

Junction Transistor

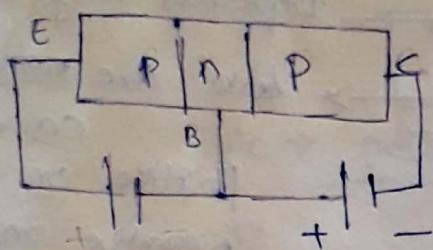
Unit-II

- ① A bipolar Junction Transistor is a solid state device, which is mainly used as the amplifier.

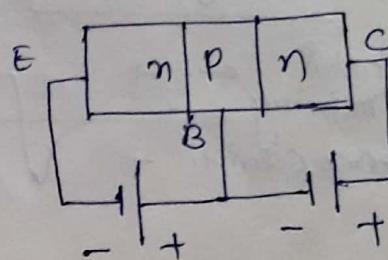
- ② Transistor transfers a weak signal from the low resistance input circuit to the high resistance output circuit.

Type of Junction Transistors:-

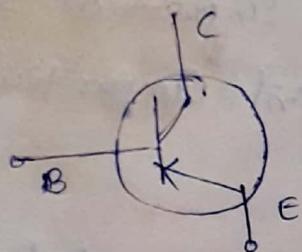
a)



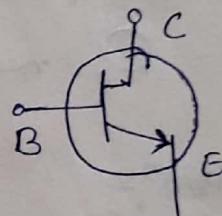
b)



Symbols



a) PNP Transistor



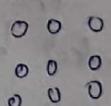
b) NPN Transistor

An arrow head is placed on the Emitter, and its direction represents the direction of Conventional Current, i.e., the direction of motion of holes and hence its opposite direction to the flow of electrons.



↓
(-)valent Impurity

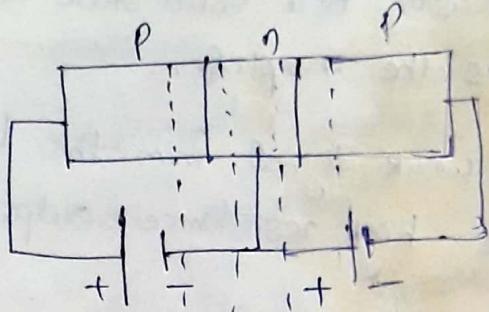
- ① (-)valent Impurity. They become the negative charged ions.



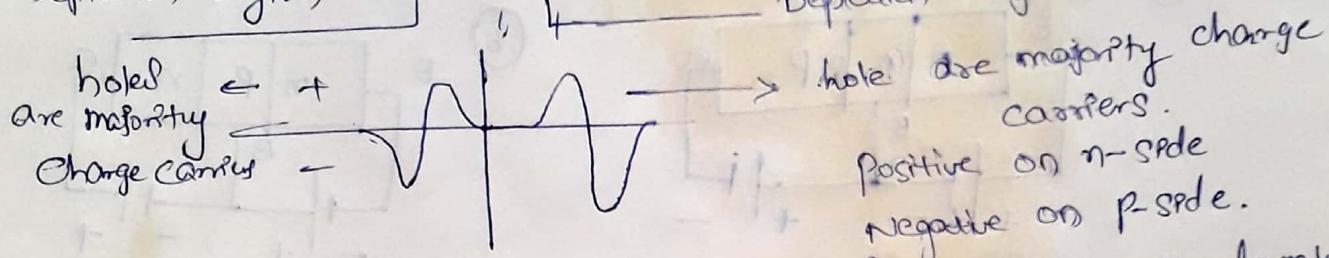
Positivevalent Impurity
They are ready to accept the electrons.

- ② Positivevalent Impurity. They are ready to donate electrons, they become the +ve charge donors.

Working of P-n-P Transistor



Depletion Region Depletion Region



- ① P-side Trivalent Impurity, so depletion is downward
- ② n-side Pentavalent Impurity, so depletion is upwards

Operation:-

- ① The Emitter-base junction is forward biased, the large number of holes present in the Emitter region are repelled by the positive potential of the bias voltage and they move towards the junction and diffuse into the base region.
- ② Since the base is n-type semiconductor, electrons are majority charge carriers in the region.
- ③ But base is lightly doped, so the most of charge carriers pass through the base region without recombination. These are collected by the Collector, Since the Collector-base junction is reverse biased, and holes are easily attracted by the negative potential of bias voltage.

clear Recombination gives rise to and collector

of electrons and hole in the base region base current. If the Emitter current I_E current I_C then $I_E = I_C + I_{B,if}$ ①

Collector - to - base leakage Current :-

- The Reverse bias voltage applied across the collector-base junction there is a small reverse current flows, denoted as I_{CBO} . This current is called as the collector-base leakage current.
- * This current is present even when the forward voltage across the base-emitter junction is removed.

Taking the leakage current into account

$$I_C = \alpha I_E + I_{CBO}.$$

— ②.

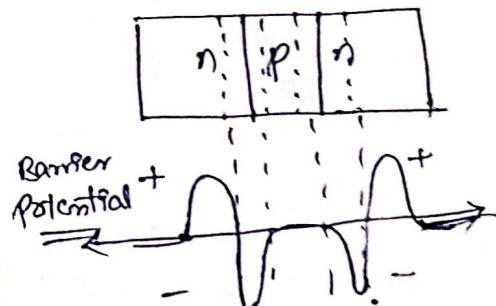
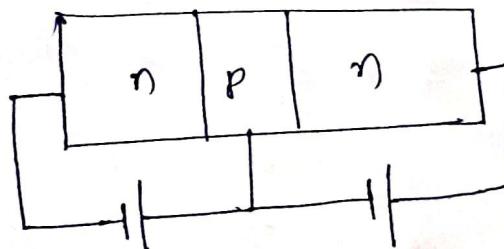
$$\alpha_{dc} \rightarrow \underline{0.96} \text{ to } \underline{0.99}$$

From ② $\alpha_{dc} = \frac{I_C - I_{CBO}}{I_C}$

By ignoring I_{CBO}

$$\alpha_{dc} = \frac{I_C}{I_E}$$

Working of n-p-n Transistor:-



→ When the emitter-base junction is forward biased, the large no. of electrons are repelled by the -ve terminal of battery and they diffuse across the emitter-base junction.

→ The base which is p-type material, is very lightly doped and hence there are few holes are in the region.

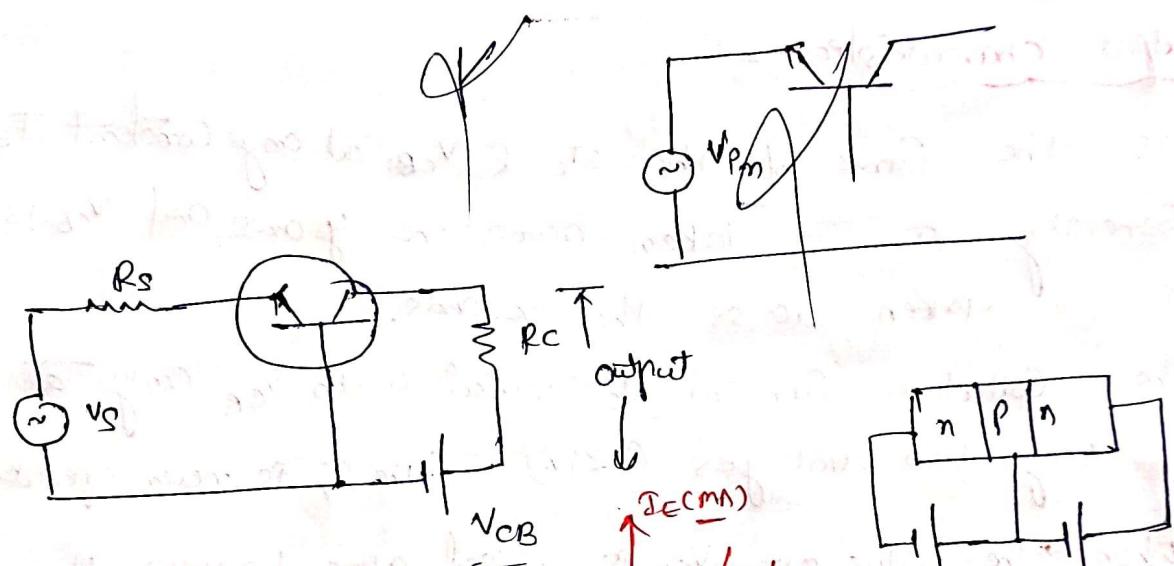
→ Some of the electrons are crossing the base region and reach the collector-base junction.

-° Transistor Connections °-

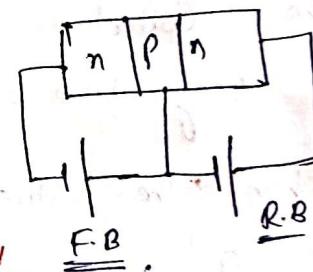
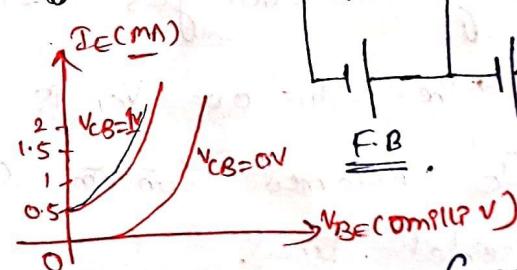
1. Common base Connection
2. Common Emitter Connection
3. Common collector Connection.

Common base Connection

The input is applied between the Emitter and base and output is taken across the Collector and base.



Input characteristics



1. It is the curve between the Emitter Current I_E and Emitter-base voltage V_{BE} at constant Collector-Base Voltage V_{CB} . The Emitter Current generally taken along x -axis and Emitter-base voltage along y -axis.

2. From the graph, the I_E increased rapidly with small increase in emitter to base voltage.

3. The Emitter Current is almost independent of Collector-to-Base voltage V_{CB} . This leads to Collector-to-Base voltage and I_E both are independent of each other.

Input Resistance:-

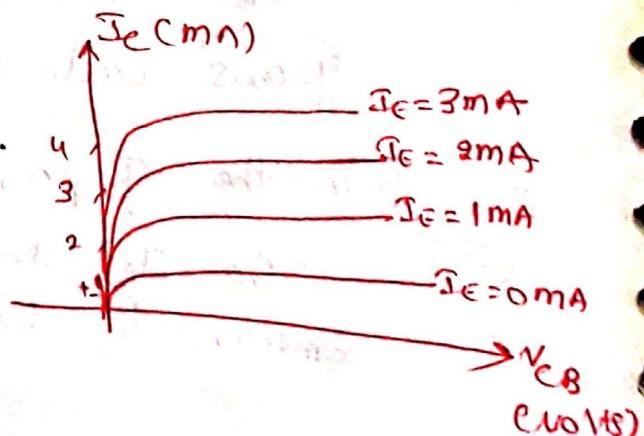
$$r_p = \frac{\Delta V_{BE}}{\Delta I_E} \text{ at Constant } V_{CE}$$

Output Resistance

Output characteristics:-

- It is the Curve b/w the I_C & V_{CB} at any constant I_E .
- Generally I_E is taken across the y-axis and V_{CB} is taken across the x-axis.
- The Collector Current I_C varies with V_{CB} only at very low voltages ($< 1V$) (The r_o is never operated)
- When the value of V_{CB} is raised above 1-2 V, the I_C becomes constant and is indicated by straight horizontal lines.
- A very large change in the Collector-Base voltage produces only a tiny change in Collector Current.

$$6. r_o = \frac{\Delta V_{CB}}{\Delta I_C} \text{ at Constant } I_E.$$



Common Emitter Connection:-

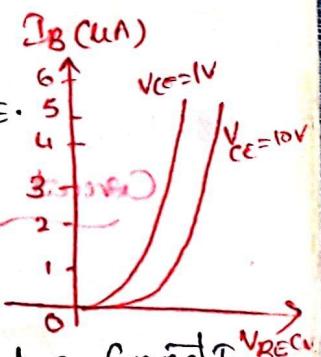
1. Input is applied b/w base and Emitter and output is taken from the Collector and Emitter.
2. Here, Emitter of the Transistor is common to both input and output Circuits.
3. The important characteristics of this circuit arrangement are the input characteristics and output characteristics.

Input Characteristics:-

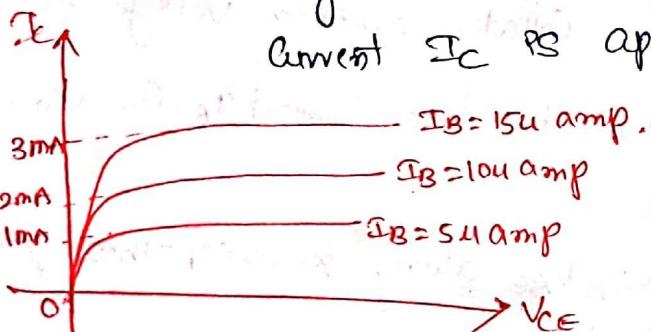
4. It is the curve between the base current I_B and base-emitter voltage V_{BE} at constant collector-emitter voltage V_{CE} .
5. Keeping V_{CE} constant, note the base current I_B for various values of V_{BE} .
6. Taking I_B along y-axis, V_{BE} along x-axis, this gives the input characteristics.
7. As compared to CB arrangement, I_B increases less rapidly with V_{BE} . Therefore, input resistance of a CE Circuit, is higher than that of CB Circ.
8. Input Resistance $r_i = \frac{\Delta V_{BE}}{\Delta I_B}$ at constant V_{CE} .

Output Characteristics:-

1. It is the curve b/w the Collector Current I_C and collector-emitter voltage V_{CE} at constant base current I_B .
2. keeping the base current I_B fixed at some value, taking I_C along y-axis, V_{CE} along x-axis. This gives the output characteristics.
3. The I_C varies with V_{CE} for V_{CE} b/w 0 & 1V only, after this I_C is almost independent of V_{CE} .



4. The value of V_{CE} upto which collector current I_C changes with V_{CE} is called knee voltage (V_{knee}).
5. Transistors are always operated in the region above knee voltage.
6. Above knee voltage, I_C is almost constant.
7. A small increase in I_C with increasing V_{CE} is caused by collector deactivation layer getting wider and capturing a few more majority carriers before electron-hole combinations occur in the base area.
8. For any value of V_{CE} above knee voltage, the collector current I_C is approximately equal to the I_B .

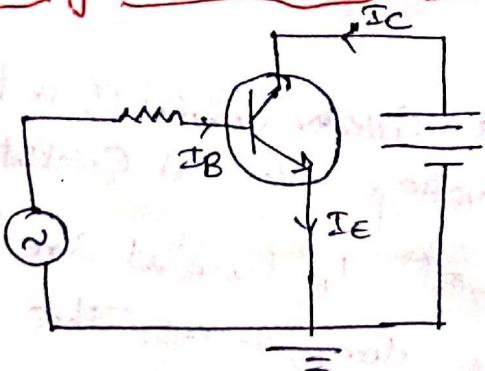


9. Output Resistance $r_o =$

$$\frac{\Delta V_{CE}}{\Delta I_C} \text{ at constant } I_B.$$

10. Output Resistance of a CE or CB circuit. This value is in the order of $50 \text{ k}\Omega$.

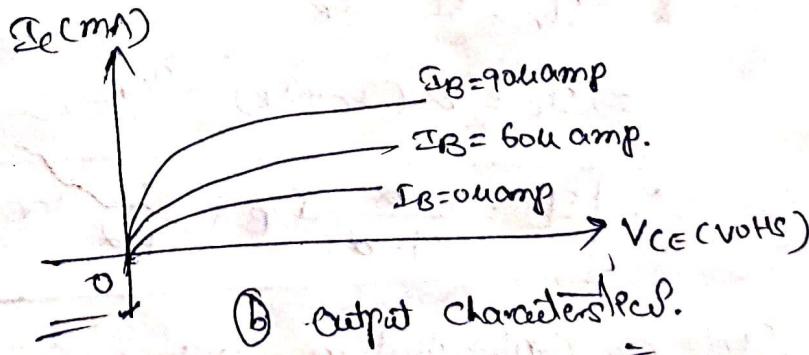
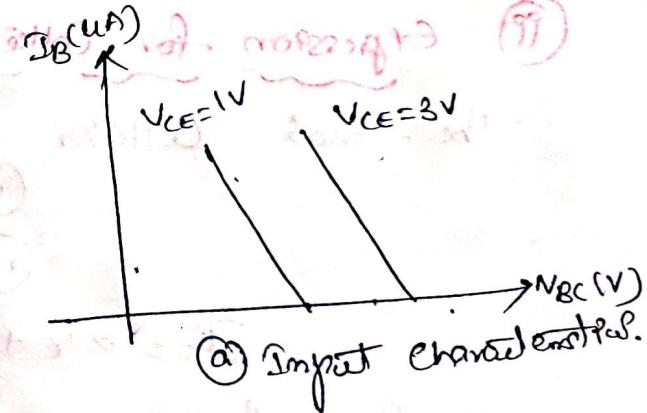
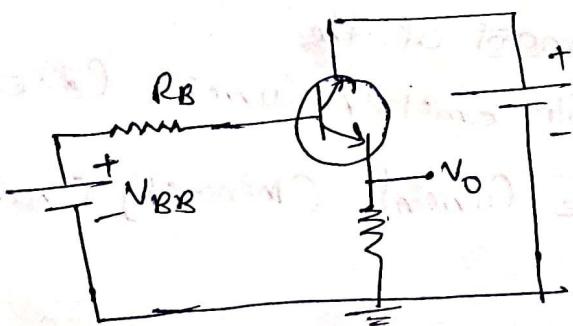
Circuit diagram for CE arrangement :-



Common Collector Connection

1. The input is applied b/w the base and collector while the output is taken between the emitter and collector.
2. Collector of transistor is common to the both input and output pins.
3. Here the Load Resistor R_L is connected to Emitter Terminal, The Load Resistor R_L itself acts as the bias for Emitter-base Junction.
4. The operation of the circuit is similar to the Common Emitter Configuration.
5. When the base current is I_{CQ} , Emitter Current will be zero. So no current flows through the load.
6. Base Current should be increased so that Emitter Current is some finite value and Transistor comes out of region. (Input characteristic I_B vs V_{BE}) ; Output characteristic I_C vs V_{CE})

Circuit Diagram



→ Some of the parameters —

① Current amplification factor (α) —

1. It is the ratio of Output Current to the Input Current.
In a Common base Connection, the Input Current is the Emitter Current I_E and output Current I_C .
2. The Ratio of change in the Collector Current to the change in the Emitter Current at constant collector-base voltage is known as the Current-amplification Factor i.e., $\alpha = \frac{\Delta I_C}{\Delta I_E}$ at constant V_{CB} .
3. $\alpha \approx 1$
4. α is increased by decreasing the Base Current.

