

PhD Thesis

Investigation of complex liquid-gas turbulent interfacial flows

A Numerical Study

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July 13, 2020

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The harmony of the world is made manifest in Form and Number, and the heart and soul and all the poetry of Natural Philosophy are embodied in the concept of mathematical beauty.

– D'Arcy Wentworth Thompson

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Introduction

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Surface tension dominated flows Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Fragmentation

Brief description of atomization Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Importance of drop size distributions Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written

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Numerical Platforms

PARIS Simulator Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Basilisk Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

NUMERICAL DEVELOPMENT

2

Methodology

In this chapter, we describe the basic numerical methodology behind our models concerning the dynamics of immiscible liquid-gas interfacial flows, at the incompressible and isothermal limits. These implementations are developed on the platforms ‘PARIS Simulator’ [1] and ‘Basilisk’ [2], with considerable overlap between the two platforms in terms of the treatment of the interface capturing schemes, transport of conserved quantities and surface tension models.¹ The numerical implementations are based on finite volume discretizations on uniform or dynamically refined Cartesian grids , utilizing state of the art methods in interfacial reconstruction coupled with geometric transport of the corresponding fluxes, curvature computation and surface tension modeling. For more detailed descriptions of the general capabilities of ‘PARIS Simulator’ and ‘Basilisk’, we refer the reader to the previously cited references.

2.1 Governing Equations

We use the one-fluid formulation for our system of governing equations, thus solving the incompressible Navier-Stokes equations throughout the whole domain including regions of variable density and viscosity, which itself depend on the explicit location of the interface separating the two fluids. In the absence of mass transfer, the velocity field is continuous across the interface at the incompressible limit, with the interface evolving according to the local velocity vector.

Conservative Formulation

Generally, we have a choice regarding how to model the convective operator of the incompressible Navier-Stokes equations. There is a well established corpus of numerical methods tailored specifically to deal with non-conservative² form of the convective operator that appear in transport equations of mass and momentum³ , which perform quite well in the context of single phase flows. However, in interfacial flows we often deal with discontinuities that arise as a consequence of the contrast in material properties between the two fluids. Therefore, even though the velocity field remains continuous throughout the domain, the otherwise smooth density (mass) and momentum fields contain sharp jumps (discontinuities) localized at the interfacial position. Therefore, we choose to formulate our governing equations in a conservative form i.e involving divergence of fluxes instead of gradients of the primitive variables when it comes to the convective operator. More detailed discussions and analyses about the comparative advantages of the conservative formulation in the context of flows involving large density-ratios is the focus of the subsequent chapters. Thus, the equations are as follows :

2.1 Governing Equations	4
2.2 Interfacial Transport : VOF . . .	6
2.3 Time Marching	10
2.4 Source Terms	12

1: The principle difference between ‘PARIS Simulator’ and ‘Basilisk’ is the ability to resolve the conservation laws on dynamically adaptive meshes in the case of ‘Basilisk’, whereas ‘PARIS Simulator’ only deals with regular Cartesian meshes.

2: also referred to as the strong form, necessitating certain orders of smoothness of the primitive variable

3: These methods are descendants of the class of numerical schemes used to solve hyperbolic partial differential equations.

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0 \quad (2.1)$$

$$\frac{\partial}{\partial t} (\rho \mathbf{u}) + \nabla (\rho \mathbf{u} \otimes \mathbf{u}) = -\nabla p + \nabla \cdot (2\mu \mathbf{D}) + \sigma \kappa \delta_s \mathbf{n} + \rho \mathbf{g} \quad (2.2)$$

with ρ and μ being the density and dynamical viscosity respectively, and therefore are the physical quantities which are discontinuous across the interface. The volumetric sources are modeled by the acceleration \mathbf{g} , and the deformation rate tensor \mathbf{D} used to model the viscous stresses is defined as:

$$\mathbf{D} = \frac{1}{2} [\nabla \mathbf{u} + (\nabla \mathbf{u})^T] \quad (2.3)$$

The term $\sigma \kappa \delta_s \mathbf{n}$ models the surface tension forces in the framework of the continuum surface-force (CSF) method. The normal vector to the interface is \mathbf{n} , with σ being the coefficient of surface tension and κ the local interfacial curvature. The operator δ_s is the Dirac delta function, the numerical approximation of which allows us to map the singular surface force distribution along the interface onto their volumetric equivalents for our Cartesian control volumes. At the incompressible limit, the advection of mass given by equation 2.1 can be treated as equivalent to that of the advection of volume.

Material Properties

Within the framework of interface capturing schemes, the temporal evolution of the interface separating the two fluids can be modeled by the following advection equation :

$$\frac{\partial \chi}{\partial t} + \mathbf{u} \nabla \chi = 0 \quad (2.4)$$

where χ is the phase-characteristic function, that has different values in each phase ⁴. Mathematically, the function χ is equivalent to a Heaviside function in space and time. At the macroscopic length scales under consideration, the interface evolution as described by equation 2.4 is modeled as having infinitesimal thickness under the continuum hypothesis. The coupling of the interfacial evolution with the equations of fluid motion as described in 2.1 and 2.2 is provided by :

$$\rho = \rho_1 \chi + (1 - \chi) \rho_2 \quad (2.5)$$

$$\mu = \mu_1 \chi + (1 - \chi) \mu_2 \quad (2.6)$$

where ρ_1, ρ_2 are the densities of fluids 1 and 2 respectively, likewise for viscosities μ_1 and μ_2 . Under certain circumstances, it is beneficial to

4: Generally, χ is assigned values of 0 in one phase and 1 in the other.

opt for a weighted harmonic mean description of the variable dynamic viscosity, instead of the weighted arithmetic mean as in equation 2.6.

The two main (and the most popular) approaches in the context of interface capturing schemes are the volume-of-fluid (VOF) method first developed by Hirt and Nichols [3], and the level set class of methods pioneered by Osher and Sethian [4]. The principal difference between the two approaches lies in the manner in which the Heaviside function χ is modeled in the discrete sense, either as a smooth differentiable field in the case of level sets, or as a sharp discontinuous field in the volume-of-fluid (VOF) context. Each class of methods has its own set of merits (and demerits) relative to each other. Generally speaking, volume-of-fluid based methods display superior mass conservation⁵ whereas in terms of interface curvature computation, level set based methods hold an advantage⁶. A detailed exposition into the different classes of interfacial transport methods can be found in the seminal monograph by Tryggvason, Scardovelli and Zaleski [5]

5: VOF based methods implicitly track the evolution of the discontinuous density field, which is not the case in level set based methods.

6: The differentiable nature of the level set function lends itself to straightforward curvature computation routines.

2.2 Interfacial Transport : VOF

Our numerical studies are based on the Volume-of-Fluid methodology. We refer to the discontinuous approximation to the Heaviside function⁷ χ as the volume fraction field or colour function interchangeably, which is defined below in the context of finite volume discretization :

$$C_{ijk}(t) = \frac{1}{\Delta V} \int_{\Delta V} \chi(x, t) dx \quad (2.7)$$

where C is the colour function with its values lying between 0 and 1, with i, j and k being the indices to the corresponding discretized control volume of volume ΔV . There are two steps involved in the VOF method, the reconstruction of the interface and its subsequent propagation (advection). We present a brief overview of the two steps in the following sections, as going into detailed descriptions of the reconstruction and propagation procedures are not the focus of the present body of work⁸.

7: A comprehensive discussion about the different types of approximations to the interface Heaviside function can be found in Popinet [6]

8: In-depth explanations into these numerical techniques can be found in [5, 7–9].

PLIC representation

We employ means of geometric reconstructions to explicitly define the interface location using the discrete colour function information. The interface is represented by disjointed line segments under the PLIC (piecewise linear interface construction) framework as illustrated in figure 2.1, with the images reproduced from the review by Scardovelli and Zaleski [7]. Such reconstructions involve the determination of interface normals using the Mixed Youngs Centered method, the detailed description of which can be found in [5].

[7]: Scardovelli et al. (1999), 'Direct numerical simulation of free-surface and interfacial flow'

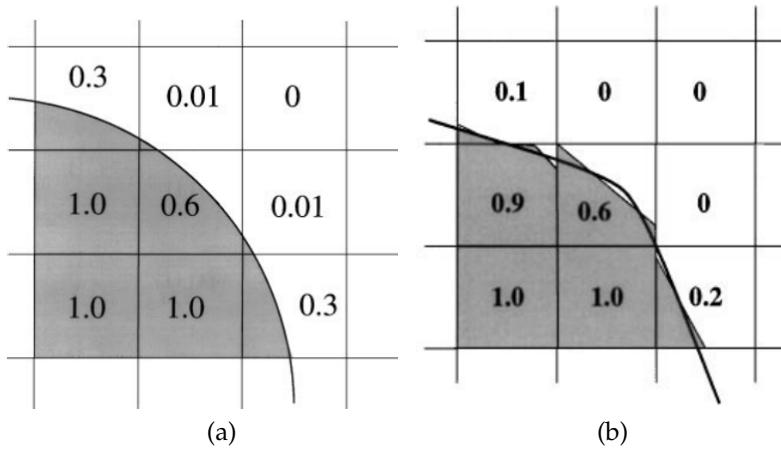


Figure 2.1: Explicit definition of the interface location using the volume-of-fluid approach. These images are reproduced with permission from Scardovelli and Zaleski [7]. (a) The exact discrete representation of a circular arc on a regular Cartesian grid using the colour function field (volume fraction). (b) The piecewise linear (PLIC) approximation to the smooth circular arc shown in (a), which entails second-order spatial accuracy.

Flux Computation

Once the geometric PLIC reconstructions have been carried out, the interface segments are advected using the velocity field. This entails computation of fluxes of the colour function, which can be computed via algebraic transport schemes (generally less accurate), or by using geometric reconstructions in either Eulerian, Lagrangian or hybrid frameworks. In the context of our numerical platforms ('PARIS' and 'Basilisk'), state-of-the-art⁹ geometrical flux reconstruction procedures are utilised. The temporal integration of the fluxes could be carried out either as a series of one dimensional propagations along each of the spatial directions, termed as direction-split, or carried out in one single sweep, termed as multidimensional or unsplit.

Direction-split methods are more intuitive and easier to develop (extension to 3D in particular), but suffer from lack of conservation (to the order of machine precision) when it comes to 3D¹⁰. Multidimensional (unsplit) methods have an advantage in that respect due to the fact that they are conservative by nature of their design, but are inherently more complicated to develop and implement, with no straightforward extension from 2D to 3D. For a more detailed and nuanced evaluation of the comparative advantages of interfacial transport methods, we refer the reader to the recent review by Mirjalili et al. [11] on the given subject. The propagation of the interface can be described by the evolution of the colour function (volume fraction field) as -

$$\frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla C = 0 \quad (2.8)$$

We can express the same in the conservative form as -

$$\frac{\partial C}{\partial t} + \nabla \cdot (C \mathbf{u}) = C (\nabla \cdot \mathbf{u}) \quad (2.9)$$

As one can observe, the "compression" term on the right hand side of equation 2.9 equals to zero in the context of incompressible flows without

9: The reader can refer to [1, 2] for further details

10: A detailed exposition of this problem along with a noteworthy solution can be found in the work by Weymouth and Yue [10]

mass transfer, but it is important to keep this term in our numerical formulation within the direction-split framework. Discretization of the above equation results in :

$$C_{i,j,k}^{n,d+1} = C_{i,j,k}^{n,d} - F_+^{n,d}(C) - F_-^{n,d}(C) + \bar{C}_{i,j,k}^{n,d} \left(\frac{\Delta u_q}{\Delta x} \right)_{i,j,k}^{n,d} \quad (2.10)$$

The above equation represents an advection substep, the superscripts n and d refer to the timestep and direction of integration respectively. The notation $d = 0$ refers to the field at the n^{th} timestep, before any integration is performed along any direction. The fluxes $F_{\pm}^{n,d}(C)$ in equation 2.10 are derived through geometrical reconstructions¹¹. The + and - subscripts refer to the orientation with respect to the central cell (i, j, k) . The subscript q refers to the direction corresponding to that given advection substep i.e either X, Y or Z. In our case, our numerical platforms are based on cubic (regular Cartesian) grids, consequently there is no requirement for a subscript with Δx . After each substep, the interface is reconstructed once again with the updated volume fraction field in order to compute the fluxes for the next advection substep. Finally, the volume fraction field for the next timestep is given by -

$$C_{i,j,k}^{n+1} = C_{i,j,k}^{n,3} \quad (2.11)$$

The interpretation and numerical approximation of the prefactor $\bar{C}_{i,j,k}^{n,d}$ to the directional divergence, as well as the fluxes $F_{\pm}^{n,d}(C)$, depend on the exact nature of the geometrical advection scheme in question, which in our context is either CIAM (Lagrangian explicit) or Weymouth-Yue (Eulerian implicit)¹². A brief outline of these two methods is presented in the subsequent sections.

11: For details regarding geometric flux reconstruction, refer to [5, 7]

Lagrangian Explicit This scheme was originally described in the work of Li [13], ‘CIAM’ being an abbreviation for the French title ‘*Calcul d’interface affine par morceaux*’, which can be thought of as a straightforward Lagrangian transport of the interface Heaviside function. After the interface segments are reconstructed from the discrete colour function at the start of the time-step, the interfacial points are transported by the component of the velocity field corresponding to the direction of transport. A geometrical interpretation of the scheme is illustrated in figure 2.2, reproduced from the seminal work of Gueyffier et al. [14].

As one can infer from the geometrical representation in figure 2.2, the fluxes $F_{\pm}^{n,d}(C)$ correspond to the volumes Φ^- and Φ^+ . Thus, the updated field $C_{i,j,k}^{n,d+1}$ is the sum of the three contributions Φ^- , Φ^0 and Φ^+ . We can rewrite equation 2.10 specifically for the CIAM scheme as -

$$C_{i,j,k}^{n,d+1} = C_{i,j,k}^{n,d} \left[1 + \left(\frac{\Delta u_q}{\Delta x} \right)_{i,j,k}^{n,d} \right] - F_+^{n,d}(C) - F_-^{n,d}(C) \quad (2.12)$$

12: The classification of Lagrangian explicit and Eulerian implicit are in accordance with the paper by Aulisa et al. [12]

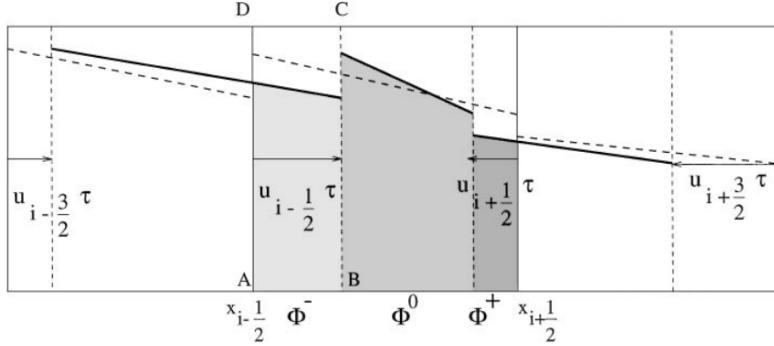
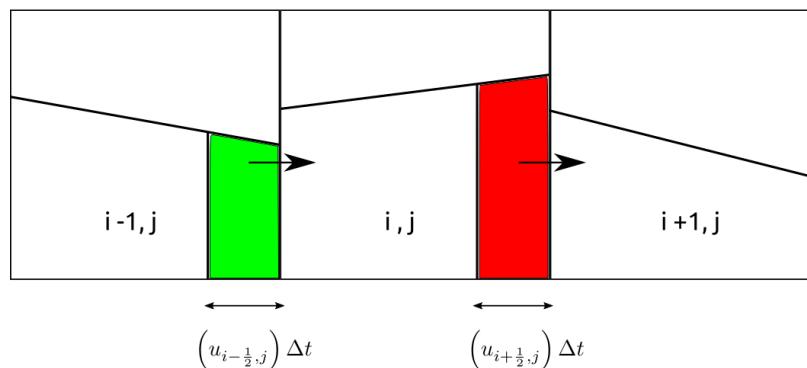


Figure 2.2: Lagrangian transport of the interface segments using the CIAM scheme, the image is reproduced with permission from Gueyffier et al. [14]. A 2D schematic of the geometric calculation of the fluxes of the volume fraction field is shown, for the advection substep along the horizontal direction. The central cell (i, j, k) undergoes a net compression during this substep. The fluxes Φ^- , Φ^0 and Φ^+ are the volumes under the advected interface segments advected by the interpolated velocity field, intersected by the (i, j, k) cell boundaries.

where the compression coefficient $\bar{C}_{i,j,k}^{n,d}$ is simply equal to the value of the colour function $C_{i,j,k}^{n,d}$ at the start of the corresponding advection substep. Although the flux terms cancel upon integration throughout the whole domain, one can clearly see that the compression terms do not sum up to zero due to the changing prefactor in front of the directional divergences. This precise issue brings us to the next advection scheme.

Eulerian Implicit This advection scheme was developed by Weymouth and Yue [10] in order to specifically tackle the problem of discrete conservation when it comes to direction-split geometrical advection schemes¹³. The scheme fundamentally employs a forward Eulerian method in order to carry out temporal integration of the fluxes, with the fluxes themselves computed as the quantity of the substance entering or exiting a given control volume through its fixed surfaces, as shown in figure 2.3. This is in contrast with the flux computation method in the case of CIAM, where the interface segments are propagated forward in time in a Lagrangian fashion.

13: By ‘discrete conservation’ we mean that the sum of the directional divergences sum upto zero, to the accuracy of machine precision.



The subtle but important tactic used in this scheme lies in the manner in which the prefactor to the compression term¹⁴ is treated, with its definition being :

$$\bar{C}_{i,j,k}^{n,d} = H \left(C_{i,j,k}^{n,0} - 1/2 \right) \quad (2.13)$$

Figure 2.3: A 2D schematic of the Eulerian (geometric) flux calculation using the Weymouth-Yue [10] scheme for the advection substep along the horizontal direction, with the interface reconstructed using the volume fraction field at the start of the substep. The colour fraction of the central cell (i, j) is updated during this substep through the addition of the fluxes (coloured regions), with the green polygon corresponding to the volume entering the cell i, j from the $i - 1, j$ and the red one corresponding to that exiting i, j into $i + 1, j$. The geometric flux calculations are made on the basis of the interfacial positions at the start of the substep, and the face centered velocities of the cell in question.

14: Compression coefficient is used as a short-hand version of ‘prefactor to the compression term’.

where H is a one-dimensional Heaviside function. This renders the compression coefficient independent of the direction of the advection substep, consequently enabling the three discrete directional divergences to sum up to zero¹⁵. Therefore, the scheme is able to demonstrate volume conservation, subject to local CFL restrictions¹⁶. To summarise, we can rewrite equation 2.10 for the Weymouth-Yue scheme as -

$$C_{i,j,k}^{n,d+1} = C \left[1 + \left(\frac{\Delta u_q}{\Delta x} \right)_{i,j,k}^{n,d} \right] - F_+^{n,d}(C) - F_-^{n,d}(C) \quad (2.14)$$

where C is a constant with a value of either 0 or 1, determined by the value of $C_{i,j,k}^{n,0}$ according to equation 2.13.

2.3 Time Marching

In order to describe the overall numerical algorithm for the one-fluid Navier-Stokes equations with variable density and viscosity, we choose to reframe our equations in a more convenient operator form, as presented below :

$$\frac{\partial}{\partial t} (\rho \mathbf{u}) = L(\rho, \mathbf{u}) - \nabla p \quad (2.15)$$

The operator L in the above expression can be decomposed in an explicit fashion as :

$$L = L_{\text{adv}} + L_\mu + L_\sigma + L_g \quad (2.16)$$

where the L_{adv} represents the conservative advection, L_μ represents the diffusive forces generated by viscous stresses, L_σ represents the capillary forces arising from the surface tension model and finally L_g represents the volumetric (body forces) source term.

Spatio-temporal Discretization

We apply the spatially discretized versions of these operators (denoted by the superscript h) onto the primary variables (C, \mathbf{u}), and march forward in time using a small, possibly variable time-step τ such that $t_{n+1} = t_n + \tau$. We shall be dropping the subscript i, j, k from this point onwards, with the understanding that the operators in equation 2.16 apply uniformly to all control volumes. In the first part of the algorithm, the volume fraction field C^n is updated to the next timestep, with the superscript n signifying discretization in time. The operation can be written as follows

15: In numerical terms, we can only ensure that they sum up to the accuracy of the Poisson solver $\sim 10^{-3} - 10^{-6}$, with the limiting factor being the level of machine accuracy ($\sim 10^{-14} - 10^{-17}$).

16: For a proof of discrete volume conservation subject to certain CFL criteria, refer to the appendix of [10].

$$C^{n+1} = C^n + \tau L_{\text{vof}}^h(C^n, \mathbf{u}^n) \quad (2.17)$$

The temporal evolution of the volume fraction field represented above by the operator L_{vof}^h is in accordance with the Lagrangian explicit or Eulerian implicit advection schemes, as described in the previous sections. Once we have obtained the updated field C^{n+1} , we can move on to the temporal update of our momentum field given by -

$$\begin{aligned} \rho^{n+1} \cdot \mathbf{u}^* &= \rho^n \cdot \mathbf{u}^n + \tau L_{\text{adv}}^h(C^n, \mathbf{u}^n) + \\ &\quad \tau \left[L_\mu^h(C^{n+1}, \mathbf{u}^n) + L_\sigma^h(C^{n+1}) + L_g^h(C^{n+1}) \right] \end{aligned} \quad (2.18)$$

The advection operator L_{adv}^h is implemented as high-order spatial schemes coupled with a choice of non-linear flux limiters such as QUICK, ENO, WENO, Superbee, Verstappen, BCG, for regions of constant density¹⁷. For control volumes in the vicinity of the interface location, we revert to lower order schemes due to the sharp jumps in the material properties across the interface. The functionality of the operator L_{adv}^h near the interface is tightly coupled to that of L_{vof}^h from equation 2.17, so as to ensure consistency in the discrete advection of mass and momentum. The details regarding this coupling shall be the focus of subsequent chapters, where it is covered in more depth.

¹⁷: These high-order spatial schemes are based on well established methods developed to deal with hyperbolic conservation laws, for more details refer to the studies of Leveque [15] and Sweby [16].

Pressure-Poisson Projection

The velocity field is evolved using a classical time-splitting projection method as described in the seminal work of Chorin [17], which involves predicting an ‘intermediate’ velocity field \mathbf{u}^* as given by equation 2.18, followed by a correction step as follows -

$$\mathbf{u}^{n+1} = \mathbf{u}^* - \frac{\tau}{\rho^{n+1}} \nabla^h p^{n+1} \quad (2.19)$$

The discrete pressure field required to correct the intermediate velocity is determined by imposing the conservation of mass, which in our incompressible framework reduces to necessitating the resulting velocity field to be divergence-free (solenoidal) -

$$\nabla^h \cdot \mathbf{u}^{n+1} = 0 \quad (2.20)$$

Thus, combining equations 2.19 and 2.20, we are left with a variable coefficient Poisson equation for the pressure :

$$\nabla^h \cdot \left(\frac{\tau}{\rho^{n+1}} \nabla^h p^{n+1} \right) = \nabla^h \cdot \mathbf{u}^* \quad (2.21)$$

The default Poisson solver used in ‘PARIS Simulator’ to invert the elliptic operator appearing in eqn. 2.21 is a red-black Gauss-Seidel (GS) solver with overrelaxation [18]. There is also has an in-house implementation of a multigrid solver for structured grids with 2^n number of points per direction, utilizing a fully parallelized V-Cycle scheme [18]. Relaxation operations are applied starting from the finest to the coarsest first, and then from the coarsest to the finest, with the number of relaxation operations being a user-adjustable parameter. Having a native multigrid solver allows for an efficient solution of the Poisson equation without the necessity of having external libraries/pre-conditioners (e.g. HYPRE) installed on the system. When it comes to ‘Basilisk’, an atypical multigrid solver is implemented using a “half” V-cycle in order to deal with the spatial inhomogeneity of the grid size arising due to adaptive mesh refinement. For more details regarding the differences between the multigrid solver of ‘Basilisk’ and the classical implementation of a multigrid, one can refer to [19].

The whole set of operations described up to this point, constitutes a temporal integration scheme of the first-order, which can be expressed as -

$$(C^{n+1}, \mathbf{u}^{n+1}) = L_1(C^n, \mathbf{u}^n) \quad (2.22)$$

where L_1 is the operator consisting of all the steps described so far, applied to the primary fields C and \mathbf{u} . Therefore, a second-order time integration can easily be computed by using L_1 to get a first prediction -

$$(C^{**}, \mathbf{u}^{**}) = L_1(C^n, \mathbf{u}^n) \quad (2.23)$$

The superscript $**$ refers to our first order prediction of the primary variables. Therefore, the second-order estimate can be obtained via averaging -

$$(C^{n+1}, \mathbf{u}^{n+1}) = \frac{1}{2} [(C^{**}, \mathbf{u}^{**}) + L_1(C^{**}, \mathbf{u}^{**})] \quad (2.24)$$

2.4 Source Terms

The detailed descriptions of the methods used in our numerical platforms to deal with surface tension, viscosity and body forces have already been carried out in [1, 2, 20], therefore we briefly touch upon certain aspects of the operators in question, in particular, their interaction with the volume fraction field.

[18]: Briggs (1987), ‘A Multigrid Tutorial, SIAM’

[19]: Popinet (2003), ‘Gerris: a tree-based adaptive solver for the incompressible Euler equations in complex geometries’

Surface Tension

We use the Continuum Surface Force method (CSF) as our model for surface tension, coupled with height functions for curvature computation. The height functions used in our implementation were first introduced in [20], subsequently tested, revised and improved in [21, 22]. In general, the height functions are used to compute the curvature field based on second-order finite differences applied to the heights. Although, in regions of poor interfacial resolution¹⁸, the method reverts to certain fallbacks, one of which is curve fitting instead of height functions. The resulting curvature field is coupled with a well-balanced discretization with respect to the discrete pressure gradient, with the same discretization stencil applied to the volumetric (body) force term as well.

Viscous Diffusion

We use second-order spatial discretizations of the viscous stresses, using centered differences¹⁹. The (variable) dynamic viscosity is computed based on the volume fraction field via weighted arithmetic or harmonic averaging (equations 2.6). The temporal treatment of the viscous term can be either in explicit or semi-implicit fashion, , but in the context of the present study we will be sticking exclusively with the explicit version.

18: These are regions where the local radius of curvature is comparable to the grid size

19: The exact implementation differs slightly between 'Basilisk' and 'PARIS Simulator'

Artificial Atomization : The Falling Raindrop

3

The focus of the present chapter shall be to take a closer look at the issues plaguing numerical methods that try to deal with flows entailing significant contrasts between the material properties of the two fluids. Arguably, the most common instances of such flows are those involving the interaction between air and water, primarily in the form of droplets and bubbles that play important roles in both natural and industrial processes. As for the numerical platform, we use ‘PARIS Simulator’¹ to carry out our simulations on this topic. A flow configuration that combines the complexities of large density-ratios with the interaction between capillary, viscous and inertial stresses is that of a water droplet falling in the air under the influence of gravitational acceleration. The contents of the chapter are primarily derived from the recent investigations of the falling raindrop in Fuster et al. [23], in which the author is a primary contributor.

3.1 Problem Setup

The problem is characterized by a combination of Reynolds, Weber and Bond numbers, the definitions of which are as follows :

$$We = \frac{\rho_g U^2 D}{\sigma} , \quad Re = \frac{\rho_l U D}{\mu_g} , \quad Bo = \frac{(\rho_l - \rho_g) g D^2}{\sigma} \quad (3.1)$$

The subscripts l and g represent liquid and gas phases respectively. In our particular numerical setup, $We \approx 3.2$, $Re \approx 1455$ and $Bo \approx 1.2$, thus corresponding to that of a 3mm diameter raindrop (a relatively large one) falling in the air at an approximate terminal velocity of 8 m/s (interpolated from empirical data, refer to Gunn and Kinzer [24]). The parameters in the problem setup are given in Table 3.1, and the schematic diagram given in Fig. 3.1. The droplet is initially placed at the center of a cubic domain (3D), whose side is 4 times the diameter of the drop.

Table 3.1: Parameter values used in the simulation of a falling water droplet in air.

ρ_g (kg/m^3)	ρ_l (kg/m^3)	μ_g ($Pa s$)	μ_l ($Pa s$)	σ (N/m)	D (m)	g (m/s^2)
1.2	0.9982×10^3	1.98×10^{-5}	8.9×10^{-4}	0.0728	3×10^{-3}	9.81

In order to properly reproduce and analyse the dynamics of a relatively large drop (high Reynolds flow) such as in our case, the numerical method has to accurately resolve the thin boundary layers², the interaction of such layers with the capillary forces and finally the non-linear feedback of the complex 3D vortical structures present in the wake behind the

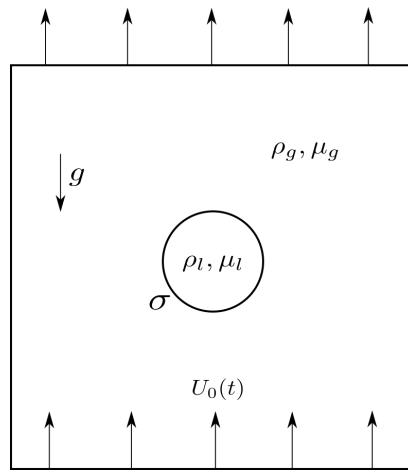
3.1 Problem Setup	14
3.2 Numerical Instabilities . . .	15
3.3 Stabilization Strategies . . .	18

1: Refer to [1] for a detailed exposition of the numerical methods implemented in ‘PARIS Simulator’.

[23]: Fuster et al. (2018), ‘A momentum-conserving, consistent, Volume-of-Fluid method for incompressible flow on staggered grids’

2: Even for simulations with 60 points across the droplet diameter, the boundary layer has only by 3-4 cells across it.

droplet. Such an undertaking was attempted by Dodd and Ferrante [25], in which they managed to delineate the different regimes concerning the behavior of the wake behind the droplet, although at relatively lower Reynolds numbers (the maximum Reynolds tested was ≈ 500 , whereas in our case it is ≈ 1500). Therefore, our objective behind the demonstration of this particular test case is *not* to develop a high fidelity model of a raindrop³, but rather carry out a stringent evaluation of the robustness of our numerical method compared to ones that are not mass-momentum consistent. For such a low Weber number the capillary forces dominate and the droplet should remain intact, and definitely not undergo any subsequent atomization.



3: In the Dodd and Ferrante [25] study , a droplet was allowed to fall from rest along a domain with a length corresponding to 32 times the droplet diameter, therefore necessitating a problem size of approximately 260 million cells.

