



Introduction

Transmission Lines: Guide TEM waves, usually at low frequencies

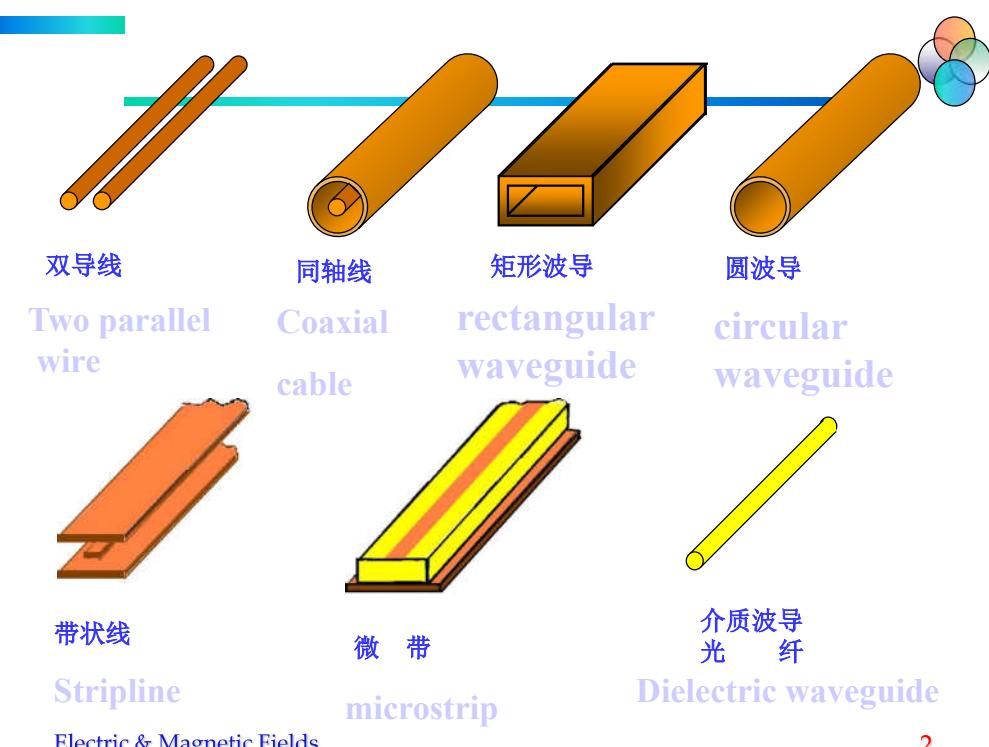
- ◆ Parallel plates
- ◆ Parallel wires
- ◆ Coaxial lines
- ◆ Microstrip(微带)

Waveguides: Guide TE & TM waves, usually at high frequencies

- ◆ **Rectangular Waveguides (emphasis of this chapter)**
- ◆ Cylindrical Waveguides

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3 Types of Electromagnetic Waves



① **TEM Wave:** Transverse Electromagnetic Wave

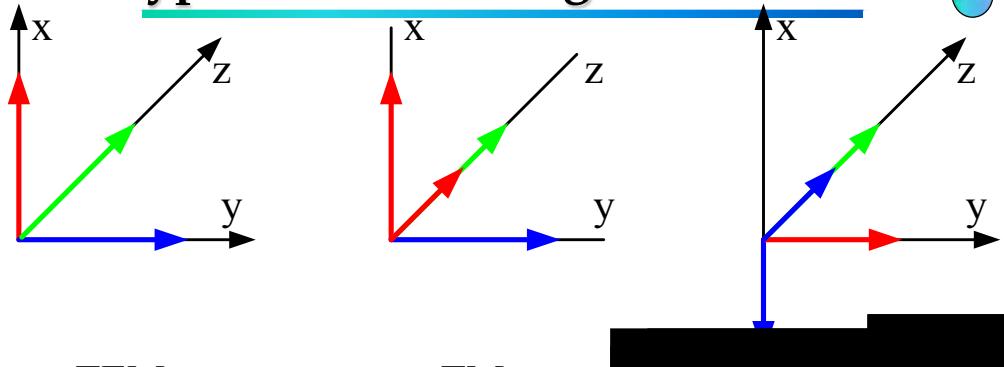
② **TM Wave:** Transverse Magnetic Wave,
also known as E-Wave,
它具有纵向电场分量 E_z , 而无纵向磁场分量 H_z

③ **TE Wave:** Transverse Electric Wave,
also known as H-Wave
它有纵向磁场分量 H_z , 而无纵向电场分量 E_z

Transverse means there is no field component along the direction of wave propagation.

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3 Types of Electromagnetic Waves



- ✿ **TEM** 波的情况下, 传播常数 $\beta=k$
- ✿ **TM、TE** 波的情况下, 传播常数 $\beta \neq k$, 但与 k 有紧密联系 $\beta=k_z$

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Further Explanation (1)



- A homogeneous plane wave (**HPW**) in **infinite media** must be a traveling **TEM** wave.
 - Its **constant phase surfaces** are a series of **parallel planes**. These constant phase planes are normal to the wave propagation direction.
 - All components of the electric & magnetic fields lie in those constant phase planes. Namely, **they are transverse with respect to the wave propagation direction**, resulting in the name of **TEM** wave.