② Expression for Collector Current —

The total Collector Current consists of the

(i) part of Emitter Current (αI_E)

(ii) Leakage Current (Minority Charge)

$$I_C = \alpha I_E + I_{CBO}$$

$$\& I_E = I_C + I_B$$

$$\Rightarrow I_C = \alpha (I_C + I_B) + I_{CBO}$$

$$\therefore I_C = \frac{\alpha}{1-\alpha} I_B + \frac{1}{1-\alpha} I_{CBO}$$

Note: In CB Configuration, a small current flows even when the Emitter Current is zero. This is leakage collector current and is denoted by I_{CBO} .

(iii) Base Current Amplification Factor

1. In Common Emitter Connection, Input Current is I_B and output current is I_C .
2. The Ratio of Change in the Collector Current (ΔI_C) to the Change in the base Current (ΔI_B) is known as the Base Current amplification factor i.e., $B = \frac{\Delta I_C}{\Delta I_B}$
3. In almost any Transistor, less than 5% of Emitter Current flows as the base current. Therefore the value of B is generally greater than the 20. Usually, its value ranges from 20 to 500.

(iv) Relation b/w the α & B

A simple relation exist b/w the α & B . This can be derived as follows:

$$B = \frac{\Delta I_C}{\Delta I_E}$$

$$\alpha = \frac{\Delta I_E}{\Delta I_C}$$

$$B = \frac{\Delta I_C}{\Delta I_E \Delta I_C} = \frac{1}{(\frac{\Delta I_E}{\Delta I_C}) - 1} = \frac{1}{(\frac{1}{\alpha}) - 1} = \frac{1}{(\frac{1}{2} - 1)}$$

$$\boxed{B = \frac{\alpha}{1-\alpha}}$$

Note,

1. As " α " approaches to unity, B approaches to ∞ .
2. In other words, Current gain in the Common Emitter Connection is very high.

(iv) Expression for Collector Current

In Common Emitter Circuit, I_B is the input current and I_C is the output current.

$$\text{we know that } I_C = \frac{\alpha}{1-\alpha} I_B + \frac{1}{1-\alpha} I_{CBO}. \quad (1)$$

From Expression (1), it is apparent that if $I_B = 0$, the collector current will be current to the emitter. This is abbreviated as I_{CEO} , means collector to emitter current when the base is open.

$$\Rightarrow I_{CEO} = \frac{1}{1-\alpha} I_{CBO}$$

$$\Rightarrow I_C = \frac{\alpha}{1-\alpha} I_B + I_{CEO}. \quad \text{method (1)}$$

$$\therefore I_C = \beta I_B + I_{CEO}$$

(v) Collector Current amplification Factor (β)

1. In Common Collector Circuit, the input current is the base current (I_B), output current is the emitter current I_E .
2. The Ratio of change in Emitter Current (ΔI_E) to the change in base current (ΔI_B) is known as the current amplification factor.
3. It is denoted by $\beta = \frac{\Delta I_E}{\Delta I_B}$

Relation between the α and β :

$$\Rightarrow \beta = \frac{\Delta I_E}{\Delta I_B} \Rightarrow \beta = \frac{\Delta I_E}{\Delta I_E - \Delta I_C} = \frac{1}{1-\alpha}$$

$$\alpha = \frac{\Delta I_C}{\Delta I_E}$$

$$\Rightarrow \beta = \frac{1}{1-\alpha}$$

Expression for Emitter Current (In terms of β)

We know that $I_C = \alpha I_E + I_{CBO}$.

$$\text{But } I_E = I_C + I_B.$$

$$I_E = I_B + (\alpha I_E + I_{CBO})$$

$$\Rightarrow I_E(1-\alpha) = I_B + I_{CBO}.$$

$$\Rightarrow I_E = \frac{1}{1-\alpha} I_B + \frac{1}{1-\alpha} I_{CBO},$$

$$\Rightarrow I_E = (1+\beta) I_B + (1+\beta) I_{CBO}$$

Problems :-

- ① In a Common base Connection, $I_E = 1\text{mamp}$, $I_C = 0.95\text{milliamp}$. Calculate the value of I_B ?

Ans:- $I_B = 0.05\text{mamp}$.

- ② In a CB Configuration, α is 0.9. If the I_E is 1mamp. Determine the value of base current?

Ans:- $I_B = 0.1\text{milliamp}$.

- ③ In a CB, $I_C = 0.95\text{milliamp}$, $I_B = 0.05\text{mamp}$ $I_E = ?$

Find the value of $\alpha = ?$

Ans:- $\alpha = 0.95$

$$\begin{aligned} I_C &= \alpha I_E \\ &= 0.95 \times 0.05 \end{aligned}$$

$$\underline{\underline{B = 19}}$$

$$\alpha = \frac{B}{1+B} = 0.95$$

- Prob ④ In a CB, the Emitter Current is 1mamp. If the Emitter Circuit is open, the Collector Circuit is open. Find the total Collector Current. Given that $\alpha = 0.92$. Ans:- $I_C = 0.97\text{milliamp}$.

$$\begin{aligned} I_C &= \beta I_B + I_{CBO} \\ I &= \alpha I_E + I_{CBO} \\ &= 0.92 \times 0.05 + 0.01 \\ &= 0.97\text{mAmp} \end{aligned}$$

⑤ In a Common base connection, $\alpha = 0.95$. The voltage drop across the $2k\Omega$ resistance which is connected in the collector is 2 Volts. Find the base current.

Ans^r from note, $I_E = \frac{2}{2k\Omega} = 1 \text{ milliamp}$.

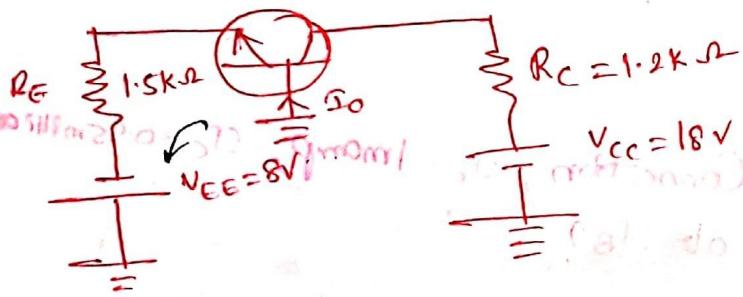
$$\alpha = 0.95$$

$$I_E = \frac{1 \text{ milliamp}}{0.95}$$

$$I_E = 1.052 \text{ milliamp.}$$

$$I_B = 0.52 \text{ milliamp.}$$

⑥ For the CB circuit, determine I_C and V_{CB} . Assume the transistor to be silicon.



$$-V_{EE} + V_{BE} + I_E R_E = 0$$

$$I_E = \frac{V_{EE} - V_{BE}}{R_E}$$

$$I_E = \frac{8 - 0.7}{1.5k}$$

$$I_E = 4.8667 \text{ milliamp}$$

$$\text{for } CB \rightarrow I_C \approx I_E$$

$$-V_{CC} + I_C R_C + V_{CB} = 0$$

$$V_{CB} = V_{CC} - I_C R_C$$

$$= 18 - 4.8667 (1.2k)$$

$$V_{BC} = 12.16 \text{ Volts}$$

⑦ Find the value of β if $\alpha = 0.9$ $\text{ii)} \alpha = 0.98$ $\text{iii)} \alpha = 0.99$

Ans^r i) $\beta = 9$ ii) $\beta = 49$ iii) $\beta = 99$.

⑧ Calculate I_E in a transistor for which $\beta = 50$ & $I_B = 20 \text{ microamp}$.

Ans^r $I_E = 1.02 \text{ milliamp.}$

- Q) Find the d_{sat}ing of the transistor shown in figure.
 Hence determine the value of I_C using both α and p_r rating
 of the transistor.
- Ans: $\alpha = 0.98; \beta = 49$ (Given)
- $I_C = 11.76 \text{ milliamp}$
-

- Q) For a Transistor, $\beta = 45$, voltage drop across the $1\text{k}\Omega$ which is connected in the Collector Circuit is 1 volt. Find the base current for Common Emitter Connection?

Ans:

$$\beta = 45; R_L = 1\text{k}\Omega$$

$$V_0 = 1$$

$$I_C = 1 \text{ milliamp.}$$

$$\left. \begin{array}{l} \beta = 45 \\ R_L = 1\text{k}\Omega \\ V_0 = 1 \text{ volt.} \end{array} \right\}$$

$$I_B = 22.22 \mu \text{Amp.}$$

- Q) A Transistor is connected in CE Configuration in which the collector Supply voltage is 8VDC and the voltage drop across the collector circuit is 0.5V. The resistance R_C is connected in the collector circuit is 800Ω . $I_B = 0.96$ determine the β value of $R_C = 800\Omega$.

① V_{CE} ② $I_B = ?$

Ans: ① $V_{CE} = 7.5 \text{ VDC}$ ② $I_C = 0.625 \text{ milliamp.}$

- Q) An n-p-n Transistor at room Temperature has its Emitter is disconnected. A voltage of 5VDC is applied between Collector and Base. With collector positive, a current of 0.211 Amp flows. When the base is disconnected and the same voltage is applied between collector and Emitter, the current is found to be 0.011 Amp. Find α , I_{CEO} , I_E is 1 milliamp.

Ans:

$$I_{EB0} = 0.211 \text{ Amp.}$$

$$I_{CEO} = 0.011 \text{ Amp.}$$

$$I_{CEO} = \frac{I_{EB0}}{1-\alpha}$$

$$\Rightarrow \alpha = 0.99$$

$$I_C = \alpha I_E + I_{CEO}.$$

$$\Rightarrow I_C = 1 \text{ milliamp.} \Rightarrow I_B = 10 \mu \text{A} ; I_E = 10 \text{ milliamp}$$

(13) For the transistor AF114 connected as shown in figure.

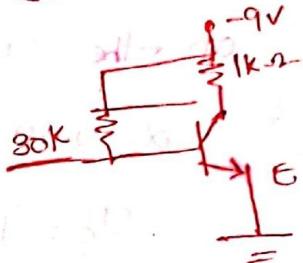
Determine values of I_B , I_C , V_{BC} given that $V_{CE} = -0.07V$

and $V_{BE} = -0.21 \text{ Volts}$

Ans: $I_C = -8.93 \text{ mA}$

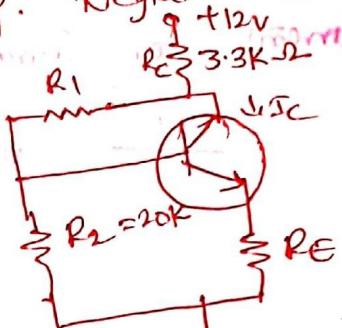
$I_B = -0.293 \text{ mA}$

$V_{BC} = -0.16 \text{ Volts}$



(14) If $\alpha = 0.98$ and $V_{BE} = 0.6 \text{ Volts}$, find R_1 in the circuit shown

Emitter Current $I_E = -2 \text{ mA}$. Neglect Reverse Saturation Cur.



(15) A transistor is operated at a forward current of 2mA.

Second part with collector open circuited. Calculate the junction voltage V_C & V_{BE} at the collector to emitter voltage

$I_E = I_C + I_O = 2 \text{ mA} + 1.6 \text{ uA}$ and $\alpha = 0.98$

Solution

$I_C = 0$ Since collector junction is open

we know that, $I = I_0 (e^{\frac{V_{BE}}{V_T}} - 1)$ ① $V_T = 25 \text{ mV}$ ②

$$I_E = I_0 (e^{\frac{V_{BE}}{V_T}} - 1) \Rightarrow V_E = n \sqrt{m \left(1 + \frac{I_E}{I_0} \right)}$$

$$\Rightarrow V_E = 0.1853 \text{ Volts}$$

Similarly by $N_C = \sqrt{m \left(1 + \frac{I_C}{I_0} \right)}$

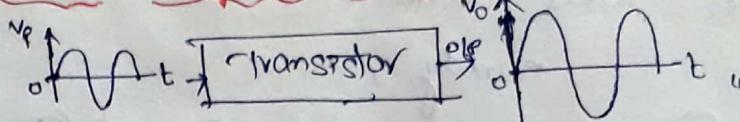
$$V_C = V_T \ln \left(1 - \frac{\alpha I_E}{I_C} \right)$$

$$\therefore V_C = 0.179 \text{ Volts}$$

$$N_{CE} = V_C - V_E = -0.006 \text{ Volts}$$

(BJT) Transistor acts as an Amplifier in CE arrangement.

Operation



- ① During the positive half cycle of the signal, the forward bias across the Emitter-base junction is increased.
Therefore, more electrons flow from the Emitter to the Collector via the base. This cause an increase in the Collector Current.
- ② The Increased Collector current produces a greater voltage drop across the Collector Load Resistance R_C .
- ③ During the negative half cycle of the signal, the forward bias across the Emitter-base junction is decreased. Therefore, Collector Current decreases.
This results in decreased output voltage in opposite direction.

In this way we achieve the faithful amplification at off side.

Operation Explanation of (Terms of Collector Currents)

- ① When no signal is applied, the Input is forward biased by the battery voltage V_{BB} .
- ② D.C. Collector Current I_C flows in the Collector Circuit. This is called zero Signal Collector Current.
- ③ When the Signal voltage is applied, the forward bias on the Emitter-base junction increases (or) decreased depends upon whether the signal is positive (or) negative.
- ④ During the positive half cycle of the signal, the forward bias on the E-Base Junction is increased, causing total current I_C to increase. Reverse will happen for the half of the cycle.

The Total Collector current consists of two components, namely:-

- (i) The D.C. collector Current (I_C) due to bias battery V_{BB} .
- (ii) The A.C. collector Current (I_C') due to signal.

Note:-

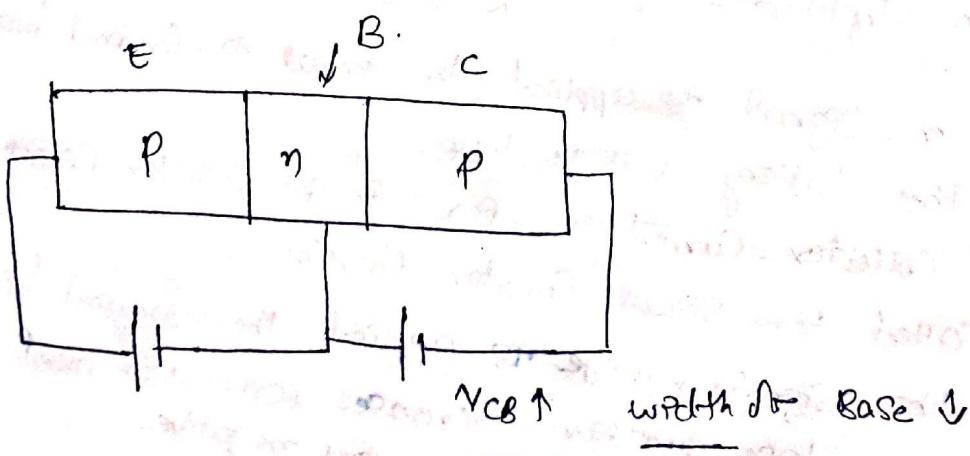
$$I_{Total} = I_C + I_C'$$

- (i) The useful output is voltage drop across the collector load R_C due to a.c. component.
- (ii) The purpose of zero signal collector Current is to ensure that the Base - Emitter junction is forward biased at all times.

Early Effect-

"The dependence of the effective width of the base on collector-to-base voltage is called as the early Effect."

Due to this reduction of the effective width of the base, there can be slight increase in the collector current even if the base - voltage is decreased slightly.



$N_C \uparrow$ width Δ Base \downarrow

Field Effect Transistors

1. BJT — Current Controlled device
(Op characteristics of the device are controlled by base current not by base voltage)
 2. FET — Voltage Controlled device.
(Op characteristics are controlled by input voltage not by input current.)

