| Introduction to Fatigue |
|---|
| S- static loading (Failure theories) - slow speeds - light loads - large factor of safety |
| - Dynamic loading [Fatigue] - fast speeds - high loeds - low factor of safety industrial revolution e.g. steam engine, water-wheel, turbines |
| Fatigue - repeated high/low stresses |
| - failure occurs at much lower strength (lower ham yield strength) |
| - Failure due to cyclic stresses is Fatigue Failure. |

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Fatigne - Life methods

The goal is to predict the number of agels to failure for a specific level of loading

Methods

- Strain-Life method: Uses crack cyles nucleation (growth) to predict failure n
- Dinear elastic fracture mechanics

 THEORY Uses crack propagation to predict failure

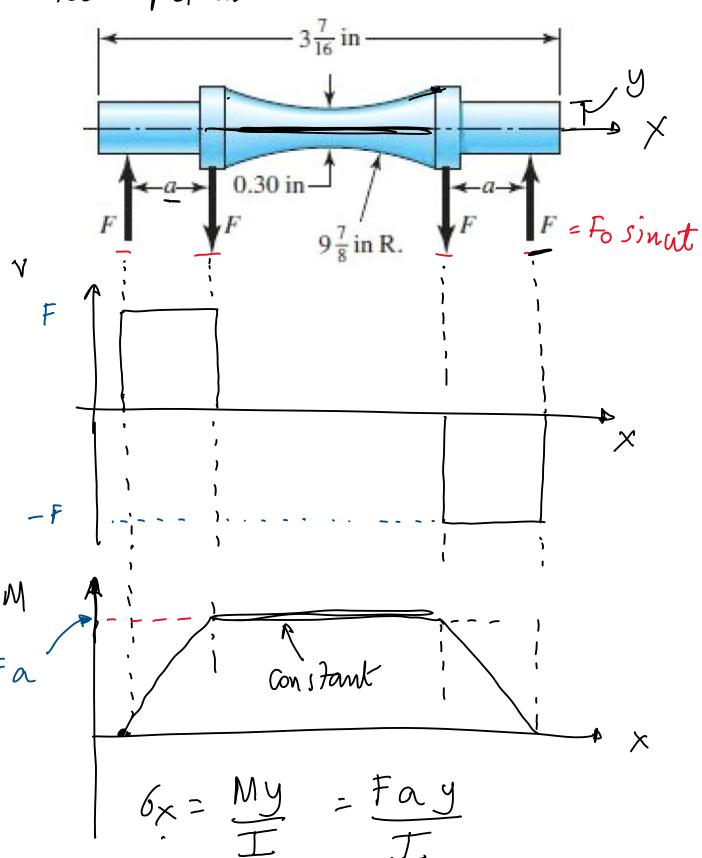
 DRZVEN Cycles

3) Stress-Life method: Uses emperical tests on test specimens to predict failure cycles [DATA DRIVEN]

0, 2 - Advanced Solid Mechanics
3 - We will use this approach

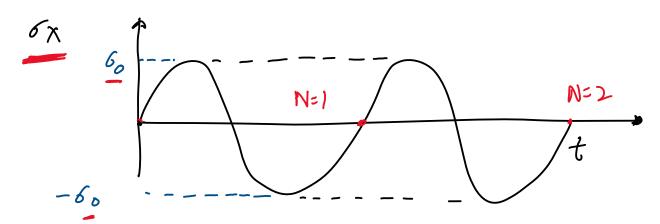
Fatigue Test

Test specimen



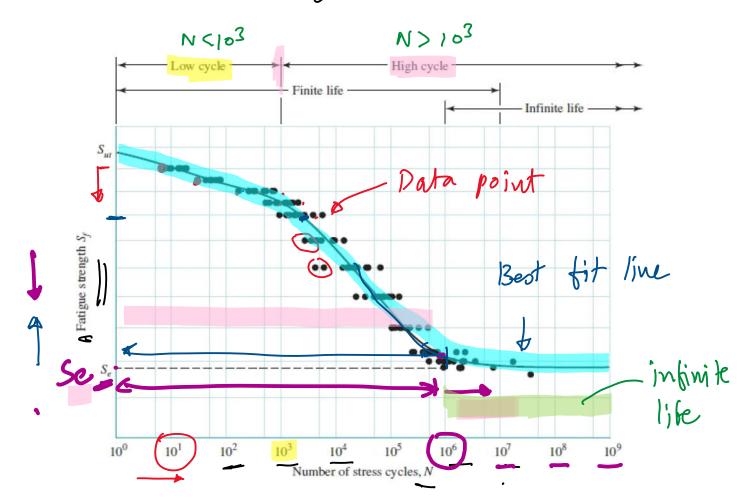
$$6x = (F_0 ay) \sin wt = 60 \sin(wt) j 60 = F_0 ay$$