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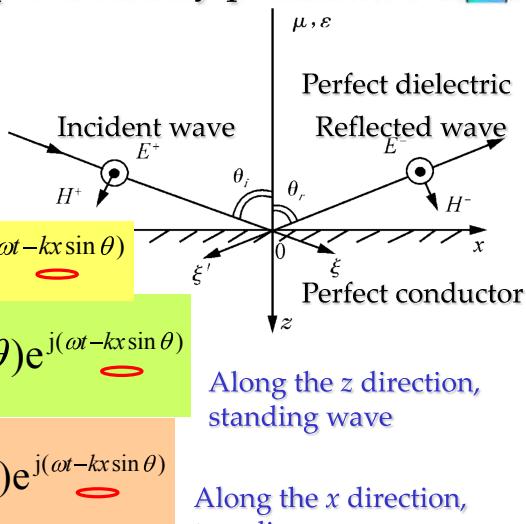
Oblique incidence of a perpendicularly polarized wave

Along the x direction,
TE waves

$$E_y = -j2E_0^+ \sin(kz \cos \theta) e^{j(\omega t - kx \sin \theta)}$$

$$H_z = -j \frac{2E_0^+}{\eta} \sin \theta \sin(kz \cos \theta) e^{j(\omega t - kx \sin \theta)}$$

$$H_x = \frac{-2E_0^+}{\eta} \cos \theta \cos(kz \cos \theta) e^{j(\omega t - kx \sin \theta)}$$



Only E lies in transverse (横向) plane, hence the name **TE-wave**.

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Further Explanation (2)



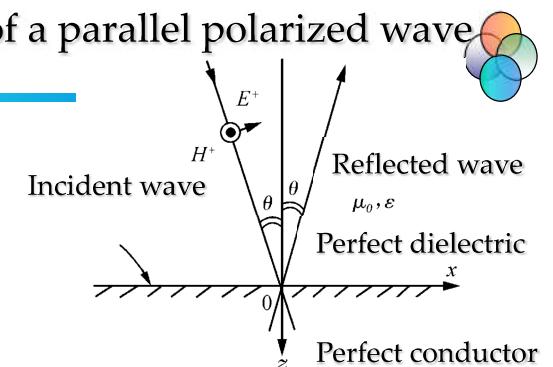
- If a TEM wave in region 1 encounters the boundary between regions 1 & 2, the incident wave may be reflected into region 1 and transmitted into region 2.
- The transmitted wave in **region 2 is still a TEM wave**, but different from the incident wave in region 1.
- The superposition of the incident wave and reflected wave **in region 1 forms a TE or TM wave**.

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Oblique incidence of a parallel polarized wave

Along the x direction,
TM waves



$$E_z = -2H_0^+ \eta \sin \theta \cos(kz \cos \theta) e^{j(\omega t - kx \sin \theta)}$$

$$E_x = -j2H_0^+ \eta \cos \theta \sin(kz \cos \theta) e^{j(\omega t - kx \sin \theta)}$$

$$H_y = 2H_0^+ \cos(kz \cos \theta) e^{j(\omega t - kx \sin \theta)}$$

Along the z direction,
standing wave

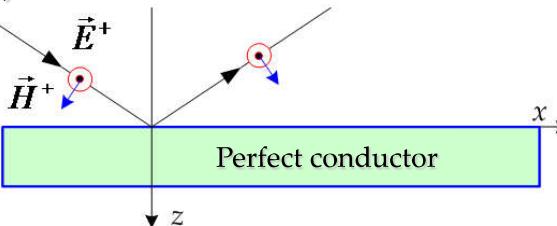
Along the x direction,
traveling wave

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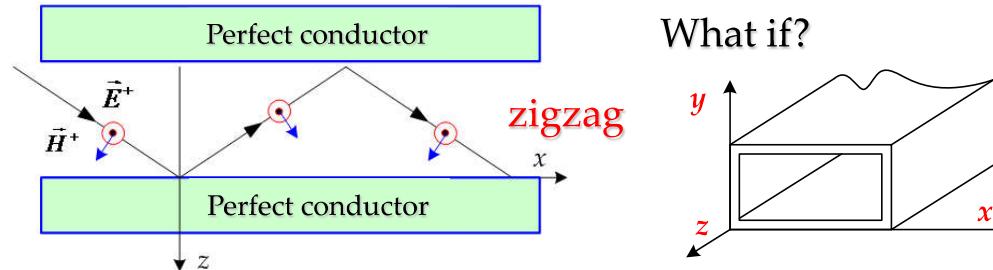
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Oblique incidence of a perpendicularly polarized wave

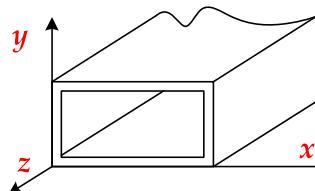
Along the x direction,
TE waves



Place another conductor



What if?