Disadvantages of BJT

Types of field effect transistors:-

- Field Effect Transistors

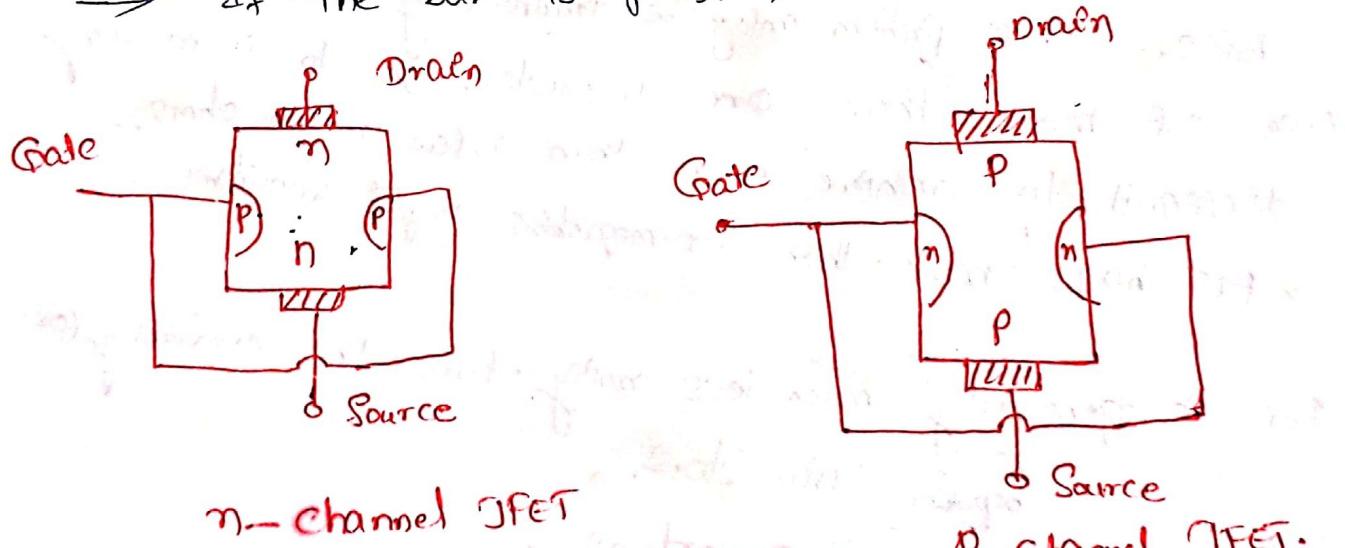
 - ① Junction Field Effect Transistor (JFET)
 - ② Metal Oxide Semiconductor Field Effect Transistor (MOSFET)

A) Junction Field Effect Transistor (JFET)

1. A JFET is a three terminal semiconductor device in which current conduction is by one type of charge carriers e.g., electrons or holes.
2. It is controlled by means of an electric field between the gate electrode and conducting channel of the device. The JFET has high input impedance and low noise level.

Construction Details :-

A JFET consists of a p-type (or) n-type silicon bar containing two PN junctions at the sides. The bar forms conducting channel for the charge carriers.
→ If the bar is n-type, it is called n-channel JFET.
→ If the bar is p-type, it is called p-channel JFET.



n-channel JFET

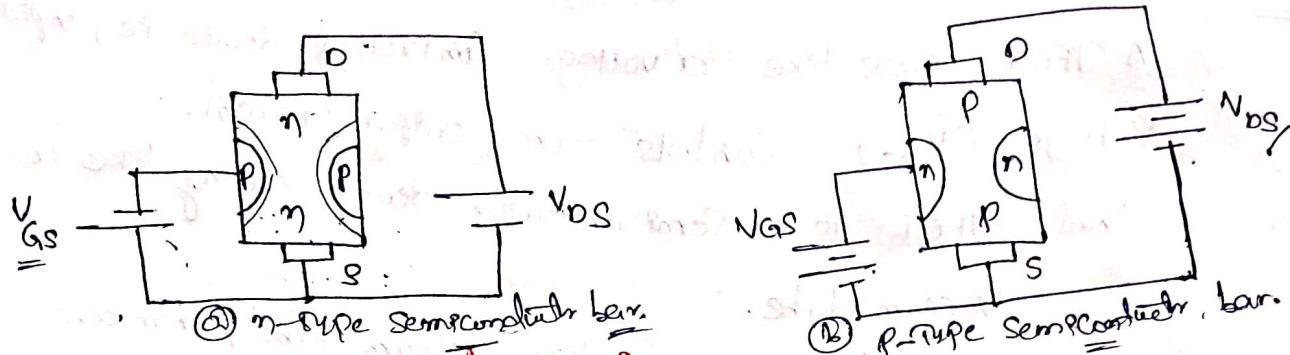
p-channel JFET

Two PN junctions are connected internally and a common terminal called gate is taken out.

Other terminals source and drain taken out from the bar.

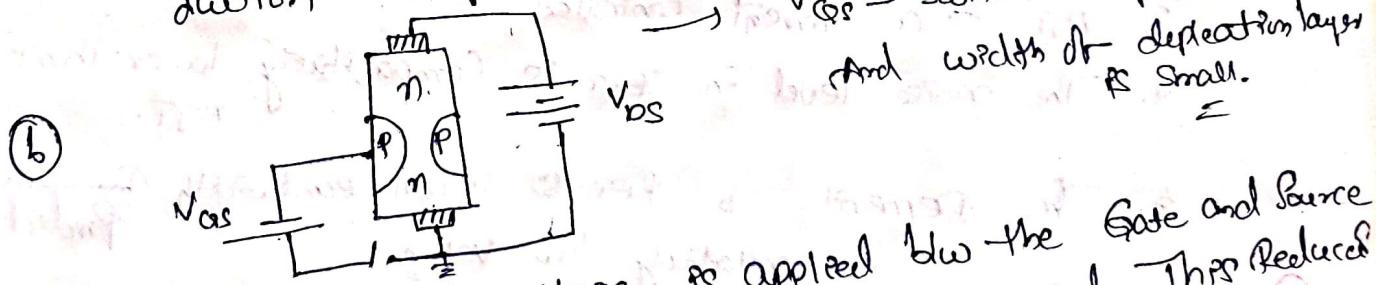
JFET polarities

- ① Voltage b/w the gate and source is interchangeable such that gate is reverse biased. This is normal way of JFET connection. The drain and source are interchanged i.e., either end can be used as the source and other end used as drain.



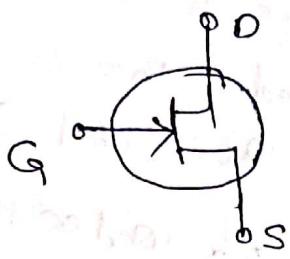
Working Principle of JFET

- a) When a V_{DS} is applied, V_{GS} is zero, the two pn junctions at sides of the bar establish depletion layers. The electrons will flow from Source to Drain through a channel b/w the depletion layers. Hence Current conduction through the bar.

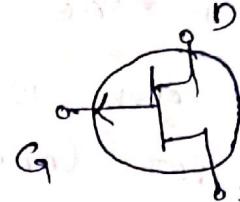


- b) When a Reverse voltage is applied b/w the Gate and Source the width of depletion layers is increased. This reduces the width of Conducting Channel, thereby increasing the resistance of n-type bar. Consequently, the current from Source to drain is decreased.

Schematic Symbol of JFETs



(a) n-channel JFET



p-channel JFET.

Note:-

- ① A JFET acts like a voltage controlled device i.e., input Voltage (V_{GS}) controls the output current. Thus, JFET is a semiconductor device acting like a vacuum tube.

→ JFET devices are more like vacuum tubes, than are bipolar Transistors and hence are able to take over many vacuum-tube functions.

Difference Between JFET and Bipolar Transistor

1. BJT is a bipolar device.
2. BJT has very low input impedance.
3. BJT is a Current Controlled device.
4. The noise level in FET is comparatively lower than the BJT.
5. The Element of FET is Gain-Bandwidth Product which is relatively low value.

- ① In a JFET, there is only one type of carrier, holes in P-type channel, and electrons in n-type channel. For this reason it is also called a unipolar transistor.
- ② As Input Circuit is reverse biased, it offers very high Input Impedance. (FET)

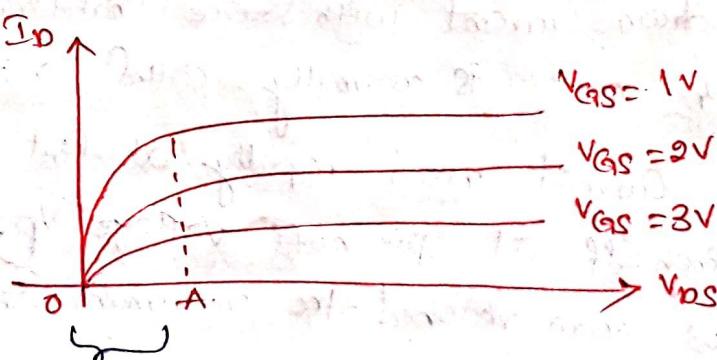
(iii) As the gate is reverse biased, therefore it carries very small current. Obviously, JFET is just like a vacuum tube where control grid carries extremely small current.

(iv) A Bipolar Transistor uses a current into its base to control a large current between the collector and emitter. Whereas JFET uses a voltage to control the input. Thus Bipolar is characterised by the current gain and whereas JFET gain is characterised by transconductance. i.e., change in output current to the input voltage.

(v) In JFET, there are no junctions, as in ordinary transistor. The conduction is through an n-type (or) p-type Semiconductor material. For this reason, noise level in JFET is very small.

Output characteristics of JFET:

- The curve between drain current (I_D) and drain-to-source voltage (V_{DS}) of a JFET at constant gate-source voltage is known as the output characteristics of JFET.



Pinch-off Region.

- At first, drain current rises rapidly, with drain-to-source voltage (V_{DS}) but then becomes constant. The drain-to-source voltage above which drain current becomes constant is known as the pinch-off voltage. The region OA is called Pinch-off Region.

ii

After pinch off, voltage \rightarrow the channel width becomes so narrow that depletion layers almost touch each other.

The drain current pass through the small passage between the layers.

Therefore increase in drain current is very small with V_{DS} above pinchoff voltage. Consequently drain current remains constant.

Parameters of JFET :-

In the analysis of a JFET circuit, the following important terms are often used

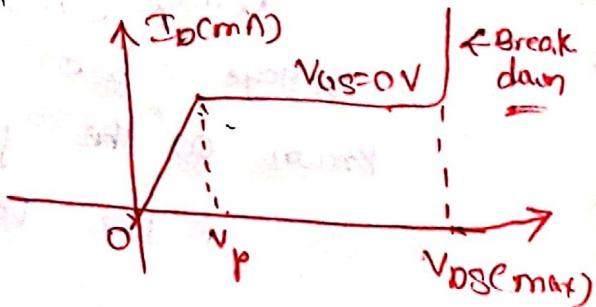
1. Shorted-gate drain current (I_{DSS})
2. Pinch-off voltage (V_p)
3. Gate-Source Cutoff voltage ($V_{GS(off)}$)

① Shorted-gate drain Current (I_{DSS}) :-

It is the drain current with source short-circuited to gate. This (i.e. $V_{DS}=0$) is normally called short-gate condition.

The drain current rises rapidly at first and then levels off pinchoff at pinchoff voltage V_p . The drain current has now reached the maximum value I_{DSS} .

When the V_{DS} is increased beyond V_p , the depletion layer expands the top of the channel. The channel now acts as a current limiter and holds drain current constant at I_{DSS} .



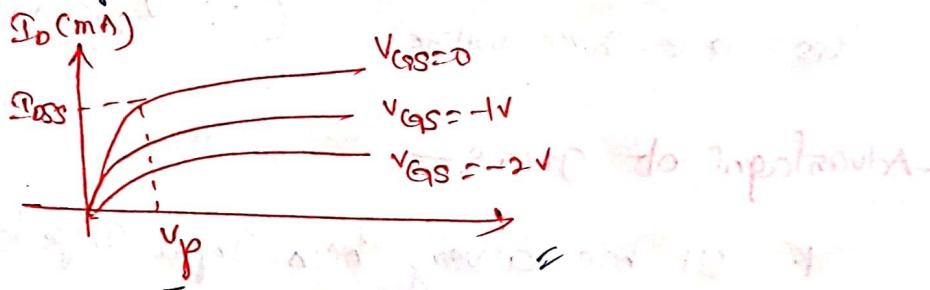
② Pinch off voltage It is the minimum drain-source voltage at which the drain current becomes constant.

→ The highest curve is for $V_{GS} = 0V$, the circuit (short) gate condition.

For values of V_{GS} greater than V_p , the drain current is almost constant.

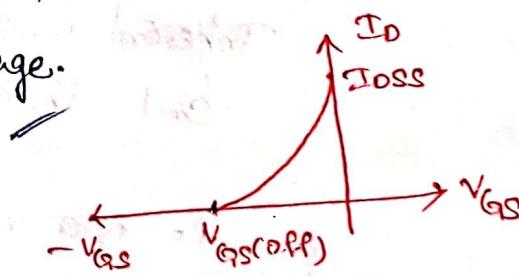
→ When V_{DS} is equal to V_p , the channel is effectively closed and does not allow further increase in drain current.

→ It may be noted that for proper function of JFET, it is always operated for $V_{DS} > V_p$.



③ Gate-Source Cutoff Voltage $V_{GS(Coff)}$ It is the gate-source voltage where the channel is completely cut off and the drain current becomes zero.

→ The gate voltage at which the channel is cut off is called Gate Source cutoff voltage.



Notes

① $V_{GS(Coff)}$ will always have the same magnitude value as V_p :

for Ex:- If $V_p = 6V$: $V_{GS(Coff)} = -6V$.

③. V_p is the value of V_{GS} that caused the JFET to become a constant current device. It is measured at $V_{GS} = 0V$ and will have a constant drain Current = I_{DSS} .

However, $V_{GS(\text{off})}$ is the value of V_{GS} that causes the I_D to drop to nearly zero.

Expression for Drain Current :-

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_p}\right)^2$$

(Or)

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_{GS(\text{off})}}\right)^2$$

I_{DSS} = shorted-gate drain current

V_{GS} = gate-source voltage

$$\therefore V_{GS(\text{off})} = V_p$$

Advantages of JFET :-

1. It has a very high input impedance. This permits high degree of isolation b/w the input & output circuits.

2. The operation of JFET depends upon the bulk material current carriers that do not cross junctions.

Inherent noise of tube (due to high-temperature) and those of transistor are not present in JFET.

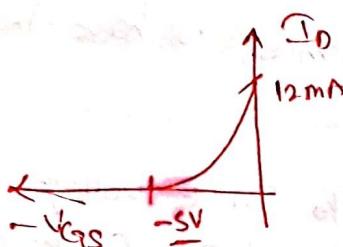
3. It is a negative temperature coefficient of Res. This avoids the risk of thermal runaway.

4. Higher power gain. Eliminated the necessity of using driver stages.

5. Smaller size, longer life, high efficiency.

Problems :-

① Figure shows the Transfer characteristic of a JFET. write the equation for a drain current?



Ans:- $I_{DSS} = 12 \text{ milli amp.}$

$$V_{GS(\text{off})} = -5 \text{ V}$$

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P} \right)^n$$

Ans:- $I_D = 12m \left(1 + \frac{V_{GS}}{5} \right)^n$

② A JFET has the following parameters:-

$$I_{DSS} = 32 \text{ milli amp.}, V_{GS(\text{off})} = -8 \text{ V}, V_{GS} = -4.5 \text{ Vols.}$$

Find the value of drain current?

Ans:-

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_P} \right)^n$$

$$= 32m \left(1 - \frac{4.5}{8} \right)^n$$

$$= 6.12 \text{ m amp.}$$

③ A JFET has a drain current of 5mA. If $I_{DSS} = 10 \text{ mamp.}$ and $V_{GS(\text{off})} = -6 \text{ volts.}$ Find the value of (i) V_{GS} (ii) $V_P.$

Ans:- $V_{GS} = -1.76 \text{ Vols}$

$$V_P = -V_{GS(\text{off})} = 6 \text{ Vols}$$

Advantages of FET :-

- ① It has good thermal stability.
- ② JFET can be used as a symmetrical bipolar switch.
- ③ By means of small charge stored on internal capacitance, it acts as a memory device.
- ④ It is simpler to fabricate and occupied less space in IC form. So package density is high.

A.C Drain Resistance :- (r_d) :-

It is denoted by r_d .

Corresponding to the A.C plate Resistance, we have the

A.C drain Resistance.

It is the ratio of change in the drain-to-source voltage to the change in the drain current at constant gate-source voltage i.e.,

$$\text{A.C drain Resistance } r_d = \frac{\Delta V_{DS}}{\Delta I_D} \text{ at const } V_{GS}$$

For instance, if a change in drain voltage of 2 Volts produced a change in the drain current of 0.02 milliamp.

$$\text{A.C Drain Resistance } r_d = \frac{2 \text{ Volts}}{0.02 \text{ mA}} = 100 \text{ k}\Omega$$

Trans Conductance :- (g_{fs}) :-

It is the ratio of change in drain current (ΔI_D) to the change in the gate-to-source voltage at constant drain-source voltage i.e.,

$$\text{Trans Conductance } (g_{fs}) = \frac{\Delta I_D}{\Delta V_{GS}} \text{ at const } V_{DS}$$

→ The control that the gate voltage has over the drain current is measured by trans conductance g_{fs} and is similar to the transconductance of tube (g_m).

→ Trans Conductance of a JFET is usually expressed either in millimhos (or microohms).

For example if a change in gate voltage of volts, causes them a change in drain current of 0.3 milliamp

Then, the transconductance $g_{fs} = \frac{0.3 \text{ mA}}{0.1} = 3 \times 10^3 \text{ mA/V}$
 $= 3000 \mu \text{hos}$

Amplification Factor (μ):-

It is the Ratio of change in drain-source voltage (ΔV_{DS}) to the change in the gate to source voltage at constant drain current. i.e.,

$$\text{Amplification Factor } \mu = \frac{\Delta V_{DS}}{\Delta V_{GS}} \rightarrow \text{constant } I_D.$$

Amplification factor of a JFET indicates how much more control the gate voltage has over drain current than has the drain voltage.

For instance, If a amplification factor of a JFET is 50, it means that the gate voltage is 50 Times as effective as the drain voltage in controlling the drain current.