Figure 3.1: A 2D schematic of the numerical setup for the falling raindrop. A droplet of diameter D is placed at the center of a cubic domain of side L and $L/D = 4$. The liquid properties (ρ_l, μ_l) correspond to that of water, and the gas properties (ρ_g, μ_g) correspond to that of air. We apply a uniform inflow velocity condition with $U_0(t)$ and an outflow velocity condition at the top which corresponds to zero normal gradient. Boundary conditions on the side walls correspond to those of impenetrable free slip (no shear stress).

3.2 Numerical Instabilities

Numerical simulations of this configuration at moderate resolution⁴ carried out with the standard version⁵ of our numerical method results in the catastrophic deformations of the droplet as illustrated in Fig. 3.5, which we describe as ‘fictitious’ or ‘artificial’ atomization.

Instability Mechanism

We propose the following explanation in order to account for such numerical artifacts. To start with, we neglect gravity and viscous effects at this relatively large Reynolds number. Also, we are interested in steady-state flow⁶. On the axis and near the hyperbolic stagnation point at the front of the droplet one has $u_2 = 0$ for the transverse (radial) velocity and for the axial momentum balance

$$u_1 \partial_1 u_1 = -\frac{1}{\rho} \partial_1 p. \quad (3.2)$$

Due to the large viscosity and density ratios, it is not possible for the air flow to immediately entrain the water, so the fluid velocity is significantly smaller inside the droplet. In the air the acceleration near the stagnation point is of the order U^2/D , whereas the pressure gradient is

4: Droplet resolutions between $D/h = 16$ to $D/h = 64$ are considered to be moderate, where D is the droplet diameter and h is the grid size.

5: The standard version is based on the non-conservative formulation of the Navier-Stokes equations, concomitantly not ensuring consistency between discrete mass and momentum transport.

6: As the simulation starts with uniform flow in the gas and a zero velocity in the drop, there is a sudden large acceleration in the gas, resulting in the development of a dipolar velocity field akin to that of potential flow around a cylinder (sphere).

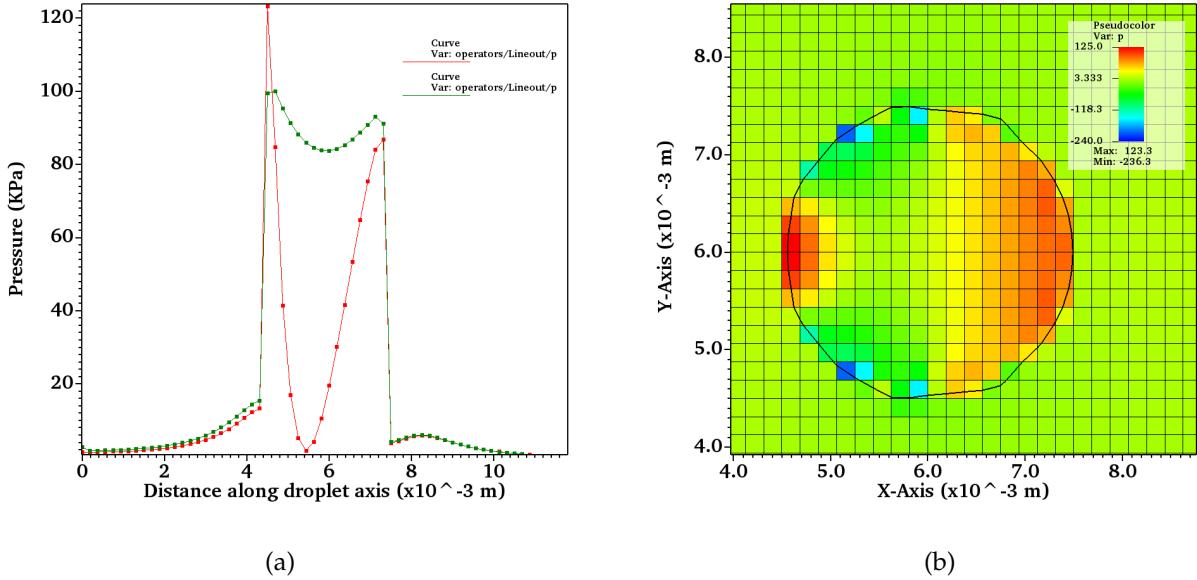


Figure 3.2: The origin of the pressure peak in the front of the droplet. (a) The profile of the pressure on the axis a few timesteps after initialisation with the standard, non-consistent method (red curve) and the consistent method based on the conservative Navier-Stokes formulation (green curve). Much larger pressure gradients are present across the interface using the non-consistent method. (b) The pressure distribution immediately after the start of the simulation using the standard, non-consistent method. The pressure peak has not yet resulted in the formation of a dimple. In all figures the droplet resolution corresponds to $D/h = 16$. The simulations are carried out with the CIAM advection method, in conjunction with the Superbee limiter.

$$\partial_1 p \sim \rho_g U^2 / D. \quad (3.3)$$

The pressure gradient in the liquid is much smaller, however, in the case of a mixed cell the water density multiplies with the gas acceleration U^2/D , so that

$$\partial_1 p \sim \rho_l U^2 / D, \quad (3.4)$$

then a large pressure gradient results in the mixed cell or cells. This large pressure gradient results in a pressure spikes inside the droplet near the front stagnation point, as shown in Figure 3.2. Such pressure gradients are balanced by surface tension only for a sufficiently large curvatures near the droplet front. This explains the presence of a “dimple” often observed in low resolution simulations of the falling drop. This artifact had been observed by Xiao [26] in a similar case⁷ involving the sudden interaction of a droplet at rest with a uniform gas flow. The resulting large un-physical pressure gradients across the interface eventually lead to its rapid destabilization and concomitant breakup.

Visualization of the flow around the droplets (Figure 3.4) illustrates the challenging nature of the flow configuration, even for such a seemingly simple physical problem. As one can observe, the boundary layers are extremely thin. Therefore, even though the velocity field is continuous across the interface (in the discrete sense) in the absence of mass transfer,

7: In the thesis of Xiao, the focus was on the analysis of droplet breakup corresponding to different Weber number regimes.

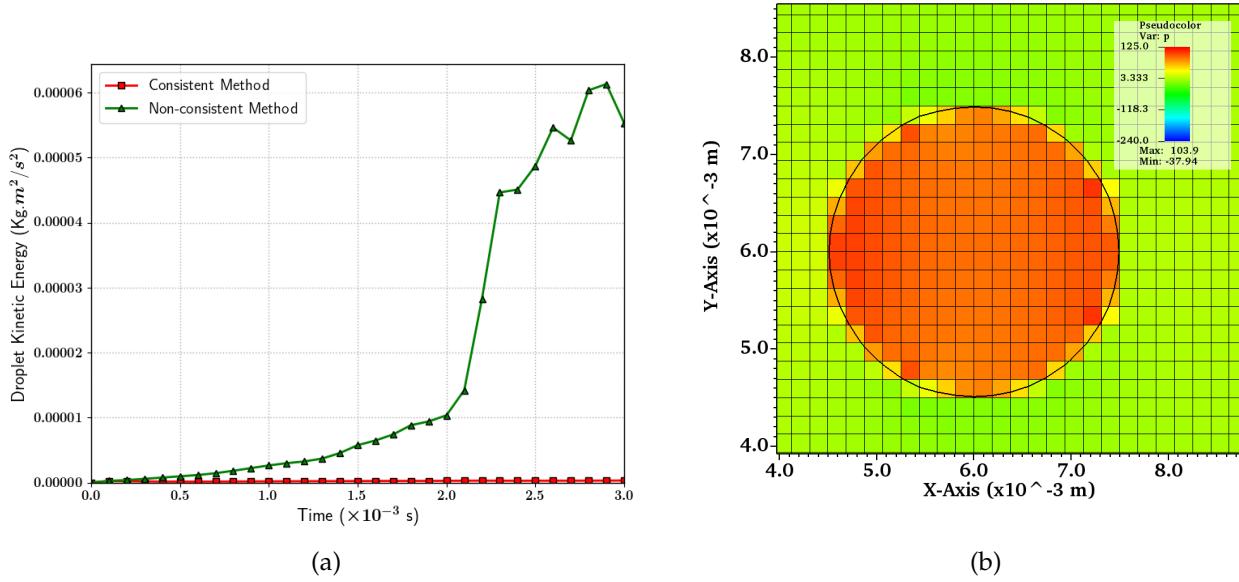


Figure 3.3: (a) Comparison of the temporal evolution of droplet kinetic energy. The standard non-consistent method displays spikes in the kinetic energy that are approximately 3 orders of magnitude larger than that of the consistent method, leading to rapid destabilization. (b) The pressure distribution immediately after the start of the simulation using the consistent method (based on a conservative Navier-Stokes formulation). In all figures the droplet resolution corresponds to $D/h = 16$. The simulations are carried out with the CIAM advection method, in conjunction with the Superbee limiter.

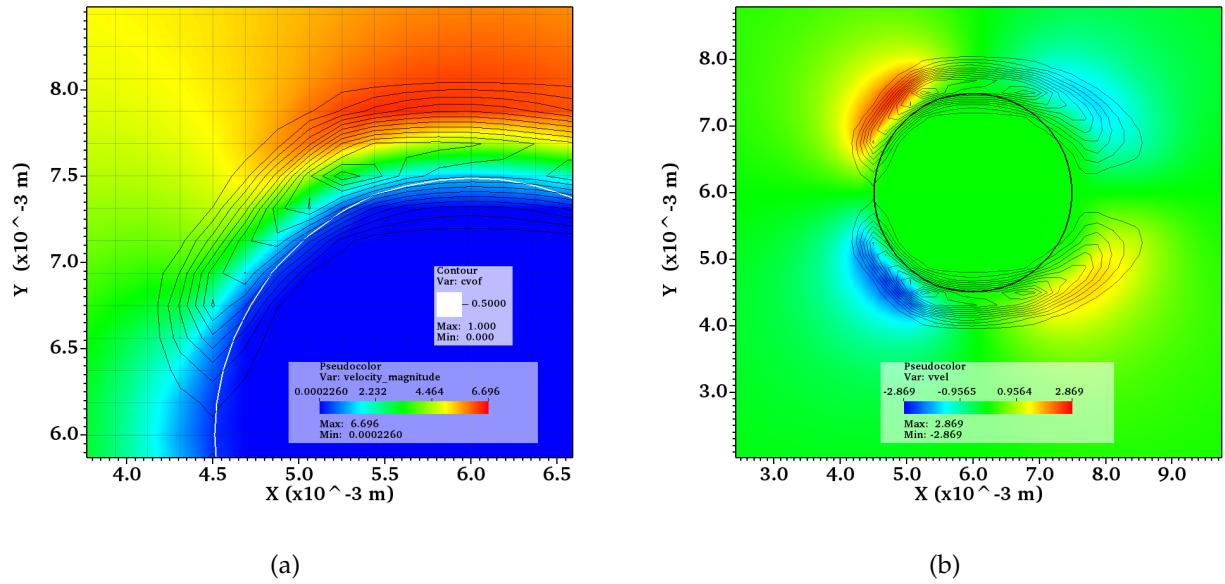


Figure 3.4: Flow field around the 3mm droplet with $D/h = 16$ immediately after the start of the simulation with the consistent method, demonstrating the contours of the norm of the vorticity field (black lines). The 2D cross-section in these figures corresponds to the mid-plane slice along the Z axis, where the inflow is along the X axis and gravity opposite to it. (a) The velocity magnitude. As one can observe, the boundary layer is resolved by only 2-3 cells. (b) The velocity component in the Y direction, perpendicular to the flow. As the flow develops further, a marked separation of the boundary layers is observed with a more complex vortical region in the wake. The figures correspond to simulations carried out with the CIAM advection method, in conjunction with the Superbee limiter.

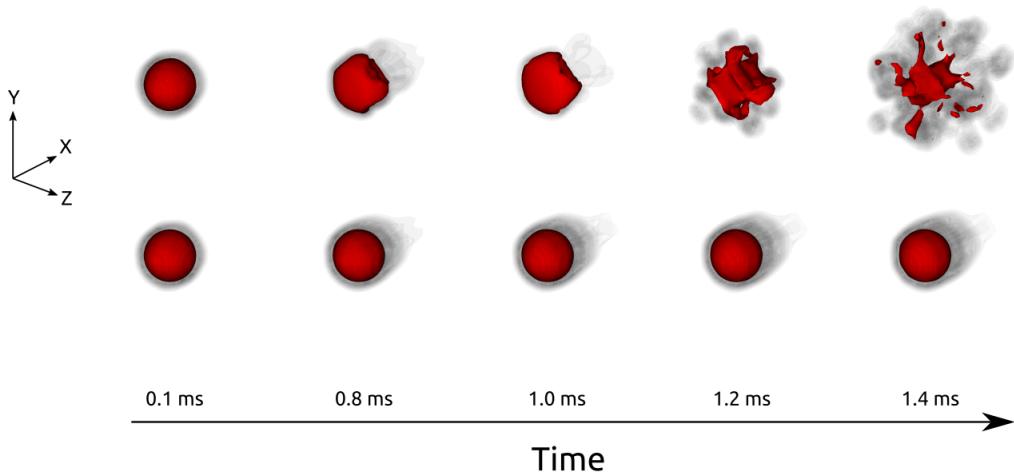


Figure 3.5: A comparison of the temporal evolution between the standard non-consistent method (top row) and the consistent method based on the conservative formulation of the governing equations (bottom row), using the combination of CIAM advection scheme coupled with the Superbee flux limiter. The flow is along the positive X direction, with gravity along the opposite direction. The red contour indicates the isosurface of the volume fraction field corresponding to a value of 0.5, whereas the black contours surrounding the drop represent isosurfaces of the magnitude of vorticity. The raindrop with the non-consistent method displays massive deformations leading to artificial breakup as a result of rapidly growing numerical instabilities. The droplet resolution for both methods is $D/h = 16$.

there is the appearance of strong velocity variations at the scale of the grid size for such coarse levels of grid refinement.

3.3 Stabilization Strategies

The cascading nature of the numerical instabilities that lead to the eventual (un-physical) fragmentation of droplet is not just a cause of concern in the context of modeling a raindrop, but it has important implications within the more broader scope of atomization and other complex fragmentation phenomena.

Primary Concern

Arguably, the most important objective of numerical investigations of physical phenomena involving fragmentation is the quantification of the size of the features that result from a series of topological changes⁸. A typical example is the statistical distributions of drop sizes, where the drops are generated via some fragmentation mechanism.⁹ As demonstrated in the present studies using the standard non-consistent method, the artificially atomized drop leads to the generation of a large number of smaller fragments, which if counted, will skew the resulting droplet size distributions towards the smaller sizes. Therefore, the falling raindrop serves as a faithful representation of the numerous under-resolved features that are typically omnipresent in numerical studies of complex fragmentation phenomena. The inability to discern between the drops resulting from physically consistent mechanisms and those that result from ‘numerical fragmentation’ is exactly why there is a need to develop numerical schemes that circumvent the occurrence of such numerical instabilities.

8: In the context of surface tension dominated flows, these features are primarily drops and bubbles, occasionally one can also be interested in transient features such as thin sheets, ligaments etc.

9: These are generally in the form of probability density functions (PDF).

Consistent Mass-Momentum Transport

The most common and brute force approach that one can apply in order to suppress or circumvent such numerical instabilities is by using a combination of extremely refined meshes coupled with larger domains¹⁰. A more computationally efficient approach would be to use a conservative formulation¹¹ of the Navier-Stokes equations, in order to achieve consistency in the discrete transport of mass and momentum. In this section, we shall take a closer look at how the utilisation of the consistent method enables us not only to stabilize majority of the numerical instabilities we have come across, but also delivers relatively good approximations of the flow dynamics involved. A thorough and detailed exposition of the principles behind the consistent method and the different strategies towards achieving consistent transport is covered in the ensuing chapter.

We observe that applying the method that ensures consistent mass-momentum transport brings a considerable and systematic improvement over a spectrum of different flux limiters (WENO, ENO, Superbee, QUICK, Verstappen) and CFL numbers, as evidenced by comparing the figures 3.2 and 3.3. To summarize, the simulations broadly fall into three categories. The first two categories concern those that use the method ensuring consistent mass-momentum transport, and as a result maintain physical values of the kinetic energy and smooth interface shapes. Certain simulations amongst the ones carried out with this consistent method display some numerical instabilities (but not leading to catastrophic deformation)¹² resulting due to the particular choice of the advection scheme (CIAM/WY) and flux limiter (QUICK/WENO/ENO/Superbee/Verstappen) combination.

Finally, in the third category are the simulations carried out with the standard non-consistent method that rapidly blow up, displaying marked peaks or spikes in kinetic energy as a function of time, associated with massively deformed interface shapes (see figure 3.5). Additionally, our studies suggest that certain combinations of the advection scheme and the flux limiter are numerically more robust than others¹³, in particular, the most stable combinations are that of CIAM advection with Superbee limiter, and the WY advection with QUICK limiter.

We illustrate the performance of the consistent method through the results of our simulations in Figure 3.7. The spatial resolutions correspond to $D/h = 8, 16, 32$ and 64 using the WY advection scheme in combination with the QUICK flux limiter, while keeping the same value for the inflow velocity boundary condition. The quantities of interest while examining the robustness of the method are the temporal evolution of the droplet kinetic energy (Fig. 3.7. (a)) and the moment of inertia of the droplet along the three directions (Fig. 3.7. (b),(c),(d)). The inflow is along the X direction with gravity opposite to it. The moment of inertia is used as a descriptor of the 'average' droplet shape, with the three moments of inertia along the different axes I_m defined as -

$$I_m = \int_{\mathcal{D}} Hx_m^2 dx , \quad \text{where, } 1 \leq m \leq 3 \quad (3.5)$$

10: In the study of Dodd and Ferrante [25], a computational domain with length corresponding to 32 times the diameter is employed, resulting in a problem size of approximately 260 million cells, that too for a relatively low Reynolds number.

11: A prerequisite of methods that use consistent mass-momentum transport is the formulation of the convective operators in the conservative manner i.e divergence of fluxes instead of gradients of the primary (discontinuous) variables.

12: This may be due certain issues regarding the treatment of outflow boundary conditions in our numerical platform 'PARIS Simulator'.

13: Further detailed investigations are required to understand the difference in code stability as a function of the choice of flux limiter and advection scheme combination.

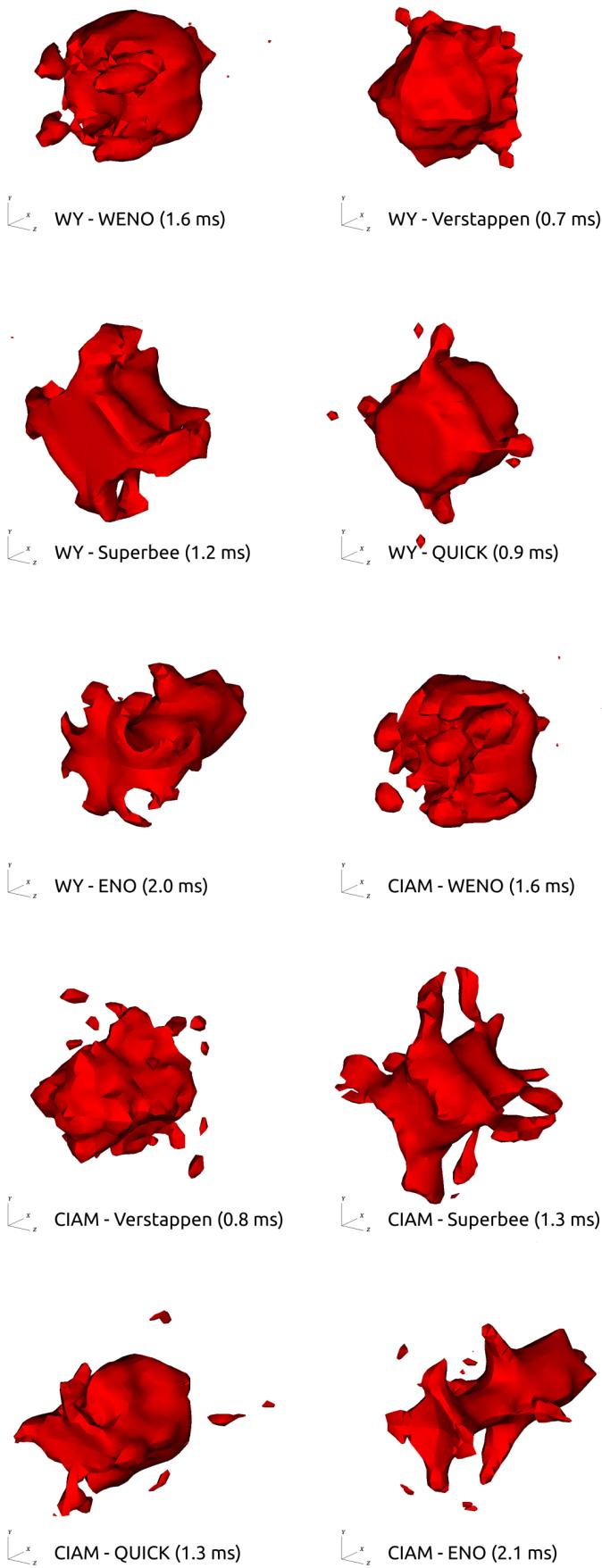


Figure 3.6: A juxtaposition of the different manifestations of ‘artificial’ atomization one encounters while using the standard method that does not involve consistency between the discrete transport of mass and momentum. The red contours indicate the isosurface of the volume fraction field corresponding to a value of 0.5, acting as a good proxy for the exact interfacial position. One can clearly observe that the un-physical fragmentation of the raindrop is symptomatic of the non-consistent method, systematically across all combinations of flux limiters and advection schemes. The symbol “WY” in the legend corresponds to those run using the Weymouth-Yue advection scheme, and “CIAM” corresponds to the CIAM scheme. Brief descriptions of these advection schemes can be found in the preceding chapter 2. The implementation of the non-linear flux limiters i.e WENO, ENO, QUICK, Superbee, Verstappen correspond to that of well established methods developed to deal with hyperbolic conservation laws, for more details refer to the studies of Leveque [15] and Sweby [16]. The time stamps are indicative of the moments at which the interface is the most deformed, and do not necessarily correspond to the moment at which the code crashes.

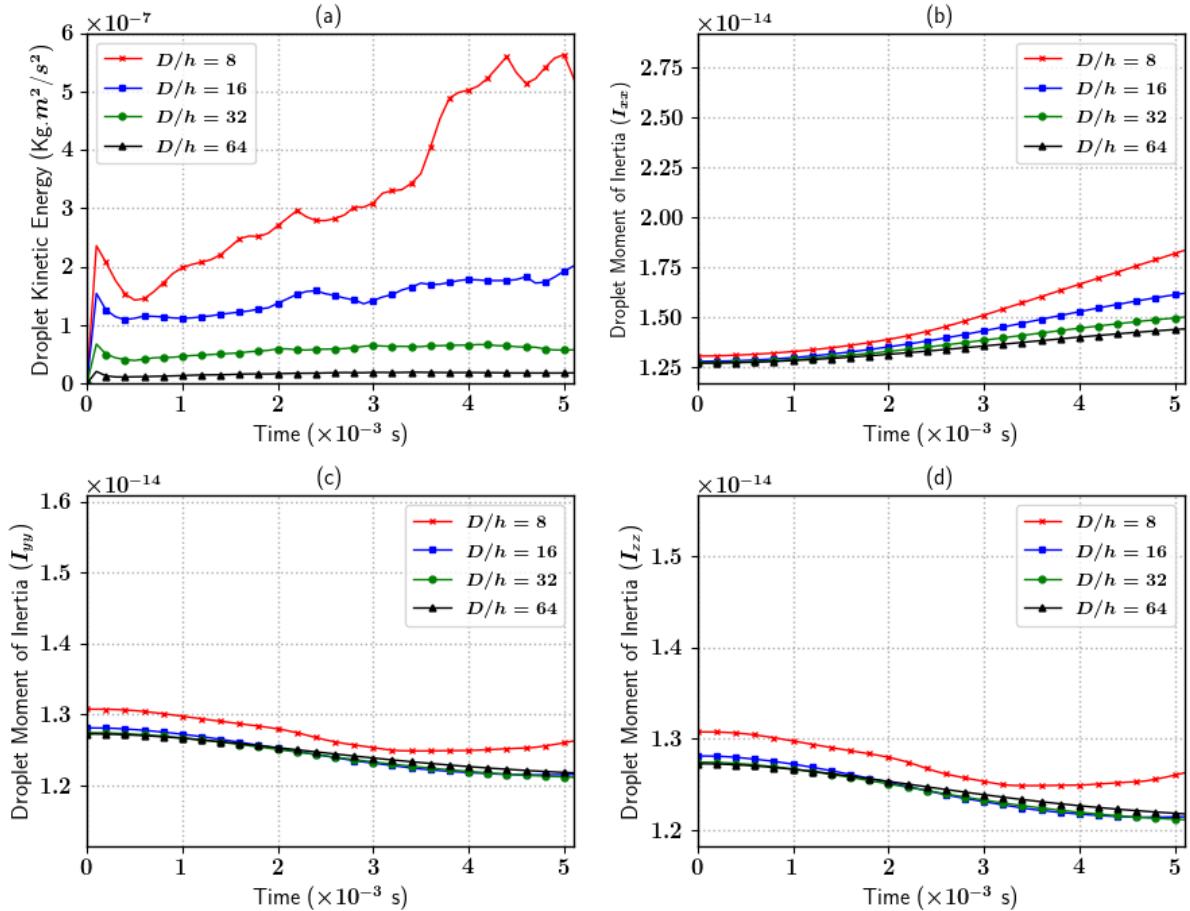


Figure 3.7: Temporal evolution of quantities of interest to evaluate the performance of the consistent scheme for different spatial resolutions. (a) Kinetic energy of the droplet. (b) Moment of inertia of the droplet along the flow (X) direction. (c) and (d) Moment of inertia of the droplet along the directions perpendicular to flow (Y,Z), evolution of I_{yy} seems to be more or less identical to I_{zz} .

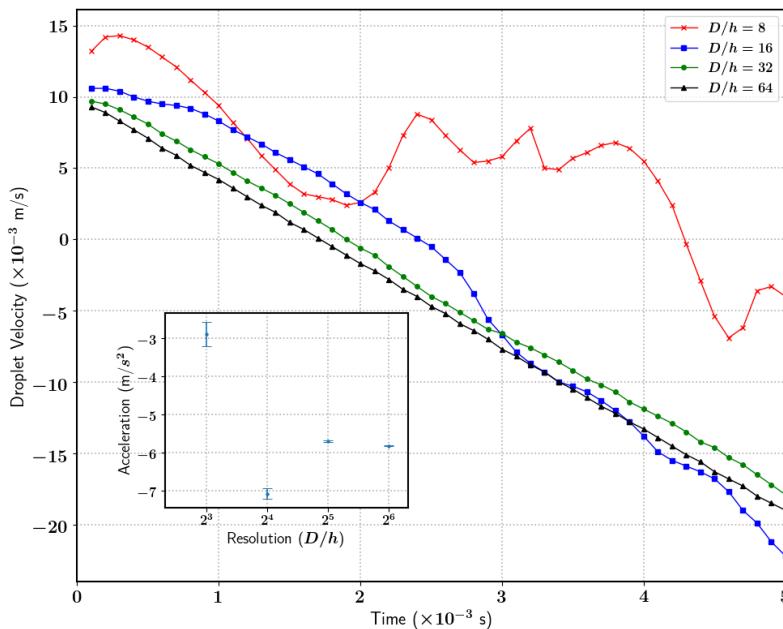


Figure 3.8: Comparison of droplet velocity as a function of time, for different droplet resolutions. The simulations were carried out with the consistent version of our method, using the combination of the WY advection scheme with the QUICK limiter. The droplet velocities correspond to that of their respective center of masses. Inset : Convergence of the droplet acceleration as a function of resolution, computed using the best linear fit over the temporal variation of their respective velocities. The error bars signify the asymptotic standard error (least-squares) corresponding to the obtained linear fits.

where \mathcal{D} is the computational domain and x_m is the distance of the interface relative to the center of mass of the droplet. The kinetic energy of the droplet evolves in a relatively smooth manner, without the presence of sudden spikes and falls which are emblematic of the standard non-consistent method (refer to Fig. 3.3). Such abrupt changes in kinetic energy of the droplet have been found to be associated with instants when the droplet undergoes ‘artificial’ atomization or breakup, henceforth resulting in the catastrophic loss of stability for the numerical method. We observe a systematic drop in the amount of the droplet kinetic energy as we increase resolution, with the most probable explanation being that of the suppression of spurious interfacial oscillations which are rampant at lower resolutions. There is also a component of the kinetic energy of the droplet associated with the internal coherent vortical structures generated due to the interaction of aerodynamic shear at the interface, evidenced by the non-zero value of the kinetic energy even for the most highly resolved droplets. Finally, the moment of inertia of the droplet appears to evolve in a smooth manner for all droplet resolutions, with higher resolutions exhibiting lower amounts of inertia as a result of the more compact shapes obtained once the spurious interfacial deformation modes are subdued. This observation holds true for the moment of inertia curves regardless of direction.

We have to keep in mind that the velocity inflow condition does not correspond to the ‘exact’ terminal velocity field an actual falling raindrop might experience, hence the droplet in our numerical setup does have some finite acceleration due to the imbalance between the aerodynamic forces and gravity. In Figure 3.8, we demonstrate the velocity of the center of mass of the droplet (in the frame of reference of the box enclosing the droplet) as a function of time, and its behavior as we increase the droplet resolution. As one can observe, due to the imbalance of forces acting on the droplet, it undergoes a net acceleration as evidenced by the approximately linear increase (absolute value) in the velocity as a function of time. The temporal variation in the droplet velocity is fitted to a linear polynomial in order to evaluate the droplet acceleration by means of a standard least-squares approach, for each droplet resolution. We illustrate (inset Figure 3.8) that we achieve more accurate fits as a consequence of higher droplet resolutions, as evidenced by a decrease in the standard error on the fits ranging from $\pm 11.1\%$ for $D/h = 8$ to a value of $\pm 0.12\%$ for the highest resolution of $D/h = 64$. The results obtained in this section indicate that especially when it comes to low resolutions, our numerical method can be used to get relatively good estimates of the underlying flow features of the droplet without observing an un-physical evolution as a consequence of discretization errors.