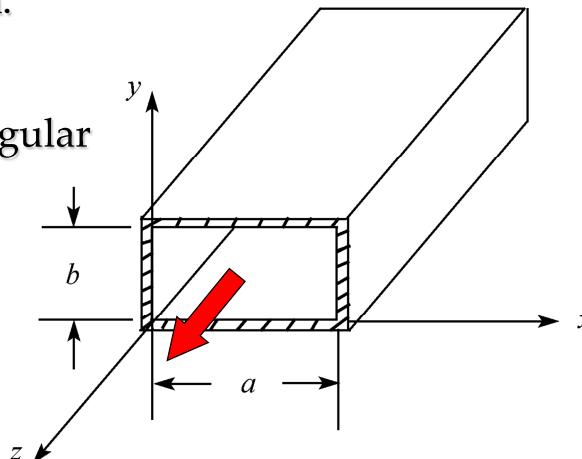
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1. Wave Equations

The wave propagates along the positive z direction.

A air-filled rectangular waveguide



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What is a waveguide?

- ◆ Any structure having the ability to guide EM wave energy or optical energy;
- ◆ The EM field may have a single mode or multiple modes;

Category :

1. Parallel-Plate Waveguide
2. Rectangular Waveguide
3. Cylindrical Waveguide

Filling :

1. hollow (air-filled)
2. dielectric

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Solutions

Recall the solutions to the wave equations in Chapter 7:

$$E_x = E_0 e^{(j\omega t - j\beta z)} = E_0 e^{j\omega t - \gamma z} \quad H_y = \frac{E_0}{\eta} e^{(j\omega t - j\beta z)} = \frac{E_0}{\eta} e^{j\omega t - \gamma z}$$

Likewise, all components of the EM wave have the factor $e^{j\omega t - \gamma z}$.

$$\therefore \frac{\partial}{\partial z} = -\gamma \quad \therefore \frac{\partial^2}{\partial z^2} = \gamma^2$$

$$\gamma = \alpha + j\beta \xrightarrow{\text{lossless}} \gamma = j\beta$$

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Wave equations in a perfect dielectric



k has the transverse & longitudinal components

$$\nabla^2 \vec{E} + k^2 \vec{E} = 0$$

$$k^2 = k_x^2 + k_y^2 + k_z^2$$

$$k^2 = k_x^2 + k_y^2 + \beta^2 \quad \gamma = j\beta$$

$$k^2 = k_x^2 + k_y^2 - \gamma^2$$

E has the transverse & longitudinal components

$$k^2 = k_c^2 - \gamma^2 \quad k_c^2 = k_x^2 + k_y^2$$

$$\frac{\partial^2 E_{x,y,z}}{\partial x^2} + \frac{\partial^2 E_{x,y,z}}{\partial y^2} + \frac{\partial^2 E_{x,y,z}}{\partial z^2} + k^2 E_{x,y,z} = 0$$

$$\nabla_T^2 E_{x,y,z} + \frac{\partial^2 E_{x,y,z}}{\partial z^2} + k^2 E_{x,y,z} = 0$$

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Wave Equations



$$\nabla_T^2 E_{x,y,z} + k_c^2 E_{x,y,z} = 0$$

$$k^2 = k_c^2 - \gamma^2$$

$$\begin{array}{c} \nabla_T^2 E_x + k_c^2 E_x = 0 \\ \nabla_T^2 E_y + k_c^2 E_y = 0 \\ \nabla_T^2 E_z + k_c^2 E_z = 0 \end{array}$$

H has the similar wave equations.

EM wave: $E_x \ E_y \ E_z \ H_x \ H_y \ H_z$

TEM: $E_x \ E_y \quad H_x \ H_y$

TE: $E_x \ E_y \quad H_x \ H_y \ H_z$

TM: $E_x \ E_y \ E_z \ H_x \ H_y$

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$$\nabla^2 \vec{E} + k^2 \vec{E} = 0$$

Wave Equations



$$\nabla_T^2 E_{x,y,z} + \frac{\partial^2 E_{x,y,z}}{\partial z^2} + k^2 E_{x,y,z} = 0 \quad \frac{\partial^2}{\partial z^2} = \gamma^2$$

$$\nabla_T^2 E_{x,y,z} + \gamma^2 E_{x,y,z} + k^2 E_{x,y,z} = 0$$

$$\nabla_T^2 E_{x,y,z} + k_c^2 E_{x,y,z} = 0$$

$$k^2 = k_c^2 - \gamma^2$$

$$\nabla_T^2 E_x + k_c^2 E_x = 0$$

$$\nabla_T^2 E_y + k_c^2 E_y = 0$$

$$\nabla_T^2 E_z + k_c^2 E_z = 0$$

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Solutions ---- TM wave (1)

TM wave: $E_x \ E_y \ E_z \ H_x \ H_y$

$$\text{Solve } E_z \quad \frac{\partial^2 E_z}{\partial x^2} + \frac{\partial^2 E_z}{\partial y^2} + k_c^2 E_z = 0$$