Relation among JFET parameters:-

The Relationship among JFET parameters can be established as under, we have the

$$\mu = \frac{\Delta V_{DS}}{\Delta V_{GS}}$$

$$\Rightarrow \mu = \frac{\Delta V_{DS}}{\Delta V_{GS}} \times \frac{\Delta I_D}{\Delta I_D}$$

$$\mu = \frac{\Delta V_{DS}}{\Delta I_D} \times \frac{\Delta I_D}{\Delta V_{GS}}$$

$$\boxed{\mu = \beta \times g_{fs}}$$

Amplification factor = a.c drain Resistance \times Transconductance

① When a Reverse gate voltage of V_{GS} is applied to a JFET the gate current is 10^{-3} microamp. Find the Resistance b/w the gate & source?

$$V_{GS} = 15V ; I_D = 10^{-3} \mu\text{Amp.}$$

$$\Rightarrow \text{Gate to Source Resistance} = \frac{V_{GS}}{I_G} = \frac{15}{10^9} = 15 \times 10^9 \\ = 15,000 \text{ M}\Omega$$

② When V_{GS} of a JFET changes from -3.1 Volts to -3 V , the drain current changes from 1 miliamp to 1.3 miliamp . What is the value of transconductance?

$$\Delta V_{GS} = -3.1 + 3 = 0.1 \text{ Volts}$$

$$\Delta I_D = 1.3m - 1m = 0.3 \text{ miliamp.}$$

$$\text{Trans Conductance } g_{fs} = \frac{\Delta I_D}{\Delta V_{GS}} = \frac{0.3 \text{ miliamp}}{0.1 \text{ V}}$$

$$= 3 \text{ milliamp/Volts}$$

$$\therefore g_{fs} = 3000 \text{ microamp/Volts}$$

③. The following readings were obtained experimentally from a JFET:-

$$V_{GS} \quad 0V \quad 0V \quad -0.2V$$

$$V_{DS} \quad 2V \quad 15V \quad 15V$$

$$I_D \quad 10 \text{ mamp} \quad 10.25 \text{ mamp} \quad 9.65 \text{ miliamp.}$$

Determine ① a.c drain Resistance ② Transconductance
③ Amplification factor.

Solution:-

- ① With V_{GS} constant at 0V, the increase in V_{DS} from 7V to 15V increased the drain current from 10mA to 10.25mAmp p.e.,

Change in drain - source voltage $\Delta V_{DS} = 15 - 7 = 8 \text{ Volts}$

Change in drain Current $= \Delta I_D = 10.25 - 10 = 0.25 \text{ mAmp}$

$$\text{A.C Drain Resistance } = (r_d) = \frac{\Delta V_{DS}}{\Delta I_D}$$

$$\therefore r_d = 32 \text{ k}\Omega$$

- ② With V_{DS} constant at 15Volts, drain current changed from 10.25mAmp to 9.65mAmp as V_{GS} is changed from the 0Volts to -0.2 Volts.

$$\Delta V_{GS} = 0.2 - 0 = 0.2 \text{ Volts}$$

$$\Delta I_D = 10.25 - 9.65$$

$$\Delta I_D = 0.6 \text{ mAmp}$$

$$\therefore \text{Transconductance} : g_{fs} = \frac{\Delta I_D}{\Delta V_{GS}} = \frac{0.6 \text{ m}}{0.2} = 3 \text{ mA/V}$$

$$\therefore g_{fs} = 3000 \mu \text{mhos}$$

- ③ Amplification factor $\mu = g_{fs} \times r_d$

$$= 3000 \mu \times 32 \text{ k}$$

$$= \underline{96000 \text{ m}} = \underline{96}$$

$$\therefore \mu = 96$$

//,

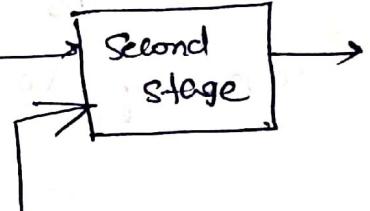
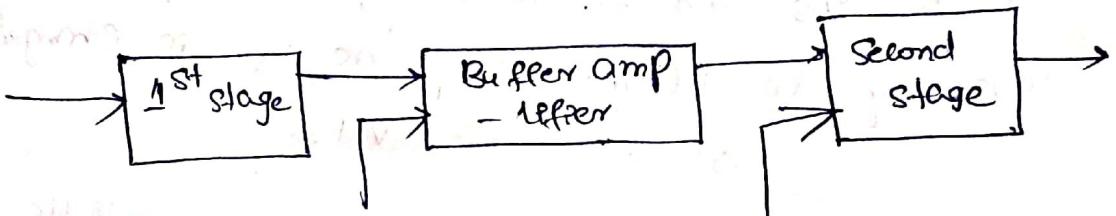
JFET Applications

The high Input Impedance, low output impedance and low noise level makes JFET more superior to the bipolar Junction Transistor.

Applications of JFET

- ① As a buffer amplifier.
- ② RF stage amplifier.
- ③ phase shift oscillator.

① As a buffer amplifier:



low output impedance.

All the output from the buffer reached to input of second stage.

The high Input Impedance of JFET means light loading of the preceding stage. This permits almost entire output from first stage to appear at buffer input side.

The low output impedance of JFET can drive heavy loads (or small load resistance). This ensures the all the output from the buffer reached to input of second stage.

⑥ Phase shift oscillators

The high input impedance of JFET is especially valuable in phase-shift oscillators to minimize the loading effect.

⑦ As RF amplifier :-

In Communication Electronics, we have to use RF (JFET) Amplifier in a Receiver instead of BJT Amplifier for the following reasons.

- =. ① The noise level of a JFET is very low. The JFET will not generate significant amount of noise and is thus useful as an RF amplifier.
- ② The Antenna of the Receiver receives weak signal that has an extremely low amount of Current. Since JFET is voltage controlled device, it will respond to low current signal provided by the antenna.

Metal Oxide Semiconductor FETs - (MOSFET)

1. It is an important Semiconductor device and is widely used in many circuit applications.
2. The Input impedance of a MOSFET is much more than that of JFET because of very small leakage current.
3. The MOSFET can be used in any of Circuits covered for the JFET.

Therefore, all the equations apply equally well to the MOSFET and JFET in amplifier circuits.

Construction Details

① It shows the construction details of n-channel MOSFET. It is similar to JFET except with the following modifications.

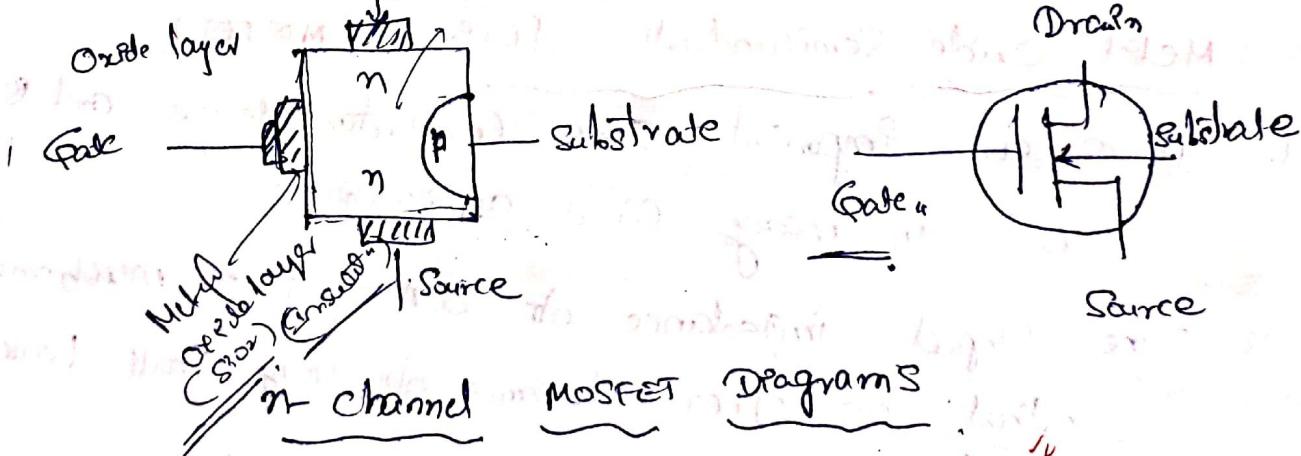
No: ① There is only one single p-region. The Region is called Substrate.

② A thin layer of metal oxide layer is deposited over the left side of the channel, and metal gate is deposited over the oxide layer.

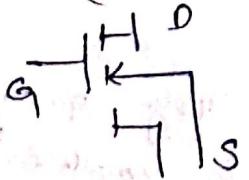
As SiO_2 is an insulator, gate is insulated from the channel. For this reason, MOSFET is sometimes called insulated gate FET.

③ Like JFET, a MOSFET has three terminals.

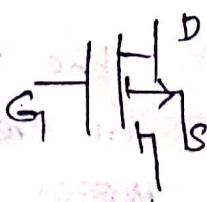
① Source, gate, drain.



n-channel MOSFET
(enhancement)

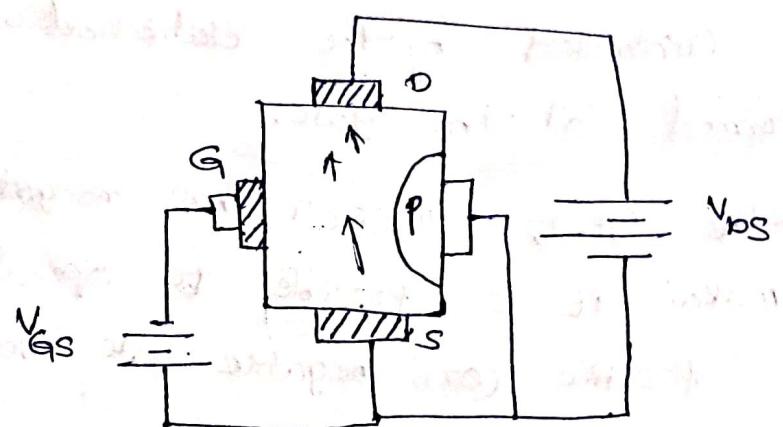


p-channel MOSFET



Working Principle of MOSFET:- (Enhancement MOSFET),

- Figure shows the circuit diagram of MOSFET.



- Instead of gate diode as in JFET, here the gate is formed as the small capacitor.
- One plate of the capacitor is the gate and other plate is the channel with metal oxide as the dielectric.
- When the -ve voltage is applied to the gate, electrons are accumulated at Pt. These electrons repel the conduction band electrons in the n-channel. Therefore less number of electrons are made available for current conduction through the channel.

- The greater negative voltage on the gate, the lesser is the current conduction from the source to drain.

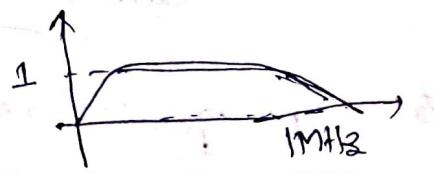
- If the gate is given positive voltage, more electrons are made available in the n-channel. Consequently, current from the source to drain increases.

1. In a mosFET, the Source to drain Current is controlled by the electric field or capacitor formed at the gate.
2. Unlike the JFET, a mosFET has no gate diode. This makes it is possible to operate the device with positive (or) negative gate voltage.
3. As the gate forms a capacitor, therefore, negligible current flows from the whether positive (or) negative voltage is applied to gate.

Gain Bandwidth Product:

Gain Bandwidth Product of an operational amp is 1MHz, it means that the gain of the device falls to unity at 1MHz. When the device is wired for unity gain, it will work up to 1MHz without excessively distorting the signal.

$$\underline{\text{Gain} \times \text{BW}} = 1$$



Enhancement Mode MOSFET

Operation: 1. If the Substrate is grounded, and a positive voltage is applied to the gate, the positive charge on the Gate "G" induced an equal amount of negative charge on the Substrate side below the Source and drain regions.

Thus an electric field is produced b/w the source and drain regions.

The direction of electric field is perpendicular to the plates of capacitor through the oxide.

The negative charge of electrons which are minority charge carriers in the P-type substrate forms an inversion layer. As the positive voltage on the gate increases, the induced negative charge in the semiconductor increases. Hence, the conductivity increased and current flows from source to drain through channel. The drain current is enhanced.

h-Parameters

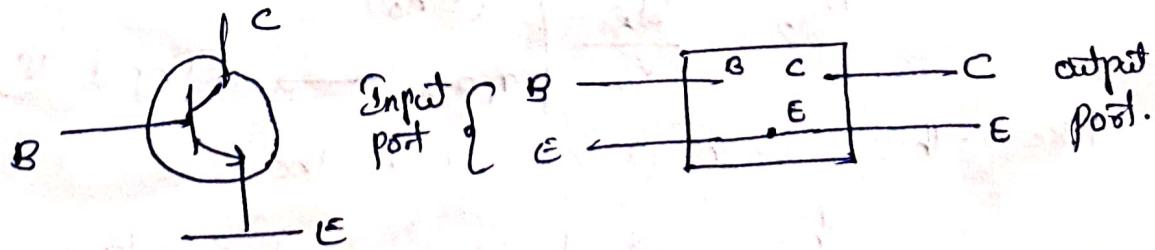
(Transistor at low frequencies)

plan :-

BJT as a Two-port network

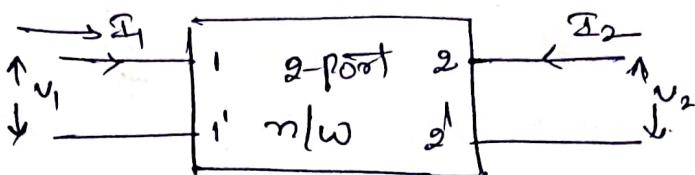
1. BJT is a 3-terminal electronic device, the three terminals are Emitter (E), base (b), Collector (C). During normal operation as an amplifier, the weak A.C. signal is applied between one pair of terminals (B and E in a CE amplifier), and the amplified signal (C and E in a CE amplifier).

Thus in a CE Transistor amplifier, the Emitter is common to the both input and output ports, and the virtually becomes a 2-port network.



II-parameters

Explanation :-



$$V_1 = f(I_1, V_2)$$

$$\textcircled{2} \quad I_2 = f(I_1, V_2)$$

Express the dependent variables in terms of independent variable
Because pt is a Current Controlled device.

$$V_1 = h_{11} I_1 + h_{12} V_2 \quad \textcircled{1}$$

So I_1, V_2 Independent

$$I_2 = h_{21} I_1 + h_{22} V_2 \quad \textcircled{2}$$

V_1, I_2 dependent

Hence $h_{11}, h_{12}, h_{21}, h_{22}$ are called hybrid parameters.

clear: $h_{11} = \frac{V_1}{I_1} \Big|_{V_2=0} \quad (= h_\pi) \rightarrow$ Output is short circuited.

$$h_{21} = \frac{I_2}{I_1} \Big|_{V_2=0} \quad (= h_f) \rightarrow$$
 Output is short circuited.

$$h_{12} = \frac{V_1}{V_2} \Big|_{I_1=0} \quad (= h_{sr}) \rightarrow$$
 Input is open circuited.

$$h_{22} = \frac{I_2}{V_2} \Big|_{I_1=0} \quad (= h_o) \rightarrow$$
 Input is open circuited.

Like this we call pt as the

h_{11} = short circuit input impedance parameter.

h_{21} = short circuit forward current transfer Ratio.

h_{12} = Open - Circuit Reverse Voltage Transfer Ratio.

h_{22} = Open - Circuit f. Admittance Parameters,
output

clear:

$h_{11}, h_{12}, h_{22}, h_{21}$ → are called hybrid parameters.

$$h_{11} = \frac{V_1}{I_1} \left| \begin{matrix} V_2=0 \\ I_2=0 \end{matrix} \right. ; \quad h_{12} = \frac{V_1}{V_2} \left| \begin{matrix} I_1=0 \\ I_2=0 \end{matrix} \right. ; \quad h_{21} = \frac{I_2}{I_1} \left| \begin{matrix} V_2=0 \\ I_2=0 \end{matrix} \right. ;$$

$$h_{22} = \frac{I_2}{V_2} \left| \begin{matrix} I_1=0 \\ I_2=0 \end{matrix} \right. ;$$

$$\Rightarrow h_{11} = h_p$$

$$h_{12} = h_r$$

$$h_{21} = h_f$$

$$h_{22} = h_o$$

\Rightarrow i) $V_P = h_p I_P + h_r V_O$, and we have the

ii) $I_O = h_p I_P + h_o V_O$

\Rightarrow The above holds good for any transistor operating in
Relationships

CB, CE, CC mode.

\rightarrow For a CE Transistor mode, we have

$$V_P = h_{pe} I_P + h_{re} V_O$$

$$I_O = h_{pe} I_P + h_{oe} V_O$$

\rightarrow For a CB Transistor mode, we have

$$V_P = h_{pb} I_P + h_{rb} V_O$$

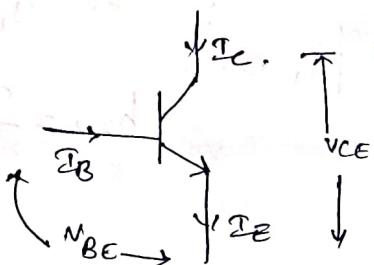
$$I_O = h_{pb} I_P + h_{ob} V_O$$

And, also for a cc Transistor amplifier, we have the
 $v_p = h_{pc} I_p + h_{rc} v_o.$

$$I_o = h_{pc} I_p + h_{rc} v_o. \quad \text{and}$$

For example

Let us consider the CE configuration.



From this Circuit

$$I_p = I_b; \quad v_o = v_{CE}; \quad v_p = v_{BE}$$

$$I_o = I_c.$$

$$V_1 = h_{11} I_p + h_{12} V_2$$

$$V_2 = h_{21} I_p + h_{22} V_1.$$

All parameters for the above circuit \Rightarrow

$$\Rightarrow v_{BE} = h_{re} I_b + h_{re} V_o.$$

$$I_c = h_{pc} I_b + h_{oc} v_{CE}.$$

My

CB

$$I_p = I_E; \quad I_o = I_c; \quad V_p = V_{BE}; \quad V_o = V_{CB}.$$

$$\Rightarrow V_{BE} = h_{re} I_E + h_{re} V_{CB}.$$

$$I_c = h_{pc} I_E + h_{oc} V_{CB}.$$

My

CC

$$I_p = I_b; \quad I_o = I_E; \quad V_o = V_{CE}; \quad V_p = V_{BC}$$

$$\Rightarrow V_{BC} = h_{pc} I_b + h_{rc} V_{CE}$$

$$I_E = h_{pc} I_b + h_{oc} V_{CE}.$$

Note:-

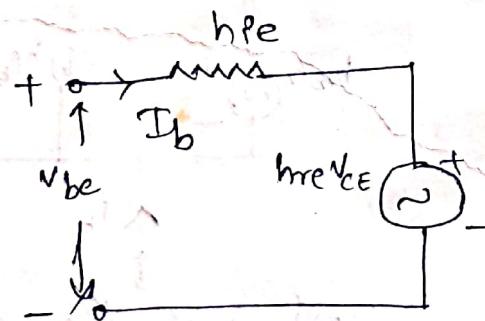
1. The First of the above Equation is called the "Voltage Equation" and Second of the above Equation is called the "Current Equation".