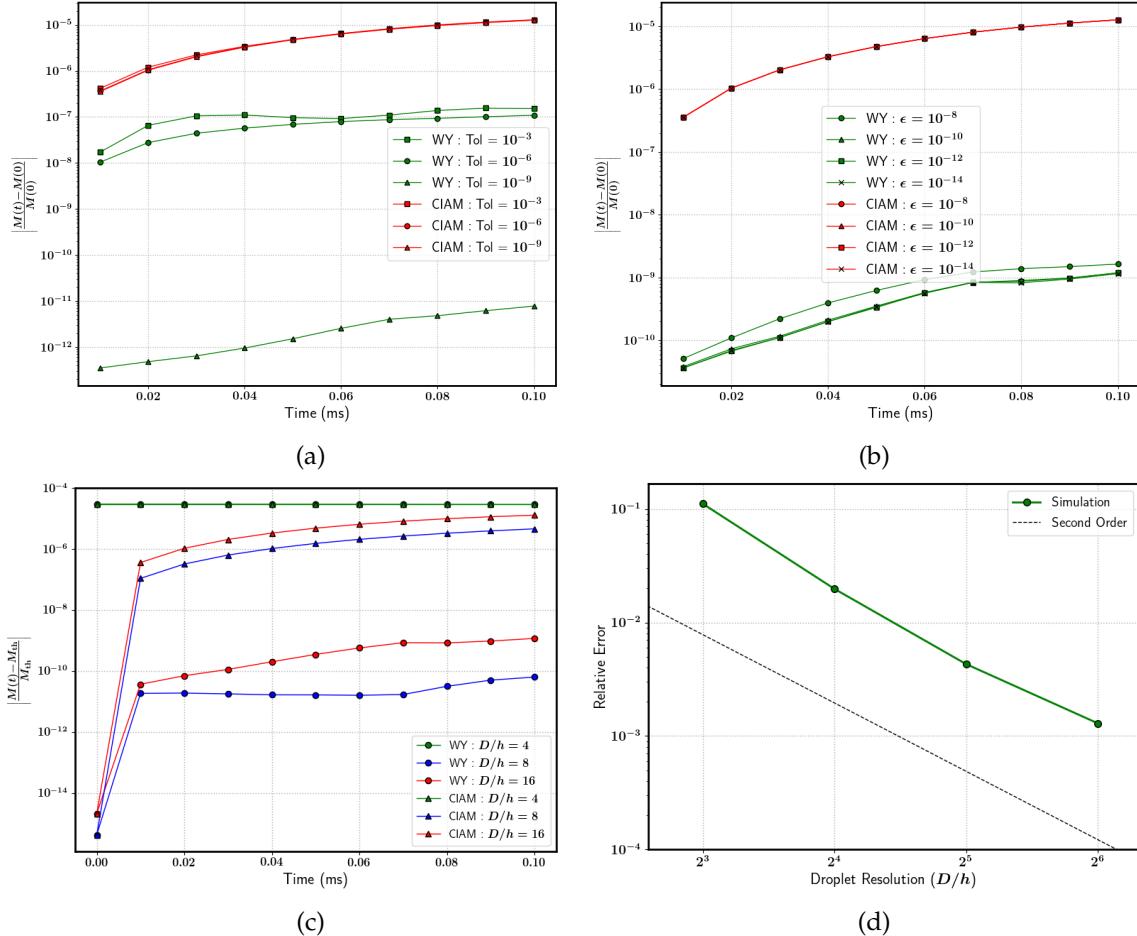


Figure 3.9: Relative change in the mass of the droplet as a function of time in plots (a), (b) and (c). The simulations are carried out with a resolution of $D/h = 16$, for a total time of 0.1 milliseconds. The symbol “WY” in the legend corresponds to those run using the Weymouth-Yue advection scheme in combination with the QUICK limiter, and “CIAM” corresponds to the CIAM scheme in combination with the Superbee limiter. (a) The dependence of the mass conservation properties of the scheme as a function of the Poisson solver tolerance is tested. For the WY-QUICK combination, using a stricter tolerance results in better mass conservation, whereas the conservation properties of the CIAM-Superbee combination seems to be independent of the tolerance. (b) Dependence of the mass conservation on the clipping parameter employed. The CIAM-Superbee combination again seems to be impervious to changes in clipping, whereas WY-QUICK seems to perform slightly better by lowering the parameter. (c) Dependence of the mass conservation properties on the droplet resolution. The WY-QUICK combination displays better results for all except the lowest resolution. (d) Variation of the relative error from the least-squares fit on the droplet acceleration, in the frame of reference of the static box. The corresponding droplet accelerations are plotted in the inset of figure 3.8. The reduction in the relative error follows roughly second-order spatial convergence.

Consistent Mass-Momentum Transport

4

The stability of numerical methods that attempt to model interfacial flows involving large density contrasts face several challenges, key amongst them being the transport of mathematical discontinuities that arise from the contrast in the material properties of the fluids involved. Extremely small numerical errors are ubiquitous as a consequence of the numerous approximations involved at each and every step of the algorithm¹. In the context of such flows, such errors generally result in physically inconsistent mass and momentum transfer across the interface, often from the denser phase towards the lighter phase. The presence of large density or viscosity contrasts tend to amplify the growth of these cascading numerical errors, eventually leading to significant (often catastrophic) interfacial deformations followed rapidly by a loss of numerical stability. In this chapter, we present a detailed exposition of our class of numerical methods which are designed specifically to circumvent or suppress the growth of such numerical instabilities when dealing with flows entailing large density-ratios. The implementations of the numerical algorithms are developed for finite volume discretizations using uniform Cartesian grids in 3D, on the ‘PARIS Simulator’ [1] numerical platform. Some contents of the chapter are primarily derived from the recent study by Fuster et al. [23], in which the author is a primary contributor.

4.1 General Principles

In the past two decades, considerable efforts have been made in the design of numerical methods to deal with large density-ratios. The underlying principle behind these endeavours is that the governing equations for the transport of mass and momentum are modeled using a conservative formulation (divergence of fluxes), instead of standard non-conservative forms which themselves were adapted directly from techniques developed originally for single-phase flows. This formulation enables one to render the discrete transport of momentum *consistent* with respect to the discrete transport of mass². Such a tight coupling of the propagation of errors between the discrete mass and momentum fields enables alleviation of many of the issues that plague such numerical methods, especially in the context of low to moderate spatial resolutions. A secondary but important mitigating factor is the advancements made in the modeling of capillary forces, resulting in the adoption of consistent and *well-balanced* surface tension formulations.³. We refer the reader to influential works of Popinet [6, 20] to get a better understanding of the issues surrounding surface tension implementations.

4.1 General Principles	24
4.2 Basic Expressions	27
4.3 Advection on Staggered Grids	34

1: Approximations are made while interfacial propagation , curvature computation, surface tension modeling etc.

[23]: Fuster et al. (2018), ‘A momentum-conserving, consistent, Volume-of-Fluid method for incompressible flow on staggered grids’

2: First of all, the transport of mass (density) has to be made consistent with that of the geometric transport of volume fraction.

3: Consistency in the context of surface tension models refers to the ability of methods to progressively achieve more accurate estimations of interfacial curvature as a result of increasing spatial resolution, whereas well-balanced refers to the ability to recover certain static equilibrium solutions pertaining to surface tension dominated flows without the perpetual presence of parasitic or spurious currents in the velocity fields.

Major Iterations in Literature

The first study to address the issue of consistency between mass and momentum transport was the seminal work of Rudman [27]. The fundamental hurdle in the implementation of mass-momentum consistent transport for staggered configurations of primary variables (pressure and velocity) is the inherent difficulty in reconstructing mass (defined on centered control volumes) and its corresponding fluxes onto the staggered control volumes on which momentum is defined. Rudman introduced the strategy of carrying out mass advection⁴ on a grid twice as fine as that of momentum, thereby enabling a ‘natural’ and intuitive way to reconstruct mass and its fluxes onto staggered momentum control volumes. However, the method uses a VOF based convolution technique for curvature computation, which is neither consistent nor well-balanced.

Bussmann et al. [28] were able to circumvent the issue surrounding staggered grids altogether by using a collocated arrangement in the context of hexahedral unstructured meshes, coupled with an unsplit Eulerian flux computation method. The study though makes no mention of any surface tension model.

Level set based methods in the context of mass-momentum consistent transport were implemented first by Raessi and Pitsch [29], followed by Ghods and Hermann [30]. In the former, the consistency problem is tackled by means of a semi-Lagrangian approach, computing geometric level set derived fluxes at two different time intervals, whereas in the latter, a collocated arrangement is used. Nonetheless, both methods face certain drawbacks, notably the applicability only to 2D in case of Raessi and Pitsch, as well as a lack of well-balanced surface tension models for both these methods.

Recent advances concerning volume-of-fluid based methods that employ unsplit (conservative) geometric flux reconstructions were made by LeChenadec and Pitsch [31], and later by Owkes and Desjardins [32]. LeChenadec and Pitsch utilize a Lagrangian remap method in order to construct consistent mass-momentum fluxes for the staggered control volumes, while Owkes and Desjardins use mass advection on a doubly refined grid (same principle as Rudman) to achieve consistency. Although [31] implements a well-balanced surface tension model, the VOF convolution based curvature computation is not consistent. In case of [32], they use mesh-decoupled height functions to compute curvature while coupling it with a well-balanced surface tension model. However, their semi-Lagrangian flux computation procedure involving streak tubes and flux polyhedra are extremely convoluted in 3D.

Certain methods attempt to combine the qualities of both VOF and level set methodologies (CLSOVF), as proposed in the works of Vaudor et al. [33], and more recently by Zuzio et al. [34]. They both tackle the consistency issue by means of projecting the direction-split geometric fluxes onto a twice finer grid, which are subsequently recombined to reconstruct consistent fluxes for mass and momentum for the staggered control volumes. This approach allows them to bypass the requirement of conducting mass advection on a twice finer grid (as in the original Rudman method), thereby deriving the benefits of a sub grid without the

[27]: Rudman (1998), ‘A volume-tracking method for incompressible multifluid flows with large density variations’

4: Mass advection was carried out using using algebraic flux reconstructions.

[28]: Bussmann et al. (2002), ‘Modeling high density ratio incompressible interfacial flows’

[29]: Raessi et al. (2012), ‘Consistent mass and momentum transport for simulating incompressible interfacial flows with large density ratios using the level set method’

[31]: Le Chenadec et al. (2013), ‘A monotonicity preserving conservative sharp interface flow solver for high density ratio two-phase flows’

[32]: Owkes et al. (2017), ‘A mass and momentum conserving unsplit semi-Lagrangian framework for simulating multiphase flows’

[33]: Vaudor et al. (2017), ‘A consistent mass and momentum flux computation method for two phase flows. Application to atomization process’

added computational cost of doubly refined mass transport. In addition, both Vaudor et al. [33] and Zuzio et al. [34] adopt well-balanced surface tension models with consistent level set based curvature estimation. However, the purported advantages of both these methods with regards to reduced computational costs is not quite evident, as additional complexities are introduced due to the projection (reconstruction) of fluxes onto a the twice finer mesh, which would not be necessary in the first place if mass transport had been carried out on the twice finer mesh itself.

Patel and Natarajan [35] developed a hybrid staggered-collocated approach to solve the consistency issue on polygonal unstructured meshes, complemented with a well-balanced surface tension model. Nevertheless, the VOF advection is based on algebraic transport, not to mention the use of a VOF convolution based curvature computation, which is inherently not consistent.

More recently, Nangia et al. [36] developed a CSLVOF method for dynamically refined staggered Cartesian grids. They utilize Cubic Upwind Interpolation (CUI) schemes to reconstruct consistent mass and momentum fluxes on the staggered control volumes, using the information from the additional mass advection equation they solve alongside the level set function. However, the reconstruction of mass fluxes using CUI schemes are inherently algebraic, with their comparative advantage against fluxes computed via geometric constructions being an open question⁵.

To get a bird's eye view of the numerous features employed by the methods in existing literature, we refer the reader to tables which respectively provide systematic overviews of the VOF based and level set based approaches.

Our Approach

In the present body of work, we start by precisely defining the essential (desired) attributes of a numerical scheme that ensures discrete consistency between mass and momentum transport :

- The discontinuity of the mass (volume fraction derived density field) should propagate at the exact 'numerical' speed as that of the discontinuity of the momentum field.
- The numerical transport of momentum should be performed in a manner consistent to the transport of mass for each direction, implying that the momentum fluxes must be obtained directly from geometrically computed fluxes of mass (volume).

In order to tackle the challenge of consistent transport on staggered control⁶ volume configurations, we have developed two different strategies, namely, the *shifted fractions* method and the *sub-grid* method. The former uses geometrical reconstructions to derive a *shifted* volume fraction field which is centered on the staggered control volumes, whereas the latter adopts the Rudman [27] strategy of volume advection on a twice finer grid in order to enable consistent reconstruction of mass and momentum on the staggered control volumes. Another key contribution of this body of work is to extend the conservative direction-split mass transport

[34]: Zuzio et al. (2020), 'A new efficient momentum preserving Level-Set/VOF method for high density and momentum ratio incompressible two-phase flows'

[35]: Patel et al. (2017), 'A novel consistent and well-balanced algorithm for simulations of multiphase flows on unstructured grids'

[36]: Nangia et al. (2019), 'A robust incompressible Navier-Stokes solver for high density ratio multiphase flows'

5: refer to Mirjalili et al. [11].

6: 'PARIS Simulator' has a staggered configuration of primitive variables on regular Cartesian control volumes.

algorithm of Weymouth and Yue [10] to the direction-split transport of momentum.

A thorough description of the shifted fractions method can be found in the recent study by Fuster et al. [23], and a detailed exposition of the sub-grid method is currently under preparation at the time of writing. We shall be taking a closer look at these two strategies in the upcoming sections.

4.2 Basic Expressions

We start with the advection of the interface position, which in the VOF framework is given by -

$$\frac{\partial H}{\partial t} + \nabla \cdot (\mathbf{u}H) = H (\nabla \cdot \mathbf{u}) \quad (4.1)$$

Integrating this equation in time after carrying out spatial discretization, one obtains -

$$C_{i,j,k}^{n+1} - C_{i,j,k}^n = - \sum_{\text{faces } f} F_f^{(c)} + \int_{t_n}^{t_{n+1}} dt \int_{\Omega} H (\nabla \cdot \mathbf{u}) dx, \quad (4.2)$$

where the first term on the right-hand side is the summation over the cell faces f of the fluxes $F_f^{(c)}$ ⁷. As one can clearly observe, the “compression” term on the right-hand side of equation (4.1) disappears for incompressible flow, however it is essential in the context of direction-split geometric advection schemes. The definition of the geometric fluxes in mathematical form is -

$$F_f^{(c)} = \int_{t_n}^{t_{n+1}} dt \int_f u_f(\mathbf{x}, t) H(\mathbf{x}, t) dx, \quad (4.3)$$

where $u_f = \mathbf{u} \cdot \mathbf{n}_f$ ⁸. Once an approximation for the evolution of $(\mathbf{u}H)$ during the time step is chosen, a four-dimensional integral remains to be computed in equation (4.3). The advection schemes used are CIAM and Weymouth-Yue, which have been described briefly in chapter 2.

Directional splitting results in the breakdown of equation (4.2) into three equations, one for each advection substep -

$$C_{i,j,k}^{n,l+1} - C_{i,j,k}^{n,l} = -F_{m-}^{(c)} - F_{m+}^{(c)} + c_m \partial_m^h u_m, \quad (4.4)$$

After each advection substep (4.4), the interface is reconstructed with the updated volumes $C_{i,j,k}^{n,l+1}$, then the fluxes $F_f^{(c)}$ are computed for the next

[10]: Weymouth et al. (2010), ‘Conservative volume-of-fluid method for free-surface simulations on cartesian-grids’

[23]: Fuster et al. (2018), ‘A momentum-conserving, consistent, Volume-of-Fluid method for incompressible flow on staggered grids’

In the VOF approach, the approximation to the interface Heaviside function contains a sharp discontinuity, in contrast to the level set approach where the approximation is continuous in the discrete sense.

$C_{i,j,k}^n$ is the colour function or volume fraction field at time step n obtained through the finite volume discretization of the interface Heaviside function.

7: These fluxes of $(\mathbf{u}H)$ are computed via geometrical reconstructions, and not via high-order non-linear interpolation schemes which are the standard (in the absence of discontinuities).

8: Component of the velocity normal to the control surface f .

The superscript $l = 0, 1, 2$ is the substep index, i.e. $C_{i,j,k}^{n,0} = C_{i,j,k}^n$ and $C_{i,j,k}^{n,3} = C_{i,j,k}^{n+1}$. The face with subscript $m-$ is the “left” face in direction m with $F_{m-}^{(c)} \geq 0$ if the flow is locally from right to left. A similar reasoning applies to the “right” face $m+$.

substep. Importantly, we have approximated the compression term in (4.2) by -

$$\int_{t_n}^{t_{n+1}} dt \int_{\Omega} H \partial_m u_m dx \simeq c_m \partial_m^h u_m \quad (4.5)$$

On the right hand sides of (4.4) and (4.5) the flux terms $F_f^{(c)}$ and the partial derivative $\partial_m u_m$ must be evaluated using identical discretized velocities. The expression $\partial_m^h u_m$ is a finite volume approximation of the spatial derivative corresponding to the m th component of the velocity vector along direction m , and the “compression coefficient” c_m approximates the color fraction. Its exact expression is dependent on the advection method⁹ and it also entails the desirable property of C-bracketing¹⁰. Due to the possible dependence of the compression coefficient c_m on the Cartesian direction corresponding to the advection substep, the sum $\sum_m c_m \partial_m^h u_m$ may not necessarily vanish even if the flow is incompressible. As mentioned previously in chapter 2, the main appeal of the Weymouth-Yue method is its ability to keep this sum to zero, within the limits of machine precision.

There is no implicit summation carried out over m , and the superscript h denotes the spatial discretization of the operator.

9: Refer to chapter 2 to see the difference in the definitions of the compression coefficient between the CIAM and Weymouth-Yue methods.

10: The preservation of $0 \leq C_{i,j,k} \leq 1$ is referred to as C-bracketing.

Advection of Conserved Scalars

In order to achieve consistent transport of the discontinuous fields of mass and momentum, we start by trying to understand the advection of a generic *conserved* scalar quantity ϕ by a continuous velocity field -

$$\frac{\partial \phi}{\partial t} + \nabla \cdot (\phi \mathbf{u}) = 0 \quad (4.6)$$

where the field ϕ is smoothly varying except at the interface position, where it may be discontinuous. The essence of this study lies in the search of a scheme that propagates this discontinuity (ϕ) at the same speed as that of the advection of volume fraction (C).

Temporal integration of the spatially discretized version of (4.6) gives us -

The smoothness of the advected quantity away from the interface is verified for fields such as density ρ , momentum $\rho \mathbf{u}$ and internal energy ρe .

$$\phi_{i,j,k}^{n+1} - \phi_{i,j,k}^n = - \sum_{\text{faces } f} F_f^{(\phi)} \quad (4.7)$$

where the fluxes are defined as -

$$F_f^{(\phi)} = \int_{t_n}^{t_{n+1}} dt \int_f u_f(x, t) \phi(x, t) dx \quad (4.8)$$

The sum on the right-hand side is the sum over faces f of cell i, j, k of the fluxes $F_f^{(\phi)}$ of ϕ , which are defined as the color function fluxes $F_f^{(c)}$ in (4.3).

In order to “extract” the discontinuity we introduce the interface Heaviside function $H(x, t)$

$$F_f^{(\phi)} = \int_{t_n}^{t_{n+1}} dt \int_f [u_f H \phi + u_f (1 - H) \phi] dx \quad (4.9)$$

Therefore, the flux can be decomposed into two components as -

$$F_f^{(\phi)} = \bar{\phi}_1 \int_{t_n}^{t_{n+1}} dt \int_f u_f H dx + \bar{\phi}_2 \int_{t_n}^{t_{n+1}} dt \int_f u_f (1 - H) dx, \quad (4.10)$$

where the face averages $\bar{\phi}_s, s = 1, 2$, are defined as -

$$\bar{\phi}_s = \frac{\int_{t_n}^{t_{n+1}} dt \int_f \phi u_f H_s dx}{\int_{t_n}^{t_{n+1}} dt \int_f u_f H_s dx}, \quad (4.11)$$

and $H_1 = H, H_2 = 1 - H$. The total flux can be rearranged as a sum of the constituents corresponding to the different ‘fluids’ -

$$F_f^{(\phi)} = \bar{\phi}_1 F_f^{(c)} + \bar{\phi}_2 F_f^{(1-c)}. \quad (4.12)$$

Expression (4.10) can be written in terms of the fluxes $F_f^{(c)}$ and $F_f^{(1-c)}$, this second one being obtained by replacing H with $1 - H$ in (4.3)

Advection of Density

The density field $\rho(x, t)$ follows the temporal evolution of the generic conserved quantity (4.6) by setting $\phi = \rho$. At the incompressible limit the velocity field is solenoidal (divergence-free), with constant densities in each phase. We can extract the density trivially from the integrals (4.11) to *exactly* obtain $\bar{\rho}_s = \rho_s$. The flux definitions corresponding to ρ becomes -

$$F_f^{(\rho)} = \rho_1 F_f^{(c)} + \rho_2 F_f^{(1-c)} \quad (4.13)$$

Using the above definitions for density fluxes, one can employ any VOF method to construct fluxes of the color function in order to obtain conservative transport for ρ . In principle, this should result in the conservation of total mass. However, as we have already pointed out the fact that the CIAM method does not conserve volume exactly¹¹, consequently, the advection of the density field (mass) is not consistent with that of the advection of C .

This apparent paradox is resolved by including the compression term on the right hand side of (4.6), in order to ensure consistency. The advection equation for the conserved quantity now becomes -

$$\frac{\partial \phi}{\partial t} + \nabla \cdot (\phi \mathbf{u}) = \phi (\nabla \cdot \mathbf{u}) \quad (4.14)$$

We use the term ‘conservative’ to express the fact that eq. (4.7) computes the temporal evolution of ρ as a difference of fluxes, instead of velocity times its gradient.

11: This again comes back to the dependence of the compression coefficient on the volume fraction field at the start of each advection substep.

This equation can be decomposed into advection substeps corresponding to the direction-split integration framework as follows -

$$\phi_{i,j,k}^{n,l+1} - \phi_{i,j,k}^{n,l} = -F_{m-}^{(\phi)} - F_{m+}^{(\phi)} + \left(\tilde{\phi}_1^m c_m^{(1)} + \tilde{\phi}_2^m c_m^{(2)} \right) \partial_m^h u_m \quad (4.15)$$

The fluxes $F_{m\pm}^{(\phi)}$ follow the definition given in (4.12), , while the cell averages $\tilde{\phi}_s^m$ are defined as -

$$\tilde{\phi}_s^m = \frac{\int_{t_n}^{t_{n+1}} dt \int_{\Omega} \phi H_s \partial_m^h u_m dx}{\int_{t_n}^{t_{n+1}} dt \int_{\Omega} H_s \partial_m^h u_m dx} \quad (4.16)$$

Rewriting the direction-split integration operation for ρ we get -

$$\rho_{i,j,k}^{n,l+1} - \rho_{i,j,k}^{n,l} = -F_{m-}^{(\rho)} - F_{m+}^{(\rho)} + C_m^{(\rho)}, \quad (4.17)$$

where the fluxes are given by (4.13) and the compression term is

$$C_m^{(\rho)} = \left(\rho_1 c_m^{(1)} + \rho_2 c_m^{(2)} \right) \partial_m^h u_m \quad (4.18)$$

For the WY method, the compression terms eventually cancel upon summation over the substeps, therefore resulting in the conservation of mass at the same accuracy as the discrete incompressibility condition $\sum_{m=1}^3 \partial_m^h u_m = 0$ is verified ¹² .

Advection of Momentum

Within the framework of advection of a generic conserved scalar, we consider momentum advection as transport of the scalar quantities $\phi = \rho u_q$, where $q = 1, 2, 3$ is the component index. Using the definition given in (4.11), we obtain the expression -

$$\overline{\rho u_q}_s = \rho_s \bar{u}_{q,s} \quad (4.19)$$

where $\bar{u}_{q,s}$ is termed as the “adverted interpolated velocity”, whose precise definition is given as -

$$\bar{u}_{q,s} = \frac{\int_{t_n}^{t_{n+1}} dt \int_f u_q u_f H_s dx}{\int_{t_n}^{t_{n+1}} dt \int_f u_f H_s dx} \quad (4.20)$$

Thus, the direction-split integration of the momentum can be represented as -

The direction-split integration steps operations for ϕ mirror that of the volume fraction C .

$c_m^{(1)} = c_m$ is the compression coefficient corresponding to the particular VOF advection method for volume fraction C , while $c_m^{(2)} = 1 - c_m$ corresponds to that of the symmetric color fraction $1 - C$.

In case of CIAM, the compression coefficient is defined as $c_m = C_{i,j,k}^{n,l}$, whereas in Weymouth-Yue the coefficient is independent of the advection substep l , defined as $c_m = H(C_{i,j,k}^n - 1/2)$, where H is the Heaviside function.

Again, there is no implicit summation rule on m .

12: This usually corresponds to the tolerance of the Poisson solver, with a typical value being 10^{-6} .

The expressions with the ‘bar’ refer to face weighted averages of the variable in question. Here, $\bar{\phi}_s = \overline{\rho u_q}_s$

The subscript s denotes the phase or fluid, and f represents the normal components defined on the face centers.

$$(\rho u_q)_{i,j,k}^{n,l+1} - (\rho u_q)_{i,j,k}^{n,l} = -F_{m-}^{(\rho u)} - F_{m+}^{(\rho u)} + \left(\rho_1 \tilde{u}_{q,1}^m c_m^{(1)} + \rho_2 \tilde{u}_{q,2}^m c_m^{(2)} \right) \partial_m^h u_m \quad (4.21)$$

where the momentum fluxes are constructed in the following manner -

$$F_f^{(\rho u)} = \rho_1 \bar{u}_{q,1} F_f^{(c)} + \rho_2 \bar{u}_{q,2} F_f^{(1-c)}, \quad (4.22)$$

The expression for the “central interpolated velocity” corresponding to the averages $\tilde{\phi}_s^m$ of (4.16) is -

$$\tilde{u}_{q,s}^m = \frac{\int_{t_n}^{t_{n+1}} dt \int_{\Omega} u_q H_s \partial_m^h u_m dx}{\int_{t_n}^{t_{n+1}} dt \int_{\Omega} H_s \partial_m^h u_m dx} \quad (4.23)$$

The superscript m is intentionally omitted for the velocities \tilde{u}_q^m in order to avoid cumbersome and complicated notations.

As a reasonable approximation we choose to put $\bar{u}_q = \bar{u}_{q,1} = \bar{u}_{q,2}$ for the “advection interpolated velocity” and $\tilde{u}_q = \tilde{u}_{q,1} = \tilde{u}_{q,2}$ for the “central interpolated velocity”. An important simplification which serves as the central model in our development is given by -

$$F_f^{(\rho u)} = \bar{u}_q F_f^{(\rho)} \quad (4.24)$$

Therefore, the advection substep for the momentum can finally be written as -

$$(\rho u_q)_{i,j,k}^{n,l+1} - (\rho u_q)_{i,j,k}^{n,l} = -\bar{u}_q F_{m-}^{(\rho)} - \bar{u}_q F_{m+}^{(\rho)} + \tilde{u}_q C_m^{(\rho)} \quad (4.25)$$

where the density fluxes are defined in (4.13) and the compression term $C^{(\rho)}$ in (4.18).

Although the weighted averages \bar{u}_q and \tilde{u}_q have been defined, but the manner in which they are estimated shall be covered in the following section.

In the context of the CIAM advection scheme, the compression coefficient for the volume fraction field is $C^{n,l}$, similarly, for the central interpolated velocity we take $\tilde{u}_q = u_q^{n,l}$. Due to the summation of the directional divergences not cancelling out, the resulting momentum transport after three directionally-split advects and the result is not exactly conservative. On the other hand, the compression coefficient is independent of the advection substep in the context of the Weymouth-Yue advection scheme. The final expression for the compression coefficient becomes -

Notice that “cloning” the advected velocities $\bar{u}_{q,1}$ and $\bar{u}_{q,2}$ would make it easier to advect a velocity field with a jump on the interface, but would render the overall algorithm quite complicated.

Due to the viscous effects and the absence of phase change in our fluid dynamics model, the velocity field maintains continuity across the interface.

To add clarity to the notion of “central interpolated velocity”, one can understand this as the face-centered interpolations of the velocity field (component normal to control surface), which is required to compute the fluxes of volume.

In the above expression the face-weighted average velocities \bar{u}_q are defined using (4.20) on the corresponding left face $m-$ or right face $m+$.

The Weymouth-Yue coefficient is a constant value c , that is independent of direction m .

$$C_m^{(\rho)} = (\rho_1 c + \rho_2 (1 - c)) \partial_m^h u_m. \quad (4.26)$$

Since there is no bracketing on the any velocity component, we take $\tilde{u}_q = u_q^n$, which is independent of the substep l .

The final expression after cancellation of the compression terms, having undergone three advection substeps (4.25) is

$$(\rho u_q)_{i,j,k}^{n,3} - (\rho u_q)_{i,j,k}^n = - \sum_{\text{faces f}} \bar{u}_q F_f^{(\rho)}. \quad (4.27)$$

Therefore, the extension of the Weymouth-Yue mass (volume) advection scheme to the consistent transport of momentum allows the discrete transport to be exactly conservative.

Velocity Interpolations

The direction-split momentum transport given by (4.25) can be carried out in either of the bulk of the phases, or at close proximity to the interface location. The treatment away from the interface is expressed as -

$$u_q^{n,3} - u_q^n = - \sum_{\text{faces f}} \bar{u}_q u_f \quad (4.28)$$

Here, we distinguish between an “advecting” velocity $u_f = \mathbf{u} \cdot \mathbf{n}_f$ ¹³, and an “advected velocity” component $\bar{u}_{q,f}$, which is basically an average over the face f . Due to the momentum transport being carried out on staggered control volumes, both these velocity components require some interpolations from their original positions onto the necessary positions on the staggered grid. Using this new nomenclature, (4.28) becomes -

$$u_q^{n,3} - u_q^n = - \sum_{\text{faces f}} \bar{u}_q^{(\text{advected})} u_f^{(\text{advecting})} \quad (4.29)$$

Now, moving onto the approximation in the neighbourhood of the interface, we get -

$$(\rho u_q)^{n,3} - (\rho u_q)^n = - \sum_{\text{faces f}} \bar{u}_q^{(\text{advected})} F_f^{(\rho)} + \sum_{m=1}^3 \bar{u}_q C_m^{(\rho)} \quad (4.30)$$

The crux of our model for momentum advection is described by these two equations ((4.29) & (4.30)). We start by pointing out the staggered spatial arrangement of our primary variables (pressure, velocity, volume fraction), as illustrated by Fig. 4.1 in a 2D representation.¹⁴

The compression terms sum up to the accuracy to which the solenoidal nature of the velocity field is discretely verified .