Using the technique of separation of variables:

$$E_z(x,y,z,t) = X \cdot Y \cdot e^{j\omega t - \gamma z}$$

$$\frac{1}{X} \frac{\partial^2 X}{\partial x^2} = -k_x^2 \quad X = A \cos(k_x x) + B \sin(k_x x)$$

$$\frac{1}{Y} \frac{\partial^2 Y}{\partial y^2} = -k_y^2 \quad Y = C \cos(k_y y) + D \sin(k_y y)$$

$$k_c^2 = k_x^2 + k_y^2$$

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Solutions ---- TM wave (2)

$$E_z(x, y, z, t) = X \cdot Y \cdot e^{j\omega t - \gamma z}$$

$$X = A \cos(k_x x) + B \sin(k_x x)$$

$$Y = C \cos(k_y y) + D \sin(k_y y)$$

$$E_z = [A \cos(k_x x) + B \sin(k_x x)] \cdot [C \cos(k_y y) + D \sin(k_y y)] e^{j\omega t - \gamma z}$$

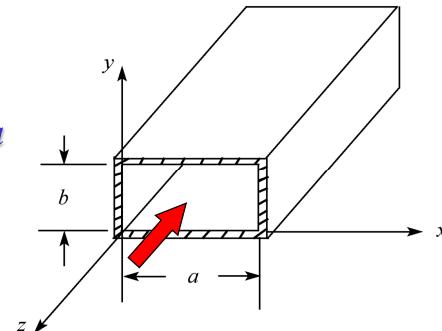
Apply the boundary conditions on the 4 walls: $E_t = 0$

$$(1) x=0, y \in [0, b], E_z = 0 \rightarrow A=0$$

$$(2) x=a, y \in [0, b], E_z = 0 \rightarrow k_x = m\pi/a$$

$$(3) y=b, x \in [0, a], E_z = 0 \rightarrow k_y = n\pi/b$$

$$(4) y=0, x \in [0, a], E_z = 0 \rightarrow C=0$$



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Express the other components in terms of the z components

$$\nabla \times \vec{H} = j\omega \epsilon \vec{E}$$

$$\partial/\partial z = -\gamma$$

$$\partial/\partial t = j\omega$$

$$\nabla \times \vec{E} = -j\omega \mu \vec{H}$$

$$\frac{\partial H_z}{\partial y} + \gamma H_y = j\omega \epsilon E_x \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$-\gamma H_x - \frac{\partial H_z}{\partial x} = j\omega \epsilon E_y \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = j\omega \epsilon E_z \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\frac{\partial E_z}{\partial y} + \gamma E_y = -j\omega \mu H_x \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$-\gamma E_x - \frac{\partial E_z}{\partial x} = -j\omega \mu H_y \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega \mu H_z \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

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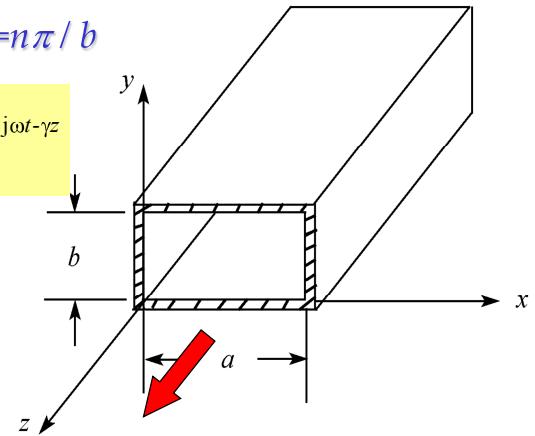
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Solutions ---- TM wave (3)

$$E_z = [A \cos(k_x x) + B \sin(k_x x)] \cdot [C \cos(k_y y) + D \sin(k_y y)] e^{j\omega t - \gamma z}$$

$$A=0 \quad C=0 \quad k_x = m\pi/a \quad k_y = n\pi/b$$

$$E_z = B_0 \sin\left(\frac{m\pi n\pi}{a} x\right) \sin\left(\frac{n\pi}{b} y\right) e^{j\omega t - \gamma z}$$



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Express the other components in terms of the z components

$$\frac{\partial H_z}{\partial y} + \gamma H_y = j\omega \epsilon E_x \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$-\gamma H_x - \frac{\partial H_z}{\partial x} = j\omega \epsilon E_y \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = j\omega \epsilon E_z \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\frac{\partial E_z}{\partial y} + \gamma E_y = -j\omega \mu H_x \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$-\gamma E_x - \frac{\partial E_z}{\partial x} = -j\omega \mu H_y \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -j\omega \mu H_z \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$E_x = -\frac{1}{k_c^2} \left(\gamma \frac{\partial E_z}{\partial x} + j\omega \mu \frac{\partial H_z}{\partial y} \right)$$

$$E_y = \frac{1}{k_c^2} \left(-\gamma \frac{\partial E_z}{\partial y} + j\omega \mu \frac{\partial H_z}{\partial x} \right)$$

$$H_x = \frac{1}{k_c^2} \left(j\omega \epsilon \frac{\partial E_z}{\partial y} - \gamma \frac{\partial H_z}{\partial x} \right)$$

$$H_y = -\frac{1}{k_c^2} \left(j\omega \epsilon \frac{\partial E_z}{\partial x} + \gamma \frac{\partial H_z}{\partial y} \right)$$

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Solutions ---- TM wave (4)