2. h_{fe} is Input Impedance }
 h_{oe} is Out Impedance }
- If there is no
reactive elements
in the circuit, then
we can calculate
it as the
 \Rightarrow Resistance
- $$\Rightarrow Z = R + jX; \quad Y = G + j\omega C$$
- $$Z = R + jX \quad Y = G + j\omega C$$

If $X = 0$: for both two cases

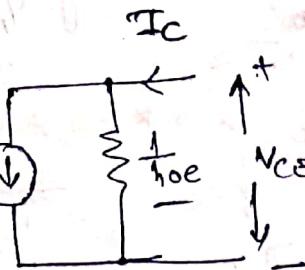
Then $Z = R; \quad Y = G$

Let us consider the circuit diagrams



$$\Rightarrow V_{be} = h_{fe}I_b + h_{re}V_{CE}$$

$$I_c = h_{fe}I_b + \frac{V_{CE}}{(Yh_{oe})}$$

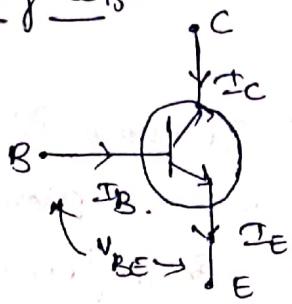


$$\Rightarrow I_c = h_{fe}I_b + h_{re}V_{CE}$$

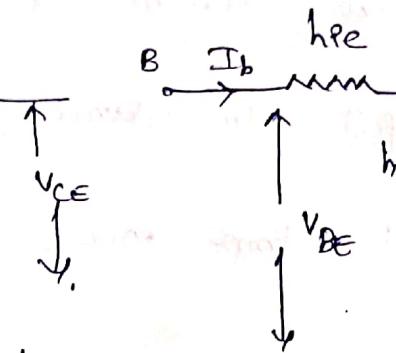
- Notes:- ① Here "h_{re}V_{CE}" — dependent Voltage Source
 ② And also "h_{fe}I_b" — dependent Current Source

Now the Transistor Amplifier can be replaced by
the same equivalent Circuits.

Symbol :-

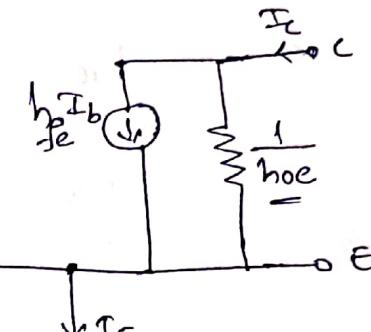


① Circuit Symbol



$$V_{BE} = h_{fe} I_B + h_{re} V_{CE}$$

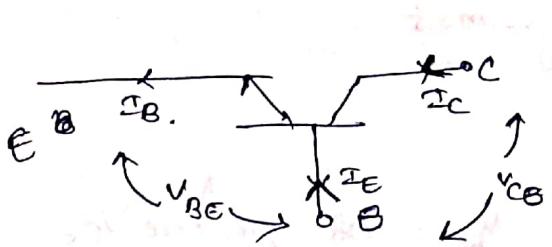
$$I_C = h_{fe} I_B + h_{re} V_{CE}$$



hybrid equivalent Circuit diagram

My (CCB) :-

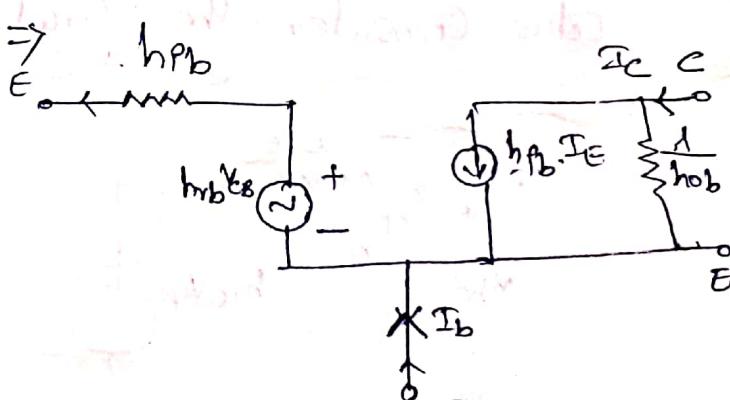
Symbol :-



② Circuit Symbol

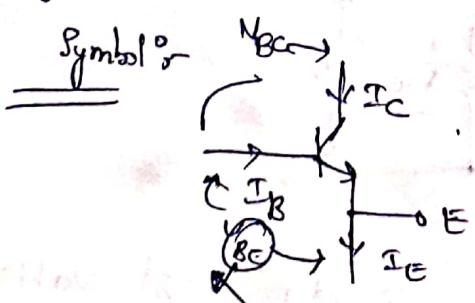
$$V_{BE} = h_{fb} I_E + h_{re} V_{CB}$$

$$I_C = h_{fb} I_E + h_{re} V_{CB}$$



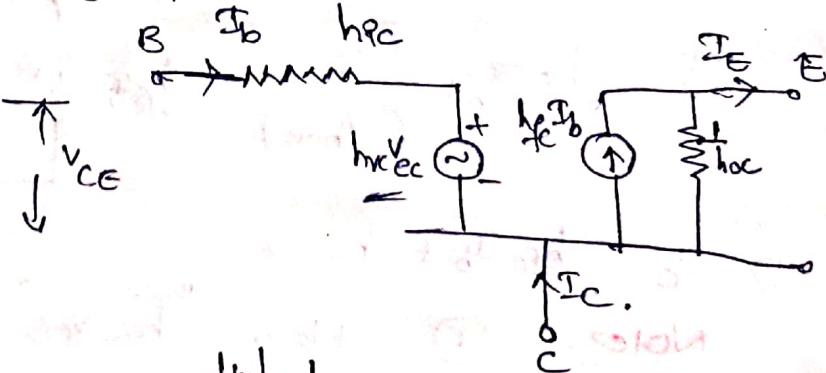
hybrid equivalent Circuit diagram.

My (CC) :-



$$V_{CE} = h_{fe} I_B + h_{re} V_{CE}$$

$$I_E = h_{fe} I_B + h_{re} V_{CE}$$



hybrid equivalent Circuit diagram

Typical parameter values

H₁-parameters

Mode of operation

		CB	CE	CC
1.	h_{11} (ohms)	20	1000	1000
2.	h_{12}	3×10^4	9.5×10^4	≈ 1
3.	h_{13}	-0.98	50	-50
4.	Y_{11} (K \cdot A)	2000	40	40

Y_{11} = output resistance.

Conversion formulae

Combinations of CB, CE, CC configurations are interconnected, and the conversion formulae are given below here:

CB	CE	CC
$h_{11b} = \frac{h_{11e}}{1+h_{11e}}$	$h_{11e} = \frac{h_{11b}}{1+h_{11b}}$	$h_{11c} = h_{11e}$
$h_{12b} = \frac{h_{12e}}{1+h_{11e}}$	$h_{12e} = \frac{h_{12b}}{1+h_{11b}}$	$h_{12c} = h_{12e}$
$h_{13b} = -\frac{h_{13e}}{1+h_{11e}}$	$h_{13e} = -\frac{h_{13b}}{1+h_{11b}}$	$h_{13c} = -(1+h_{11e})$
$h_{11b} = \frac{h_{11e} \cdot h_{12e}}{1+h_{11e}} - h_{13e}$	$h_{11e} = \frac{h_{11b} \cdot h_{12b}}{1+h_{11b}} - h_{13b}$	$h_{11c} \approx 1$

Ans- 1. CB parameters are obtained directly from the CE parameters, by replacing the e by b.

2. Similarly CE parameters are obtained from CB parameters by replacing "b by e".

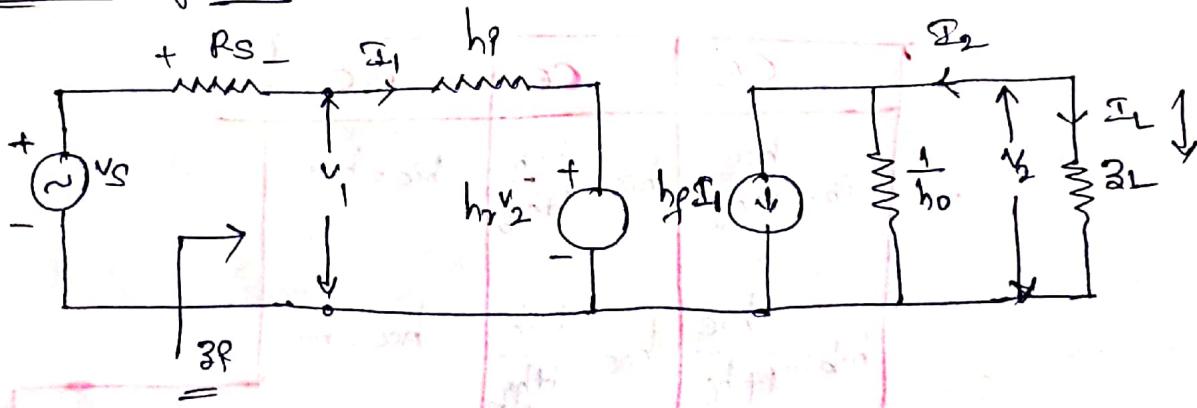
Transistor Amplifier Parameters

The following parameters are of importance, in the context of a transistor amplifier...

1. Input Impedance (Z_I)
2. Output Impedance (Z_O)
3. Current Gain (A_I)
4. Voltage Gain (A_V)

whatever the mode of operation, the Transistor can be visualised as a 2-port network, and hence the amplifier can be visualized (or) represented as the

Circuit Operation



Current gain of the Transistor Amplifier is the ratio of the Output Current to Input Current.

It is denoted by $A_I = \frac{\text{Output Current}}{\text{Input Current}}$

$$A_I = \frac{I_L}{I_p} = -\frac{I_2}{I_1}$$

$$I_2 = ?$$

$$V_2 +$$

$$I_2 + h_f I_1 + \frac{V_2}{(1+h_o)} = 0 \quad \text{--- (1)}$$

$$\Rightarrow I_2 = h_f I_1 + h_o V_2.$$

$$\text{But } V_2 = ?$$

$$I_2 = h_f I_1 + h_o (+I_L \beta_L)$$

$$I_2 = h_f I_1 + h_o (-I_2 \beta_L)$$

$$I_2 (1 + h_o \beta_L) = h_f I_1$$

$$\Rightarrow -\frac{I_2}{I_1} = \frac{h_f}{1 + h_o \beta_L}$$

$$\Rightarrow A_I = -\frac{h_f}{1 + h_o \beta_L}$$

This is the most general form of the expression for current gain.

Input Impedance (Z_I)

The Input Impedance of a Transistor Amplifier is the Impedance we can see, looking into input terminals.

$$\text{Input Impedance } Z_I = \frac{V_I}{I_I}$$

$$-V_I + h_f I_1 + h_o V_2 = 0.$$

$$V_I = h_f I_1 + h_o V_2$$

$$\text{clear } V_2 = I_L \beta_L \Rightarrow V_2 = -\frac{I_2 \beta_L}{1 + h_o \beta_L}$$

$$V_P = h_P I_P + h_R (-I_2 B_L)$$

$$V_P = h_P I_1 + h_R (-I_2 B_L)$$

$$I_1 = h_P I_1 + h_R \left(-\frac{I_1 \cdot h_F}{1+h_O R_L} \right) \cdot B_L$$

$$\Rightarrow \boxed{\frac{N_1}{I_1} = h_P - \frac{h_R h_F}{1+h_O R_L} \cdot B_L}$$

(on)

$$\boxed{\frac{V_1}{I_1} = h_P - \frac{h_R h_F}{1+h_O R_L} \cdot R_L}$$

Voltage gain — $(A_V)^o$ —
voltage gain of the Transistor amplifier is the ratio of the output voltage to the input voltage.

then $A_{VS} = ?$

$$A_{VS} = \frac{V_S}{V_S}$$

$$= \frac{N_2}{V_1} \cdot \frac{N_1}{V_S}$$

$$A_{VS} = A_V \cdot \frac{V_1}{V_S}$$

Input Current

$$I_1 = \frac{V_1}{R_S + B_L}$$

$$V_1 = I_1 B_L$$

$$\Rightarrow A_V = \frac{V_2}{V_1} = \frac{+I_L B_L}{V_1}$$

$$= \frac{-I_2 \cdot B_L}{V_1}$$

$$= + \frac{A_I \cdot I_P \cdot B_L}{V_P}$$

$$\Rightarrow \boxed{A_V = \frac{-A_I \cdot B_L}{B_L}}$$

$$N_1 = \left(\frac{V_S \cdot 3P}{R_S + 3P} \right) \quad //$$

$$\therefore A_{VS} = \frac{A_V \cdot 3P}{R_S + 3P} \quad //$$

If, in the above Expression if we get $R_S = 0$ then

$$A_{VS} = \frac{A_V \cdot 3P}{3P}$$

$$\therefore A_{VS} = A_V \quad //$$

My $\therefore A_{IS} = ? \quad //$

$$A_{IS} = \frac{I_1}{I_S}$$

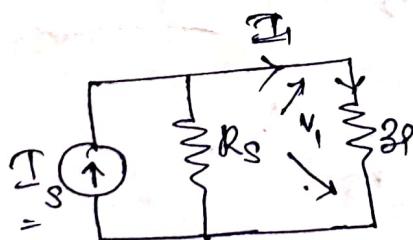
or

$$A_{IS} = -\frac{I_2}{I_S} \quad \text{since } I_1 = -I_2 \quad //$$

$$A_{IS} = -\frac{I_2}{I_1} \cdot \frac{I_1}{I_S}$$

If input is Current Source:

From the Circuit diagram (Input side)



$$-I_S + \frac{V_1}{R_S} + I_P = 0.$$

$$\Rightarrow I_1 = I_S - \frac{V_1}{R_S}$$

$$\therefore \frac{I_1}{I_S} = \frac{R_S}{R_S + 3P} \quad //$$

$$\therefore A_{IS} = A_I \cdot \frac{R_S}{R_S + 3P}$$

$$I_1 = I_S - \frac{I_S \cdot 3P}{R_S}$$

$$I_1 \left(1 + \frac{3P}{R_S}\right) = I_S \quad \Rightarrow$$

$$\frac{I_1}{I_S} = \frac{R_S}{R_S + 3P}$$

Output Admittance $\text{Y}_o = (\text{Y}_D)$.

Output Admittance $(\text{Y}_D) = \frac{1}{30}$.

$$\text{Y}_D = \frac{1}{(\frac{V_2}{I_2})} = \frac{I_2}{V_2}$$

from output loop

$$-I_2 + h_f I_p + \frac{V_2}{(\text{Y}_{ho})} = 0$$

$$-I_2 + h_f I_p + h_o V_2 = 0$$

$$\Rightarrow I_2 = h_f I_p + h_o V_2$$

$$\Rightarrow \frac{I_2}{V_2} = h_f \left(\frac{I_p}{V_2} \right) + h_o$$

Again from Circuit diagram, Input Side ✓

Input loop

By applying KVL:- $-V_1 + h_r I_p + h_r V_2 = 0$

$$\text{If } V_1 = 0 \Rightarrow \text{Then } V_1 = -I_1 R_S$$

$$\Rightarrow I_1 R_S + h_r I_p + h_r V_2 = 0$$

$$\frac{I_p}{V_2} = -\frac{h_r}{R_S + h_r}$$

$$\Rightarrow \frac{I_2}{V_2} = h_f \left(\frac{-h_r}{h_r + R_S} \right) + h_o$$

Output admittance is dependent upon the same resistance

$$h_o = \frac{I_2}{V_2} = -\frac{h_f h_r}{h_r + R_S} + h_o$$

$$\therefore j_o = h_o - \frac{h_r h_f}{h_r + R_S}$$

Example Problems

① A Voltage Source V_S of internal resistance $R_S = 750\Omega$, drives a CE Transistor amplifier. The load R_L is a resistance of 2000Ω . The h-parameters are: $h_{RE} = 1000\Omega$, $h_{RE} = 2.5 \times 10^4$, $h_{FE} = 50$ and $h_{OE} = 25\mu A/V$.

Find the ① Current gain ② Voltage gain ③ Overall current gain A_{IS} ④ Overall voltage gain ⑤ Input impedance ⑥ Output impedance Z_O . Also compute the power gain.

