Trajectory generation

1) Joint space:

9 lt), 9 lt), 9 (t)

9 - joint angles

91 92 93)

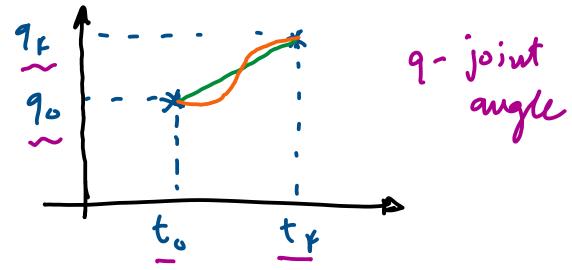
2 Task space ×e(t), xe(t), xe(t)

Xe - end-effector position/orientation

Xe Xe

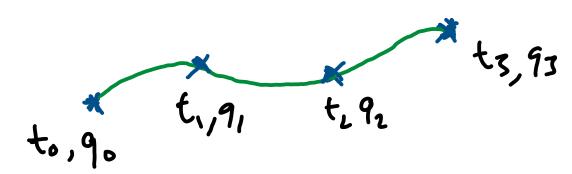
1) Joint space

(i) Point -to-point



linear, quadratic, quintic polynomials

(ii) Via point



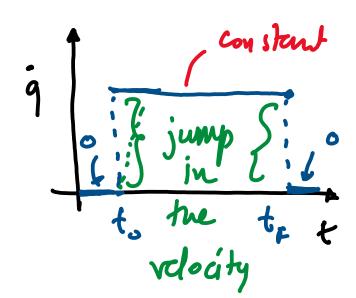
piecewise cubic spline

1) Linear poofile

$$\Rightarrow 90 = a_0 + 9, t_0?$$
 $\Rightarrow 9F = 90 + 9, t_0?$

$$\begin{bmatrix} 90 \\ 9F \end{bmatrix} = \begin{bmatrix} 1 & t_0 \\ 9 & t_F \end{bmatrix} \begin{bmatrix} 90 \\ 91 \\ X \end{bmatrix}$$

$$\begin{array}{c}
X = A^{4}b \\
\begin{bmatrix} a_{0} \\ a_{1} \end{bmatrix} = \begin{bmatrix} 1 & t_{0} \end{bmatrix}^{4} \begin{bmatrix} q_{0} \\ q_{F} \end{bmatrix} \\
= \begin{pmatrix} t_{F} + t_{0} \end{pmatrix} \begin{bmatrix} t_{F} - t_{0} \\ -1 \end{bmatrix} \begin{bmatrix} q_{0} \\ q_{F} \end{bmatrix} \\
\begin{bmatrix} a_{0} \\ a_{1} \end{bmatrix} = \begin{bmatrix} \frac{q_{0} t_{F} - q_{F} t_{0}}{t_{F} - t_{0}} \\ \frac{q_{F} - q_{0}}{t_{F} - t_{0}} \end{bmatrix} \\
q(t) : \begin{pmatrix} q_{0} t_{F} - q_{F} t_{0} \\ t_{F} - t_{0} \end{pmatrix} + \begin{pmatrix} q_{F} - q_{0} \\ t_{F} - t_{0} \end{pmatrix} + \\
q_{0} & q_{1} & q_{2} & q_{3} & q_{4} \\
\hline
q_{1} & q_{2} & q_{3} & q_{4} & q_{5} & q_{5} \\
\hline
q_{1} & q_{2} & q_{3} & q_{4} & q_{5} & q_{5} \\
\hline
q_{2} & q_{3} & q_{4} & q_{5} & q_{5} & q_{5} & q_{5} \\
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q_{1} & q_{2} & q_{3} & q_{5} & q_{5} & q_{5} & q_{5} & q_{5} \\
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q_{1} & q_{2} & q_{3} & q_{5} & q_{5}$$