TM wave: $E_x \ E_y \ E_z \ H_x \ H_y$

$$E_z = B_o \sin\left(\frac{m\pi n\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)}$$

$$H_z = 0$$

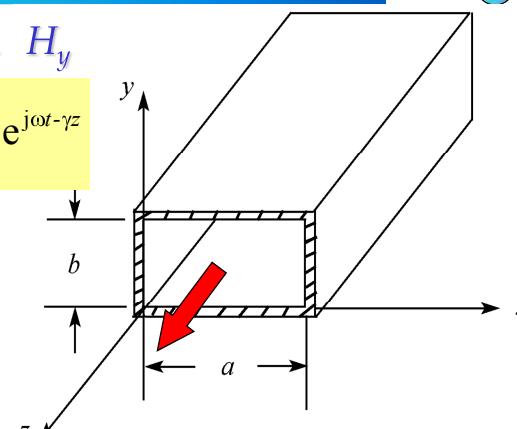
$$E_x = -\frac{1}{k_c^2} \left(\gamma \frac{\partial E_z}{\partial x} + j\omega\mu \frac{\partial H_z}{\partial y} \right)$$

$$H_x = \frac{1}{k_c^2} \left(j\omega\epsilon \frac{\partial E_z}{\partial y} - \gamma \frac{\partial H_z}{\partial x} \right)$$

$$E_y = \frac{1}{k_c^2} \left(-\gamma \frac{\partial E_z}{\partial y} + j\omega\mu \frac{\partial H_z}{\partial x} \right)$$

$$H_y = -\frac{1}{k_c^2} \left(j\omega\epsilon \frac{\partial E_z}{\partial x} + \gamma \frac{\partial H_z}{\partial y} \right)$$

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TM 波的 传输特点

◆ 1, 电磁波的相位仅与变量 z 有关, 而振幅与 x, y 有关。

在 Z 方向上为行波, 在 X 及 Y 方向上形成驻波

◆ 2, z 等于常数的平面为波面, 但振幅与 x, y 有关

TM 波为非均匀的平面波

◆ 3, 当 m 或 n 为零时, 上述各个分量均为零, 因此 m 及 n 应为非零的整数。

m 及 n 的物理意义: m 为宽壁上的半个驻波的数目, n 为窄壁上半个驻波的数目

◆ 4, 由于 m 及 n 为多值, 因此场结构均具有多种模式。 m 及 n 的每一种组合构成一种模式, 以 TM_{mn} 表示。例如 TM_{11} 表示 $m=1, n=1$ 的场结构, 具有这种场结构的波称为 TM_{11} 波。

◆ 5, 数值大的 m 及 n 模式称为高次模, 数值小的称为低次模。 矩形波导中 TM 波的最低模式是 TM_{11} 波。 Dominant mode

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$$E_z = B_o \sin\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)}$$

$$E_x = -j \frac{\beta}{k_c^2} \frac{m\pi}{a} B_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)}$$

$$E_y = -j \frac{\beta}{k_c^2} \frac{n\pi}{b} B_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)}$$

$$H_x = j \frac{\omega\epsilon}{k_c^2} \frac{m\pi}{b} B_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)}$$

$$H_y = -j \frac{\omega\epsilon}{k_c^2} \frac{m\pi}{a} B_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)}$$

$$H_z = 0$$

$$k_c^2 = k_x^2 + k_y^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2$$

TM
wave

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Neither m nor n is zero!

Solutions ---- TE wave

TE wave: $E_x \ E_y \ H_x \ H_y \ H_z$

$$\text{Solve } H_z \quad \frac{\partial^2 H_z}{\partial x^2} + \frac{\partial^2 H_z}{\partial y^2} + k_c^2 H_z = 0$$

Using the technique of separation of variables:

$$H_z(x, y, z, t) = X \cdot Y \cdot e^{j\omega t - \lambda z}$$

$$H_z = [A \cos(k_x x) + B \sin(k_x x)] \cdot [C \cos(k_y y) + D \sin(k_y y)] e^{j\omega t - \lambda z}$$

Apply the boundary conditions on the 4 walls: $E_t = 0$

$$H_z = A_o \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j\omega t - \lambda z}$$

$$E_z = 0$$

$$E_x = -\frac{1}{k_c^2} \left(\gamma \frac{\partial E_z}{\partial x} + j\omega\mu \frac{\partial H_z}{\partial y} \right)$$

$$H_x = \frac{1}{k_c^2} \left(j\omega\epsilon \frac{\partial E_z}{\partial y} - \gamma \frac{\partial H_z}{\partial x} \right)$$

$$E_y = \frac{1}{k_c^2} \left(-\gamma \frac{\partial E_z}{\partial y} + j\omega\mu \frac{\partial H_z}{\partial x} \right)$$

$$H_y = -\frac{1}{k_c^2} \left(j\omega\epsilon \frac{\partial E_z}{\partial x} + \gamma \frac{\partial H_z}{\partial y} \right)$$