In the bulk, the expression simplifies considerably due to the density and volume fraction being constant, hence resulting in the cancellation of the spurious compression terms. .

13: The “advecting” velocity computes the fluxes of volume fraction.

In the previous section we had derived a new expression for the momentum fluxes and the compression term, i.e. the RHS of (4.30), that is consistent with the discrete transport of the volume fraction. .

14: Figure 4.1 has the same variables arrangement that is found in 3D on a plane perpendicular to the z -axis and through the pressure point $p_{i,j,k}$.

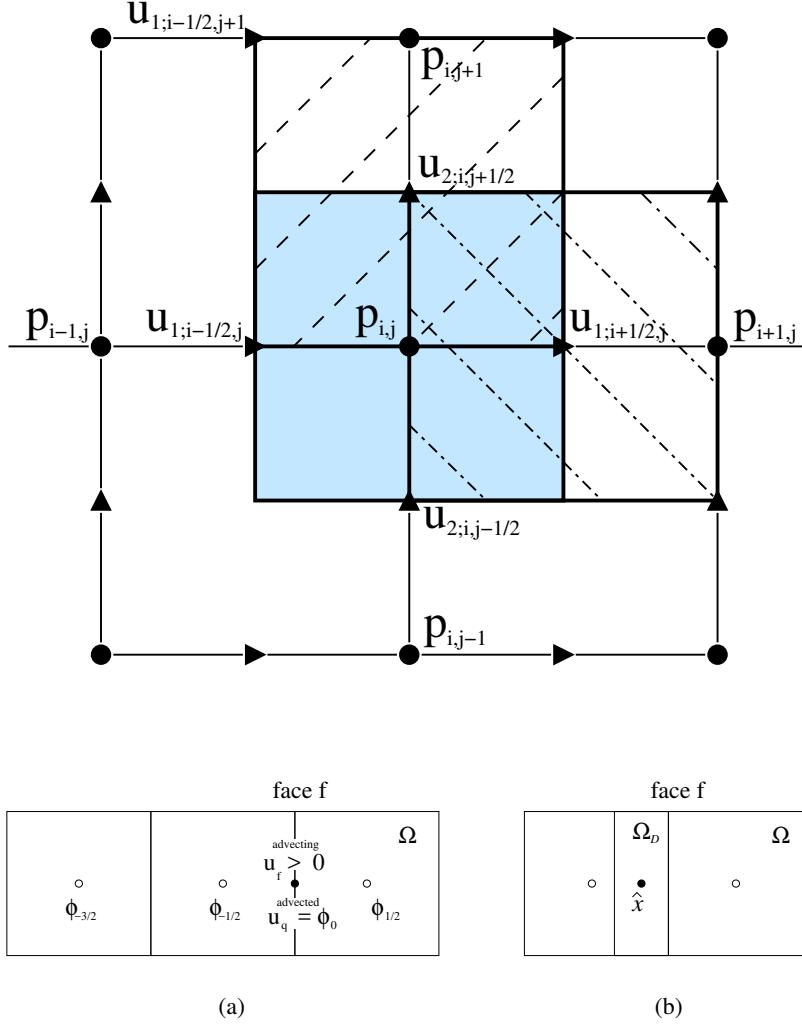


Figure 4.1: A 2D schematic of the staggered spatial configuration of the pressure and velocity variables. The pressure $p_{i,j}$ is based on the center of its control volume (light colour area); the horizontal velocity component $u_{1;i+1/2,j}$ is defined in the middle of the right edge of the pressure control volume and centered on its control volume (dash-dotted area); the vertical velocity component $u_{2;i,j+1/2}$ is defined in the middle of the top edge and centered on its corresponding control volume (dashed area). The volume fraction is defined at the same location as that of the pressure, resulting in pressure and density being centered on identical control volumes.

Figure 4.2: The reference control volume Ω for the advected velocity component $\phi = u_q$ is shown. A horizontal advection is here considered and both the advecting velocity u_f and the advected velocity require an interpolation for their value on the left face $f = 1-$: (a) the value $\bar{u}_q = \phi_0$ (full circle) is interpolated (see 8.3) from the values $\phi = u_q$ on the nodes (open circles); (b) a more sophisticated interpolation predicts the value $\phi(\hat{x})$ where \hat{x} is at the center of the “donating” region Ω_D (see 8.3).

To estimate the advecting velocities $u_f^{(\text{advecting})}$ we use a centered scheme. Consider a face perpendicular to the horizontal direction 1¹⁵. There are two cases, the first corresponding to when the advected component is not aligned with the face normal, which is the case with $q = 2$.

The advecting velocity $u_{1-}^{(\text{advecting})}$ is not given on this point, therefore it has to be interpolated as -

$$u_{1;i-1/2,j+1/2,k}^{(\text{advecting})} = \frac{1}{2}(u_{1;i-1/2,j,k} + u_{1;i-1/2,j+1,k}) \quad (4.31)$$

In the second case the advected component is aligned with the face normal, corresponding to $q = 1$. In this case, the interpolation becomes -

$$u_{1;i,j,k}^{(\text{advecting})} = \frac{1}{2}(u_{1;i-1/2,j,k} + u_{1;i+1/2,j,k}) \quad (4.32)$$

Thus far, we have covered only interpolations concerning the “advecting”

15: In particular, $f = 1-$.

The u_2 control volume in Fig. 4.1 is centered on $i, j + 1/2, k$, and face $f = 1-$ is then centered on $i - 1/2, j + 1/2, k$.

The u_1 control volume in Fig. 4.1 is centered on $i + 1/2, j, k$ and face $f = 1-$ is then centered on i, j, k .

velocity, which is basically used to compute fluxes of the volume fraction. Now we turn our attention to interpolations of the *adverted* velocity \bar{u}_q which appears in (4.30). In Fig. 4.2, we demonstrate the principle behind our interpolation scheme along the horizontal direction 1, with the lighter notation $\phi = u_q$. The objective is to interpolate the “adverted” velocity on the left face of the reference control volume Ω . In case of advected velocity u_1 and the advecting velocity (4.32) on face $f = 1-$, the relationship with the ϕ values in Fig. 4.2 is -

$$\phi_{-3/2} = u_{1;i-3/2,j,k}, \quad \phi_{-1/2} = u_{1;i-1/2,j,k}, \quad \phi_{1/2} = u_{1;i+1/2,j,k}, \quad \dots \quad (4.33)$$

whereas in the case of the “adverted” velocity u_2 and the advecting velocity (4.31), the relationship turns out to be -

$$\phi_{-3/2} = u_{2;i-2,j+1/2,k}, \quad \phi_{-1/2} = u_{2;i-1,j+1/2,k}, \quad \phi_{1/2} = u_{2;i,j+1/2,k}, \quad \dots \quad (4.34)$$

In order to get a prediction of ϕ_0 on the face $f = 1-$ in Fig. 4.2¹⁶ we utilize an interpolation function f that computes this value as a function of the four nearest points, and in an upwind manner based on the sign of the *advecting* velocity u_f . Thus, the interpolation can be expressed in the functional form as -

$$\phi_0 = f(\phi_{-3/2}, \phi_{-1/2}, \phi_{1/2}, \phi_{3/2}, \text{sign}(u_f)) \quad (4.35)$$

Throughout this body of work, we have extensively tested and used two variants of such interpolation functions, the exact implementation of which can be found in Appendix A. The interpolation functions are :

1. A scheme based on the QUICK third order interpolant in the bulk, away from the interface and a simple first order upwind flux near the interface.
2. A scheme based on the Superbee slope limiter [37] for the flux in the bulk and a modified Superbee limiter tuned to a shifted interpolation point near the interface.

4.3 Advection on Staggered Grids

The development of the consistent transport schemes should be integrated into the broader context of our numerical algorithm which deals with the coupling between the conservative formulation of the one-fluid Navier-Stokes equations and the geometric transport of the interface. We briefly recapitulate the overall algorithm in operator form as previously described in chapter 2

The interpolants we use in this case are one-dimensional and operate on the velocities u_q , on the center of their control volumes, that are regularly spaced on a segment aligned with the direction of the advection, that is also perpendicular to face f .

¹⁶: ϕ_0 serves as an approximation of \bar{u}_q given in (4.20).

The extension of these approximations to advection along the other two directions $q = 2, 3$ is straightforward.

The reader can refer to influential works of LeVeque [15] and Sweby [16] regarding the role of non-linear flux limiters such as QUICK, Superbee, WENO/ENO etc in the context of numerical methods for hyperbolic conservation laws.

[37]: Roe (1985), ‘Some contributions to the modelling of discontinuous flows’

The superscript h refers to discretization in space, and n corresponds to that in time.

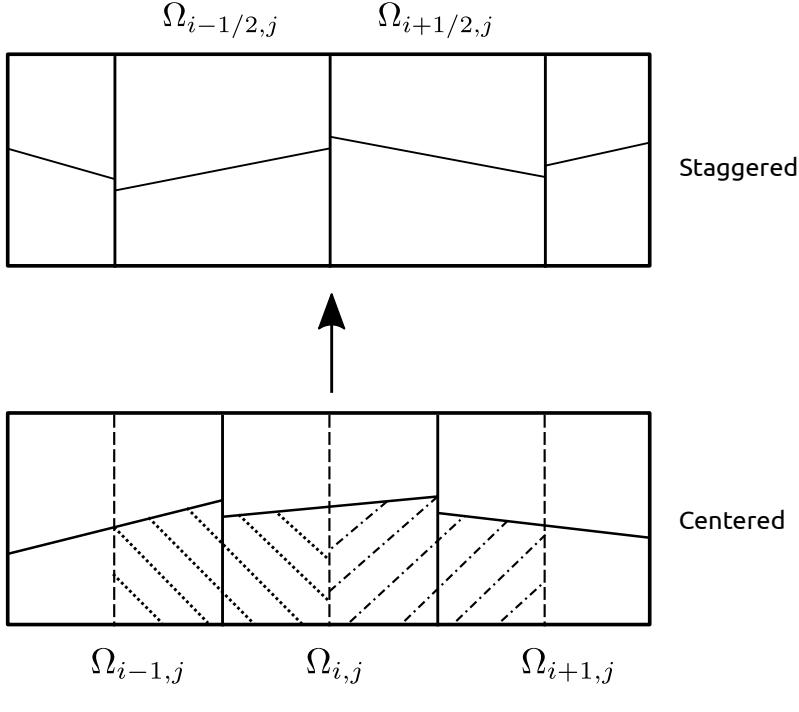


Figure 4.3: A 2D schematic of the reconstruction procedure used in the *shifted fractions* method. In this case, advection of the horizontal component of momentum is considered. The half-fractions from the centered control volumes $\Omega_{i,j}$ and $\Omega_{i+1,j}$ (dash-dotted area) are added together to obtain the volume fraction in the shifted (staggered) volume $\Omega_{i+1/2,j}$. Similarly, the half-fractions from $\Omega_{i-1,j}$ and $\Omega_{i,j}$ (dotted area) are combined to obtain the volume fraction $\Omega_{i-1/2,j}$. Once this horizontally shifted volume fraction field is reconstructed, the corresponding density, momentum and “adverted” velocity fields can be computed in order to carry out consistent transport of mass and momentum on this staggered configuration.

$$C^{n+1} = C^n + \tau L_{\text{vof}}^h(C^n, \mathbf{u}^n) \quad (4.36)$$

$$\begin{aligned} \rho^{n+1} \cdot \mathbf{u}^* &= \rho^n \cdot \mathbf{u}^n + \tau L_{\text{adv}}^h(C^n, \mathbf{u}^n) + \\ &\quad \tau \left[L_\mu^h(C^{n+1}, \mathbf{u}^n) + L_\sigma^h(C^{n+1}) + L_g^h(C^{n+1}) \right] \end{aligned} \quad (4.37)$$

In the preceding sections, we have thus far dealt with the intricacies concerning the coupling of the VOF advection (L_{vof}^h) with that of the momentum advection (L_{adv}^h). In this section, we describe two distinct strategies that we have implemented in order to achieve discrete consistency between mass (VOF) and momentum transport, specifically in the context of staggered Cartesian grids, with the configuration already illustrated in Fig. 4.1.

Shifted Fractions Method

This strategy tackles the problem of staggered control volumes by reconstructing¹⁷ the centered volume fraction field onto the staggered control volumes, thereby resulting in a field of *shifted* fractions.

A 2D schematic of this reconstruction procedure is given in Fig. 4.3, considering the advection of the horizontal component of momentum. At the beginning of the operations summarized by L_{adv} , each velocity (momentum) control volume overlaps two pressure/VOF (centered) control volumes i.e. $\Omega_{i+1/2,j}$ overlaps $\Omega_{i,j}$ and $\Omega_{i+1,j}$. Therefore, the two half-fractions from $\Omega_{i,j}$ and $\Omega_{i+1,j}$ are added together to obtain an estimate¹⁸ of the shifted fraction $C_{i+1/2,j}$ in $\Omega_{i+1/2,j}$. Once this key reconstruction step is carried out, the mass and momentum fields, as well

L_{adv} represents the conservative advection, L_μ represents the diffusive forces generated by viscous stresses, L_σ represents the capillary forces arising from the surface tension model and finally L_g represents the volumetric (body forces) source term.

17: The reconstructions involve geometrical operations, thus are not easily translated into equations.

18: These estimations utilize the set of geometric operations that are used in the reconstruction of the interface and fluxed volumes. The reader can refer to chapter 2 for a brief reminder.

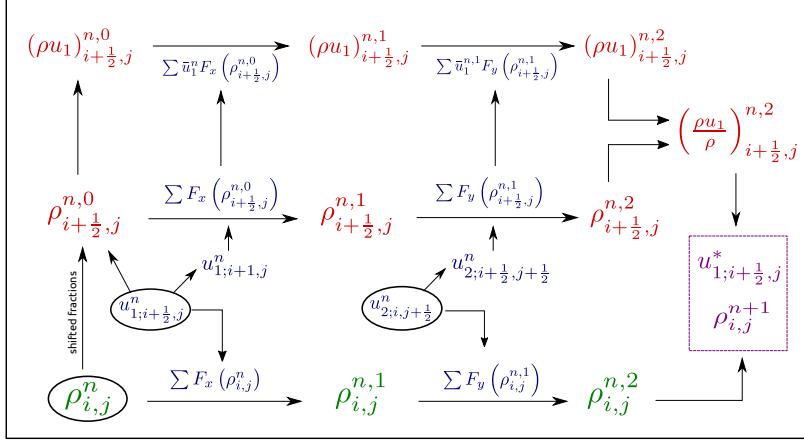


Figure 4.4: A bird's eye view of the *shifted fractions* method, highlighting the operations performed at each time step. This method achieves consistency in the discrete transport of mass and momentum on the staggered control volumes. In the interest of brevity, we present a 2D case for the density on the grid i, j and horizontal velocity u_1 on the staggered grid $i + 1/2, j$. The evolution of the velocity component u_2 on the staggered grid $i, j + 1/2$ is similar. The initial variables ρ^n, u_1^n, u_2^n are inside the ellipses. The interpolated "adverting" components u_1 and u_2 have superscript n . The shifted density $\rho^{n,0}$ is constructed with the shifted fractions of C to initialize the momentum component $(\rho u_1)^{n,0}$. The first split advection is along the x direction to variables with superscript $n, 1$, the second one is along the y direction to variables with superscript $n, 2$. The updated density is $\rho^{n,2} = \rho^{n+1}$ while the horizontal velocity $u_1^{n,2} = u_1^*$ enters the RHS of the Poisson-like equation 2.21.

as their corresponding fluxes can all be derived using the information from the shifted volume fraction field. These operations performed at each time step are summarized in the following steps :

1. Interface reconstruction at time t_n using data C^n .
2. Computation of half-fractions as shown in Fig. 4.3, in order to obtain the "shifted" fraction field C_q^n and ρ_q^n in the staggered control volumes.
3. Computation of all three momentum components $(\rho_q u_q)^n$ at t_n .
4. Advection of all three momentum components along one coordinate direction, say x direction, using (4.25) to obtain the updated momentum components $(\rho_q u_q)^{n,1}$ after the first substep.
5. Advection of the "shifted" density field ρ_q^n on the staggered volumes using VOF consistent advection, along the x direction in order to obtain the updated volume fractions after the first substep.
6. Extraction of the provisional velocity components¹⁹ $u_q^{n,1}$ after the first substep, i.e. $u_q^{n,1} = (\rho_q u_q)^{n,1} / \rho_q^n$.
7. The above operations are repeated for the different momentum components, shifted volume fractions and densities, and velocity components for the next two substeps with split advects along the y and z directions.²⁰ Finally, we obtain $(\rho_q u_q)^{n+1} = (\rho_q u_q)^{n,3}$ and $\tilde{\rho}_q^{n+1} = \rho_q^{n,3}$.
8. In parallel, the centered volume fraction field C^n is advected in order to obtain $C^{n+1} = C^{n,3}$ using the VOF advection method.

An important point to note from the above algorithm is that the advected velocity components u_q are updated at each substep, while the advecting velocities u_f are interpolated from the initial velocity field u^n at time t_n . The shifted fractions of Fig. 4.3 are computed using routines that are already part of our geometrical toolbox, used primarily in flux computation.

In essence, we have a consistent transport of density (mass) and momentum on the staggered grids, while simultaneously carrying out advection

$q = 1, 2, 3$ is the component index, e.g ρ_1 in $\Omega_{i+1/2,j,k}$ for the horizontal momentum component $\rho_1 u_1$.

The fluxes of momentum are derived from those of mass using the relation (4.24), which in turn are obtained in a consistent fashion from the fluxes corresponding to 'shifted' volume fraction field.

19: These provisional velocities are required to compute the "advected" velocities using the non-linear flux limiters, as described in (4.30).

20: At each time step, the sequence x, y, z is permuted, in order to avoid any systematic biases in error propagation.

of the volume fraction field on the centered grid. As a consequence, the momentum components $(\rho_q u_q)^{n+1}$ (at time step t_{n+1}) that are derived from the corresponding “shifted” volume fractions C_q^{n+1} and densities ρ_q^{n+1} (obtained from C^{n+1}) are different from the densities $\tilde{\rho}_q^{n+1} = \rho_q^{n,3}$, which were computed during the previous time step by directly advecting the “shifted” volume fractions C_q^n . The origin of this discrepancy is the approximate nature of the linear reconstruction of the interfaces, which is not even continuous on the boundary of its control volume. Therefore, this implies that the momentum is not exactly conserved between two time steps, even though the Weymouth-Yue method ensures conservative transport of the momentum on the staggered control volumes.

Sub-Grid Method

In this strategy, the difficulty associated with consistent transport on staggered control volumes is resolved by advecting the volume fraction (mass) on a twice finer grid²¹, very much in the spirit of Rudman’s [27] original work.

The primary motivation regarding the development of this method is the issue of conservation (lack of) concerning the discrete transport of momentum in case of the shifted fractions method. Basically, the issue arises quite simply due to the fact that the volume fraction C^{n+1} used to construct the staggered momentum field at the start of a new time step is *not* the identical to that which is obtained via advection on the staggered control volumes itself (C_q^{n+1}).²² The sub-grid method is able to evade these complications that arise due to the parallel evolution of two different volume fraction fields by conducting volume fraction on solely on the twice refined grid. An additional advantage of the having the sub-grid volume fraction field is that it facilitates a more ‘natural’ computation of not only the staggered volume fraction field C_q^{n+1} , but more importantly its fluxes. This method is currently only compatible with the implicit fluxes computed in the Weymouth-Yue VOF advection method.

Considering the overall approach, the *key differences* between our present algorithm and the implementations in the original works of Rudman and Weymouth-Yue are :

Rudman (1998)[27] The use of a conservative geometrical mass (volume fraction) transport framework instead of an algebraic one in the original method, which is applied to sub-grid volume fraction field.

Weymouth & Yue (2010) [10] The extension of the original method for conservative direction-split mass transport to the momentum field, culminating in the discrete consistency between mass momentum transport in the context of staggered Cartesian grids in 3D.

Spatial Configuration : Coarse & Sub-Grid Variables

To start, we describe the spatial orientation of the different variables on the two refinement levels of the grid. At the coarse grid level, the pressure and velocity fields are defined in a staggered configuration, with pressures at the cell centers (centroids in 3D) and velocities on the

A naive attempt to achieve momentum conservation could entail always using the shifted fields C_q^n and evolve them by the VOF method on the staggered cells. Such an approach would render the scheme conservative, but would result in the independent evolution of the three staggered grids, eventually leading to divergence.

21: The grid is twice as fine when compared to the control volume for momentum.

22: In the shifted fractions method, flux computations on the staggered cells necessitate another round of interfacial reconstructions based on the shifted volume fraction field, whereas the sub-grid volume fraction information enables one to circumvent the reconstructions and obtain the fluxes directly using simple surface integrals.

The notations for the variables are slightly different than those used in the previous sections (Fig. 4.1.) The velocity component in the horizontal and vertical directions are now denoted as U and V respectively, and the pressure by p .

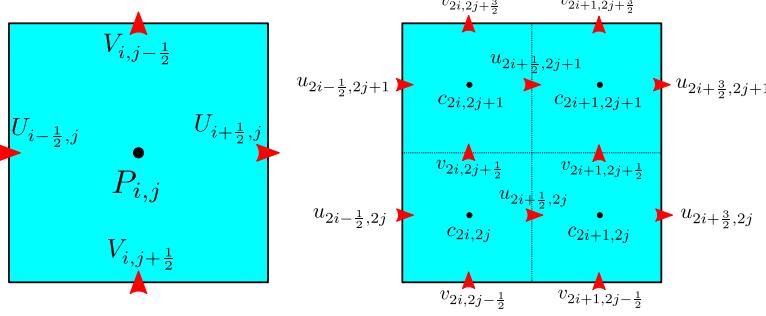


Figure 4.5: A 2D schematic of the arrangement of primary variables on the coarse and sub-grid levels. The control volume is decomposed into the two figures, the one on the left corresponding to the coarse grid variables, while the one on the right corresponding to the sub-grid. Superposition of these two figures, one on top of each other, represent the spatial relationships between the two sets of variables. The velocities on the sub-grid level are simple first or zeroth order interpolations of the coarse grid velocities.

cell face centers. In Fig. 4.5, we demonstrate the arrangement of variables, which one can easily extrapolate to 3D during implementation, but for the sake of clarity we illustrate its 2D equivalent. The volume fraction C ²³ is only defined on a grid that is twice as fine than that of the pressure/velocity grid, which we refer to as the sub-grid. Therefore in 3D, each cubic control volume is divided into eight constituent smaller cubic volumes at the centroids of which, the volume fraction field is centered.

Multiscale Coupling : Restriction & Prolongation Operations

As is paradigmatic for dual-grid methods in the context of Navier-Stokes solvers, we carry out mass transport at the sub-grid level, and momentum transport at the coarse level. In pressure-projection based methods such as ours, the predominant bottleneck in terms of computational speed is the iterative solution to the discrete Poisson equation.²⁴ Therefore, solving the mass advection equation on the fine grid allows us not only to obtain more accurate solutions to the flow physics involved, but also enables us to avoid the significantly higher computational costs associated with solving a Poisson problem at a twice finer resolution.

Prolongation In order to advect the volume fraction at the sub-grid level, we need to reconstruct a velocity field at that level of resolution using information from the coarse grid velocity field. In order to achieve this, we have implemented a prolongation operator which asserts the following relations between the velocities on the two refinement levels

$$u_{2i-\frac{1}{2},2j} = u_{2i-\frac{1}{2},2j+1} = U_{i-\frac{1}{2},j} \quad (4.38)$$

$$u_{2i+\frac{3}{2},2j} = u_{2i+\frac{3}{2},2j+1} = U_{i+\frac{1}{2},j} \quad (4.39)$$

$$u_{2i+\frac{1}{2},2j} = u_{2i+\frac{1}{2},2j+1} = \left(U_{i+\frac{1}{2},j} + U_{i-\frac{1}{2},j} \right) / 2 \quad (4.40)$$

$$v_{2i,2j-\frac{1}{2}} = v_{2i+1,2j-\frac{1}{2}} = V_{i,j+\frac{1}{2}} \quad (4.41)$$

$$v_{2i,2j+\frac{3}{2}} = v_{2i+1,2j+\frac{3}{2}} = V_{i,j-\frac{1}{2}} \quad (4.42)$$

$$v_{2i,2j+\frac{1}{2}} = v_{2i+1,2j+\frac{1}{2}} = \left(V_{i,j+\frac{1}{2}} + V_{i,j-\frac{1}{2}} \right) / 2 \quad (4.43)$$

The notations in the above equations refer to the description of the coarse and sub-grid variables in Fig. 4.5. The first-order interpolation applied to

23: The volume fraction field C is denoted as c in Fig. 4.5.

24: The problem size of such elliptical partial differential equations is governed by the number of cells/points discretizing the velocity (or pressure) field. If we choose to solve the problem on a mesh with twice the resolution in 3D, that would lead to an 8 fold increase in the problem size for the discrete pressure-Poisson problem.

The prolongation operator has to be used at the start of each new time step, in order to compute the sub-grid velocity field.

the coarse grid velocity field ensures discrete incompressibility²⁵ at the sub-grid level. The choice of interpolation order used in the prolongation operator is identical to that of the original method of Rudman ([27]). In the current version of the sub-grid method, we have chosen to eschew the added complexity of solving local Poisson problems²⁶ through our prolongation operators, therefore sticking with the much simpler Rudman inspired interpolations.

25: This is a direct consequence of the solenoidal nature of the coarse grid velocity field.

26: The use of higher order interpolation schemes would necessitate finding the solutions of local Poisson problems, in order to render the sub-grid velocity field discretely divergence-free.

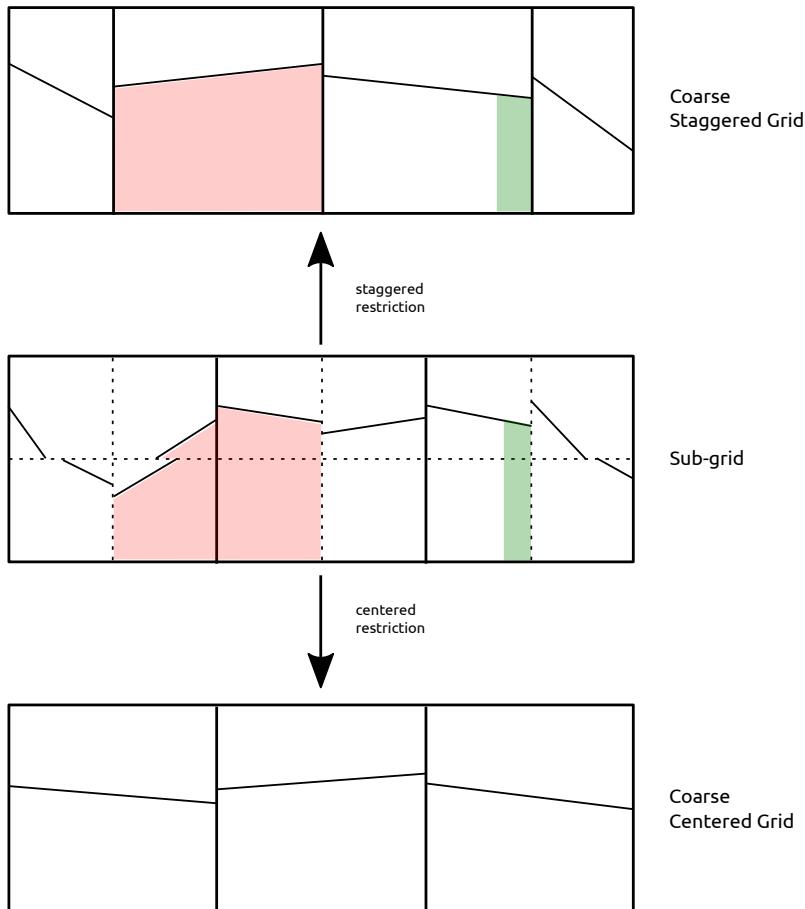


Figure 4.6: A 2D illustration of the restriction operations involved between the different grid resolutions, where the sub-grid grid boundaries are denoted by the dashed lines, and that of the overlapping coarse grid by solid lines. Restriction operations in the form of simple volume integrals are performed on the sub-grid volume fraction in order to compute the staggered and centered volume fraction fields at the coarse grid level. Restriction operators in the form of surface integrals are also performed in order to compute the volume fluxes at the boundaries of the coarse staggered control volumes. The red shaded areas correspond to the volume fractions, whereas the green shaded area corresponds to that of volume fluxes. The interface segments as depicted at the coarse grid level are just for purpose of illustration, and are not ‘reconstructed’. Unlike the shifted fractions method, the interfacial reconstructions on the staggered volumes are not necessary, due to the fact that sub-grid volume fluxes are simply combined to compute the staggered fluxes.

Restriction In order to compute the required density and momentum fields on the staggered grid (coarse level), we implement restriction operators that use information from the sub-grid volume fraction field. In Fig. 4.6, we demonstrate the different mappings between the two grid levels, which essentially boils down to volume integrals for the centered fields, and surface integrals for their corresponding fluxes. A description of the different functions performed by the restriction operator is as follows :

- *Fine Grid $\longleftarrow\rightarrow$ Coarse Staggered Grid*

Density & Momentum The sub-grid volume fraction field is restricted to obtain a staggered density field at the coarse grid level (see Fig. 4.6), which on combining with the appropriate component of the velocity field produces the staggered momentum field.

Fluxes The geometric fluxes from the sub-grid volume fraction field are restricted in order to obtain coarse grid fluxes for the

The restriction operators work in an identical manner as in Rudman ([27]), which are nothing but simple volume integrals of the sub-grid field mapped onto the domains corresponding to the coarse grid control volumes.