Ans^o

$$\textcircled{1} \quad \text{Current gain } A_I = -\frac{h_{FE}}{1+h_{OE}R_L}$$

$$A_I = -\frac{-50}{1 + (25\mu A/V \cdot 2000)}$$

$$R_L = 2000\Omega$$

$$R_S = 750\Omega$$

$$h_{RE} = 1000\Omega$$

$$h_{RE} = 2.5 \times 10^4$$

$$h_{FE} = 50$$

$$h_{OE} = 25\mu A/V$$

$$A_I = -47.6190$$

$$\textcircled{2} \quad \text{Voltage gain } A_V = \frac{A_I \cdot Z_L}{Z_P}$$

Here $Z_P = \text{Input Impedance}$

$$A_V = \frac{A_I \cdot Z_L}{Z_P}$$

$$= \frac{(-47.6190) \times 2000}{976.190}$$

$$Z_P = h_{RE} + h_{RE} A_I \cdot Z_L$$

$$= h_{RE} + \frac{h_{RE} h_{FE}}{1+h_{OE} R_L} \cdot R_L$$

$$\Rightarrow Z_P = 1000 + \frac{(2.5 \times 10^4 \times 50) \times 2000}{1 + (25\mu A/V \times 2000)}$$

$$= 1000 - 23.8095$$

$$\underline{Z_P = 976.190 \text{ ohms}}$$

$$A_V = -97.5608$$

\Rightarrow

(iii). Overall Current gain (A_{IS}) = ?

$$A_{IS} = \frac{A_I \cdot R_S}{R_S + 3\beta}$$

$$\Rightarrow A_{IS} = \frac{(-47.6190) \times 750}{750 + 976.190}$$

$$A_{IS} = -20.6896$$

(iv). Overall Voltage gain (A_{VS}) = ?

$$A_{VS} = \frac{A_V \cdot 3\beta}{R_S + 3\beta}$$

$$= \frac{(-97.5608) \times (976.190)}{750 + (976.190)}$$

$$\Rightarrow A_{VS} = -55.172$$

v. Output Admittance:-

$$y_0 = h_o - \frac{h_{re}}{h_{re} + R_S}$$

$$y_0 = (25\text{m}) - \frac{(2.5 \times 10^4 \times 50)}{1000 + 750}$$

$$\Rightarrow y_0 = 1.7857 \times 10^{-5}$$

$$\Rightarrow y_0 = 1.7857 \times 10^{-5}$$

Output Impedance: $Z_0 = \frac{1}{y_0} = 56,000$

$$\underline{Z_0 = 56\text{k ohms.}}$$

(vii)

$$\text{Power gain} = \text{Current gain} \times \text{Voltage gain}$$

$$A_p = A_I \times A_V$$

$$= (-47.6190) \times (-97.5760)$$

$$= 4,646.47$$

$$A_p = 4.646 \text{ k} \quad \underline{\underline{}}$$

Answers :-

$$A_I = -47.6190, \quad Z_P = 976.190 \Omega; \quad A_V = -97.5760,$$

$$A_{IS} = -20.6896; \quad A_{VS} = -55.172; \quad Y_0 = 1.7852 \times 10^5 \text{ V}$$

$$Z_0 = 5 \text{ k ohms}; \quad A_p = 4,646.47.$$

- (2) A Common base Transistor has the following h-parameters
 $h_{FB} = 20, \quad h_{RB} = 3 \times 10^4, \quad h_{EF} = -0.98, \quad h_{OB} = 5 \times 10^3 \text{ mhos}$. It is driven by voltage source V_S of internal resistance $R_S = 1000 \Omega$. If the load resistance is 3000Ω , find A_I, A_V, A_{IS}, A_{VS} , Z_P, Z_0 and A_p ?

Current gain

$$\textcircled{1} \quad A_I = \frac{-h_{FB}}{1 + h_{OB} \cdot R_L}$$

$$A_I = \frac{-(-0.98)}{1 + (5 \times 10^3) \times 3000}$$

$$A_I = 0.97853$$

Voltage gain

$$\textcircled{2} \quad A_V = \frac{A_I \cdot Z_L}{Z_P}$$

$$A_V = 140.593$$

CB - Configuration

$$h_{FB} = 20$$

$$h_{RB} = 3 \times 10^4$$

$$h_{EF} = -0.98$$

$$h_{OB} = 5 \times 10^3 \text{ mhos}$$

$$R_S = 1000 \Omega$$

$$R_L = 3000 \Omega$$

$$Z_P = h_{FB} - \frac{h_{RB} \cdot R_L}{1 + h_{OB} \cdot R_L}$$

$$Z_P = 20 - \frac{(3 \times 10^4 + -0.98) \times 3000}{1 + 5 \times 10^3 \times 3000}$$

$$= 20.880$$

(iv). Overall Current gain (A_{IS}) = ?

$$A_{IS} = \frac{A_I \cdot R_S}{R_S + 2f}$$
$$= \frac{(0.97853) \times (1000)}{1000 + 20.880}$$

$$A_{IS} = \underline{\underline{0.9585}}$$

(v). Overall Voltage gain (A_{VS}) = ?

$$A_{VS} = \frac{A_V \cdot 2f}{2f + R_S}$$
$$= \frac{(140.593) \times (20.880)}{20.880 + 1000}$$

$$A_{VS} = \underline{\underline{2.8755}}$$

(vi) Output Admittance (y_o) = ?

$$y_o = h_o - \frac{h_i h_f}{h_f + R_S}$$
$$= (5 \times 10^{-7}) - \frac{(3 \times 10^4 \times 0.98)}{20 + 10000}$$
$$= (5 \times 10^{-7}) + \frac{(3 \times 10^4 \times 0.98)}{1020}$$

$$y_o = \underline{\underline{7.882 \times 10^{-7}}}$$

$$y_o = \underline{\underline{788.23 n^{-7}}}$$

$$\text{Output Impedance } Z_o = \frac{1}{y_o} = \underline{\underline{1.2686 M \text{ ohms}}}$$

(vip) Power gain $A_p = A_V \times A_I$

$$= (140.593) \times (0.97853)$$

$$A_p = \underline{\underline{137.524}}$$

(3) A voltage source V_S of internal resistance $R_S = 800\Omega$, drives a cc-transistor amplifier. The load resistance R_L is 2500Ω . The transistor h-parameters are $h_{PC} = 1000$, $h_{RC} = 1$, $h_{FC} = -50$, $h_{OC} = 25u\text{amp/V}$. Compute A_I , A_{IS} , A_V , A_{VS} , β_P , β_0 and power gain?

Ans:-

i) Current gain

$$A_I = \frac{-h_{FC}}{1+h_{OC}R_L}$$

$$= \frac{-(-50)}{1 + (25u)(2500)}$$

$$= \frac{50}{1.0625}$$

$$A_I = 47.058$$

ii) Overall Current gain

$$A_{IS} = \frac{A_I \cdot R_S}{R_S + \beta_P}$$

$$A_{IS} = \frac{A_I \cdot R_S}{R_S + \beta_P} \quad \text{But } \beta_P = ?$$

$$\beta_P = h_{PC} - \frac{h_{RC}h_{FC}}{1+h_{OC}R_L} \cdot R_L$$

$$= 1000 - \frac{(1)(-50)(2500)}{1 + (25u)(2500)}$$

$$\beta_P = \underline{118.64K \text{ ohms}}$$

$$R_S = 800\Omega$$

$$R_L = 2500\Omega$$

$$h_{PC} = 1000$$

$$h_{RC} = 1$$

$$h_{FC} = -50$$

$$h_{OC} = 25u\text{amp/V}$$

(iii) Voltage gain

$$A_V = \frac{A_I \cdot Z_L}{R_P}$$

$$= \frac{(47.058) \times 2500}{118.64K} = \underline{\underline{11.75}}$$

$$= 0.99155$$

$$\approx \underline{\underline{1}}$$

Overall voltage gain

$$A_{VS} = \frac{A_V \cdot R_P}{R_P + R_S}$$

$$= \frac{(0.99155) \times (118.64K)}{118.64K + 800}$$

$$= \underline{\underline{0.9849}}$$

$$A_{VS} \approx \underline{\underline{1}}$$

(iv)

Output Impedance:-

$$Z_O = h_o - \frac{h_{rf} h_{if}}{h_{if} + R_S}$$

$$= (250) - \frac{1 \times (-50)}{1000 + 800}$$

$$Z_O = \underline{\underline{27.80m \Omega}}$$

$$Z_0 = \frac{1}{Z_O} = \frac{1}{27.80m}$$

$$\rightarrow Z_0 = \underline{\underline{35.96 \Omega}}$$

(v)

Power gain

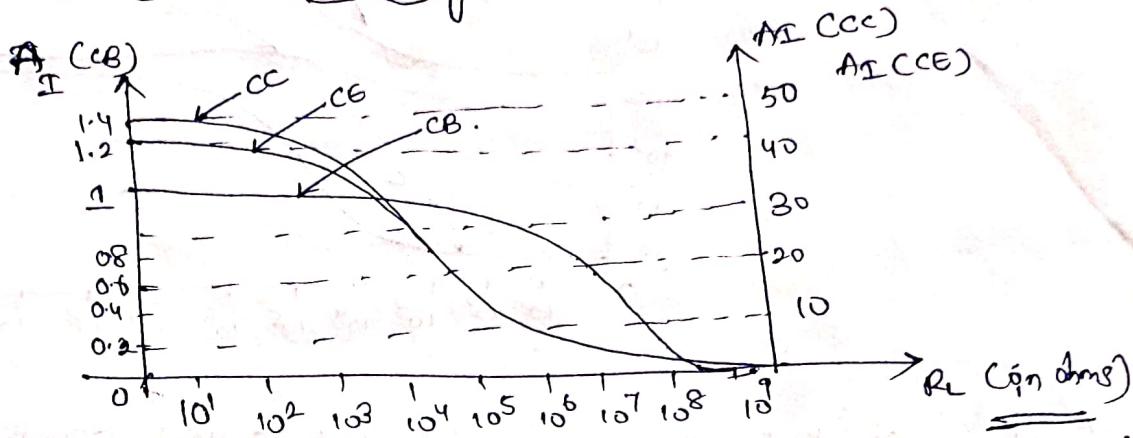
$$A_P = A_V \times A_I$$

$$= \underline{\underline{46.66D}}$$

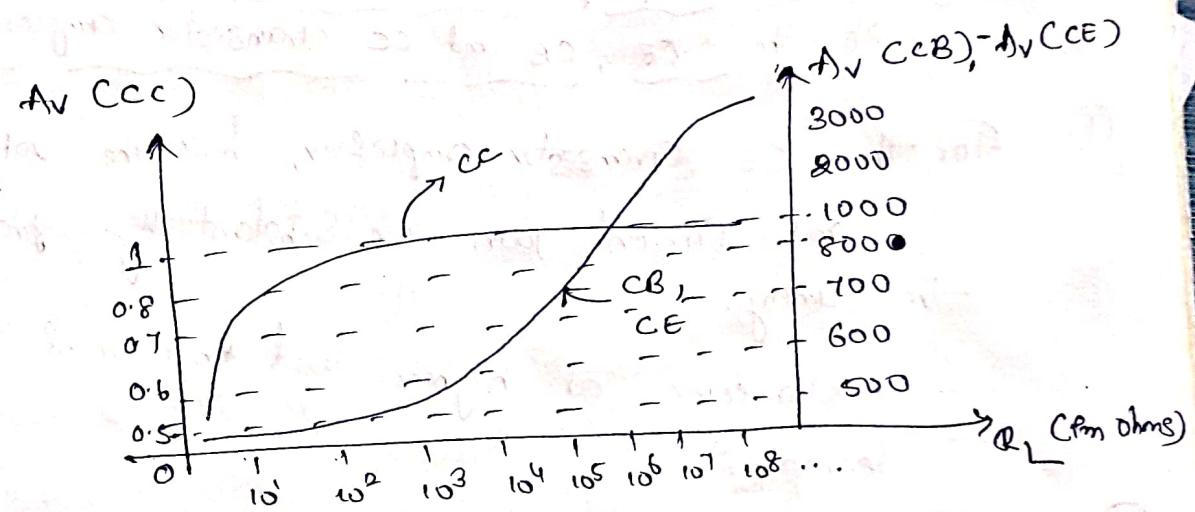
Variation of A_f , A_v , β_f and Z_o -

A_f , A_v , β_f and Z_o are vary with the load impedance.

(i)

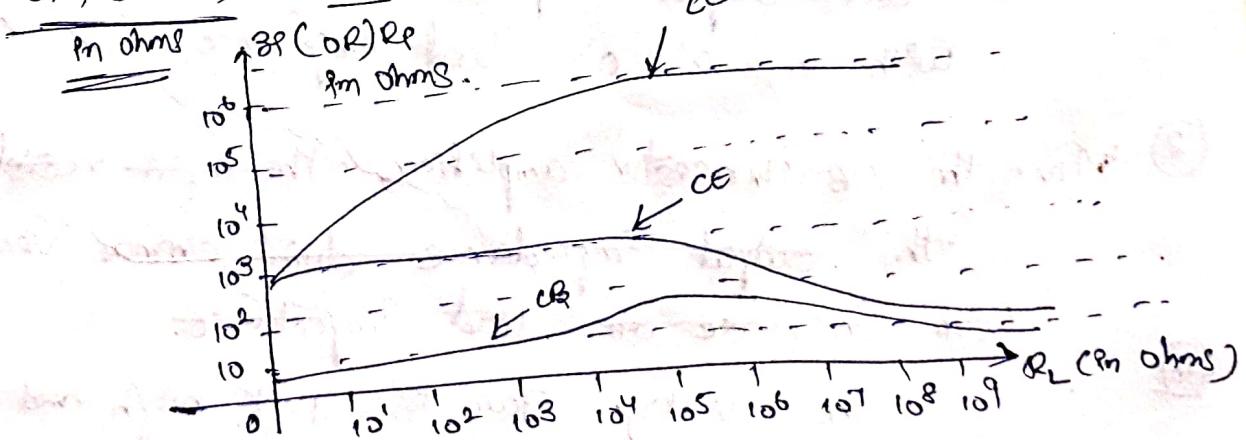


(ii)



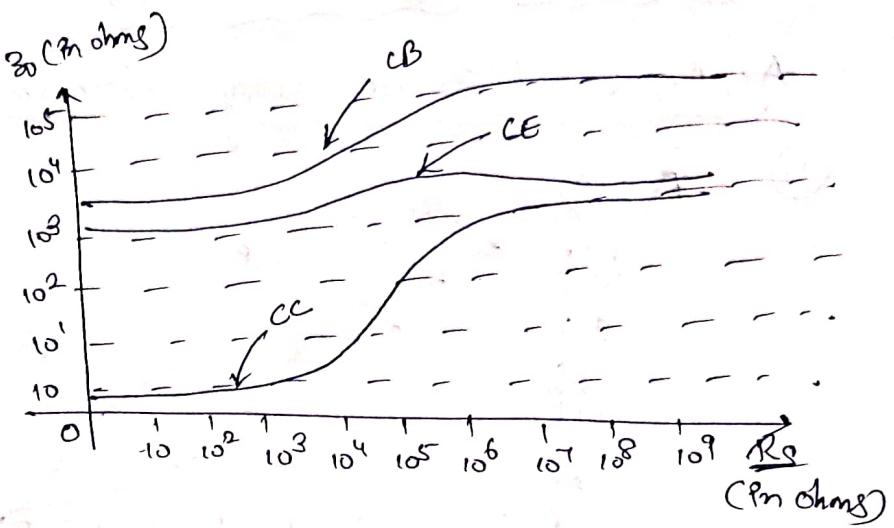
(iii)

Z_{out} (or R_p) vs Z_L



(iv)

$$=\frac{30}{15} \cdot \frac{R_S}{R_L}$$



A study of these graphs reveals that sixteen aspects of performance of the CE, CB and CC transistor amplifiers,

- ① For the CE Transistor amplifier, both the voltage gain and Current gain are substantially greater than the unity.
→ However at higher load impedances, Current gain decreases.
- ② For the CE Transistor amplifier, the input impedance is and output impedance do not change very much with increase of load impedance.
- ③ For the CB Transistor amplifier, the input resistance and the output impedance do not change very much, with increase of load impedance.
- ④ → The voltage gain is quite high and it is increased with R_L , although gain is less than unity.
- ⑤ For the CB Transistor amplifier, the input resistance is the least, and output impedance is the highest. Its find useful application, when a load (high imped.) is

required a to be driven from the low impedance source.

- ⑤ For the CC - Transistor amplifier, the current gain is quite high, but the voltage gain is less than unity.
- ⑥ For CC — R_f is highest, R_o is lowest.
— The main application of CC is buffer stage b/w a high impedance source and low impedance load.
- ⑦ The CB - Configuration ideally suits when a constant current source is needed.

Comparison of the Three Configurations

<u>Parameter</u>	<u>CE</u>	<u>CC</u>	<u>CB</u>
1. Current gain	High	High	Low
2. Voltage gain	High	Low	High
3. Input impedance	Medium	High	Low
4. Output impedance	Medium	Low	High

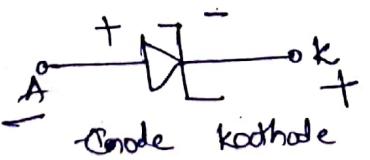
Regulators & Regulation

Zener diode :-

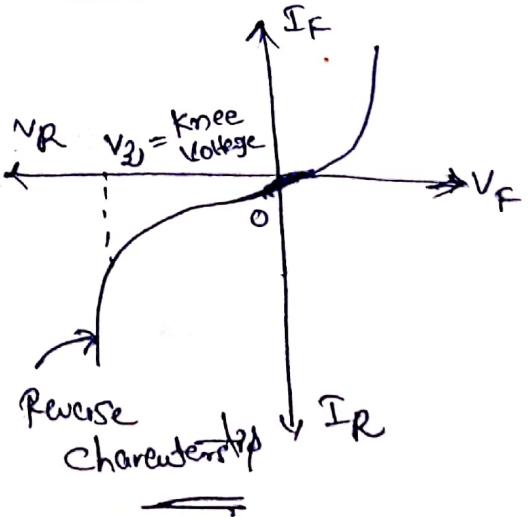
A ^{heavily} ~~properly~~ doped crystal diode which has a sharp breakdown voltage is known as the zenerdiode.

- ① A Zener diode is like an ordinary diode except that it is ~~properly~~ doped so as to have a sharp breakdown voltage.
- ② A Zener diode is always reverse connected. i.e. it is always reverse biased.
- ③ A Zener diode has sharp Breakdown Voltage, called Zener voltage V_Z .
- ④ When forward biased, its characteristics are those of just ordinary diode.
- ⑤ A Zener diode is not immediately burnt just because it has entered the breakdown region. As long as the external voltage is connected to the diode limits the circuit current to less than the burnt value, the diode will not burn out.