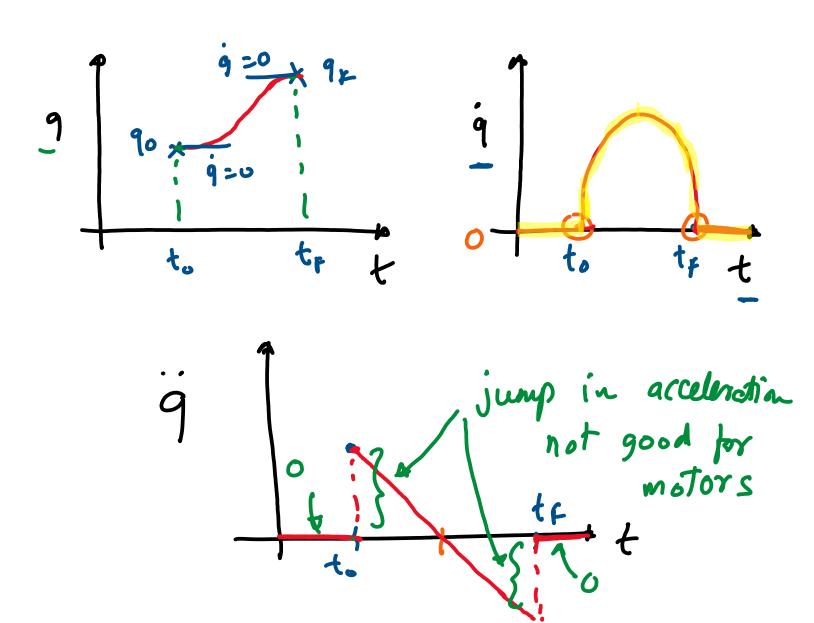


Cubic Profile

To avoid this, we set 4 conditions.

4 Conditions

$$\begin{cases} q(t_0) = q_0 \implies q_0 = a_0 + q_1 t_0 + q_2 t_0^2 + q_3 t_0^3 \\ q(t_p) = q_p \implies q_p = q_0 + q_1 t_p + q_2 t_p^2 + q_3 t_p^3 \\ q(t_0) = 0 \implies 0 = q_1 + 2q_2 t_0 + 3q_3 t_0^3 \\ q(t_p) = 0 \implies 0 = q_1 + 2q_2 t_p + 3q_3 t_p^3 \\ q(t_p) = 0 \implies 0 = q_1 + 2q_2 t_p + 3q_3 t$$



this, we add a more anditions St: to t: tr 9=90 9=9+ 9=0 (t > t. { t= t= 'g =0 st>to $\frac{1}{9} = 0$

Assume 9 = 90 + 9, t + 92 t²+ 93 t³+ 94 t⁴+ 95 t⁶
6 constants

jork.

add 2 more conditions q (t,) = q(t,) = 0 this will give a 7th order polynomial

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9 - Snap

g - crackle

ig - pop

Manipulator - 5th order polymonial quintic

Doone — 7th order polynomial Septic

Given (U+1) [to, &), [t,], [tz,], [tz,]... [tn, on] Assume a 3rd order polynomial 9: [ti, oi] and [tin, oin] between aio+ ai, (t-ti) + aiz(t-ti) + aiz(t-ti) n third order polynomials, 90, 91, ... 92-1

9i = aio+ ai, (t-ti) + aiz(t-ti)2+ ais(t-ti)3

 $q_i(t_{i+1}) > q_{i0} + q_{i1}(t_{i+1} - t_i) + ...$ $q_i(t_{i+1}) + q_{i1}(t_{i+1} - t_i) + q_{i2}(t_{i+1} - t_i)^2 + q_{i3}(t_{i+1} - t_i)^3 = Q_{i+1}$

Conjuste the # of constants and # of equations

n- 3rd order polynomials qi 4 constant for every 3rd order poly. # constant: 4n

2 (n-1) position equations (1 to n-1)

n-1 velocity equations

n-1 acceleration equations

2 of and on 1 in

n-1

equations: 4n-2

4 n constants > 4n-2 equations

equations to compute all constants.