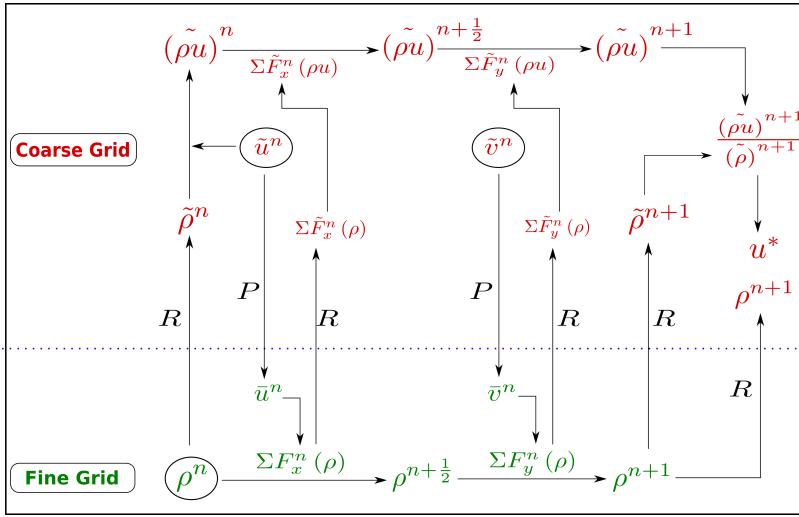


Figure 4.7: A bird's eye view of the *sub-grid* method, highlighting the operations performed at each time step, and additionally ensures conservation of momentum. For sake of clarity, present a 2D case for the density on the grid i, j and horizontal velocity \bar{u} on the staggered grid $i + 1/2, j$. The variables in red are all defined on the coarse level, and those in green are at the sub-grid level. The operators R and P denote the restriction and prolongation operations respectively. The 'tilde' on top of the variables (e.g. $\tilde{\rho}^n$) are used to convey that the variables are centered on the staggered control volumes at the coarse grid level, whereas the 'bar' on top conveys that the variables are staggered with respect to the sub-grid. The starting variables are enclosed in elliptical borders, and the variables at the end of the direction-split integrations are u^* and ρ^{n+1} , where u^* is subsequently fed into the RHS of the Poisson problem.

corresponding staggered volumes, which on combining with relation (4.24) gives us the corresponding momentum fluxes.

► *Fine Grid \longleftarrow Coarse Centered Grid*

Density & Viscosity The sub-grid volume fraction field is restricted to compute a centered volume fraction field at the coarse grid level, which is subsequently used to derive the centered density and viscosity fields at the coarse grid level.

Algorithm

To summarize the operations performed at each time step pertaining to the advection operator in our one-fluid Navier-Stokes framework, we present Fig. 4.7, which illustrates a 2D version of the sub-grid method that ensures consistent and conservative mass-momentum transport, highlighting the interactions between the variables defined on the different grids. The algorithm is also summarized in the following steps, corresponding to a 2D setup :

1. Interface reconstruction at time t_n , at the sub-grid level, using data c^n .
2. Restriction of the sub-grid volume fraction in order to compute the "shifted" fraction fields C_q^n and ρ_q^n in the staggered control volumes.
3. Computation of all momentum components $(\rho_q u_q)^n$ at t_n .
4. Advection of the sub-grid volume fraction c^n along one coordinate direction, say x direction, to obtain $c^{n+1/2}$, using the Weymouth-Yue explicit advection method.
5. Advection of all momentum components along the x direction, in sync with the sub-grid VOF advection, using (4.25) to obtain the updated momentum components $(\rho_q u_q)^{n+1/2}$ after the first substep.
6. Restriction of the sub-grid field $c^{n+1/2}$ as shown in Fig. 4.6 , in order to compute the "shifted" density field $\rho_q^{n+1/2}$ on the staggered volumes.

$q = 1, 2$ is the component index, e.g ρ_1 in $\Omega_{i+1/2,j}$ for the horizontal momentum component $\rho_1 u_1$.

The fluxes of momentum are derived from those of mass using the relation (4.24) , which in turn are obtained via restriction operations applied to the sub-grid volume fraction fluxes.

7. Extraction of the provisional velocity components ²⁷ $u_q^{n+\frac{1}{2}}$ after the first substep, i.e. $u_q^{n+\frac{1}{2}} = (\rho_q u_q)^{n+\frac{1}{2}} / \rho_q^{n+\frac{1}{2}}$.
8. The above operations are repeated for the different momentum components, in sync with the direction-split advection of the sub-grid volume fraction along the remaining direction. ²⁸ Finally, we obtain $u_q^* = (\rho_q u_q)^{n+1} / \rho_q^{n+1}$ on the staggered grid.
9. In parallel, the updated centered volume fraction field C^{n+1} is obtained at the coarse grid level, by applying the restriction operator on the updated sub-grid volume fraction c^{n+1} .

The resulting method not only maintains discrete consistency between mass and momentum transport on the staggered grid, but also ensures that the transport of momentum is consistent in 3D. The other time-split terms in equation (4.37) that arise from the source term discretizations, as well as the terms in the projection step (2.19) are solved in a standard non-conservative way. The density on the faces of the central cells are estimated using the restriction operations described previously, with these densities appearing via the ρ_q pre-factor in front of all the different source terms. Additionally, the sub-grid volume fraction can be used to get better estimates of the curvature field, which itself is defined on the staggered control volumes. At the time of writing, two different approaches are being developed and tested in order to get more accurate curvature fields.

In the following chapter, we shall take a look at some performance aspects of these mass-momentum consistent methods, using both quantitative and qualitative comparisons.

27: These provisional velocities are required to compute the “adverted” velocities using the non-linear flux limiters, as described in (4.30).

28: At each time step, the sequence x, y is permuted, in order to avoid any systematic biases in error propagation.

Generally, the face-centered density field is estimated using a simple average i.e. $\rho_{i+1/2,j,k} = (\rho_{i,j,k} + \rho_{i+1,j,k})/2$.

Numerical Benchmarks

In the upcoming sections, we demonstrate the robustness and accuracy of our class of mass-momentum consistent numerical methods when applied to challenging high density-ratio flow configurations, primarily in comparison to the version of our method which does not maintain consistency between the mass and momentum advection. Most of the standard tests that exist in the current literature concerning numerical methods to tackle liquid-gas flows such as the decay of spurious currents in static and moving droplets, viscous damping of capillary waves etc., are carried out in the absence of any density jump (or viscosity jump) across the interface separating the fluids. In this chapter, we shall take a closer look in detail at the behavior of our methods when dealing with difficulties that arise due to the non-linear coupling between interfacial deformation/propagation, capillary and viscous forces, especially in the regime where the material properties across the interface are separated by orders of magnitude, particularly in which the flow features in question are poorly resolved.

In order to assess the performance of the different methods, we shall use an easier nomenclature to describe the different methods, which are as follows :

- ▶ **M1** Method with non-consistent momentum-mass transport.
- ▶ **M2** Method with consistent momentum-mass transport, but not conservative. Uses half-fractions strategy.
- ▶ **M3** Method with consistent and conservative momentum-mass transport. Uses sub-grid strategy.

5.1 Static Droplet

A popular numerical benchmark in the existing literature relevant to surface tension dominated flows is the case of a spherical droplet of the denser fluid immersed in a quiescent surrounding medium of the lighter fluid. In the hydrostatic limit of the Navier-Stokes equations, the droplet should stay in equilibrium, with a curvature induced pressure jump across the interface corresponding to Laplace's equilibrium. In practice however, numerically reproducing such a trivial equilibrium condition is not as straightforward, as there exists a slight difference between the initial numerical interface and the exact analytical shape of the sphere, thereby resulting in the generation of the well documented '*'spurious'*' or '*'parasitic'*' currents of varying intensity in the velocity field [38–40]. A lot of progress has been made since in the context of *well-balanced* surface tension formulations, that ensure consistency between the numerical stencils used for the discretization of the pressure gradient and the Heaviside approximation ($n\delta_s$) that projects the the surface force distribution onto the control volumes [20, 41]. A significant contribution to the interpretation of these parasitic currents within the well-balanced

5.1 Static Droplet	42
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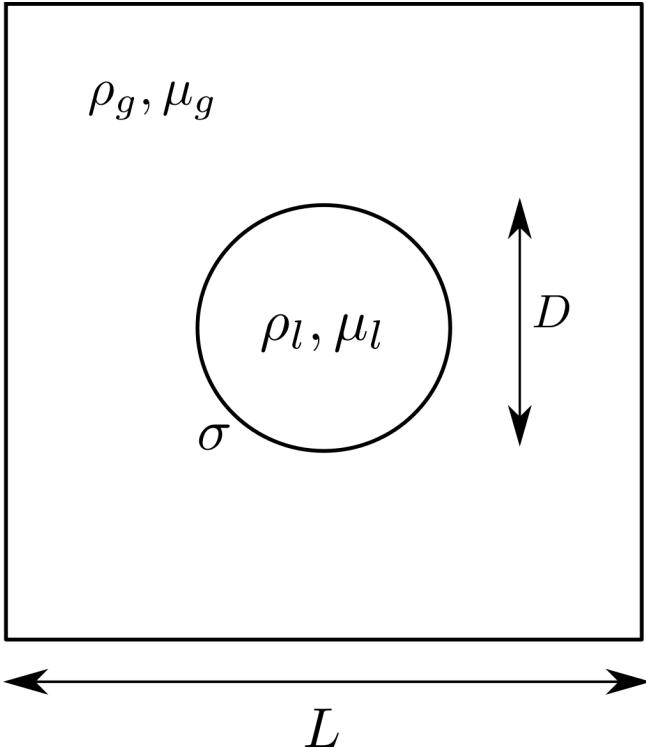
[38]: Lafaurie et al. (1994), 'Modelling merging and fragmentation in multiphase flows with SURFER'

[39]: Harvie et al. (2006), 'An analysis of parasitic current generation in volume of fluid simulations'

[40]: Popinet et al. (1999), 'A front-tracking algorithm for accurate representation of surface tension'

framework was made by Popinet [20] which demonstrated that given sufficient time (of the order of viscous dissipation time-scales), a well-balanced method will relax to the '*numerical*' equilibrium shape through the damping of the 'physically consistent' numerical capillary waves, therefore allowing us to recover the exact (to machine precision) Laplace equilibrium condition.

Setup



The key difference in our implementation of this classic test case from that of Popinet [20] is that we consider the effect of density contrast across the interface separating the fluids. As we have previously discussed, a sharp density jump across the interface may have an amplification effect on the numerical errors incurred as a result of interfacial reconstructions, curvature estimation and various other truncations, thereby rendering the method unstable. We demonstrate that in our framework of mass consistent momentum transport coupled with a well-balanced surface tension discretization, density-ratios as large as 1000 : 1 can be simulated without loss of numerical stability, in conjunction with the ability to recover the exact numerical equilibrium through the dissipation of spurious currents within relevant time-scales¹.

We consider a circular droplet of size D placed at the centre of a square domain of side L . The densities of the heavier and lighter phases are ρ_l and ρ_g respectively, likewise for the viscosities μ_l and μ_g , and σ being the surface tension coefficient (fig. 5.1). The ratio of the droplet size to the box is chosen as $D/L = 0.4$, coupled with a numerical resolution of $D/\Delta x = 16$ (where Δx is the grid size). As for boundary conditions, we use symmetry conditions on all sides of the square domain.

Figure 5.1: Schematic of the static droplet of dense fluid surrounded by a quiescent medium of lighter fluid. A 40×40 grid is employed to spatially discretize the domain.

[20]: Popinet (2009), 'An accurate adaptive solver for surface-tension-driven interfacial flows'

1: The viscous time-scale corresponding to the droplet length-scale is the most commonly used in literature.

The problem incorporates two natural time-scales, the capillary oscillation scale and the viscous dissipation scale, which are defined below :

$$T_\sigma = \left(\frac{\rho_l D^3}{\sigma} \right)^{1/2}, \quad T_\mu = \frac{\rho_l D^2}{\mu_l} \quad (5.1)$$

The ratio of these time-scales give us -

$$\frac{T_\mu}{T_\sigma} = \sqrt{\rho_l \sigma D} / \mu_l = \sqrt{La} \quad (5.2)$$

where La is the Laplace number based upon the heavier fluid. In the present study, we introduce the density-ratio ρ_l/ρ_g as another important parameter. In order to rescale our 'parasitic' velocity field, we define a velocity scale based on capillary oscillations as -

$$U_\sigma = \sqrt{\sigma / \rho_l D} \quad (5.3)$$

Additionally, the time-step in our numerical simulation must be smaller than the oscillation period corresponding to the grid wavenumber (fastest capillary wave with a time period $\sim (\rho_l \Delta x^3 / \sigma)^{1/2}$) as a stability criterion², as our surface tension model is explicit in time. For the scope of the present study, we shall not consider any viscosity contrast between the two fluids while varying the density-ratio, therefore $\mu_l/\mu_g = 1$ for all the cases under study.

2: Similar criteria are defined on the basis of the viscous and advection operators as well, with the smallest amongst the three selecting the numerical time-step

Decay of Spurious Currents

In figures 5.2 to 5.4, we illustrate the decay of the root-mean-square of the spurious currents as a function of time, in the case of four different density-ratios, with three different Laplace numbers for each ratio. The first figure (5.2) refers to simulations carried out without consistency between the momentum-mass transport (**M1**), the second (5.3) corresponds to that of the consistent but not conservative method (**M2**), and final one (5.4) refers to that of the consistent and conservative method (**M3**). The time is rescaled by the viscous dissipation scale, and the spurious currents by the capillary velocity scale. We have two main observations, the rapid decay of the rescaled spurious currents for all combinations of density-ratios and Laplace numbers within approximately $0.2T_\mu$, and the slower re-growth of the currents in question for combinations of non-unity density-ratios and large Laplace numbers, in all simulations except those carried out with **M3**. With method **M3**, the decayed currents keep hovering around levels of machine precision for remainder of time. Although there is a re-growth of the currents using the consistent method (**M2**) after $0.2T_\mu$, the behavior is not quite alarming as the rate of this re-growth is quite low. Therefore, out of all the methods tested, the consistent and conservative method (**M3**) does seem to demonstrate the

desired performance, especially when it comes to combinations of large density contrasts coupled with large Laplace numbers.

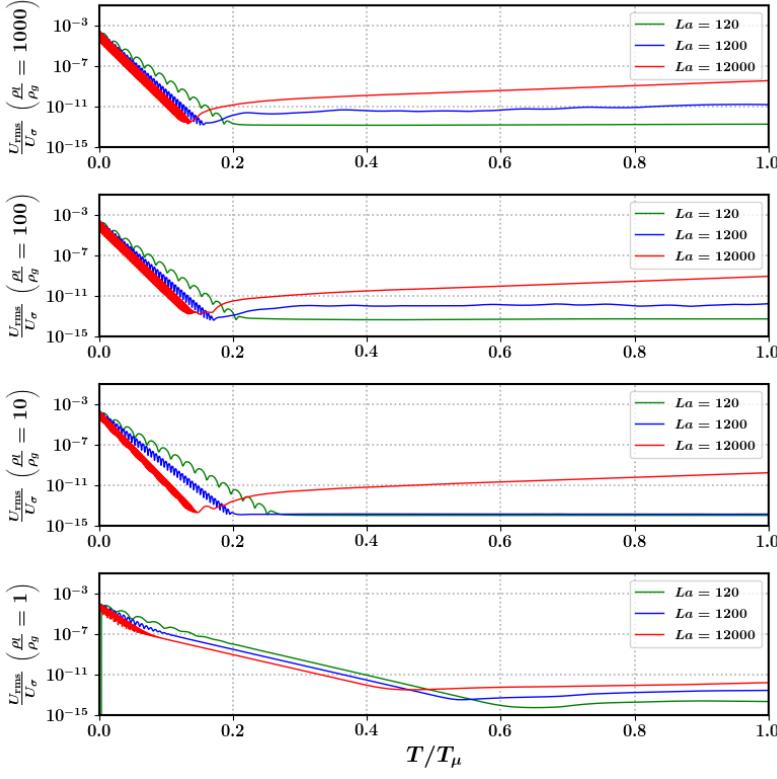


Figure 5.2: M1 Decay of normalized spurious currents as a function of viscous dissipation time-scales for different density ratios and Laplace numbers. The currents seem to initially decay quickly for all higher density-ratios, and relax to the numerical equilibrium curvature even within $0.2 \cdot T_\mu$. For combinations of large ρ_l/ρ_g and large La , the spurious currents seem to grow back to an order of magnitude (10^{-8}) which is quite far from that of machine precision (10^{-14}).

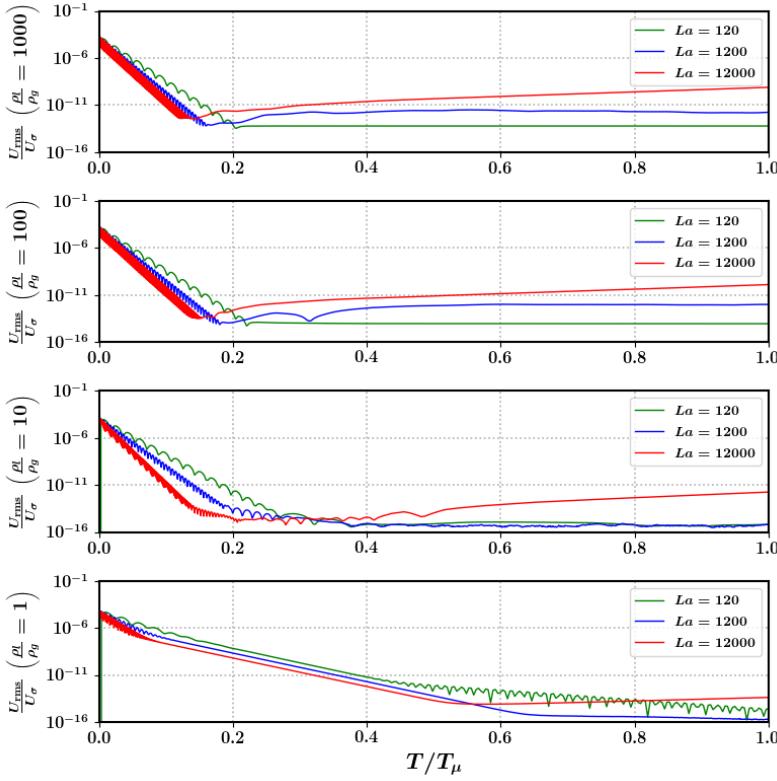


Figure 5.3: M2 Decay of normalized spurious currents as a function of viscous dissipation time-scales for different density ratios and Laplace numbers. The currents seem to initially decay quickly for all higher density-ratios, and relax to the numerical equilibrium curvature even within $0.2 \cdot T_\mu$. For combinations of large ρ_l/ρ_g and large La , the spurious currents seem to grow back to an order of magnitude (10^{-8}) which is quite far from that of machine precision (10^{-14}). No considerable improvement is observed with respect to M1.

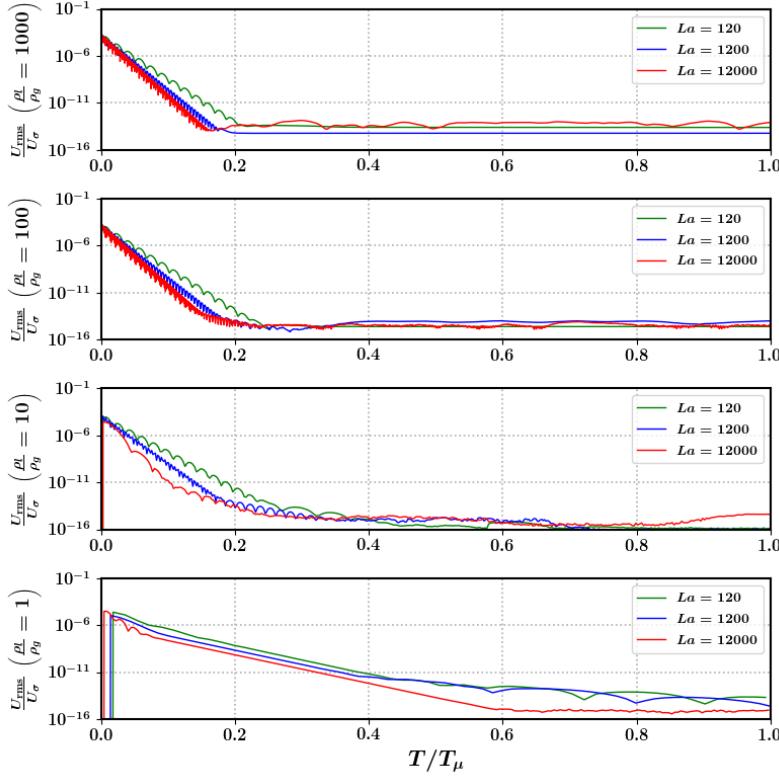


Figure 5.4: M3 Decay of normalized spurious currents as a function of viscous dissipation time-scales for different density-ratios and Laplace numbers. The currents seem to decay very quickly in the case of higher density-ratios, and relax to the numerical equilibrium curvature even within $0.2 \cdot T_\mu$. For all combinations of ρ_l/ρ_g and La numbers, the decayed spurious currents are not observed to grow back as in the cases of **M1** and **M2**, and hover around values close to machine precision (10^{-14}).

Spatial Convergence

Once the solution relaxes to a numerical equilibrium curvature (spurious currents are approximately at the order of machine precision), there still exists a difference between the numerical curvature and the exact analytical curvature corresponding to the spherical (circular) shape. We use the definitions of the shape errors as introduced in the seminal work of Popinet [20] to assess the convergence of our class of methods to the exact (analytical) curvature as we increase spatial resolution. The norms are defined as follows :

$$L_2 = \sqrt{\frac{\sum_i (C_i - C_i^{\text{exact}})^2}{\sum_i}} , \quad L_\infty = \max_i (|C_i - C_i^{\text{exact}}|) \quad (5.4)$$

where C_i is the volume fraction of a cell after the solution has relaxed to the numerical equilibrium curvature, and C_i^{exact} is the volume fraction corresponding to the exact circular shape which was initialized at the start of the simulation.

Fig. 5.5 demonstrates the behavior of the shape errors defined in eqn. 5.4 for the case of the most stringent parameter combination ($\rho_l/\rho_g = 1000$, $La = 12000$) as a function of the droplet resolution. As one can clearly observe, all the methods tested display a roughly second-order convergence in space for both the error norms. In terms of the L_2 norm, the consistent and conservative method (**M3**) does indeed achieve smaller errors as compared to both **M1** and **M2** for all spatial resolutions. As a

minor remark, there is not much to discern in terms of shape error when it comes to comparing the performances of the consistent (**M2**) method with the non-consistent one (**M1**).

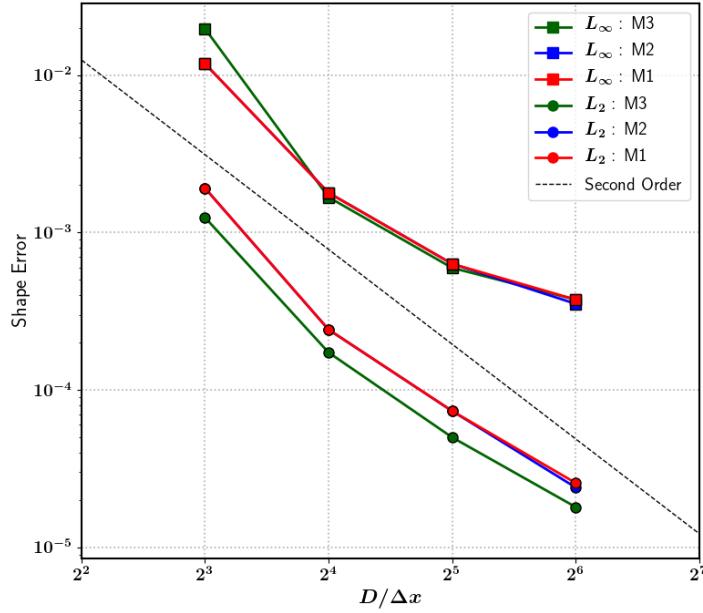


Figure 5.5: Second-order spatial convergence for the spurious current error norms corresponding to the most stringent parameter combination ($\rho_l/\rho_g = 1000$, $La = 12000$). Both of the norms (L_∞ and L_2) seem to demonstrate a roughly second order rate of spatial convergence with each of the methods tested. However, **M3** has a marginally lower L_2 error compared to both **M1** and **M2** for all resolutions tested. There is negligible difference observed in the shape errors between **M1** and **M2** in both of the norm definitions.

5.2 Moving Droplet

An incisive numerical setup that enables us to evaluate the accuracy of the coupling between interfacial propagation and surface tension discretization was first proposed by Popinet [20], and subsequently employed in the comparative study of Abadie et al. [42]. The manner in which this test differs from that of the static droplet is the addition of a uniform background velocity field, therefore serving as a better representation of droplets in complex surface tension dominated flows where they might be advected by the mean flow. In terms of the Laplace equilibrium, the hydrostatic solution is still valid in the frame of reference of the moving droplet. The point at which the solution in the moving reference frame diverges from that of the static droplet (5.1) is through the continuous injection of noise at the scale of the grid size. This ‘numerical’ noise emanates from the perturbations to the curvature estimates, which are in turn induced by the interfacial reconstructions carried out to propagate the interface (temporal integration). These fluctuating errors act as source terms for the momentum, thereby transforming the problem into that of viscous dissipation in the presence of continuous forcing (in the reference frame of the moving drop).

[42]: Abadie et al. (2015), ‘On the combined effects of surface tension force calculation and interface advection on spurious currents within Volume of Fluid and Level Set frameworks’

Setup

In the present study, we evaluate our class of methods using the advection of a droplet in a spatially periodic domain using an identical setup as [20], but with the important difference of including sharp density jumps across the interface as well as using lower spatial resolutions.

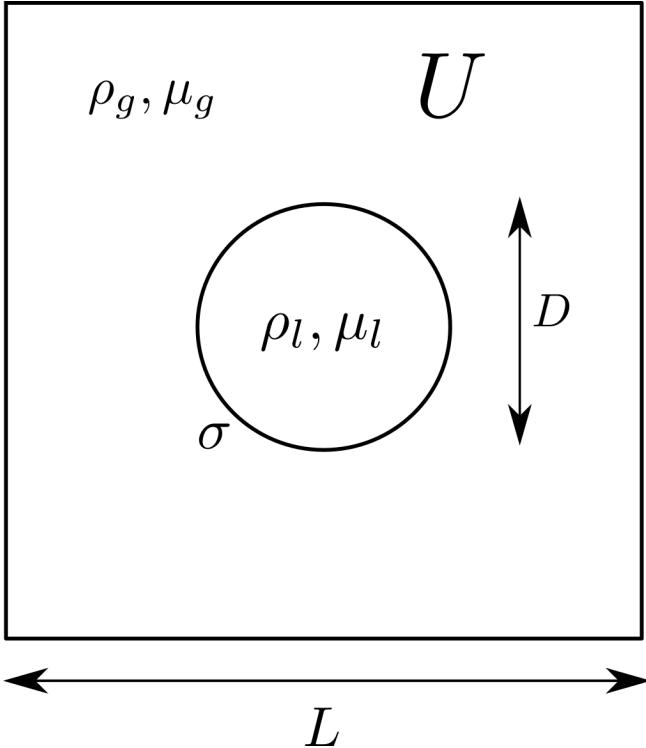


Figure 5.6: Schematic of the droplet of dense fluid advected in a surrounding medium of lighter fluid. A 50×50 grid is employed to spatially discretize the domain, which is spatially periodic in the direction of droplet advection.

As previously discussed (5.1), high density-ratios tend to amplify the fluctuations induced by the myriad numerical approximations (interface reconstruction, curvature estimation etc) involved in the algorithm.

We consider a circular droplet of diameter D placed at the centre of a square domain of side L . The densities of the heavier and lighter phases are ρ_l and ρ_g respectively, likewise for the viscosities μ_l and μ_g , and σ being the surface tension coefficient (fig. 5.6). A uniform velocity field U is initialized on the entire domain (only a horizontal component). The ratio of the droplet size to the box is $D/L = 0.4$, with $D/\Delta x = 20$ (Δx being the grid size.³). As for boundary conditions, we use symmetry conditions on the top and bottom sides, and periodic boundary conditions on the horizontal direction (along which advection by U takes place). We characterize by problem by introducing the following adimensional parameters (based on the heavier fluid) :

$$La = \frac{\rho_l \sigma D}{\mu_l^2} , \quad We = \frac{\rho_l U^2 D}{\sigma} \quad (5.5)$$

In addition to the capillary and viscous time-scales for the static case (eqns. 5.1), we have an additional scale defined as :

$$T_u = D/U \quad (5.6)$$

which is the time-scale of advection. In our subsequent analysis, we shall use T_u and U as the time and velocity scales, repectively.

3: In Popinet [20], a resolution of $D/\Delta x = 25.6$ corresponding to a grid of 64×64 is used

Evolution of Spurious Currents

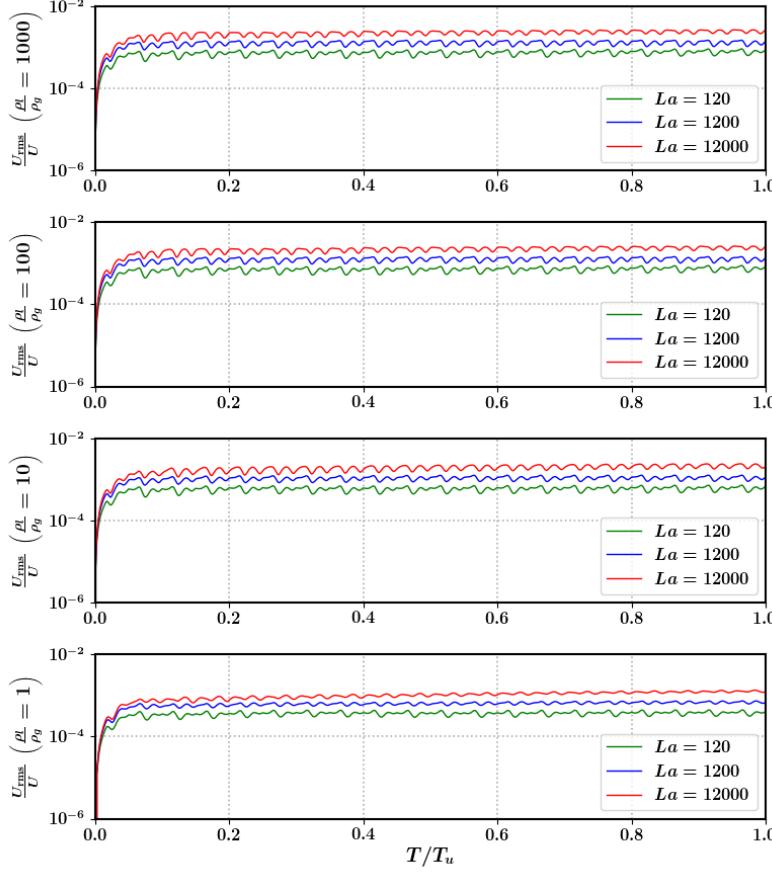


Figure 5.7: M1 Time evolution of normalized spurious currents as a function of advection time-scales (T_u) for different combinations of density-ratio and Laplace numbers. The currents seem to hover around 10^{-3} , with a larger Laplace number corresponding to a higher error for all density-ratios. $We = 0.4$ for all the cases presented.