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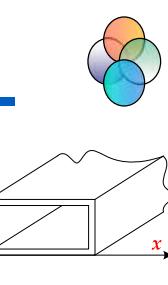
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$$\left. \begin{aligned} H_z &= A_o \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_x &= j \frac{\beta}{k_c^2} \frac{m\pi}{a} A_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_y &= j \frac{\beta}{k_c^2} \frac{n\pi}{b} A_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_x &= j \frac{\omega\mu}{k_c^2} \frac{n\pi}{b} A_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_y &= -j \frac{\omega\mu}{k_c^2} \frac{m\pi}{a} A_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_z &= 0 \end{aligned} \right\}$$

TE wave

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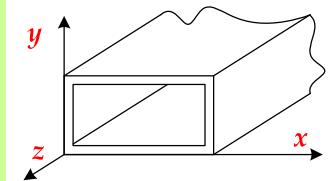
$$k_c^2 = k_x^2 + k_y^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2$$

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$$\left. \begin{aligned} E_z &= B_o \sin\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_x &= -j \frac{\beta}{k_c^2} \frac{m\pi}{a} B_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_y &= -j \frac{\beta}{k_c^2} \frac{n\pi}{b} B_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_x &= j \frac{\omega\epsilon}{k_c^2} \frac{n\pi}{b} B_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_y &= -j \frac{\omega\epsilon}{k_c^2} \frac{m\pi}{a} B_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_z &= 0 \end{aligned} \right\}$$

TM mode

Mode
For given m & n , the mode of the EM wave is called **TM_{mn} mode**



m & n indicates the numbers of maximum field values along the x & y directions, respectively, e.g. TM₃₂

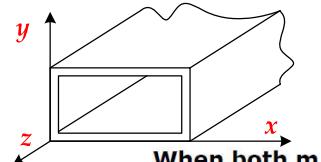
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$$\left. \begin{aligned} H_z &= A_o \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_x &= j \frac{\beta}{k_c^2} \frac{m\pi}{a} A_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_y &= j \frac{\beta}{k_c^2} \frac{n\pi}{b} A_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_x &= j \frac{\omega\mu}{k_c^2} \frac{n\pi}{b} A_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_y &= -j \frac{\omega\mu}{k_c^2} \frac{m\pi}{a} A_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_z &= 0 \end{aligned} \right\}$$

Mode

For given m & n , the mode of the EM wave is called **TE_{mn} mode**



When both m and n are zero, all other field components but H_z will disappear, so TE₀₀ cannot exist in a waveguide.

TE₁₀ is the lowest-order mode ($a>b$).

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2. Parameters of TE & TM waves

- ◆ The Propagating Mode
 - ◆ The EM energy is transmitted.
- ◆ In other words,
 - ◆ The EM energy cannot be transmitted in any mode in a waveguide;
 - ◆ The EM energy cannot be transmitted in any frequency in a waveguide;
- ◆ The Cutoff Frequency: f_c
 - ◆ When the propagation constant $\gamma^2 \geq 0$, the wave cannot be transmitted.
 - ◆ When the frequency (wavelength) of the EM field is above (below) a certain frequency (wavelength), the wave can be transmitted.

$$k^2 = k_x^2 + k_y^2 + \beta^2$$

$$k^2 = k_x^2 + k_y^2 - \gamma^2$$

$$E(x,y,z,t) = E_0 \cdot e^{j\omega t - \gamma z}$$

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$$k^2 = k_c^2 - \gamma^2$$

$$\gamma^2 = k_c^2 - k^2 \geq 0$$

The wave is said to be evanescent. 逐漸消失

$$\therefore k_c^2 \leq k^2 = \omega^2 \mu \epsilon = (2\pi f)^2 \mu \epsilon$$

$$\therefore k_c^2 = k_x^2 + k_y^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n}{b}\right)^2 \leq (2\pi f)^2 \mu \epsilon$$

The cutoff frequency

$$f_c = \frac{1}{2\sqrt{\epsilon\mu}} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2} = \frac{v}{\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}} = \frac{v}{\lambda_c}$$

$\lambda < \lambda_c$ or $f > f_c$, the wave can propagate.

v is phase velocity in the unbounded medium



$$k^2 = k_c^2 - \gamma^2 = k_c^2 + \beta^2$$

$$\beta^2 = k^2 - k_c^2$$

$$j\beta = \gamma$$

$$k^2 - \beta^2 = k_x^2 + k_y^2 \Rightarrow \beta = \sqrt{\omega^2 \epsilon \mu - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2}$$

$$k^2 = \omega^2 \mu \epsilon = (2\pi f)^2 \mu \epsilon \quad \frac{k^2}{f^2} = (2\pi)^2 \mu \epsilon$$

$$f_c = \frac{1}{2\sqrt{\epsilon\mu}} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

$$\beta^2 = k^2 \left(1 - \frac{f_c^2}{f^2}\right) = k^2 \left(1 - \frac{\lambda^2}{\lambda_c^2}\right)$$



The phase constant β

$$\beta^2 = k^2 \left(1 - \frac{f_c^2}{f^2}\right) = k^2 \left(1 - \frac{\lambda^2}{\lambda_c^2}\right)$$

$$\beta = k \sqrt{1 - (\lambda / \lambda_c)^2}$$

The Waveguide wavelength: $\lambda_g = \frac{2\pi}{\beta} = \frac{2\pi}{k \sqrt{1 - (\lambda / \lambda_c)^2}} = \frac{\lambda}{\sqrt{1 - (\lambda / \lambda_c)^2}}$