$$I$$



SN experimental

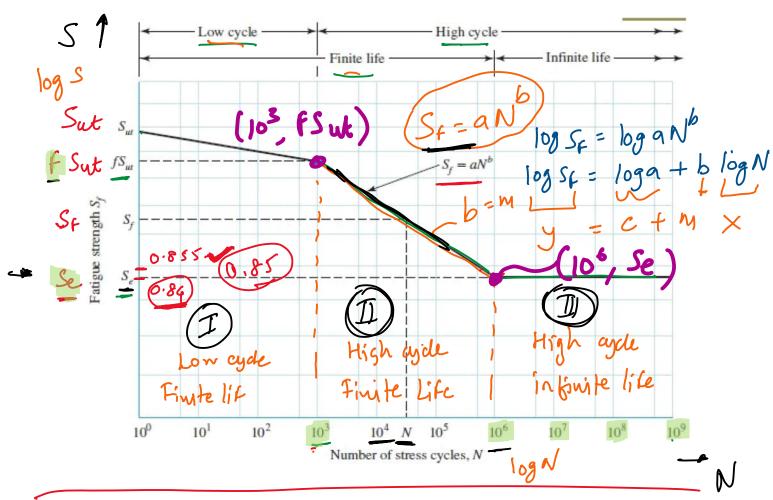
- 1 Choose 60
- 2) Keep increasing N till speimen bails



3) keep repeating (1) and (2) and plotting on strength vs. log N plot shown above.

S-N aurre; Wöhler aurre; stren-like aurre

Idealized SN curve



$$I$$
 $0 \le N \le 10^3$
Sut $\le S \le F Sut$

f = 0.8 - 0.9 (eugerical)

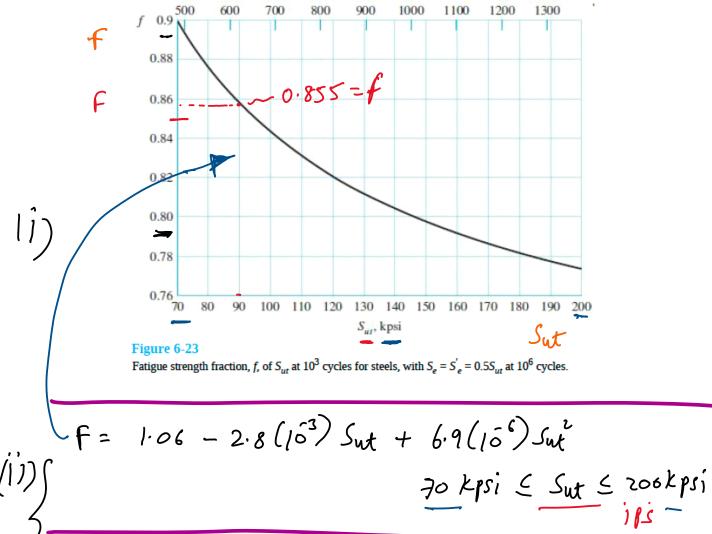
Se - endurance limit

1) Se is found emperically

For steel
$$S_{e}' = \begin{cases} 0.5 \text{ Sut} \\ 100 \text{ Kps}; \end{cases}$$

- Se endurance strength of the lab specimen
- Se endurance strength of actual moderial in the field.

Se + Se due to împerfections in actual material in the field.



 $f = 1.06 - 4.1(15^6)$ Sut $+ 1.5(15^7)$ Sut +

f = 0,8 or 0.9 i) graph (ii) tornula (îii) f=0.8 or 0.9 Conjute the constant a, b in $S_f = a N^b$

We know that the curre passes through (103, f Sut) and (106, Se)

$$- + (f Sut) = a (103)b - (I)$$

$$- (Se) = a (10^6)^b - 1$$

$$\frac{\text{I}}{\text{I}} \frac{\text{f Suk}}{\text{Se}} = \frac{10^{3b}}{10^{6b}} = 10^{-3b}$$

taking log10

$$logio\left(\frac{Se}{fSut}\right) = logio\left(\frac{3b}{10}\right) = 3b$$

$$Se = a (10)^{6b} \qquad b = \frac{1}{3} \log_{10} \frac{Se}{fSut}$$

$$\log_{10} Se = \log_{10} a + 66 \log_{10} 10$$

$$\log_{10} Se = \log_{10} a + 2\log_{10} \frac{Se}{fSut}$$

$$\log_{10} a = \log_{10} Se - \log_{10} \left(\frac{Se}{fSut}\right)^{2}$$

$$\log_{10} a = \log_{10} \left(\frac{Se}{fSut}\right)^{2}$$

$$\log_{10} a = \log_{10} \left(\frac{Se}{fSut}\right)^{2}$$

$$a = \frac{f^{2} Sut}{Se}$$

$$S_f = a N^b$$
; $a = \frac{f^2 Sut}{Se}$; $b = \frac{1}{3} \log_{10} \left(\frac{Se}{f Sut} \right)$

$$\Rightarrow N = \left(\frac{6}{a}\right)^{1/b}$$

=) $N = \left(\frac{6}{a}\right)^{1/b}$ a, b are computed using formulae given earlier.