Figures 5.7 to 5.9 depict the evolution of the root-mean-square (RMS) error of the velocity field in the moving frame of reference, as a function of different Laplace numbers, spanning over density-ratios separated by orders of magnitude. The first figure (5.7) refers to simulations carried out without consistency between the momentum-mass transport (**M1**), the second (5.8) corresponds to that of the consistent but not conservative method (**M2**), and final one (5.9) refers to that of the consistent and conservative method (**M3**). We again have a couple of important observations, the first being that spurious currents do not decay to machine precision as in static droplet case for all of the combinations and methods tested, instead they oscillate around a mean value of the order of 0.1 – 0.01% of the constant field U . The second observation is regarding the significantly smaller error (almost by one order of magnitude) in the case of the consistent and conservative method (**M3**) when compared to that of **M1** and **M2**. As a minor remark, in case of large Laplace numbers, the **M3** method displays a slight upward trend in the error evolution, which is not the case in either **M1** or **M2**. This is not too worrisome as the growth is over a time-scale much larger than T_u , with the oscillations corresponding to a time-scale of the order $U / \Delta x$. All of the plots in figures 5.7 to 5.9 correspond to $We = 0.4$, alongside an additional simplification of equal viscosities across the interface i.e $\mu_l / \mu_g = 1$.

As evidenced by the persistence of these spurious currents due to the

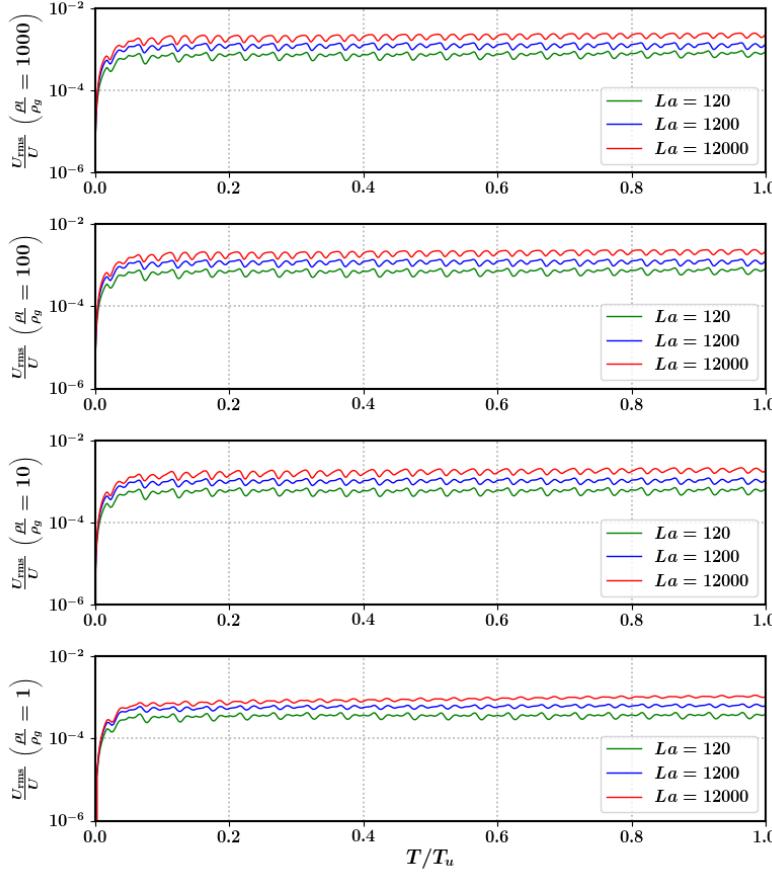


Figure 5.8: M2 Time evolution of normalized spurious currents as a function of advection time-scales (T_u) for different combinations of density-ratio and Laplace numbers. There seems to be no appreciable difference from the evolution seen in the case of M1 (fig. 5.7). The currents seem to hover around 10^{-3} , with a larger Laplace number corresponding to a higher error for all density-ratios. $We = 0.4$ for all the cases presented.

addition of grid-level noise emanating from interfacial reconstructions, further advancements should be made with respect to the combined performance of the interfacial transport, curvature computation and the surface tension model. Nonetheless, all the methods tested do seem to be quite numerically stable when dealing with the high density-ratios, and are not subject to rapid uncontrollable amplifications of the interfacial perturbations even for high Laplace numbers.

Spatial Convergence

In order to evaluate the performance of our class of methods at different resolutions, we define the errors as the maximum values of the norms L_∞ and L_2 of the rescaled field U_{rms}/U over time (5 times T_u). In fig. 5.10, we show the scaling of the error as a function of spatial resolution for the most stringent case of $\rho_l/\rho_g = 1000$, $La = 12000$, for each of our different methods. As similarly observed in section 5.1, in terms of both L_∞ and L_2 norms, there is no appreciable difference in the behaviors of M1 and M2. For M3, we do observe significantly lower maximum errors compared to other two methods, but at a cost of slightly less than first-order convergence. The overall convergence behavior of the class of methods we have tested seem to be consistent with earlier studies of Popinet [20] and others⁴.

4: In existing literature, convergence rates have only been studied in case of equal density fluids across the interface

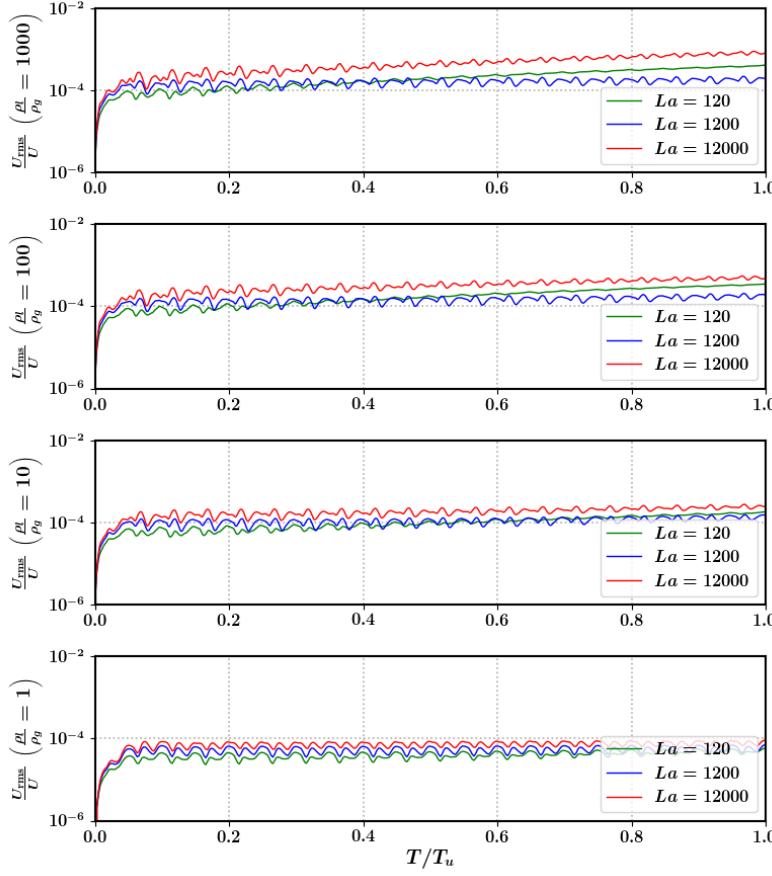


Figure 5.9: M3 Time evolution of normalized spurious currents as a function of advection time-scales (T_u) for different combinations of density-ratio and Laplace numbers. In terms of the errors observed in **M1** and **M2**, we observe a decrease of roughly one order of magnitude. Although an upward trend is observed for large Laplace numbers, the growth rate is quite low. The currents seem to hover slightly above 10^{-4} , with larger Laplace numbers corresponding to larger errors for all density-ratios. $We = 0.4$ for all the cases presented.

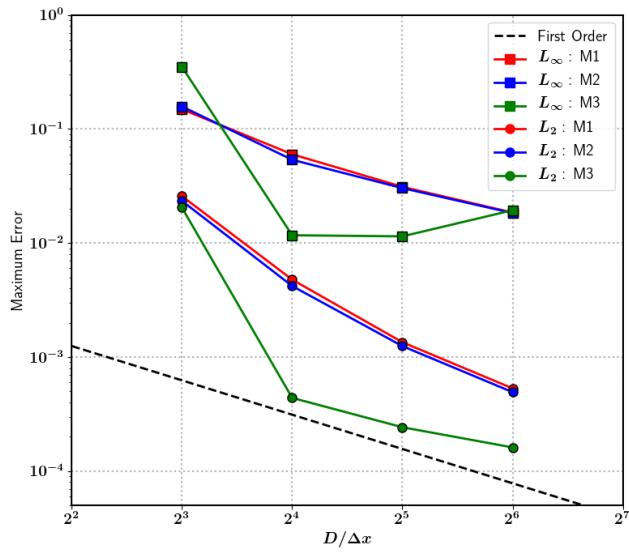


Figure 5.10: First-order (approximately) spatial convergence of the maximum of the spurious current error norms in the frame of reference of the moving droplet, for the most stringent parameter combination ($\rho_l/\rho_g = 1000$, $La = 12000$, $We = 0.4$). Methods **M1** and **M2** display similar convergence properties, whereas **M3** leads to significantly lower errors even though it doesn't quite follow the first-order convergence rate.

Error Dependence : Laplace & Weber numbers

As the final point of inquiry into the performance of our class of methods, figures 5.11 and 5.12 demonstrate the influence of the Laplace and Weber numbers on the behavior of the maximum error norm, carried out for the largest density-ratio ($\rho_l/\rho_g = 1000$). We only present the results obtained using the consistent and conservative method (**M3**), for a resolution corresponding to $D/\Delta x = 25.6$. As we can observe, the error (both L_∞

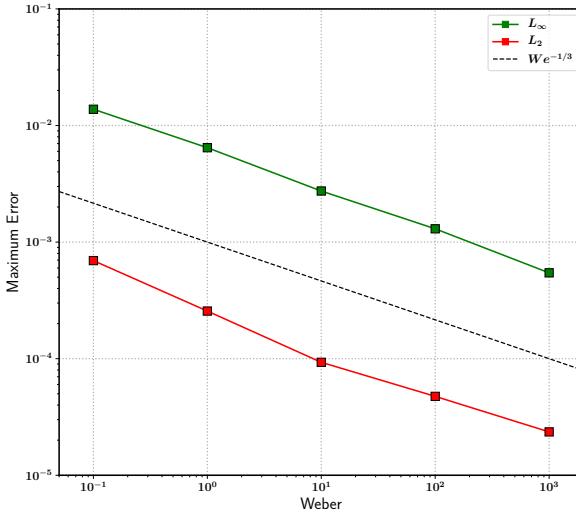


Figure 5.11: Scaling of the maximum error norm as a function of Weber ($La = 12000$, $\rho_l/\rho_g = 1000$).

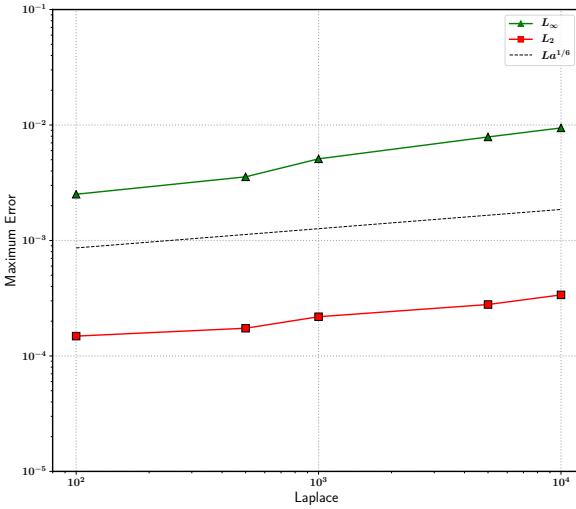


Figure 5.12: Scaling of the maximum error norm as a function of Laplace ($We = 0.4$, $\rho_l/\rho_g = 1000$).

and L_2) scales as $We^{-1/3}$ over 4 orders of magnitude, which is different from the $We^{-1/2}$ scaling observed by Popinet [20]⁵. In terms of Laplace numbers, the errors scale as $La^{1/6}$ over two orders of magnitude, which is the same as that observed in [20] (for equal densities).

5: Although Popinet [20] had equal densities ($\rho_l/\rho_g = 1$)

5.3 Capillary Wave

One of fundamental features of immiscible multiphase flows involving interfaces are the presence and propagation of capillary waves. Therefore, a robust and accurate numerical method should not only be able to adequately resolve, but also accurately emulate the spatio-temporal evolution of such surface tension induced oscillations. A brief outline on the state-of-the-art numerical implementations of capillary waves (and surface tension models in general) existing in current literature is provided by Popinet in the comprehensive review [6].

[6]: Popinet (2018), ‘Numerical models of surface tension’

Setup

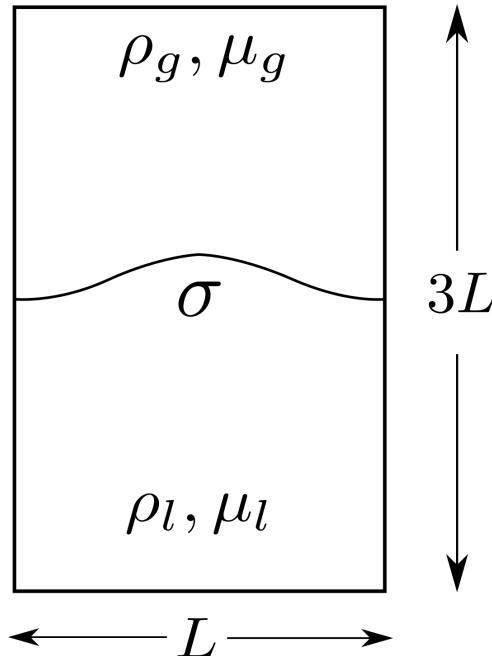


Figure 5.13: Schematic of the initially perturbed planar interface separating two immiscible fluids of different densities and viscosities. A spatial resolution of 32×96 is used for spatial discretization (compared to 64×192 in Popinet [20]), with the width of the box corresponding to the size of the perturbed wavelength.

In the present study, we evaluate the accuracy of our class of methods by comparing with an analytical solution of damped capillary oscillations. Generally, analytical solutions exist only for cases corresponding to extremely small initial perturbations, that too either in the inviscid limit (Lamb [43]) or the asymptotic limit of vanishing viscosity (Prosperetti [44, 45]). For our purposes, we use the configuration of the viscosity-damped capillary oscillations of a planar interface, as was first implemented and popularized by Popinet & Zaleski [40].

We consider a rectangular domain of dimensions $L \times 3L$, where L corresponds to the wavelength of our initial perturbation. The densities of the heavier and lighter phases are ρ_l and ρ_g respectively, likewise for the viscosities μ_l and μ_g , and σ being the surface tension coefficient (fig. 5.13). An intial perturbation amplitude of $L/100$ is used, coupled with a numerical resolution given by $L/\Delta x = 32$ (Δx being the grid size). Symmetry conditions are applied on the top and bottom sides, with periodic conditions along the horizontal direction. We use the following adimensional parameters to characterize our problem :

$$T_0 = T\omega_0 \quad , \quad La = \frac{\rho_l \sigma L}{\mu_l^2} \quad (5.7)$$

where La is the Laplace number based on the heavier fluid, and ω_0 is defined using the dispersion relation used in Popinet [20] given as :

$$\omega_0^2 = \frac{\sigma k^3}{2\rho_l} \quad , \quad \text{where } k = \frac{2\pi}{L} \quad (5.8)$$

[43]: Lamb (1993), *Hydrodynamics*

[44]: Prosperetti (1980), ‘Free oscillations of drops and bubbles: the initial-value problem’

[45]: Prosperetti (1981), ‘Motion of two superposed viscous fluids’

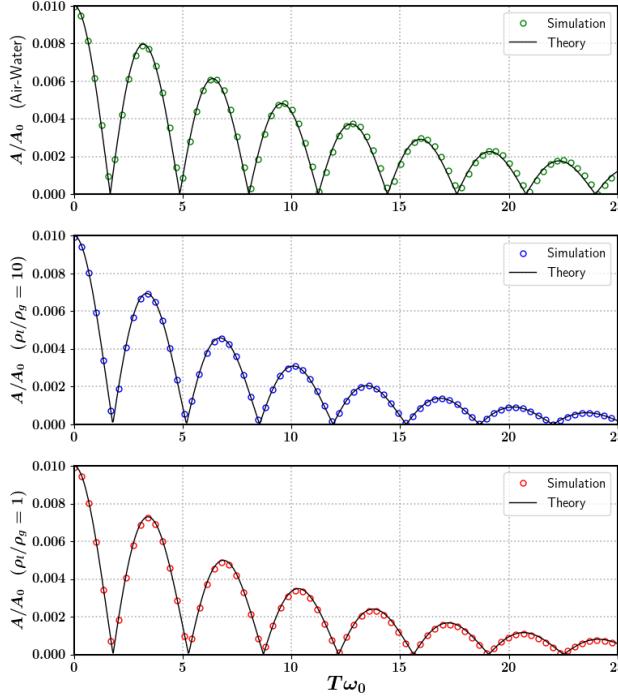
The dispersion relation is obtained via linear stability analysis at the inviscid limit [43]. In order to evaluate the influence of density-ratio on the performance of our class of methods, we use three different numerical setups keeping the same Laplace number ($La = 3000$) as follows :

- $\rho_l/\rho_g = 1, \mu_l/\mu_g = 1$ (Popinet [20])
- $\rho_l/\rho_g = 10, \mu_l/\mu_g = 1$
- $\rho_l/\rho_g = 1000.0/1.2, \mu_l/\mu_g = 1.003 \cdot 10^{-3}/1.8 \cdot 10^{-5}$ (Air-Water)

The final setup corresponds to that of an air-water interface (physical properties corresponding to 20° Celsius), which is the most stringent due to the significant density and viscosity jumps.

Comparison with Prosperetti Solution

The theoretical solution to this configuration corresponds to the closed-form expressions of the planar interface shape evolution established by Prosperetti [44, 45], which takes into account the finite time-scales at which the vorticity (generated due to interface oscillations) diffuses into the bulk medium. These closed-form expressions are subsequently integrated using a fourth-order Runge-Kutta time integrator (details of which not described here), and used to assess the accuracy of the results obtained by our class of numerical methods.



[43]: Lamb (1993), *Hydrodynamics*

As we can in figures 5.14 to 5.16, solutions from our class of numerical methods (circles) are compared to that of the theoretical (Prosperetti) solution (black curves), where the amplitude is normalized by the initial value (A_0) and the time rescaled by T_0 . The first figure (5.14) refers to simulations carried out by the non-consistent method, the second (5.15) corresponds to that of the consistent method, and the final one (5.16) refers to that of the consistent and conservative method. We observe that

Figure 5.14: M1 Time evolution of the amplitude of the planar interface undergoing damped capillary oscillations, comparing the solution obtained by our numerical method with the closed-form Prosperetti solution. More or less good agreement with theory is observed for all the density-ratios tested.

there is hardly any appreciable qualitative difference between the results obtained via the different methods **M1**, **M2** and **M3**, although **M3** does seem to perform marginally better when it comes to the most stringent case (air-water configuration). Surprisingly, even the non-consistent method (**M1**) does not seem to show any un-physical interfacial deformations for all the density-ratios tested, and that it is difficult to distinguish between the different methods for the lower density-ratios.

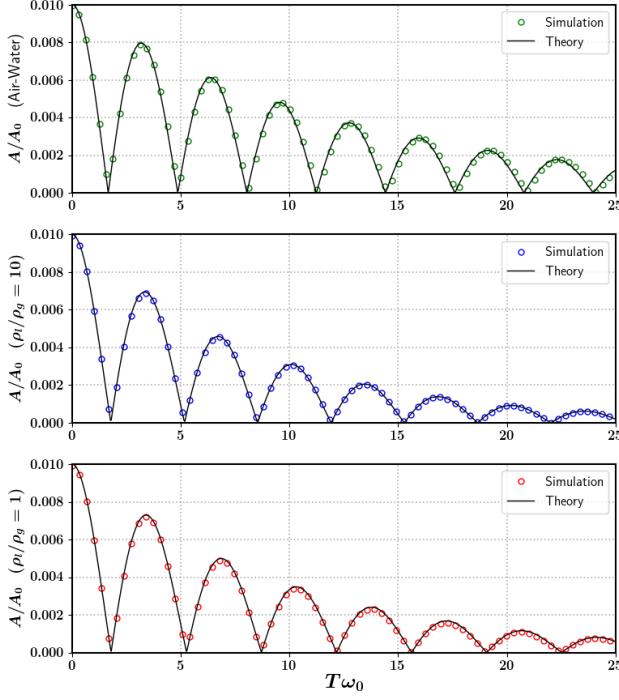


Figure 5.15: **M2** Time evolution of the amplitude of the planar interface undergoing damped capillary oscillations, comparing the solution obtained by our numerical method with the closed-form Prosperetti solution. Behavior is quite similar to **M1**, with good agreement with theory for all the density-ratios tested.

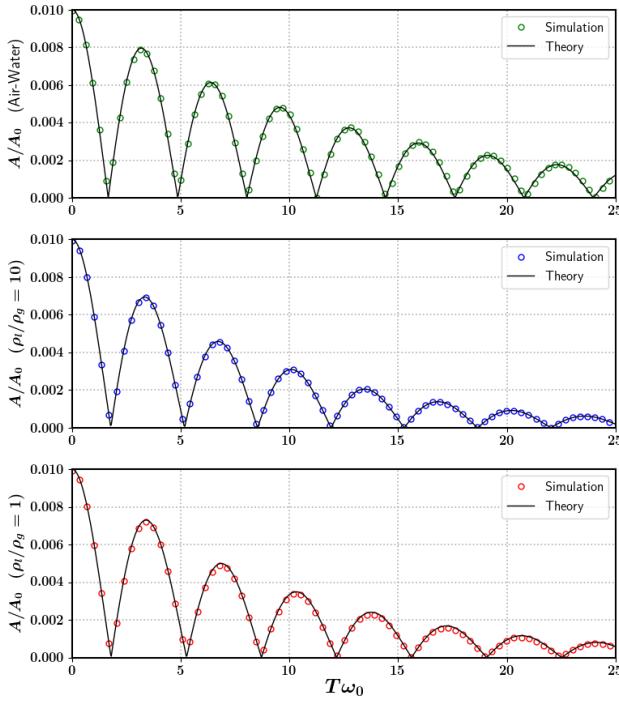


Figure 5.16: **M3** Time evolution of the amplitude of the planar interface undergoing damped capillary oscillations, comparing the solution obtained by our numerical method with the closed-form Prosperetti solution. Slightly better agreement with theory when comparing to **M1** and **M2**, for all density-ratios tested.

Spatial Convergence

The next step in our evaluation would be to quantify the accuracy of our numerical results to the Prosperetti solution using an integral (in time) error norm, the same as defined in [20] :

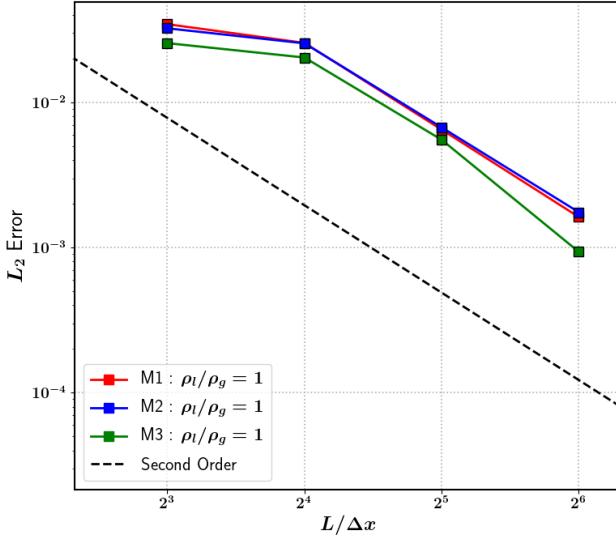


Figure 5.17: Comparison of spatial convergence for the case of $\rho_l/\rho_g = 1$, $La = 3000$, for our class of methods. There is no viscosity jump across the interface. All methods seem to demonstrate approximately second-order convergence. There seems to be no appreciable difference in the behavior of **M1** and **M2**, with **M3** displaying marginally lower errors compared to the others.

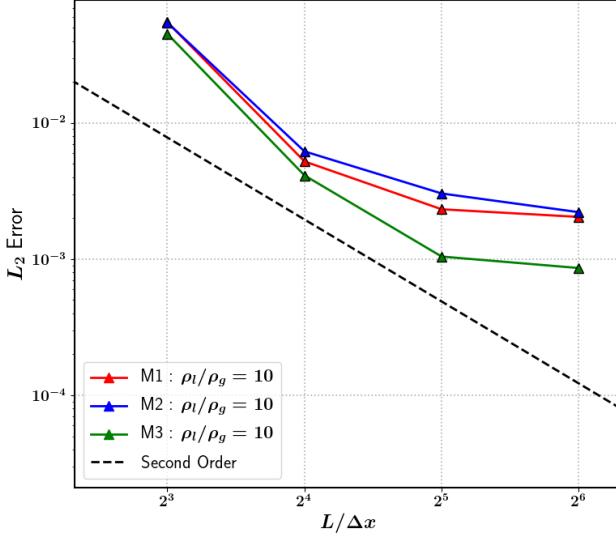


Figure 5.18: Comparison of spatial convergence for the case of $\rho_l/\rho_g = 10$, $La = 3000$, for our class of methods. Again, there is no viscosity jump across the interface. All methods seem to demonstrate approximately second-order convergence upto $L/\Delta x = 32$, beyond which there is a slight saturation in the rate of convergence. Qualitatively, **M1** and **M2** demonstrate similar behavior, with **M3** delivering slightly lower errors. In case of **M3**, the errors are marginally lower compared to **M1** and **M2** for higher resolutions.

$$L_2 = \frac{1}{L} \sqrt{\frac{\omega_0}{25} \int_{t=0}^T (h - h_{exact})^2} \quad (5.9)$$

where h is the maximum interface height obtained using our numerical simulations, and h_{exact} being the maximum height obtained via time integration of the Prosperetti solution. In figures 5.17 to 5.19 we demonstrate the rate of spatial convergence of the L_2 error norms for different density-ratios, simultaneously comparing the behavior of the different methods **M1**, **M2** and **M3** at each density-ratio. In all the results presented, we maintain $La = 3000$ for all density-ratios, spatial resolutions

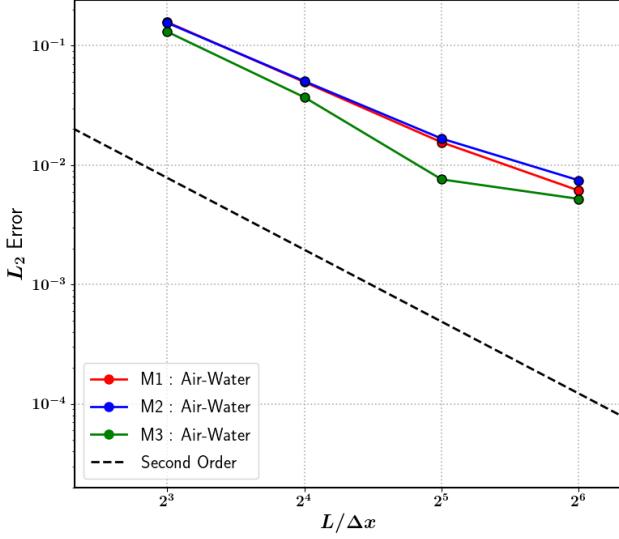


Figure 5.19: Comparison of spatial convergence for the Air-Water case corresponding to $\rho_l/\rho_g = 1000.0/1.2$, $\mu_l/\mu_g = 1.003 \cdot 10^{-3}/1.8 \cdot 10^{-5}$, $La = 3000$, for our class of methods. All methods seem to demonstrate approximately second-order convergence. No appreciable difference is observed between **M1** and **M2**, with **M3** delivering slightly lower errors although there is some saturation in the convergence rate at higher resolutions.

and methods tested.

In figure 5.17 we observe roughly second-order spatial convergence when it comes to equal densities across the interface, with **M1** and **M2** displaying nearly identical behavior, whereas **M3** does marginally better with lower errors for all resolutions. When it comes to $\rho_l/\rho_g = 10$ in figure 5.18, we observe a saturation in the initial second-order convergence rate irrespective of whichever method is used, however **M3** performs slightly better in terms of error when compared **M1** and **M2**. Finally, figure 5.19 demonstrates the roughly second-order convergence of all three methods when it comes to the air-water configuration, again, with **M3** performing marginally better with lower errors. Not surprisingly, the largest errors arise for the air-water configuration errors across all methods.

PHYSICS OF FRAGMENTATION

6

Ligament Mediated Paradigm

6.1 Mechanism of Drop Formation

Disintegration of Jets & Shear Layers Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Expansion of Sheets Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Effervescent Atomization Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Drop Impacts Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

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6.2 Theories of Fragmentation

Cascade Mechanism : Log-Normal Distribution Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Corrugation-Coalescence Mechanism : Gamma Distribution Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Droplet Generation in Corrugated Ligaments

7

Ligaments constitute the penultimate stage in the complex sequence of capillary-driven topological changes that are typical of liquid fragmentation processes, finally resulting in the generation of polydisperse collections of drops. In the context of the present body of work, we shall only concern ourselves with the dynamics of Newtonian ligaments, which are well described by the Navier-Stokes equations at the incompressible and isothermal limits. The rearrangement of the liquid volumes that constitute the ligaments play a key role in determining the size of the droplets that emerge immediately after the disintegration of the thread-like structure (Fig. 7.1).

The dynamics of these rearrangements prior to breakup are governed by non-linear interactions between several physical mechanisms such as the growth and propagation of capillary waves along the ligament surface, remnants of the internal flow, stretching induced either by the surrounding gas flow or by acceleration of the liquid into the surrounding medium itself, not to mention the dissipative effects of viscosity. Although we present a convoluted picture of ligament dynamics prior to breakup, it is ultimately the capillary force that drives the eventual topology change from the thread-like structure to that of the drop. The primary role of the both the inertial and viscous forces is to oppose or dampen the destabilizing effects of the capillarity induced deformations. An additional mechanism to consider is the merger or coalescence of the newly created droplets (post-breakup) along the axis of the former ligament structure, or with droplets originating from other sources in the near vicinity. The generation of drops whose diameters are significantly larger than the width of original ligament are predominantly driven by the aforementioned coalescences. Therefore, considering the combined effects of the above mechanisms, we expect a significant departure of the resulting drop size distribution from that predicted by the classical analysis of the Rayleigh-Plateau instability [47, 48].

