%</b>	0,0045	90			382	3820



### What causes drag?

The drag force is due to pressure losses caused by recirculation of flow. Simply put; eddies and vortices which are caused by abrupt changes in geometry.

In figure 3, although much smaller, the cylinder experiences the same drag force as the much larger but more aerodynamic airfoil. This is due to the relatively greater amount of "turbulence" in the wake.

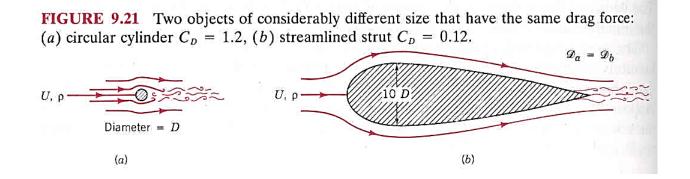


Fig 3.