Circuit Symbols



Characteristics of Zenerdiode :-

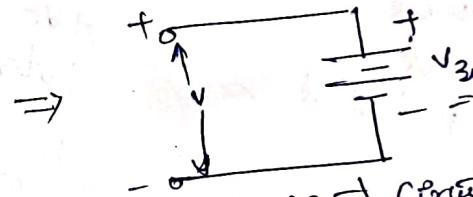
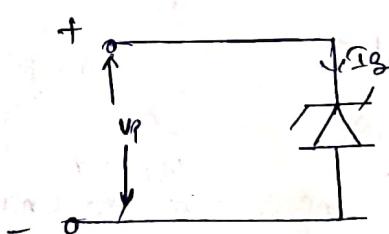


Equivalent Circ. of Zener diode:-

The analysis of zener diode can be made quite easy by replacing the zenerdiode by its equivalent circ.

(i) ON State:

- When the reverse voltage across a zener diode is equal to or more than breakdown (V_3) voltage, the current increases very sharply. In this region, the curve is almost vertical.
- It means that the voltage across zener diode is constant at V_3 , even though the current through the qt changes.
- Therefore in the breakdown region, an ideal zener diode can be represented by battery voltage V_3 .
- Under such condition the diode is said to be in the "ON" state.

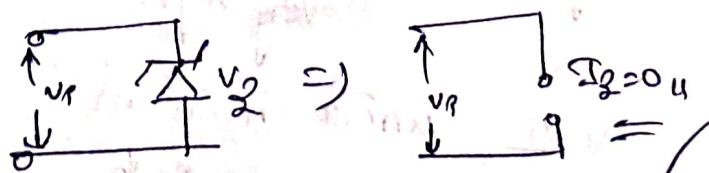


Equivalent Circ. of zener for
ON state. =

(ii) OFF State:

When the reverse voltage across the zener diode (V_R) is less than the V_3 but greater than the 0 volts, the zener diode is in the OFF state.

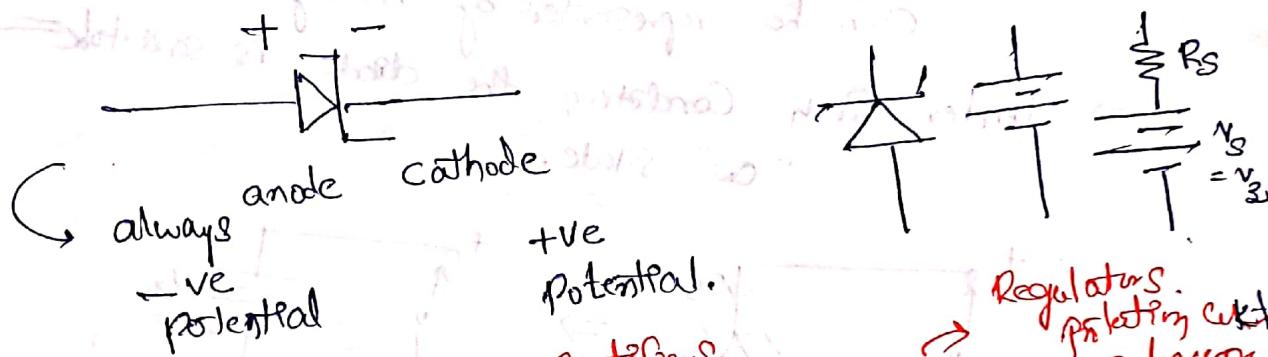
Under such conditions, the zener diode can be represented by an open-circled as shown in figure.



Zener Diode as a Voltage Regulator (Stabiliser) :-

In spite of change in Supply voltage (on load) always maintained at a constant level.

Zener Diode :- Operated in reverse biased heavily doped P-N junction diode, which is operated in breakdown region.



Ideal P-n Junction Diode

Rectifiers, clippers, clampers, v.m.

Voltage multipliers

Regulators
protecting circuits
Reverberation

Zener Diode characteristics

Only Reverse

It works in both
Forward | Reverse

2. Lightly doped

heavily doped.

3. Dynamic Reverse R.B. is low.
is very high

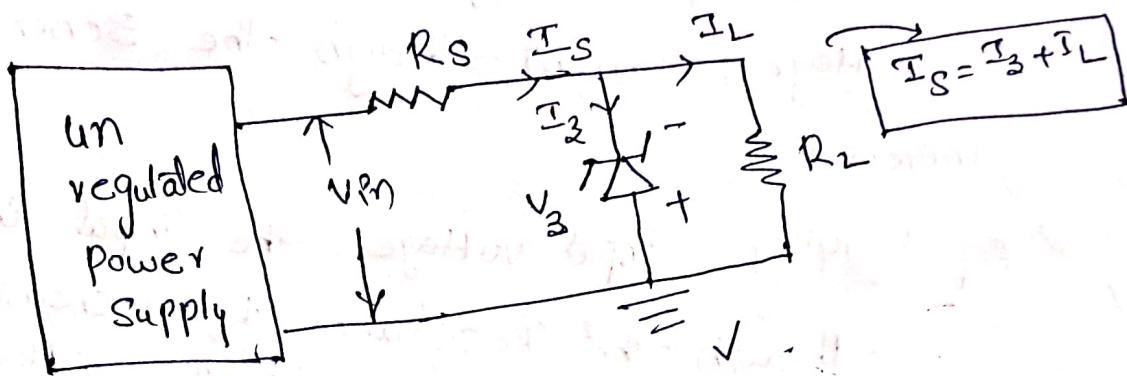
R.B. characteristics

are P.I
III rd quadrant.

4. $V-I$ Current characteristics
are in both
First quadrant &
III rd quadrant.

Zener Voltage Regulation

Below figure shows the simplest zener shunt regulator ckt.



The principle:

Zener Diode operates in a breakdown region, thereby maintaining a constant voltage across it for a large input current through it.

In the circuit, Serial Resistance (R_S) absorbs output voltage fluctuations and maintains a constant output voltage across the load resistance.

Thus the

Zener Diode maintains constant output voltage across the load.

If the circuit is properly biased and doped, then the load voltage V_o remains constant irrespective of variations of input voltage V_{in} and load resistance R_L .

→ There are two types of regulation:

1. Regulation with Supply voltage (Regulation)
2. Regulation with load volt (load Regulation)

Regulation with line voltage —

— When the input voltage is more than the Zener voltage, current through the Zener Diode increases.

By varying input voltage, the input current increases.

— Increase in the input affects the voltage across the series resistor.

This would further affect both the Zener voltage and load voltage but these changes would not happen in our circuit.

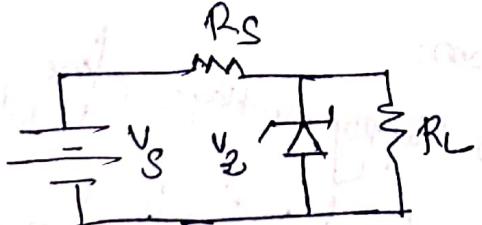
The reason is by that time the diode enters into breakdown region.

So it maintains a constant voltage across the load.

Mathematical Derivation :-

$R_S \uparrow$ varies
(min - max)

$V_S \uparrow I_S \uparrow I_3 \uparrow I_L$ (constant)



$$I_3 = \frac{V_S - V_Z}{R_L + R_S}$$

$$\Rightarrow V_S = V_Z \cdot \left(\frac{R_L + R_S}{R_L} \right) \text{ volt}$$

This is the minimum required voltage to turn on the Zener Diode.

V_S $\uparrow \rightarrow \uparrow$ max value.

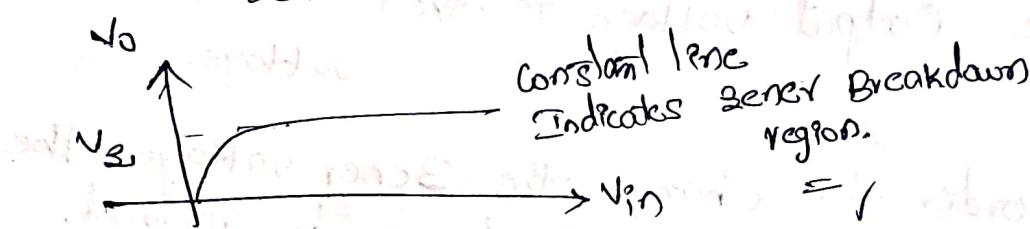
$$\Rightarrow \text{Then } I_S \uparrow = I_R \uparrow +$$

$$I_R \uparrow = I_Z \uparrow + I_L.$$

$$\Rightarrow V_S = V_R + V_Z$$

$$V_S = (I_R R_S)_{\max} + V_Z.$$

This is the maximum voltage (V_{in}) limited by the maximum Zener Diode current.



Regulation with load :- (R_L) .

V_o may change.

$R_L \uparrow I_L \downarrow \rightarrow V_o$ may change.

\Rightarrow we need to find the minimum R_L required

To turn on Zener Diode.

$$V_Z = V_o \cdot \frac{R_L}{R_L + R_S}$$

$$\Rightarrow V_o = V_Z \cdot \left(\frac{R_L + R_S}{R_L} \right)$$

$$V_o = V_Z \cdot \left(\frac{R_L + R_S}{R_L} \right)$$

$$V_o \cdot R_L = V_Z \cdot R_L + V_Z \cdot R_S.$$

$$(V_o - V_Z) R_L = V_Z \cdot R_S.$$

$$R_L = \frac{V_Z \cdot R_S}{(min) V_o - V_Z}$$

this is the minimum Resistance required to turn the Zener Diode.

$$R_L(\max) \rightarrow I_L \downarrow \\ I_S \downarrow \underline{I_R} \downarrow I_Z \downarrow I_L(-).$$

$$\Rightarrow I_L(\min) = \underline{I_R - I_Z}(\text{min}).$$

$$\boxed{\therefore (V) R_L(\max) = \frac{V}{I_L \min}.} \quad \checkmark$$

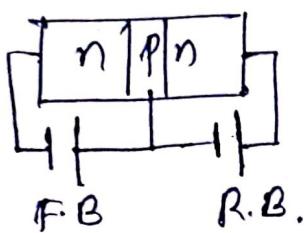
Limitations:

1. The output voltage is fixed and equal to Zener voltage.
 2. In order to change the Zener voltage, the Zener diode has to be replaced.
 3. Maximum current rating of Zener diode limits current drawn by load.
 4. There is no short circuit protection.
- Zener Breakdown allows the current to attain the Controlled Breakdown Voltage. Zener Breakdown Voltage.

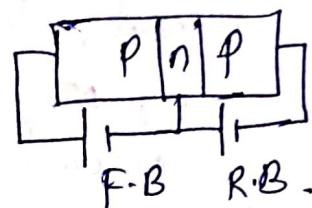
characteristic

SSN

a).

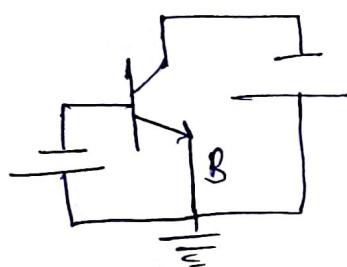
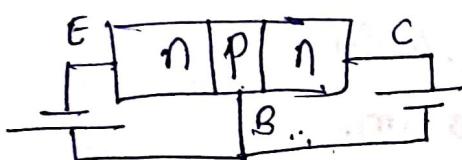


b).



C.B

configuration:



Input characteristic:
 I_E, V_{BE} $\perp V_{CB}$.

$$I_E \quad V_{CB}=0, \quad V_{CB}=0.$$



Output characteristic:

$$I_C, V_{CB}, I_E$$

$$I_C \quad I_E=0.$$



Transistor Biasing

This chapter presents methods for establishing the quiescent operating point of a transistor amplifier in the active region.

The operating point shifts with the changes in temperature.

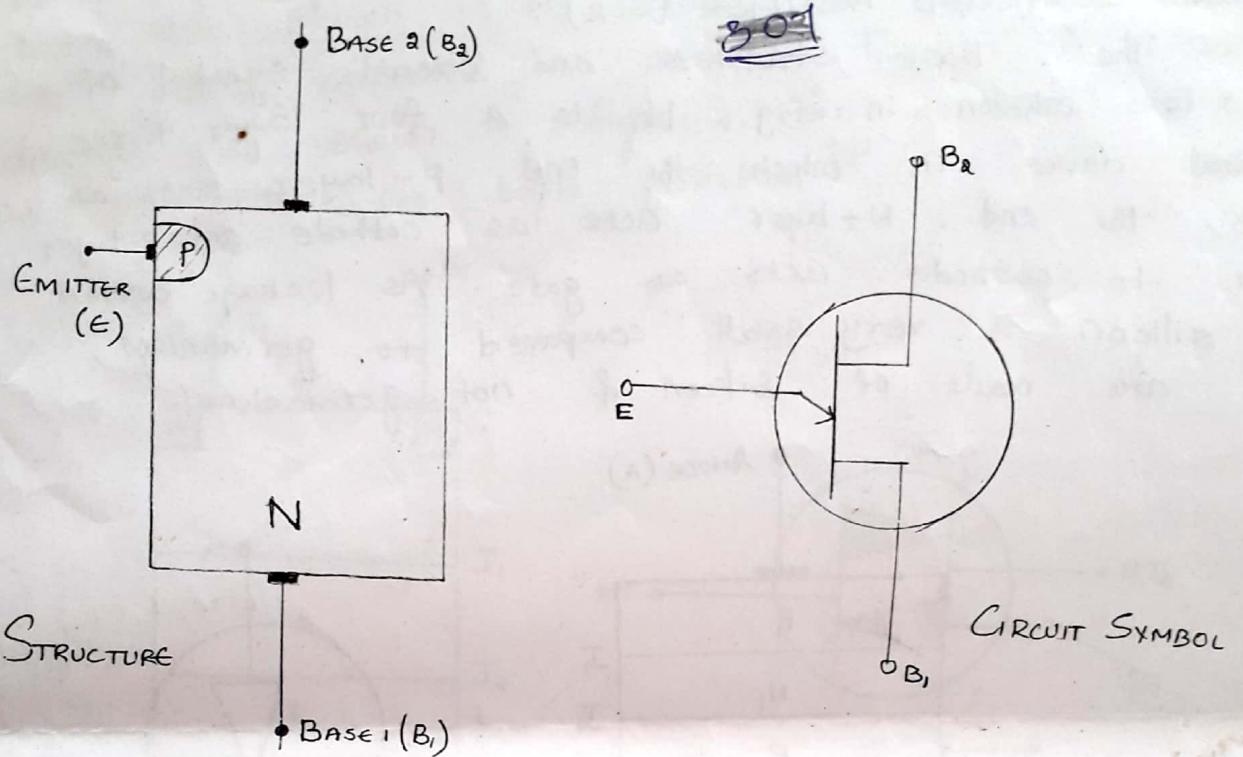
(i) because the transistor parameters ($\beta, I_{C0} \dots$)

are functions of T .

A criterion is established for comparing the stability of different biasing circuits.

UNI JUNCTION TRANSISTOR (UJT)

UJT is a three terminal semiconductor switching device. As it has only one PN Junction and three leads, it is commonly called as unijunction transistor.



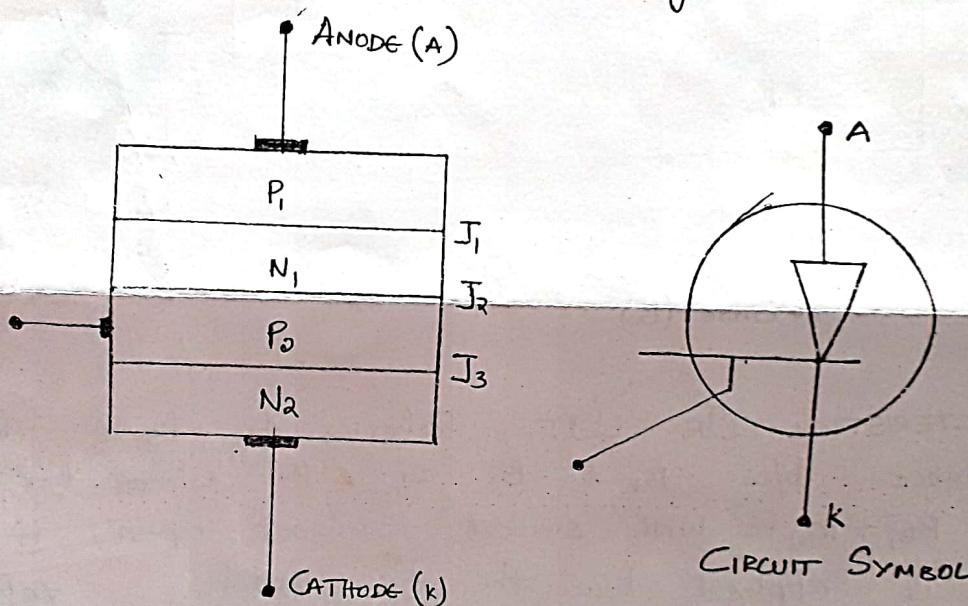
CHARACTERISTICS OF UJT: Referring to figure, the interbase resistance b/w B_2 & B_1 of the silicon bar is $R_{BB} = R_{B_1} + R_{B_2}$. With emitter terminal open, if voltage V_{BB} is applied b/w the two bases, a voltage gradient is established along the N-type bar. The voltage drop across R_{B_1} is given by $V_1 = nV_{BB}$ where the intrinsic stand. off voltage = $R_{B_1}/(R_{B_1} + R_{B_2})$. The typical value on n ranges from 0.56 to 0.75. This voltage V_1 reverse biases the PN-junction & emitter current is cut off. But a small leakage current flows from B_2 to emitter due to minority carriers. If a positive voltage V_E is applied to the emitter, the PN junction will remain reverse biased so long as V_E is less than V_1 . If V_E

exceeds V_f by the certain voltage V_g the diode becomes forward biased. Under this condition, holes are injected in to N-type base.