The phase velocity

$$v_p = \frac{\omega}{\beta} = \frac{\omega}{k \sqrt{1 - (\lambda / \lambda_c)^2}} = \frac{v}{\sqrt{1 - (\lambda / \lambda_c)^2}}$$

$$\text{The group velocity } v_g \quad v_g = \frac{d\omega}{d\beta} = \frac{1}{d\beta/d\omega}$$

$$2\pi = k\lambda = k_c \lambda_c \quad \beta = \sqrt{k^2 - k_c^2} = \sqrt{\left(\frac{\omega}{v}\right)^2 - \left(\frac{2\pi}{\lambda_c}\right)^2}$$

$$v_g = v \sqrt{1 - (\lambda / \lambda_c)^2}$$

Thus, a waveguide acts as a dispersive medium.

Discussion:

$$v_p = \frac{\omega}{\beta} = \frac{v}{\sqrt{1 - (\lambda/\lambda_c)^2}} \quad v_g = v \sqrt{1 - (\frac{\lambda}{\lambda_c})^2} \quad \beta = k \sqrt{1 - (\frac{\lambda}{\lambda_c})^2}$$

When $\lambda < \lambda_c$,

β is real, v_p & v_g are also real, TE & TM waves can propagate.

When $\lambda = \lambda_c$,

$$e^{j(\omega t - \beta z)}$$

$\beta = 0$, $v_g = 0$, $v_p = \infty$, the wave is evanescent. 电磁波刚好截止

When $\lambda > \lambda_c$,

$$e^{j(\omega t - \beta z)} = e^{j\omega t} \cdot e^{-|\beta|z}$$

β , v_p & v_g are imaginary, the wave is evanescent.



$$Z_{W(TM)} = \frac{\gamma}{j\omega\epsilon} = \frac{j\beta}{j\omega\epsilon} = \frac{\beta}{\omega\epsilon}$$

Likewise, $Z_{W(TE)} = \frac{j\omega\mu}{\gamma} = \frac{\omega\mu}{\beta}$

Recall $Z_{TEM} = \eta = \sqrt{\frac{\mu}{\epsilon}} = \frac{k}{\omega\epsilon} = \frac{\omega\mu}{k}$

$$\beta = k \sqrt{1 - \left(\frac{\lambda}{\lambda_c}\right)^2}$$

Wave impedance for a TM wave:

$$Z_{W(TM)} = \frac{E_T}{H_T} = \frac{\gamma}{j\omega\epsilon}$$



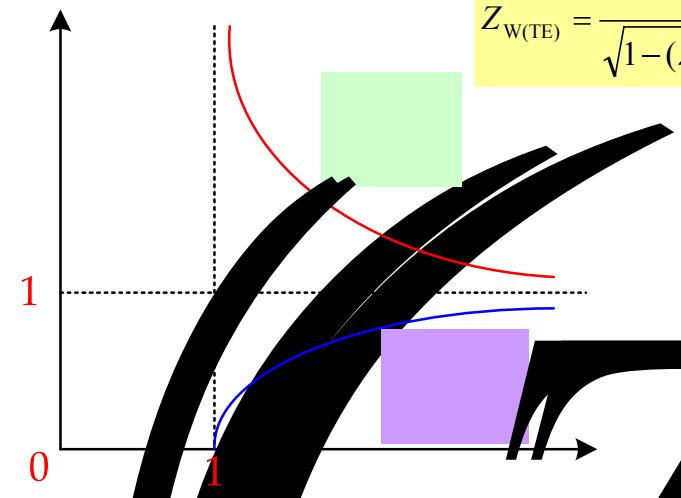
$$\left. \begin{aligned} E_x &= -j \frac{\beta}{k_c^2} \frac{m\pi}{a} B_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_y &= -j \frac{\omega\epsilon}{k_c^2} \frac{m\pi}{a} B_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ j\omega\epsilon E_x &= \gamma H_y \\ E_y &= -j \frac{\beta}{k_c^2} \frac{n\pi}{b} B_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_x &= j \frac{\omega\epsilon}{k_c^2} \frac{n\pi}{b} B_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ j\omega\epsilon E_y &= -\gamma H_x \end{aligned} \right\}$$

$$\vec{E}_T = \vec{e}_x E_x + \vec{e}_y E_y = \vec{e}_x \left(\frac{\gamma}{j\omega\epsilon} H_y \right) + \vec{e}_y \left(\frac{-\gamma}{j\omega\epsilon} H_x \right) = \frac{\gamma}{j\omega\epsilon} [\vec{e}_x H_y - \vec{e}_y H_x]$$

Wave Impedance

$$Z_{W(TM)} = \eta \sqrt{1 - (\lambda/\lambda_c)^2} = \eta \sqrt{1 - (f_c/f)^2}$$

$$Z_{W(TE)} = \frac{\eta}{\sqrt{1 - (\lambda/\lambda_c)^2}} = \frac{\eta}{\sqrt{1 - (f_c/f)^2}}$$



$$Z_{W(TM)} = \eta \sqrt{1 - (\lambda / \lambda_c)^2}$$

$$Z_{W(TE)} = \frac{\eta}{\sqrt{1 - (\lambda / \lambda_c)^2}}$$



3. The lowest-order mode & single-mode propagation



When $\lambda < \lambda_c$, TE & TM waves can propagate.