Given a 1050 HR steel, estimate

(a) the rotating-beam endurance limit at 10^6 cycles.

(b) the endurance strength of a polished rotating-beam specimen corresponding to 10^4

cycles to failure. S *f*(c) the expected life of a polished rotating-beam specimen under a completely reversed stress of 55 kpsi. 6 = 55 kpsi ; N = 2

| | n |
|---------|--------|
| | I : |
| | J= aNb |
| \perp | |
| ı | |

| 1 | 2 | 3 | 4 Suf Tensile | 5 Yield | 6 | 7 | 8 |
|---------|------------------------|-----------------|------------------------|-------------------------|-----------------------|----------------------|---------------------|
| UNS No. | SAE and/or AISI No. | Process- ing | Strength MPa (kpsi) | Strength, MPa (kpsi) | Elongation in 2 in, % | Reduction in Area, % | Brinell Hardness |
| G10060 | 1006 | HR | 300 (43) | 170 (24) | 30 | 55 | 86 |
| | | CD | 330 (48) | 280 (41) | 20 | 45 | 95 |
| G10100 | 1010 | HR | 320 (47) | 180 (26) | 28 | 50 | 95 |
| | | CD | 370 (53) | 300 (44) | 20 | 40 | 105 |
| G10150 | 1015 | HR | 340 (50) | 190 (27.5) | 28 | 50 | 101 |
| | | CD | 390 (56) | 320 (47) | 18 | 40 | 111 |
| G10180 | 1018 | HR | 400 (58) | 220 (32) | 25 | 50 | 116 |
| | | CD | 440 (64) | 370 (54) | 15 | 40 | 126 |
| G10200 | 1020 | HR | 380 (55) | 210 (30) | 25 | 50 | 111 |
| | | CD | 470 (68) | 390 (57) | 15 | 40 | 131 |
| G10300 | 1030 | HR | 470 (68) | 260 (37.5) | 20 | 42 | 137 |
| | | CD | 520 (76) | 440 (64) | 12 | 35 | 149 |
| G10350 | 1035 | HR | 500 (72) | 270 (39.5) | 18 | 40 | 143 |
| | | CD | 550 (80) | 460 (67) | 12 | 35 | 163 |
| G10400 | 1040 | HR | 520 (76) | 290 (42) | 18 | 40 | 149 |
| | | CD | 590 (85) | 490 (71) | 12 | 35 | 170 |
| G10450 | 1045 | HR | 570 (82) | 310 (45) | 16 | 40 | 163 |
| | | CD | 630 (91) | 530 (77) | 12 | 35 | 179 |
| G10500 | 1050 | HR | 620 (90) | 340 (49.5) | 15 | 35 | 179 |
| | | CD | 690 (100) | 580 (84) | 10 | 30 | 197 |
| G10600 | 1060 | HR | 680 (98) | 370 (54) | 12 | 30 | 201 |
| G10800 | 1080 | HR | 770 (112) | 420 (61.5) | 10 | 25 | 229 |
| G10950 | 1095 | HR | 830 (120) | 460 (66) | 10 | 25 | 248 |

(a) Sut = 90 kps; for 1050 HR steel

Since Sut < 200 kps;

Se = 0.5 Sut
Se = 0.5 (90)

E = 45 kps;

(b)
$$N = 10^4$$
; $S_F = ?$

$$S_F = \stackrel{?}{a} \stackrel{?}{N_F}$$

$$a = \frac{(F Sut)^2}{Se V}$$

$$a = \frac{([0.655])(90)^2}{45} \implies a = 131.58$$

$$b = \frac{1}{3} \frac{1.9}{1.9} = \frac{(S_F Sut)^2}{F Sut}$$

$$b = \frac{1}{3} \log_{10} \left(\frac{Se}{FSut} \right)$$

$$b = \frac{1}{3} \log_{10} \left(\frac{45}{(0.855)(90)} \right) = b = -0.0776$$

$$S_{F} = a N^{b}$$

 $S_{F} = (131.58)(164)^{-0.0776}$
 $S_{F} = 64.39 \text{ Kpsi}$

(1)
$$S_F = \delta = a N^b$$

 $55 = (137.58) N (-0.0776)$
 $N = \left(\frac{SS}{131.58}\right) \frac{1}{-0.0776}$
 $N = 7.62 (104)$

 $N \approx 76000$ cycles