7.1 Coalescence Cascade

Linear theory based on the Rayleigh breakup of infinitely long liquid cylinders in a quiescent medium predicts the disintegration of the thread along regular intervals, the length of which is governed by the fastest growing spatial frequency. The drops generated according to this model would be uniform in size, in sharp contrast to the significant variances in the size distributions observed in reality. Even in the simpler case of decaying liquid jets, non-linearities near the breakup zone kick into effect beyond the initial exponential growth phase predicted by linear theory, eventually resulting in the jet breaking up into “main” drops and significantly smaller “satellite” droplets¹. Thus, simply taking into account the non-linear effects driving the breakup would lead to

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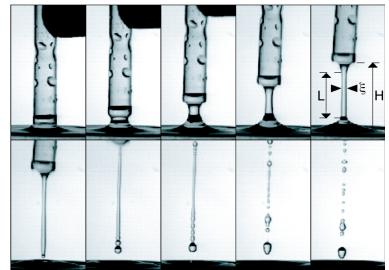


Figure 7.1: Fragmentation of stretched liquid (Newtonian) ligaments formed immediately after retraction of a capillary tube. Image reproduced from Marmottant & Villermoux [46]. The complex rearrangement of the liquid volumes inside the ligament plays a key role in its subsequent disintegration into droplet of various sizes.

1: Refer to the high quality photographs in the work of Rutland and Jameson [49], where they demonstrate the formation of “satellite” droplets that manifest due to the non-linear effects driving the jet breakup.

a bimodal distribution of droplet size, but this explanation still fails to account for the broad distribution of sizes observed in the outcomes of the majority of natural [50] and industrial [51] processes.

As we have seen in the previous chapter, there are several hypotheses in existing literature [52] that attempt to model the underlying physical mechanisms that are responsible for the selection of droplet size. A model first proposed by Villermaux and coworkers [53, 54] asserts that the variance in the droplet sizes is strongly correlated to the initially corrugated shape of the ligament, from which the drops originate. In this model, the corrugated ligament is represented as a collection of ‘blobs’ (see Fig. 7.2), with the continuous interaction between such blobs throughout the destabilization phase accounting for the rearrangement and concomitant aggregation of the liquid volumes prior to breakup. The key parameter concerning the predictions of this model is n , which characterizes the corrugations in the initial geometrical shape of the ligament, defined as

$$n \equiv \frac{1}{(\langle d^2 \rangle - \langle d \rangle^2) / \langle d \rangle^2}, \quad (7.1)$$

where the quantities in the brackets $\langle \rangle$ represent the mean and the diameters d_i correspond to that of the blobs as shown in Fig. 7.2. These studies essentially demonstrate that the degree of polydispersity in the drop sizes can be simply explained by examining the degree of “smoothness” in the initial geometry of the ligaments, with the standard deviation or distribution width of the size of the emerging drops scaling as $1/\sqrt{n}$. As a corollary to this prediction, a broader distribution of drop sizes arise out of the disintegration of strongly corrugated (rough) ligaments, whereas smoother ligaments with uniform thickness lead to a narrower (monodisperse) distributions.

Over the last two decades, a handful of studies have been conducted with the aim of carrying out detailed observations surrounding the aforementioned “coalescence cascade”, whereby the drops constitutive of the ligament tend to coalesce and form larger drops as and when they detach from the initial thread-like structure. Most notable amongst those studies is the one by Marmottant and Villermaux [46], wherein they illustrate the successive stages of the disintegration of liquid ligaments formed when capillary tubes are rapidly retracted from the surface of a liquid pool (refer to Fig. 7.1). Another set of observations were presented by Lhuissier and Villermaux [60], where the disintegration phase sets in starting from a transient configuration of the ligaments arranged in a spider-web like network (Fig. 7.3). A more recent experiment is that of Keshavarz et al. [59], which is inspired by the capillary tube retractions of [46] but directed towards the behaviour of non-Newtonian fluids. The fundamental limitation that is common to experiments cited above is the inability to precisely control the initial conditions. In other words, generating ligaments conforming ‘exactly’ to a specified geometrical shape is practically (almost) impossible due to the inherent difficulties associated with the control of free-surface flows. In the absence of such precise control and reproducibility of the initial ligament corrugations, one has to resort to a posteriori correlations between the width of the final drop size

[52]: Villermaux (2007), ‘Fragmentation’

[53]: Villermaux et al. (2004), ‘Ligament-mediated spray formation’

[54]: Marmottant et al. (2004), ‘On spray formation’

The corrugation-coalescence mechanism has been popularized in several studies such as [46, 52, 55–57], and more recently in [58, 59].



Figure 7.2: Representation of the liquid volumes in an isolated ligament as ‘blobs’ of sizes d matching the corresponding the local thicknesses, just before the destabilization into droplets. Image reproduced from Villermaux [52].

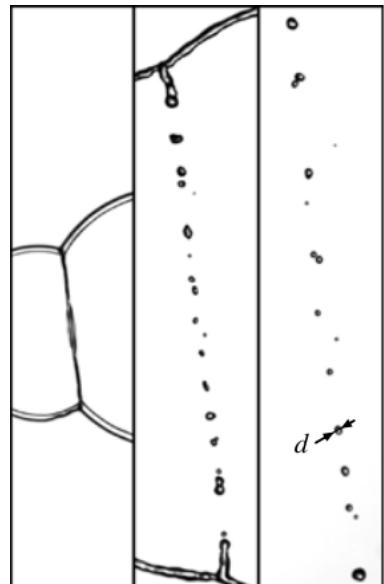


Figure 7.3: Successive stages in the breakup of a ligament into drops. The system shown here is that of a perforated liquid sheet, where the growth of such perforations due to capillary retraction of the liquid rims lead to the formation of networks of connected ligaments. Image reproduced from Lhuissier and Villermaux [60].

distributions and qualitative descriptions of the initial surface profiles. A central theme of the current chapter is concerning the design and conception of ‘numerical’ experiments that lend themselves to accurate and repeatable specifications of the initial conditions of the ligaments in question. An additional advantage offered by our high-fidelity numerical approach is the access to a much wider range (compared to physical experiments) within the space of all control parameters that influence the dispersion in the drop size distributions, not to mention the higher levels of temporal resolution on offer that enable better tracking of the non-linear dynamics near pinch-off². The combination of these two features enables us to quantitatively map the influence that the degree of smoothness of the initial ligament has on the ensuing liquid rearrangements, as well as the coalescence dynamics following the ligament.

7.2 Breakup Regimes

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7.3 Numerical Setup

Our numerical experiments entail direct numerical simulations of the two-phase Navier-Stokes equations, employing the one-fluid model which solves only a single set of governing equations throughout the

2: The characteristic time-scale of the flow near the vicinity of the breakup is given by $t_\sigma \sim (\rho r^3/\sigma)^{1/2}$, thus leading to faster flows and contraction of the time-scales as the local thickness (r) decreases to zero. In our numerical methods, we can adaptively select the time interval over which the integration of the governing equations are carried out, to accommodate such non-linearly accelerating flows.

whole domain, where the domains are composed of regions of variable density and viscosity. In order to reproduce the free-surface dynamics, a Volume-of-Fluid (VOF) approach is used to capture the interface, the explicit location of which marks the separation between the two fluids.

A more detailed evaluation of the comparative advantages of different interfacial tracking approaches (e.g. VOF, level set, phase field etc) can be found in the comprehensive review by Scardovelli and Zaleski [7], or in a more recent exposition by Mirjalili et al. [11] on the same topic. The immiscible nature of the flows under consideration translates to the absence of mass transfer across the interface, thereby rendering the velocity field continuous across the interface at the incompressible limit. The study is primarily focused on isothermal air-water systems, with the material properties corresponding to that at 20 degrees Celcius.

Numerical Platform : Basilisk We solve our set of governing equations using the open-source toolbox Basilisk [2], which couples finite-volume discretization on octree meshes (Fig. 7.4) to solve the two-phase Navier-Stokes equations with surface tension. The use of adaptive mesh refinement (AMR) in conjunction with the octree structure allows an extremely efficient (compared to uniform grids) utilization of computational resources especially when dealing with the multiscale nature (see Fig. 7.5) of surface tension dominated flows, where the bulk of the computational power is diverted towards resolving regions in close proximity to the interface location. The solver utilizes a robust and accurate implementation of the CSF [62] (Continuum Surface Force) surface tension model that governs the volumetric distribution of the capillary forces on the dynamically refined grid (refer to [20] for more details). The numerical methods used in Basilisk have been extensively validated through studies conducted on a variety of free-surface flows, recent examples being on the topic of air entrainment through wave breaking [63, 64], jets created due to bursting bubbles [65, 66] modeling of viscoelastic droplet splashes [67] and many more.

Computational Schematic

As discussed in the previous sections, the dynamics of the liquid volume rearrangements within the ligaments are quite involved due to the non-trivial interactions between the inertial, viscous and capillary effects at different length and time scales that span over several orders of magnitude. In order to isolate the direct influence of initial geometrical shape of the ligament on the subsequent dynamics, we have decided to exclude the inertial forces³ with respect to the initial conditions. Therefore, we opt for a very particular type of setup, with infinitely long ligaments having zero initial kinetic energy, and spatial periodicity in the geometrical shape along the axis. We carry out the simulations in an axisymmetric framework, therefore excluding any azimuthal variations in the initial shape as a consequence of this simplification. Fig. 7.6 illustrates the a 2D schematic of the computational setup, where the domain is a square of side L . The bottom side of the box acts as the axis of symmetry for the corrugated ligament (detailed view in the inset of Fig. 7.6), which has an unperturbed (mean) radius R . Due to the periodicity of the ligaments in the axial direction, we impose periodic boundary conditions for the

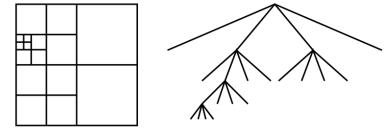


Figure 7.4: A schematic of the octree grid used in Basilisk, and its corresponding logical structure (quadtree in 2D). Image reproduced from Agbaglah et al. [61].

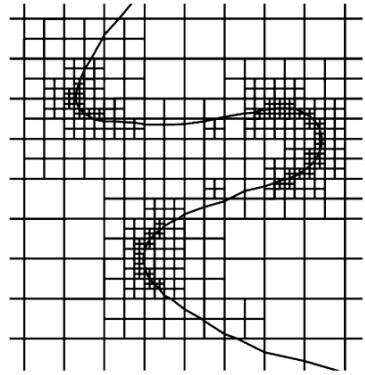


Figure 7.5: A demonstration of multiscale capabilities of Basilisk, wherein the mesh dynamically adapts in order to resolve the smaller scale features of the interface. Image reproduced from Agbaglah et al. [61].

3: We use inertial forces as an umbrella term to describe all the forces that might contribute to the “stretching” of the ligament, thus opposing the capillary deformations. These primarily include the remnant flow within the ligament bulk, the aerodynamic shear at the interface and the acceleration of the ligament itself into the surrounding gas medium.

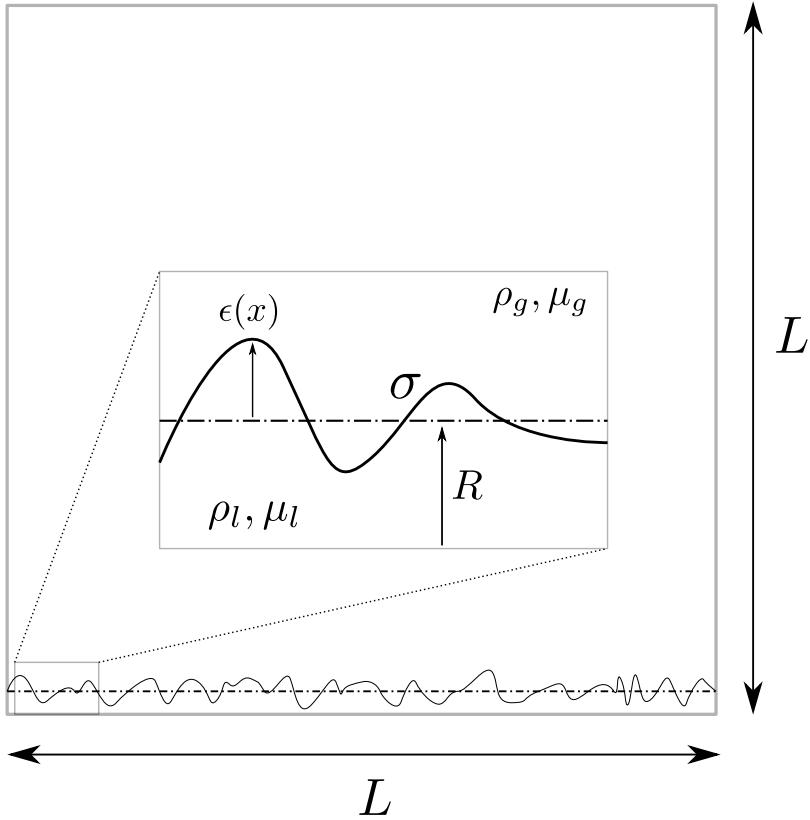


Figure 7.6: A 2D schematic of the computational domain. An infinitely long and axis-symmetric corrugated ligament of mean radius R is placed in a square box of side L . The bottom side of the box acts as the axis of symmetry for the ligament, with spatial periodicity along the horizontal direction. Inset : A close up view of the corrugated profile of the ligament, where the local radius is defined as the sum of the unperturbed (mean) radius R and the local perturbation $\epsilon(x)$. The material properties of the liquid and gas phases are denoted with the subscripts l and g respectively, which in our case corresponds to an air-water system with the surface tension coefficient σ .

primary variables on the left and right faces of the domain. Symmetry conditions are imposed on the bottom side, with impenetrable free-slip conditions applied on the top side.

Random Surface Generation

A key ingredient of this investigation on the impact of corrugations is the ability to precisely control the quantitative aspects of the initial corrugated surface profile of the ligament. Towards that objective, we construct a surface using the superposition of random overlapping waves, corresponding to an overall spatial period L of the resulting profile. The aspect of “randomness” is achieved by using a state of the art white noise generation algorithm, introduced in the seminal work of Matsumoto and Nishimura [68]. A robust and open source implementation of the aforementioned algorithm is available in the GNU Scientific Library toolkit [69], and thus readily incorporated into our numerical platform Basilisk.

The discretization of the radial profile $R(x)$ is expressed as some random perturbation added to the mean value

$$R_i = R(1 + \epsilon_i) \quad , \quad \epsilon_i = \epsilon_0 \cdot \lambda_i^{\text{rng}} \quad (7.2)$$

where i represents the discretization of the continuous profile along the axis, R is the mean (unperturbed) radius, ϵ_0 is the mean corresponding to the amplitudes⁴ of the random waves, and finally λ_i^{rng} are the set of

[68]: Matsumoto et al. (1998), ‘Mersenne twister: a 623-dimensionally equidistributed uniform pseudo-random number generator’

4: As pointed out in the inset of Fig. 7.7, the amplitudes of the random waves generated by the random noise generator are normally distributed.

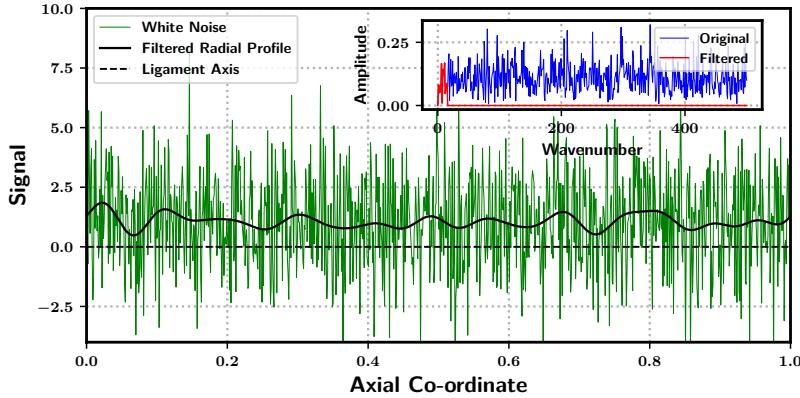


Figure 7.7: Radial profile of the noisy and the subsequently low-pass filtered surface of the ligament, corresponding to one spatial period along its axis. Inset : Spectral densities of the initial noisy signal and the corresponding filtered signal. Only a handful of small wavenumbers are chosen to create the surface.

random values between 0 and 1 generated by the white noise algorithm. The sequence of numbers λ_i^{rng} is uniquely determined by the value of the seed given as input to the white noise generator. This ensures that there are no unforeseen correlations between any two ligament surface profiles, with the exact shape of any given ligament depending on the value of the seed, the mean amplitude of the perturbations and the number of random waves left in the filtered signal.

The initial noisy surface generated by the white noise algorithm contains extremely sharp edges corresponding to infinite values of interfacial curvature (see Fig. 7.7), which are present due to the inclusion of perturbations corresponding to large wavenumbers. In order to avoid the “smoothening” of these edges by our numerical method, we remove these high frequency modes *a priori* in a controllable fashion. As demonstrated in Fig. 7.7, the noisy surface is treated by a low-pass filter in order to obtain the final description of the ligament’s radial profile.

It is interesting to note that we can independently control both the mean amplitude ϵ_0 and the dispersion in the initial white noise signal, where a smaller mean corresponding to a ‘narrower’ distribution of λ_i^{rng} .

Adimensional Groups

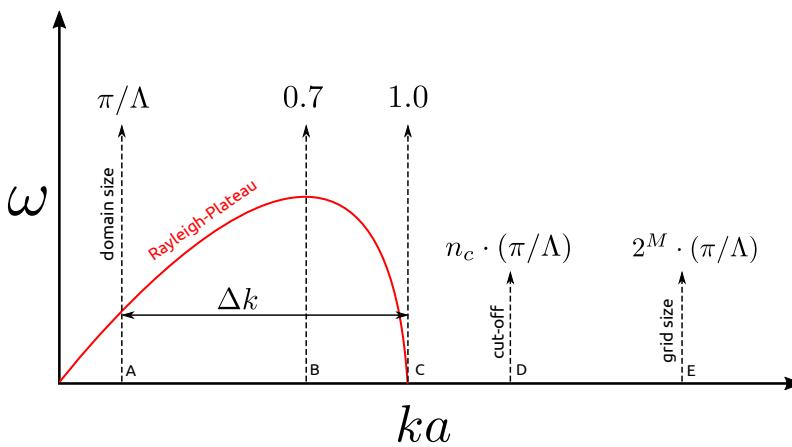
The initial conditions of the computational setup can be characterized by Weber and Ohnesorge numbers, as defined below

$$We = 0 \quad , \quad Oh = \mu / \sqrt{\rho \sigma R}. \quad (7.3)$$

The Weber number is zero due to the ligaments initially being at rest, but during the rapid destabilization phase a part of the surface potential is instantly transformed into kinetic energy of the liquid. The Ohnesorge number is simply the square-root of the ratio of the viscous length scale (l_μ)⁵ to the characteristic length scale of the problem (R). The geometrical shape of the ligament can be characterized by a combination of the corrugation amplitude (ϵ), cut-off wavenumber (K) and the aspect ratio (Λ), defined as

$$\epsilon = \epsilon_0 / R \quad , \quad K = n_c \cdot (2\pi W / L) \quad , \quad \Lambda = L / W, \quad (7.4)$$

5: The viscous length is defined as $l_\mu = \mu^2 / \rho \sigma$. It is intrinsic to the system of the liquid and its free-surface, therefore is not influenced by initial conditions or any global parameters specific to the problem.



where $W = 2R$ denotes the mean width of the ligament, with only the n_c smallest (discrete) wavenumbers passing through the low-pass filter. As in the case with most surface tension dominated flows, the capillary time scale ($t_\sigma = (\rho R^3/\sigma)^{1/2}$) is the most natural choice of time interval by which we can rescale our physical time. Thus, our non-dimensional time is given by

$$T = t \cdot (\rho R^3/\sigma)^{-1/2}. \quad (7.5)$$

Active Wavenumbers

As a consequence of the discrete nature of space in the context of numerical simulations, we can inject energy only into certain spatial frequencies⁶. The general and important result that a liquid cylinder is unstable only to perturbations of wavelength larger than π times the diameter was first demonstrated in the original work of Plateau [70]. The subsequent evolution of these low frequency modes is determined by the dynamical response of the system in question, subject to the underlying governing equations. In the context of inviscid flows, the dispersion relation resulting from linear stability analysis of the potential flow inside a liquid cylinder subject to sinusoidal perturbations is given by

$$\omega = \frac{\omega_0 I_1(x)}{I_0(x)} (1 - x^2), \quad (7.6)$$

where $\omega_0 = \sqrt{\sigma/\rho a^3}$, with a being the radius of the cylinder, and $x = ka$ is the reduced wavenumber of the initial perturbations. The relation (7.6) describing the classical Rayleigh-Plateau instability [47, 70] demonstrates that only the perturbations corresponding to $x \leq 1$ undergo an exponential growth phase, while the remaining perturbations are immediately damped out.

A similar analysis for the full Navier-Stokes equations was carried out by Chandrasekhar [72]. The corresponding dispersion relation for viscous

Figure 7.8: The dispersion relation of the Rayleigh-Plateau instability [47, 70], expressing the growth rate of the small amplitude perturbations as a function of the reduced wavenumber (7.6). The vertical dashed line A represents the upper limit to the perturbation wavelength, corresponding to the domain size L . At the opposite end of the spectrum, E represents smallest wavelength limited by the grid size $1/2^M$, where M is the maximum level of resolution for our octree grid. B corresponds to the wavenumber with the maximum growth based on linear theory, whereas C represents the limit beyond which all perturbations are stable. The number of discrete modes that fall within the unstable part of the spectrum (Δk) is a linear function of the ligament aspect ratio.

The volume of the corrugated ligament per unit spatial period is controlled by the aspect ratio, thus indirectly setting the upper limit to the size of the largest drop that could theoretically form if all the volume of the ligament were to congregate into a single shape.

6: In our particular case, only the modes corresponding to the longest n_c wavelengths ($L, L/2, L/3 \dots L/n_c$) are left with any excitation once the initial noisy profile is passed through the low-pass filter.

I_0 and I_1 are modified Bessel's functions of the first kind, corresponding to order 0 and 1 respectively. Detailed derivations of (7.6) and (7.7) can be found in the comprehensive review by Eggers [71].

flows incorporating the long wavelength approximation of Weber [73], at the limit of low Reynolds is given by

$$\omega = \frac{\omega_\mu}{6} (1 - x^2), \quad (7.7)$$

where $\omega_\mu = \sigma/\mu a$. A similar conclusion can be drawn from (7.7), that all the perturbations corresponding to $x \geq 1$ are stable with respect to linear theory. In Fig. 7.8, we illustrate this principle using the dispersion relation of the inviscid Rayleigh-Plateau instability as a toy model. As one can observe, the number of discrete modes in the unstable part of the spectrum amongst the n_c modes initially excited is given by

$$\Delta k = \Lambda/\pi - 1. \quad (7.8)$$

Thus, the aspect ratio (Λ) of our ligaments is the parameter responsible for selecting the number of modes actually playing a role in the destabilization of the ligament into the eventual drops. To this effect, in the present study we opt to study the dynamics of slender ligaments i.e. large aspect ratios, so that we excite a large enough number of discrete frequencies that are unstable with respect to linear theory. The expectation is that the competition and interactions⁷ between these unstable modes will play a key role in the complex liquid rearrangements within the ligament bulk.

Numerical Fine Tuning

As we have discussed in the previous part (A) of the thesis, one has to pay particular attention to several aspects pertaining to the numerical stability of solvers when dealing with surface tension dominated flows involving significant contrasts in material properties across the interface (such as our system of water ligaments in air). In our use of ‘Basilisk’, we opt to use the standard non-conservative formulation of the Navier-Stokes equations, which does not maintain consistency between mass and momentum transport. But, in this case we are able to circumvent effects such as ‘artificial atomization’ mainly due to two reasons :

- ▶ The use of adaptive mesh refinement based on the octree grids in Basilisk allows us to attain much higher levels of numerical resolution for the smaller/thinner liquid structures, while using significantly coarser meshes away from the interface. For example, in our current simulations (see Fig. 7.9), the number of cells in the domain (2D) are of the order 10^4 , whereas an equivalent *uniform* mesh (2D) would result in a problem size of order 10^6 , thereby differing by a factor of 100.
- ▶ The absence of the interaction of aerodynamic shear forces with the interface, in our particular problem configuration. This prohibits the ‘numerical mixing’ of the gas velocity with the liquid density in

7: Beyond the exponential and independent growth phase of the modes in the linear regime, non-linear effects eventually kick into place, hence the interaction between the different modes.

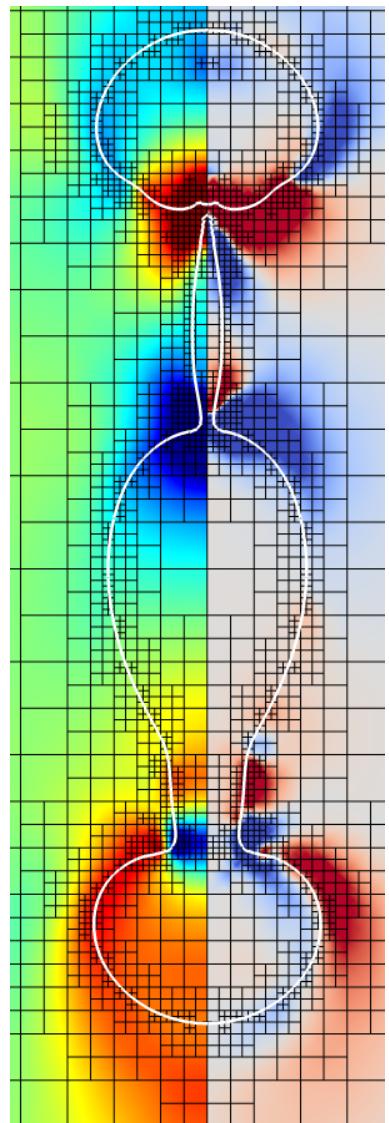


Figure 7.9: Dynamically adapted octree meshes in the periphery of the interface location, with the refinement criteria based on limiting gradients of volume fraction and velocity. The interface is represented by the white contours, the colormap on the left half is based on the axial velocity component, whereas the one on the right corresponds to that of vorticity. The colors red and blue correspond to the higher and lower end values respectively, in case of both colormaps.

the vicinity of poorly resolved interfacial cells, the concomitant unphysical momentum transfer resulting in the rapid destabilization of the interface.

Furthermore, we have to tune the ‘knobs’ of the solver concerning the criteria and corresponding thresholds regarding the dynamic mesh refinement. In all of the simulations/results demonstrated from this point onwards, the mesh adaptation is made according to the value of the local gradients of the volume fraction field, as well as local gradients of the velocity field components. The corresponding values of the thresholds are 10^{-3} and 10^{-1} for the volume fraction and velocity components respectively. The time step for the numerical integration is in itself dependent on the size of the smallest cells, as well as the local velocities. Therefore, we opt for a fixed CFL criteria in order to choose the time step, with the upper bound of the local CFL number throughout the domain being set to 0.05.

Another numerical parameter that has a big influence on the performance of the numerical method is what we refer to as “droplet removal”, which essentially removes extremely small and poorly resolved structures that float around in the domain. In our experience, these small ‘debris’ like structures (see Fig. 7.10) hamper the simulations in several ways e.g. demanding extra computational resources in the form of additionally refined cells, or by imposing extremely small time steps (due to restrictions of local CFL number based on cell size) used for the numerical integration. The removal of these structures do not have any effect on the underlying dynamics of the breakups and coalescences, and their sizes are verified to be orders of magnitude below those corresponding to satellite drops. Our threshold for removal corresponds to structures that are resolved by 10 cells or less. With regards to the iterative Poisson solver, we set a tolerance of 10^{-3} , which in our operator-split framework (see (2.19)) corresponds to the accuracy by which the incompressibility condition (2.20) is verified.

2D versus 3D

An important question to ask ourselves before we conduct any large scale study is the feasibility of carrying out full 3D simulations. In Basilisk, we have the option of carrying out axisymmetric simulations that resolve the underlying governing equations on cylindrical coordinates. Due to the axial symmetry in the construction of our ligaments, carrying out 2D axisymmetric simulations instead of full 3D ones seem to offer a more computationally efficient approach, especially as we are interested in studying the dynamics of thousands of such ligaments. We start with ligaments that correspond to the following parameters

$$Oh = 10^{-2} , \quad \varepsilon = 0.4 \quad (7.9)$$

$$\Lambda = 50 , \quad K = 2\pi \quad (7.10)$$

The numerical resolution in our feasibility studies (in both 2D and 3D) correspond to $W/\Delta x_{\min} = 10.24$, where Δx_{\min} is the size of the smallest grid cell in the octree (quadtree in 2D) mesh. The computations

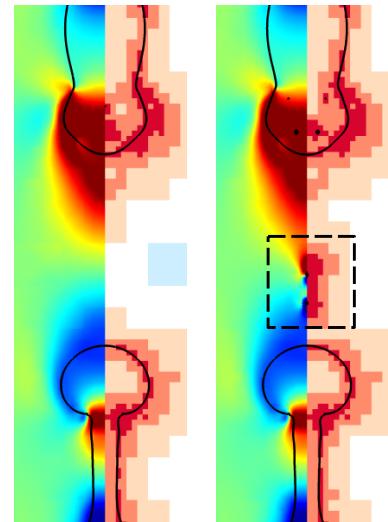


Figure 7.10: Illustration of the effects of our “droplet removal” feature, with the figure on the left corresponding to simulations that filter out structures that are resolved by 10 cells or less, with the one on the right showing results with no droplet removal in place. The box (dashed line) in the right hand side figure displays the extremely small structures that consume a disproportionate amount of computational resources, without having any meaningful impact on the dynamics that we are interested in. The colormap on the left side of the axis of symmetry corresponds to the axial component of velocity, whereas the one on the right refers to the level of numerical resolution. The colors red and blue correspond to the higher and lower end values respectively, in case of both colormaps.

were carried out on 16 processors in parallel, within the framework of parallelization through domain decomposition. The computational times required to resolve the dynamics up to $T = 30$ are 54 seconds and 976 seconds for the 2D and 3D cases, respectively. In figures 7.11 and 7.12, we illustrate the differences in the temporal evolution between a full 3D simulation and its 2D (axisymmetric) equivalent, on fast and slow time scales respectively. As one can observe, the major qualitative difference lies in the excitation of certain azimuthal modes in the 3D case, which cannot be captured in the 2D case due to the imposition of symmetry about the central axis. Such a subtle difference in the dynamics may explain the slightly higher tendency towards coalescence in the 2D case, due to the fact that some of the energy from the axial modes is transferred into the azimuthal modes in the 3D case. Apart from that, the 3D simulations also resolve some finer thread like structures that appear in the vicinity of the breakup region, the details of which are missing in the 2D simulations.

