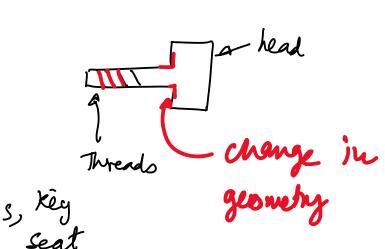
## Stress Concentration

## Example

- 1) Bolts
- (2) Transnission shafts The with keys, key ways, key seat



(3) Shouldress on shaft grooves, holes, notches, etc. will cause stress concentration.

Stress conentration factor: Lt, Kts

60, To are the nominal stresses in the absence of discontinuity / change in geometry

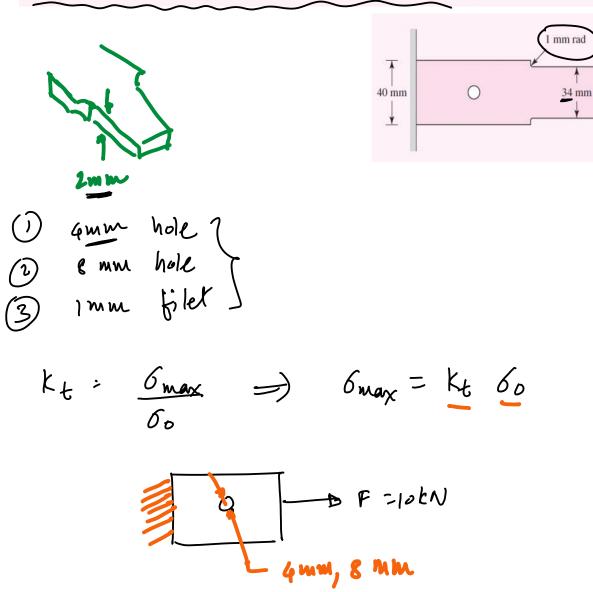
Swar, Twax are the maximum stresses due to discontinuity / change in geometry

Ke, kes - non-dinunsimal; >1 defend only on

Ke, kes - non-dimensional: >1 defend only on geometry.

The 2-mm-thick bar shown in Fig. 2-30 is loaded axially with a constant force of 10 kN. The bar material has been heat treated and quenched to raise its strength, but as a consequence it has lost most of its ductility. It is desired to drill a hole through the center of the 40-mm face of the plate to allow a cable to pass through it. A 4-mm hole is sufficient for the cable to fit, but an 8-mm drill is readily available. Will a crack be more likely to initiate at the larger hole, the smaller hole, or at the fillet?

➤ 10 kN



1) 4 mm hole

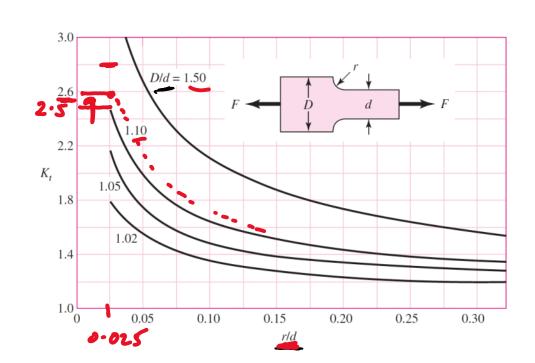
$$d = 4mm$$
 $W = 40mm$ 
 $2.5$ 
 $k = 2.65$ 
 $2.0$ 
 $3.0$ 
 $4 = 4mm$ 
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(2) 
$$d = 8mm$$
;  $W = 40mm$   
 $d = \frac{8}{40} = 0.2$ ;  $kt = \frac{25}{40}$   
 $60 = \frac{F}{A} = \frac{F}{(W-d)}t = \frac{(10)(10^3)}{(40-8)(10^3)(10^3)}$   
 $6max = \frac{kt}{60} = (2.5)(156) = 6max = 390 MPa$ 



$$\frac{D}{d} = \frac{40}{34} = 1.18$$

$$\frac{Y}{d} = \frac{1}{34} = 0.026$$



KE = 2.5 (Better Value would be 2.6 + to

be more conservative)

$$l_0 = \frac{F}{dt} = \frac{(10)(10^3)}{(34)(10^3)(2)(10^3)}$$

## Summary

1) 4 mm hole: 6 max = 368.35 MPa

3 8 mm bole: 6 max = 390 MPa at the smm hole.

3) Imm fillet: 6max = 368 MPa