there are few ways of imposing the 2 conditions

- 1) Natural spline $q_0''(t_0) = 0 & q_{n-1}''(t_n) = 0$
- 2) Clamped condition

 90' (to) = 0 & 9/14 (tin) = 0
- 3 Not-a-Knot condition $q_{0}^{11}(t_{1}) = q_{1}^{11}(t_{1}) \quad & q_{n-2}^{11}(t_{n-1}) = q_{n-1}^{11}(t_{n-1})$

(i) position (3D) [X, Y, Z]

position (3D) [X, Y, Z]

Some as joint space, use linear, cubic, quintic polynomials, or splines.

Once we get a profibe prend-effector, use the inverse kinewatics to compute the joint angles

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$$9 = Fk^{-1}(x,y,Q) = Ik(x,y,Q)$$
code

(ii) Orientation:

$$t = t_i$$
 $e_i = [\phi_i, \phi_i, \psi_i]$
 $t = t_f$ $e_f = [\phi_f, \phi_f, \psi_f]$

Issues

- 1) Gimbal lock . eg. 0 = T/2 (1-2-3)
- Discontinuities due to wrapping of angles at 211
- 3) May not jive the shortest path.

(b) Rotalin matrices

This does ensure RTR=I to bix this use SVD

$$=) \left(U S V^{T} = R \right)$$

U, V are orthornormal matrices S is diagonal matrix, that contains the length parameters.

- (i) to make R orthornormal: $R = UV^T$ But $det(R) = det(UV^T) = -1$
- (ii) To worke det(R) = 1 Simply Hip the Sign of the last Column of U = U[:,-1] *= -1
 - (i) and (ii) are done at every interpolation step.

Issues:

1) may not give the shortest

(c) quaternions

This does not ensure | 9 /=1

This is fixed by normalizing at each time step

Issue

Deads to non-constant angular velocity (although angles used) with (linear interpolation) W = 29.9, $W_b = 29.9$ q = con stant

9: [90, 91, 72, 93) 90+ 9,+ 92+ 93=1 SLERP Geodesic path (orientation should follow this path) Enclidean

$$\Theta = \cos^{1}(9i \circ 9f)$$

SLERP fixes both issues of LERP (i) |9sterp|= 1 while |9terp| = 1

We can also calculate acceleration $\dot{w} = 2\ddot{q} \circ \ddot{q} + 2|\dot{q}|^2$ $\dot{w}_b = 2\ddot{q} \circ \ddot{q} + 2|\dot{q}|^2$

(, w , w, w,



LERP) SCERP with time scaling

To enforce a relocity/acceleration profile one can scale the time as follows.

Note that $t' = \frac{t - Ei}{t_f - Ei}$ is such that

At
$$t = t$$
: $t' = 0$
 $t = t_{f}$ $t' = 1$

Lets choose
$$s(t')$$
 such that

 $s(t'=0)=0$, $s(t')=1$
 $\dot{s}(t'=0)=\dot{s}(t'=1)=0$
 $\ddot{s}(t'=0)=\dot{s}(t'=1)=0$
 $\ddot{s}(t'=0)=\dot{s}(t'=1)=0$
 $s(t)=a_0+a_1(t')+a_2(t')^2+a_3(t')^3+a_4(t')^4+a_5(t')^5$

6 constants

Solve for the 6 constants using the 6 conditions gives

 $s(t')=6(t')^5-1s(t')^4+1o(t')^3$

Now use LERP | $s(t')^4+1o(t')^3$

Now use LERP | $s(t')^4+1o(t')^3$

Now use $s(t')=s(t')^4+1o(t')^3$
 $s(t')=s(t')^4+1o(t')^3$
 $s(t')=s(t')^4+1o(t')^3$
 $s(t')=s(t')^4+1o(t')^3$
 $s(t')=s(t')^4+1o(t')^5+$