DE AC
To
ching

SILICON CONTROLLED RECTIFIER (SCR) :

The basic structure and circuit symbol of SCR is shown in fig. It is a four layer three terminal device in which the end P-layer acts as anode, the end N-layer acts as cathode and P-layer nearer to cathode acts as gate. As leakage current in silicon is very small compared to germanium, SCRs are made of silicon & not germanium.



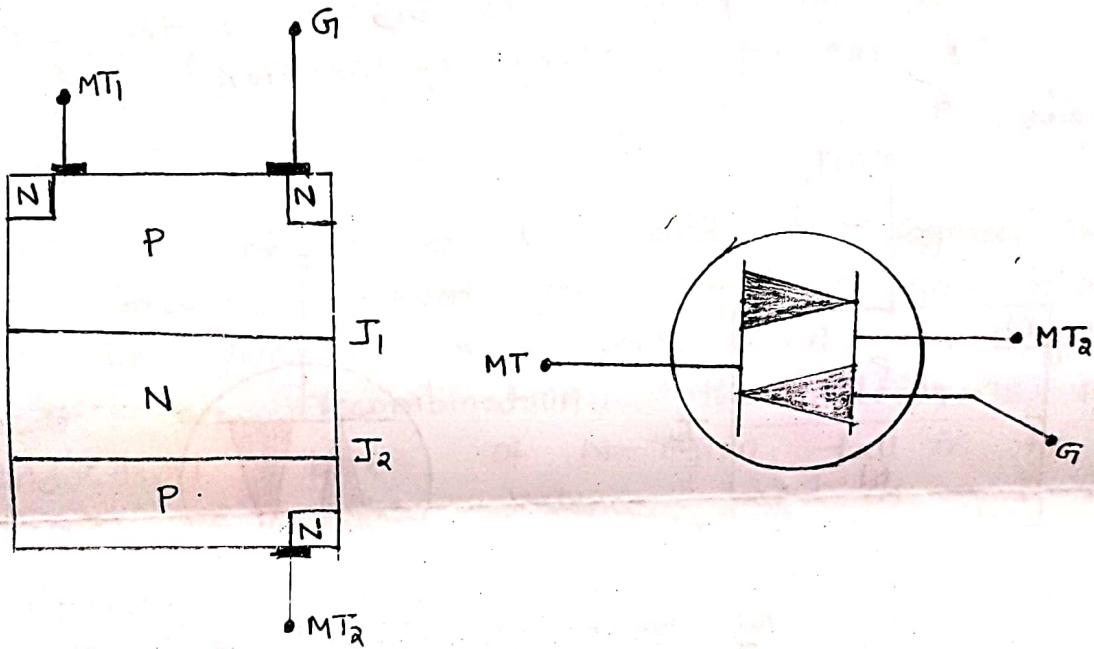
CIRCUIT SYMBOL

CHARACTERISTICS OF SCR :- The characteristics of SCR are shown in fig. SCR acts as a switch when it is forward biased. When the gate is kept open, if gate current $I_g = 0$ operation of SCR is similar to PNPN diode. When $I_g < 0$, the amount of reverse bias applied to J₂ is increased. So the break over voltage V_{BO} is increased. When $I_g > 0$ the amount of reverse bias applied to J₂ is decreased thereby decreasing the break over voltage. Similar to that of ordinary PN-diode. As the voltage at which SCR is switched 'ON' can be controlled by varying the gate current I_g . It is commonly called as controlled switch.

(2)

TRIODE AC SWITCH (TRIAC):

Triac is a three terminal semi conductor switching device which can control alternating current in a load. Its three terminals are MT_1 , MT_2 are the gate (G). The basic structure & circuit symbol of a Triac are shown in fig. Triac is equivalent to two SCR's connected in parallel but in the reverse directions as shown in figure. So a triac will act as a switch for both direction.

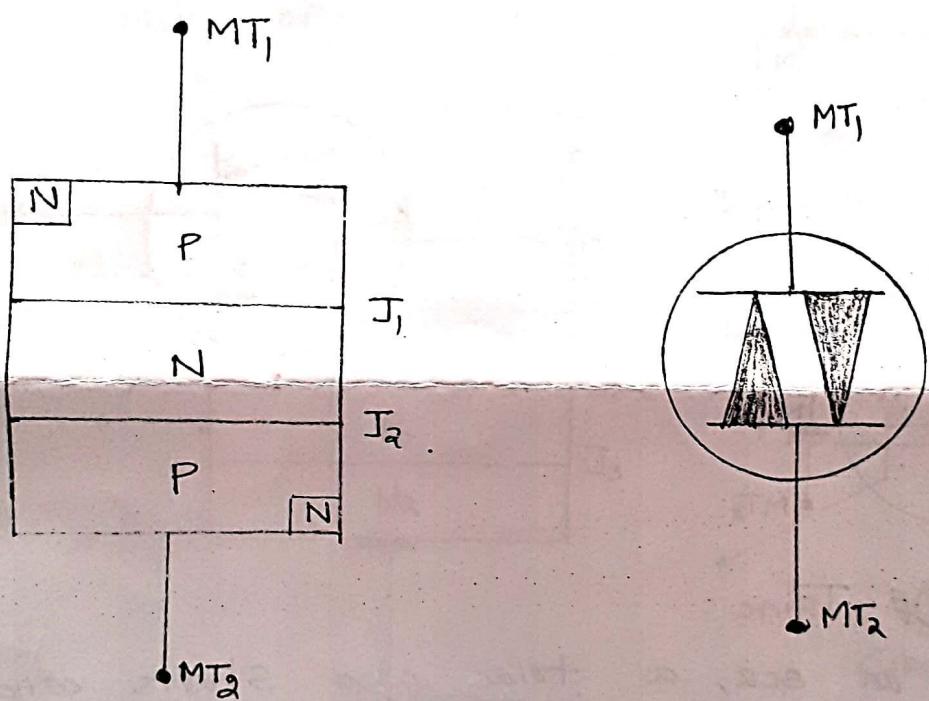


CHARACTERISTICS OF TRIAC:

Like an SCR, a triac also starts conducting only when the break over voltage is reached. Earlier to that the leakage current which is very small in magnitude flows through the device and therefore remains in the OFF state. The high inrush of current must be limited. Using external resistance, or it may otherwise damage the device. Triac is used for illumination control, temperature control.

DIODE AC SWITCH (DIAC):

The construction and symbol of diac are shown in fig. Diac is a three layer, two terminal semi-conductor device. MT₁ & MT₂ are the two main terminals which are interchangeable. It acts as a bidirectional. A Avalanche diode. It does not have any control terminal. It has two junctions J₁ & J₂. Though the Diac resembles a bi polar transistor, the central layer is free from any connection with the terminals.



CHARACTERISTIC OF A DIAC: The characteristic of a Diac shown in fig, it acts as a switch in both directions. As the doping level at the two ends of the device is the same, the diac has identical characteristics for both positive and negative half of an a.c. cycle. During the positive half cycle, MT₁ is positive with respect to MT₂, in the negative half cycle. It is used as triggering device in Triac control circuits. Used for light dimming, motor speed control and heater control.

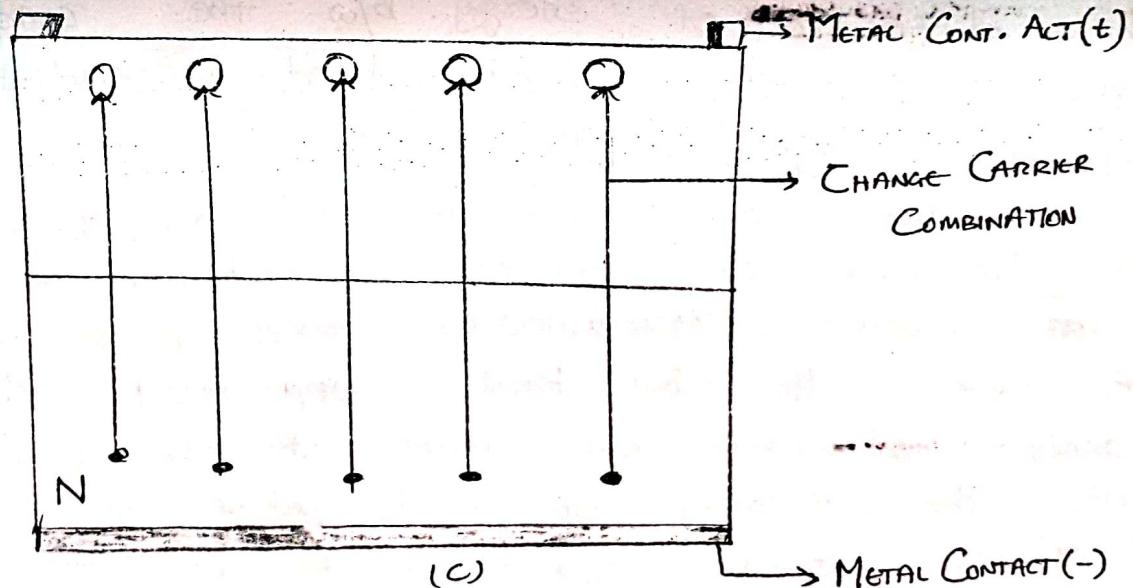
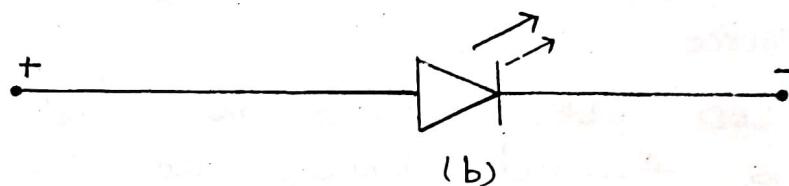
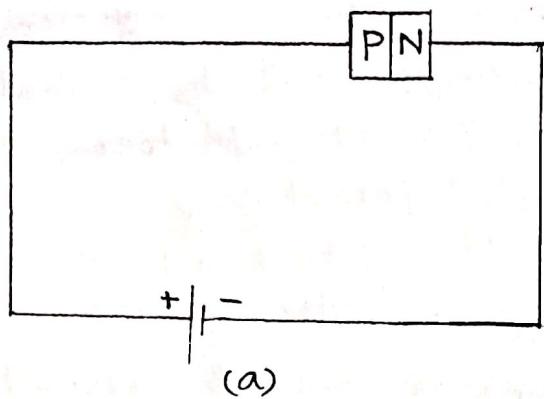
LIGHT EMITTING DIODE (LED):

(3)

The light emitting diode (LED) is a PN junction device which emits light when forward biased, by a phenomenon called electroluminescence. In all semi-conductors PN junction, some of the energy will be radiated as heat and some in the form of photons. In silicon & germanium, greater percentage of energy is given out in the form of heat & the emitted light is insignificant. In other materials such as gallium phosphide (GaP) or gallium arsenide phosphide (GaAsP), the no. of photons of light energy emitted is sufficient to create a visible light source.

: LED under forward bias and its symbol when an LED is forward biased. the electrons and holes move towards the junction & recombination takes place. As a result of recombination, the electrons lying in the conduction bands of N-region fall in to the holes lying in the valence band of a P-region. The difference of energy b/w the conduction band & the valence band is radiated in the form of light energy.

The basic structure of an LED shows recombinations of carriers & emission of light. Since carrier recombination takes place in the P-layer, it is kept uppermost. The metal anode connections are made at the outer edges of the P-layer so as to allow more central surface area for the light to escape. LED's are manufactured with damped lenses in order to reduce the reabsorption problem.



● ELECTRONS
○ HOLES.

LED :

- LED UNDER FORWARD BIAS .
- SYMBOL .
- RE - COMBINATIONS AND EMISSION OF LIGHT .

PHOTO DIODE:

Silicon photo diode is a light sensitive device also called photo detector, which converts light signals into electrical signals. The diode is made of a semi-conductor PN junction kept in a sealed plastic or glass casing. The cover is so designed that the light rays are allowed to fall on one surface across the junction. The remaining sides of the casing are painted to restrict the penetration of light rays. A lens permits light to fall on the junction, when light falls on the reverse biased PN photo diode junction, hole-electron pairs are created. The magnitude of the photo current depends on the number of charge carriers generated and hence, on the illumination of the diode element. This current is also affected by the frequency of the light falling on the junction of the photodiode. The magnitude of the current under large reverse bias is

$$I = I_s + I_o (1 - e^{V/nV_T})$$

Where,

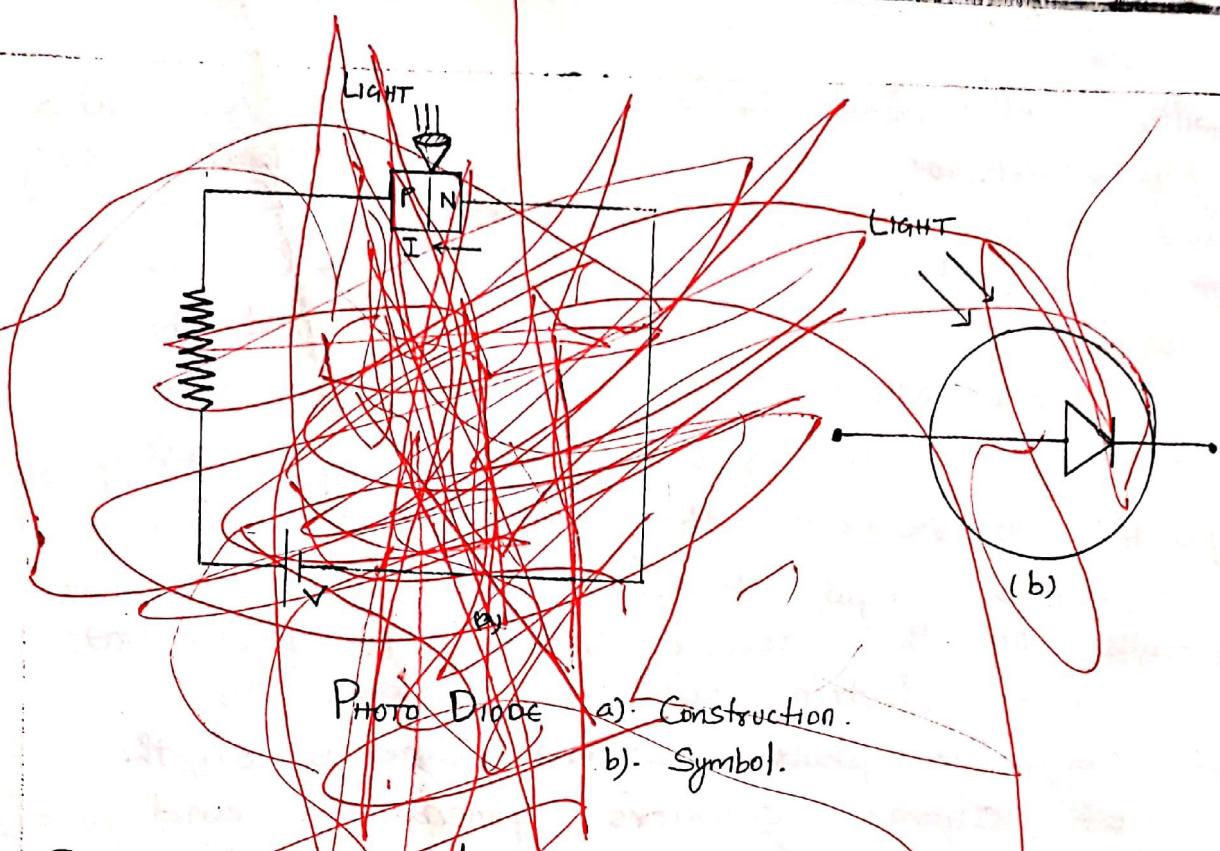
I_o = Reverse saturation current.

I_s = Short circuit current which is proportional to the light intensity.

V = Voltage across the diode.

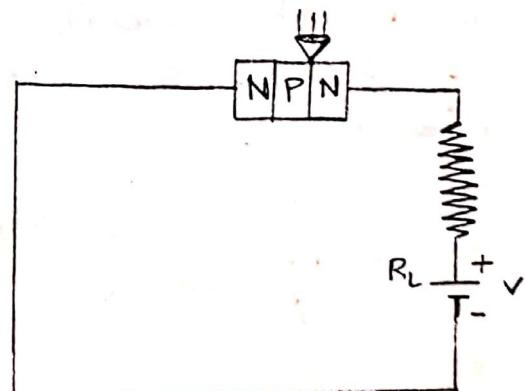
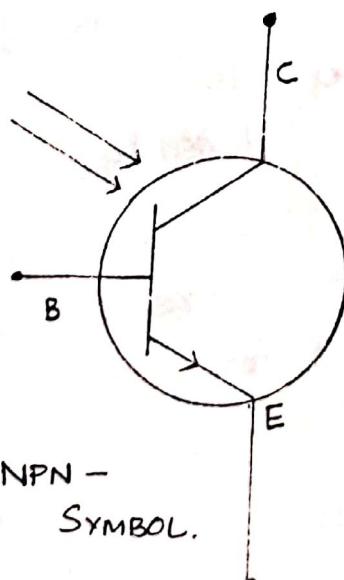
V_T = Volt equivalent of temperature.

n = Parameter, 1 for Ge & 2 for Si.



~~Photo Transistor / Photo Diode :~~

~~It is a much more sensitive semiconductor photo device than the PN Photodiode.~~ The current produced by a photodiode is very low which cannot be directly used in control applications. Therefore this current should be amplified before applying to control circuits. When the photo-transistor is illuminated, it permits a greater flow of current.



NPN -
SYMBOL.

When $I_B = 0$, the collector current is given by

$$I_C = (\beta + 1) I_{C0}$$

When the light is turned ON, additional minority