Spatial Resolution

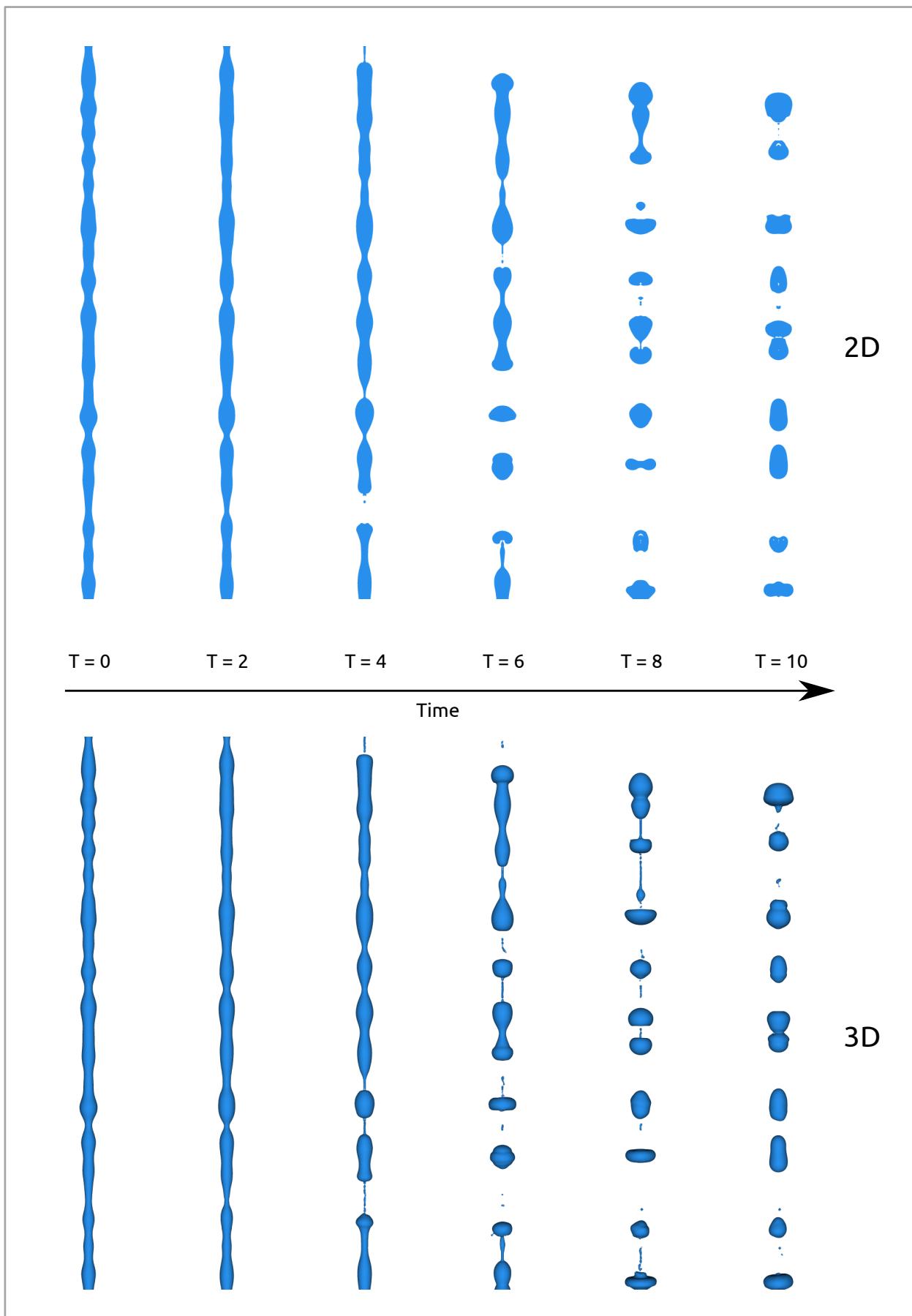


Figure 7.11: Fragmentation of stretched liquid (Newtonian) ligaments formed.

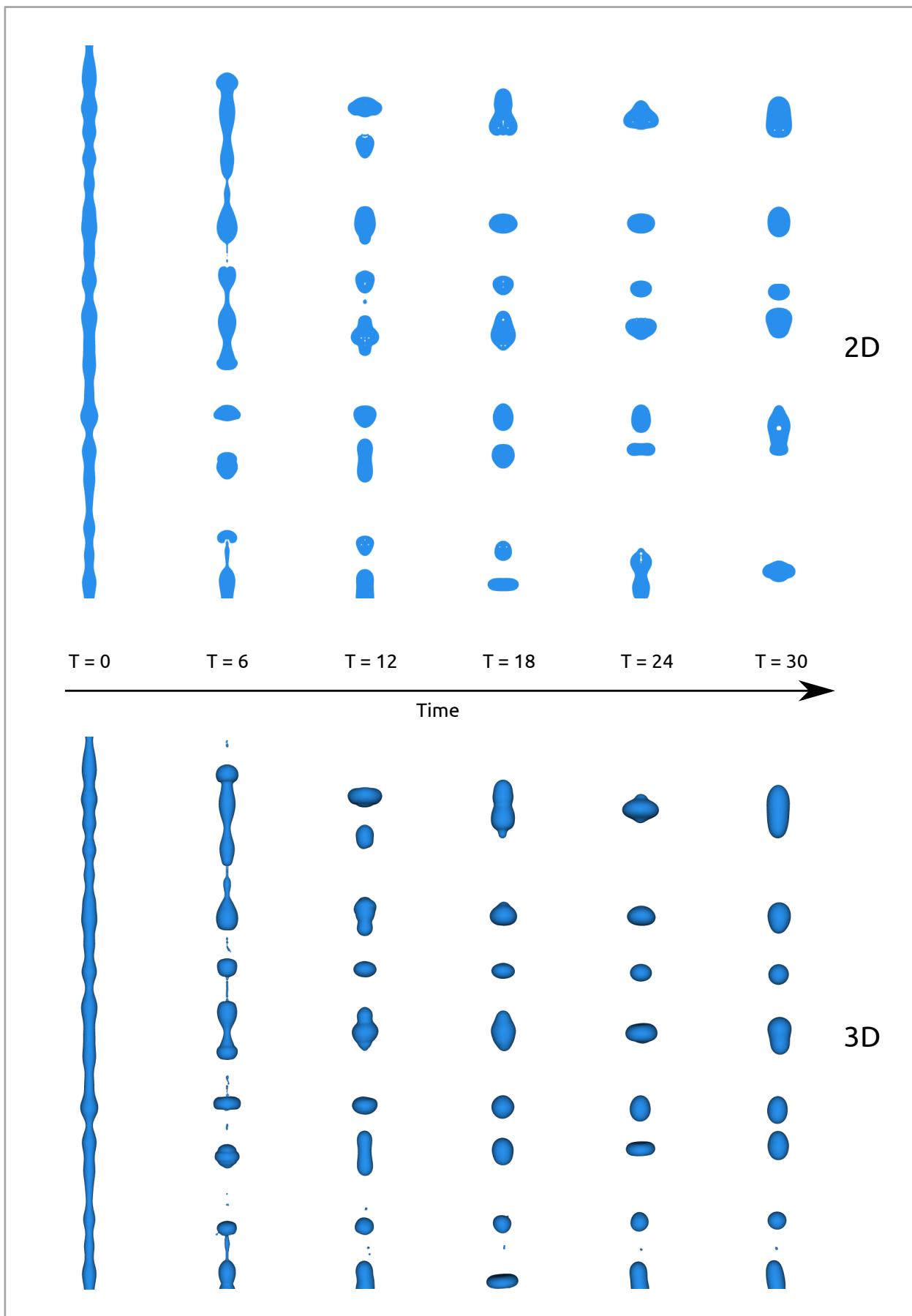


Figure 7.12: Fragmentation of stretched liquid (Newtonian) ligaments formed.

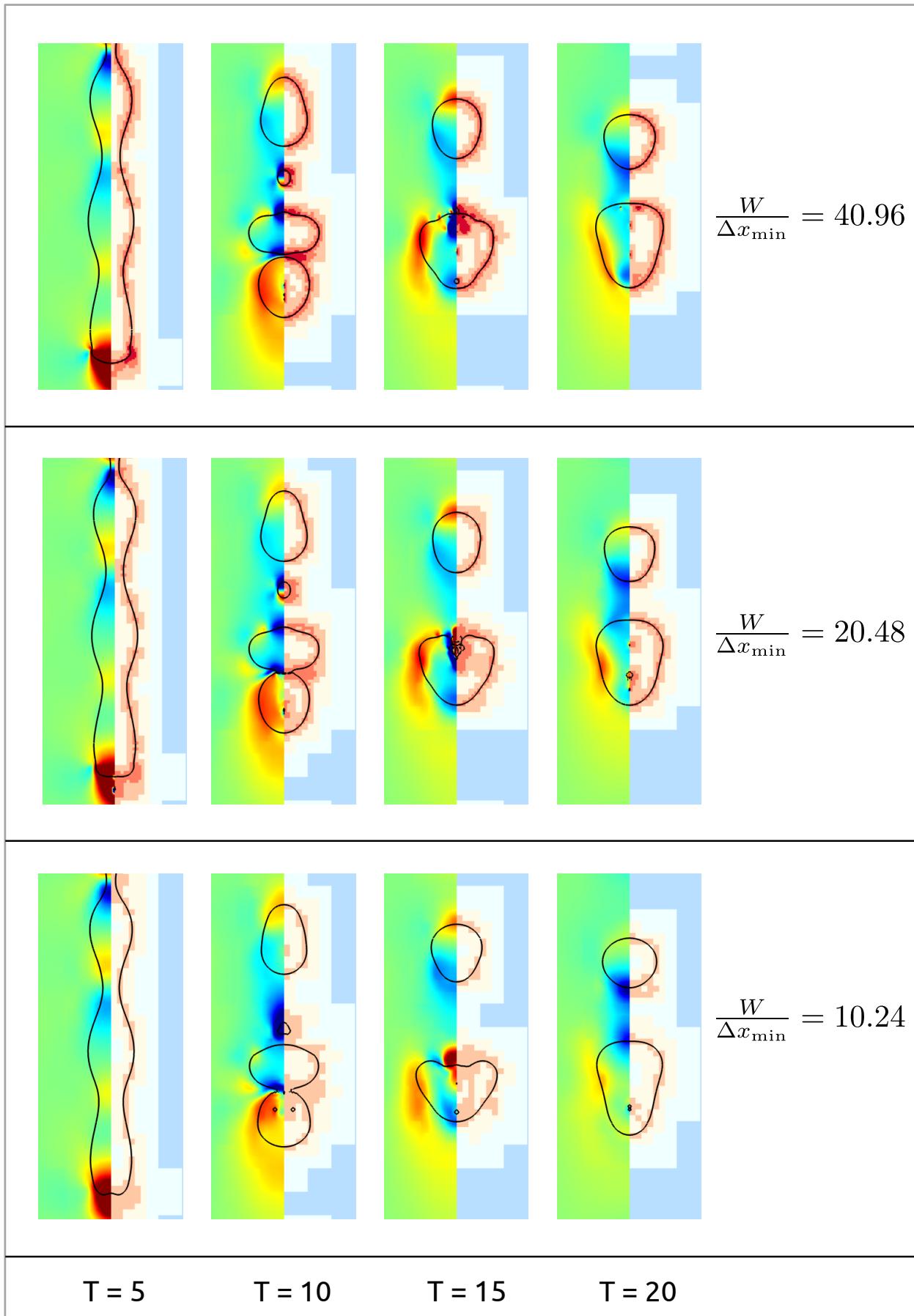


Figure 7.13: Fragmentation of stretched liquid (Newtonian) ligaments formed.

7.4 Impact of Initial Conditions

Corrugation Amplitude

Ohnesorge Number

Cut-Off Frequency

Aspect-Ratio

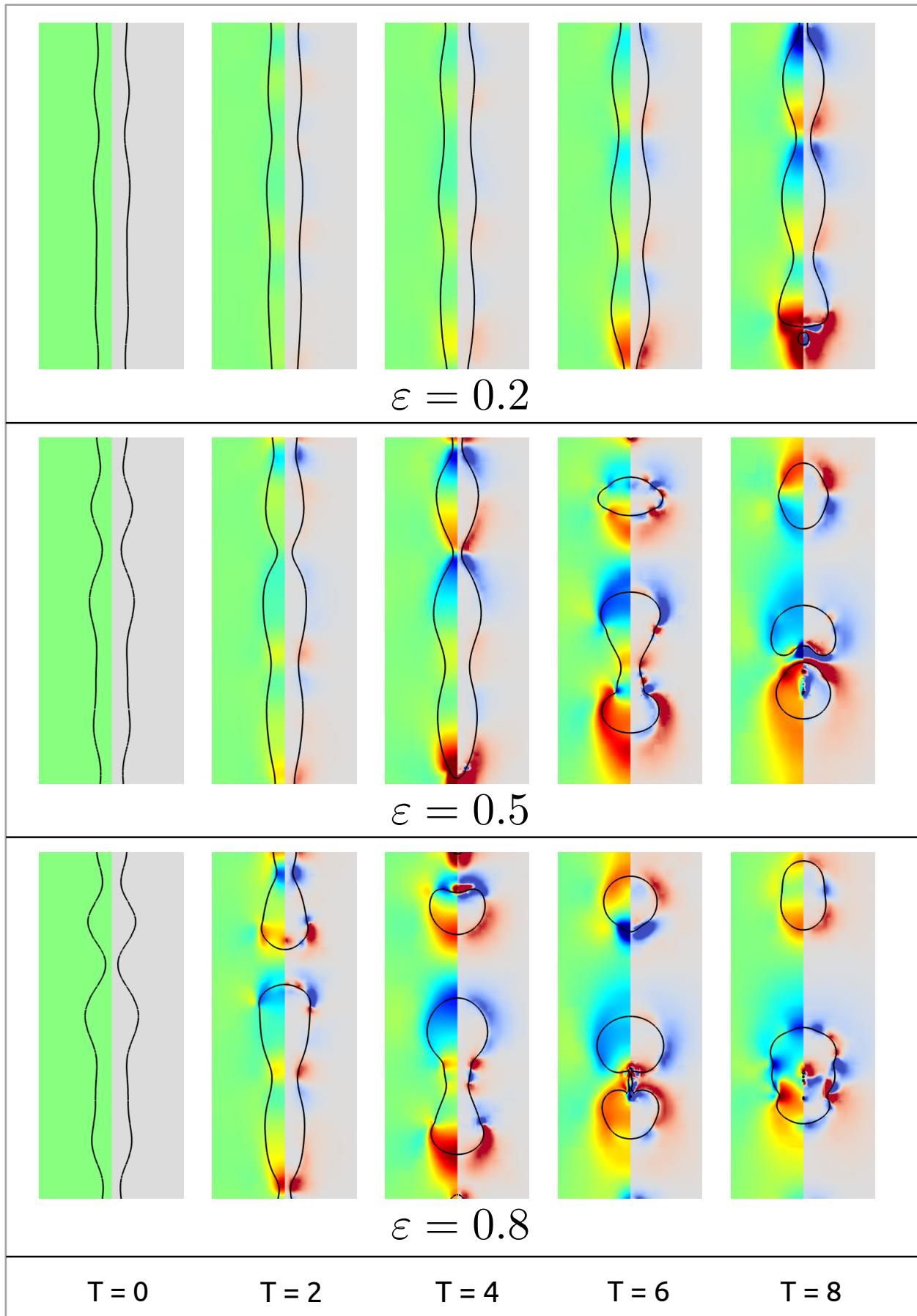


Figure 7.14: Fragmentation of stretched liquid (Newtonian) ligaments formed.

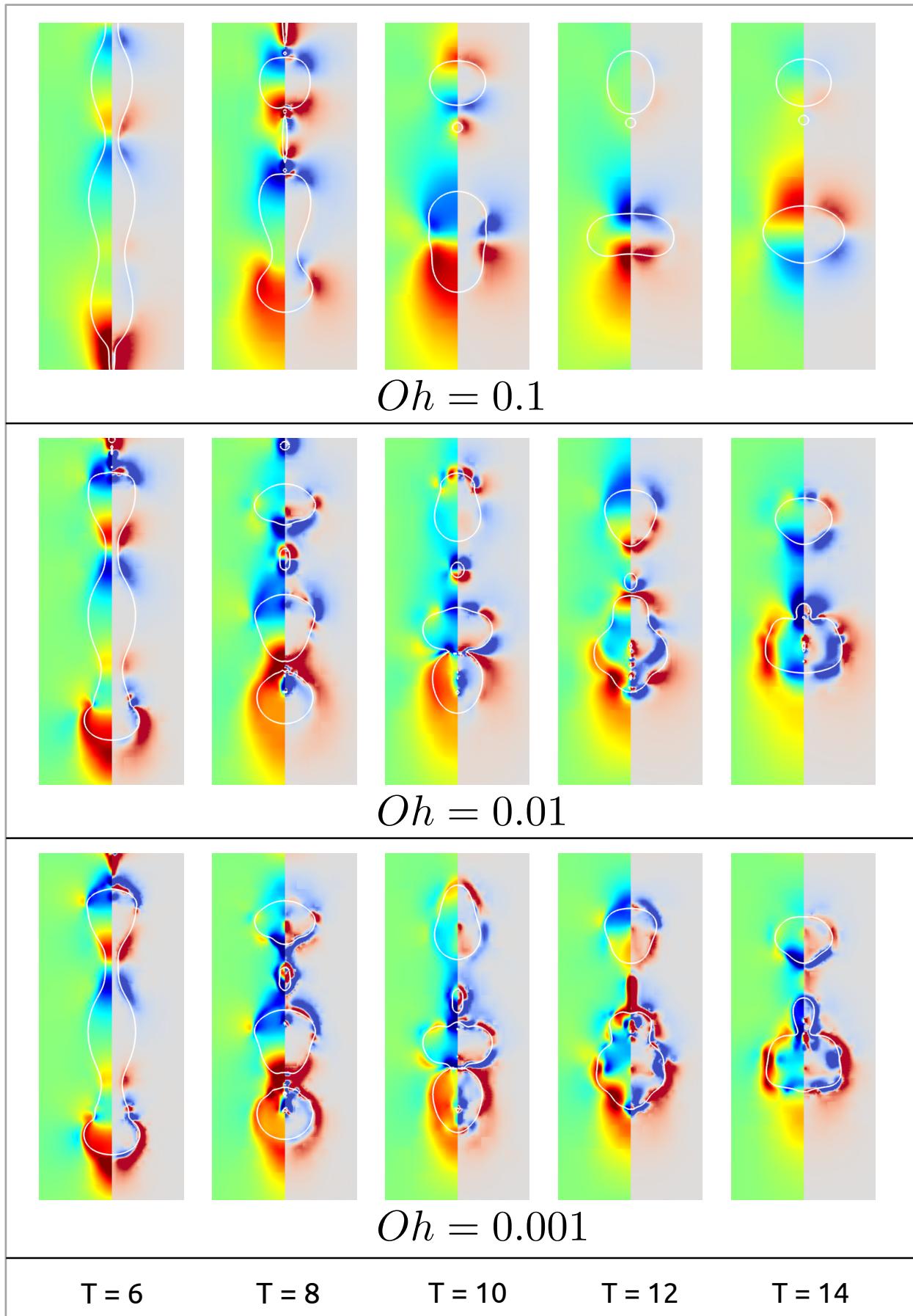


Figure 7.15: Fragmentation of stretched liquid (Newtonian) ligaments formed.

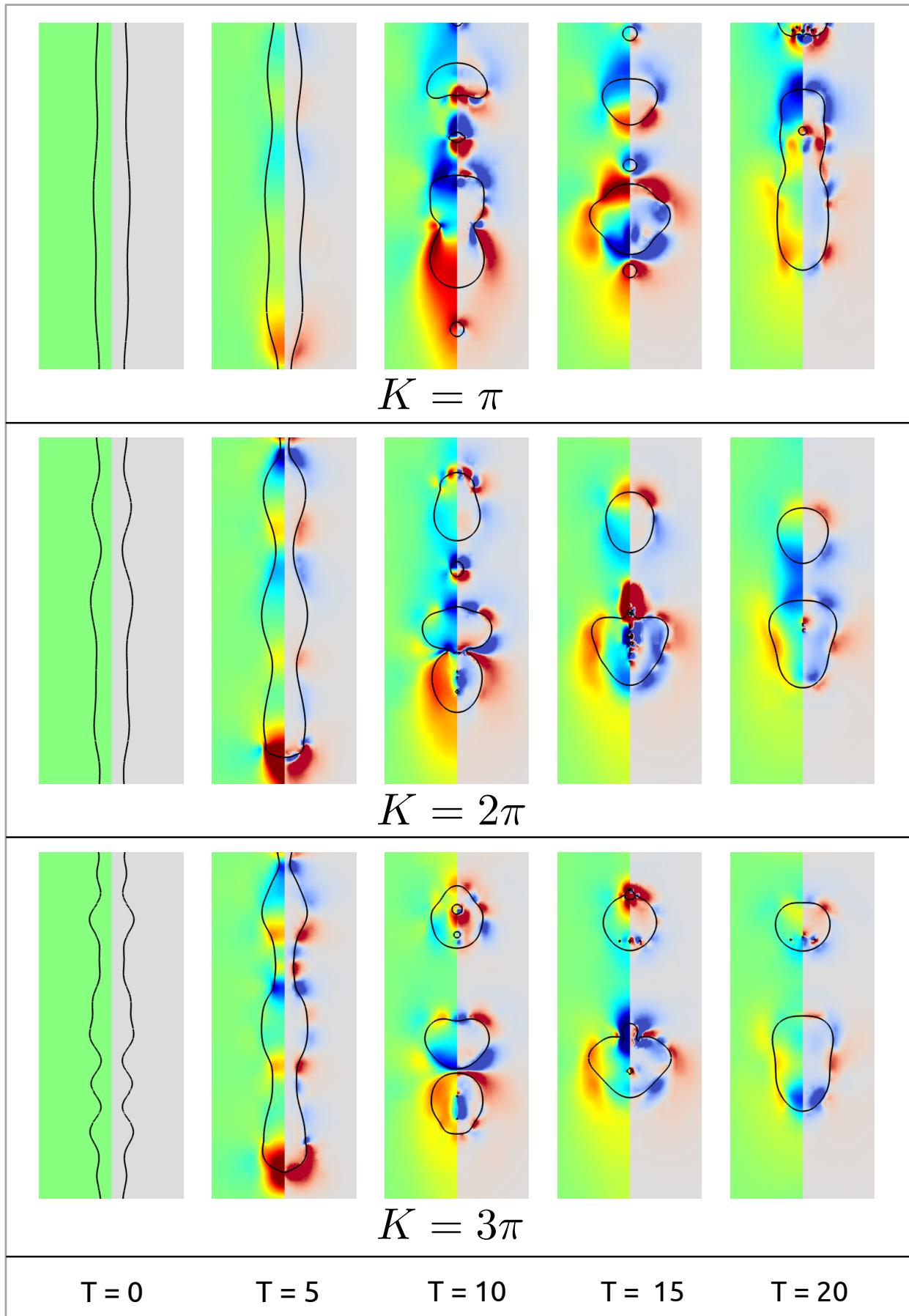


Figure 7.16: Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefbun"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

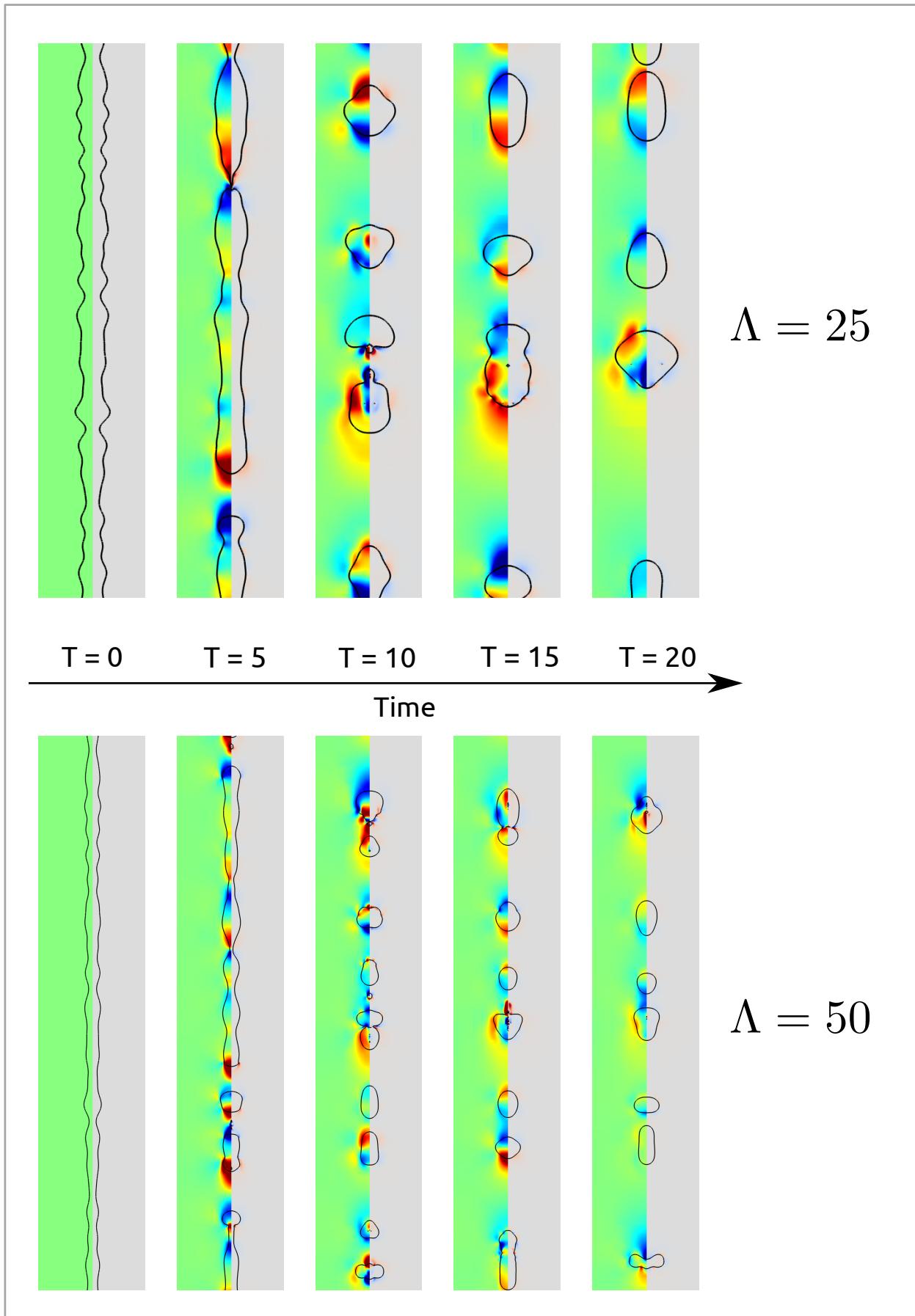


Figure 7.17: Fragmentation of stretched liquid (Newtonian) ligaments formed.

8

Statistics of Drop Sizes

8.1 Monte Carlo Approach to DNS

Characterization of Ligament Ensembles Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

8.2 Millimeter Scale Ensembles

Diameter Distributions Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Mass Distributions Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Equivalent Diameters Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet

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8.2 Millimeter Scale Ensembles	79
8.3 Exploration of Parameter Space	
Φ	80

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Local Distribution of Large Drop Sizes Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

8.3 Exploration of Parameter Space Φ

Bifurcation Parameter : Corrugation Amplitude Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Scaling of D/W : Function of Parameter Space Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

To be added Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

CONCLUSIONS & PERSPECTIVES

Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

This is the second paragraph. Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

And after the second paragraph follows the third paragraph. Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

After this fourth paragraph, we start a new paragraph sequence. Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

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APPENDIX

A

Heading on Level 0 (chapter)

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A.1 Heading on Level 1 (section)

Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Heading on Level 2 (subsection)

Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Heading on Level 3 (subsubsection)

Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift –

not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

Heading on Level 4 (paragraph) Hello, here is some text without a meaning. This text should show what a printed text will look like at this place. If you read this text, you will get no information. Really? Is there no information? Is there a difference between this text and some nonsense like "Huardest gefburn"? Kjift – not at all! A blind text like this gives you information about the selected font, how the letters are written and an impression of the look. This text should contain all letters of the alphabet and it should be written in of the original language. There is no need for special content, but the length of words should match the language.

A.2 Lists

Example for list (itemize)

- ▶ First item in a list
- ▶ Second item in a list
- ▶ Third item in a list
- ▶ Fourth item in a list
- ▶ Fifth item in a list

Example for list (4*itemize)

- ▶ First item in a list
 - First item in a list
 - * First item in a list
 - . First item in a list
 - . Second item in a list
 - * Second item in a list
 - Second item in a list
 - ▶ Second item in a list

Example for list (enumerate)

1. First item in a list
2. Second item in a list
3. Third item in a list
4. Fourth item in a list
5. Fifth item in a list

Example for list (4*enumerate)

1. First item in a list
 - a) First item in a list
 - i. First item in a list
 - A. First item in a list
 - B. Second item in a list
 - ii. Second item in a list
 - b) Second item in a list
2. Second item in a list

Example for list (description)

First item in a list

Second item in a list

Third item in a list

Fourth item in a list

Fifth item in a list

Example for list (4*description)

First item in a list

Second item in a list

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Notation

The next list describes several symbols that will be later used within the body of the document.

c Speed of light in a vacuum inertial frame

h Planck constant

Greek Letters with Pronunciation

Character	Name	Character	Name
α	alpha <i>AL-fuh</i>	ν	nu <i>NEW</i>
β	beta <i>BAY-tuh</i>	ξ, Ξ	xi <i>KSIGH</i>
γ, Γ	gamma <i>GAM-muh</i>	\omicron	omicron <i>OM-uh-CRON</i>
δ, Δ	delta <i>DEL-tuh</i>	π, Π	pi <i>PIE</i>
ϵ	epsilon <i>EP-suh-lon</i>	ρ	rho <i>ROW</i>
ζ	zeta <i>ZAY-tuh</i>	σ, Σ	sigma <i>SIG-muh</i>
η	eta <i>AY-tuh</i>	τ	tau <i>TOW (as in cow)</i>
θ, Θ	theta <i>THAY-tuh</i>	υ, Υ	upsilon <i>OOP-suh-LON</i>
ι	iota <i>eye-OH-tuh</i>	ϕ, Φ	phi <i>FEE, or FI (as in hi)</i>
κ	kappa <i>KAP-tuh</i>	χ	chi <i>KI (as in hi)</i>
λ, Λ	lambda <i>LAM-duh</i>	ψ, Ψ	psi <i>SIGH, or PSIGH</i>
μ	mu <i>MEW</i>	ω, Ω	omega <i>oh-MAY-guh</i>

Capitals shown are the ones that differ from Roman capitals.