$Z_{W(TM)}$ & $Z_{W(TE)}$ are both real.

When $\lambda = \lambda_c$, the wave is evanescent.

$Z_{W(TM)} = 0, Z_{W(TE)} = \infty$

When $\lambda > \lambda_c$, the wave is evanescent.

$Z_{W(TM)}$ & $Z_{W(TE)}$ are both imaginary; $Z_{W(TM)}$ is capacitive, $Z_{W(TE)}$ is inductive.

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The cutoff wavelengths of TE_{mn} modes



When $a = 2b$,

$$\lambda_{c(10)} = 2a \quad \text{for } TE_{10}$$

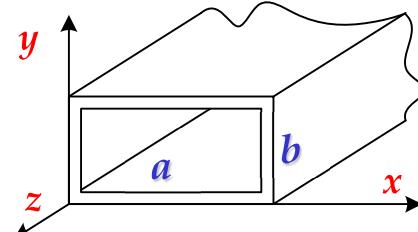
$$\lambda_{c(20)} = a \quad \text{for } TE_{20}$$

$$\lambda_{c(01)} = 2b = a \quad \text{for } TE_{01}$$

$$\lambda_{c(11)} = 2a / \sqrt{5} \quad \text{for } TE_{11}$$

$$\lambda_{c(30)} = 2a / 3 \quad \text{for } TE_{30}$$

$$\lambda_{c(02)} = b = a / 2 \quad \text{for } TE_{02}$$



$$\lambda_c = \frac{2\pi}{k_c} = \frac{2}{\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}}$$

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The lowest-order mode is the one with the maximum cutoff wavelength.

$$\lambda_c = \frac{2\pi}{k_c} = \frac{2}{\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}}$$

When $\lambda < \lambda_c$, the wave can propagate.

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The maximum cutoff wavelength of TE waves



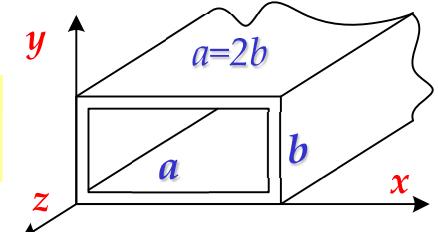
$$\lambda_{c(10)} = 2a$$

TE_{10} mode is the lowest-order mode in all TE modes.

Likewise, for TM waves

$$\lambda_{c(11)} = 2a / \sqrt{5}$$

TM_{11} mode is the lowest-order mode in all TM modes.



Therefore,

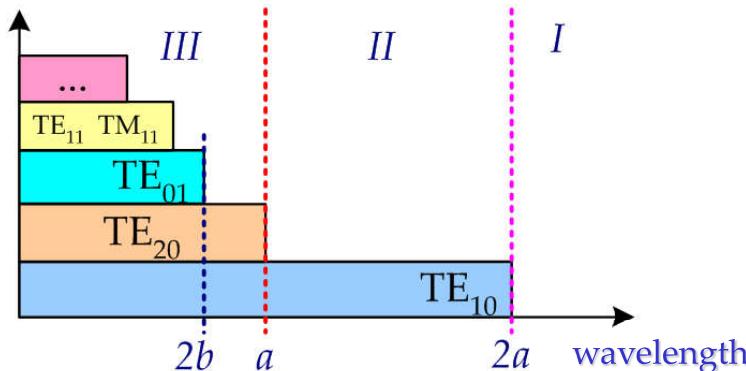
When $a=2b$, the lowest-order mode is TE_{10} .

$$\lambda_{c(10)} = 2a$$

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The distribution of cutoff wavelength



When $\lambda < \lambda_c$, the wave can propagate.

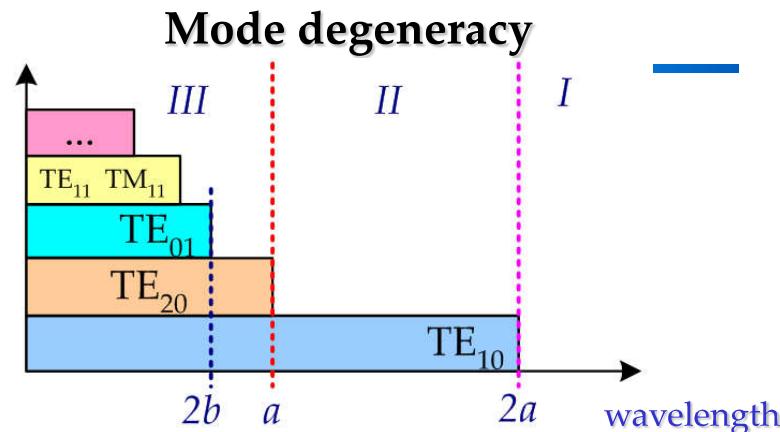
Region I: cutoff—evanescent

Region II: single-mode —only one mode can exist

Region III: multi-mode—more than one mode can exist

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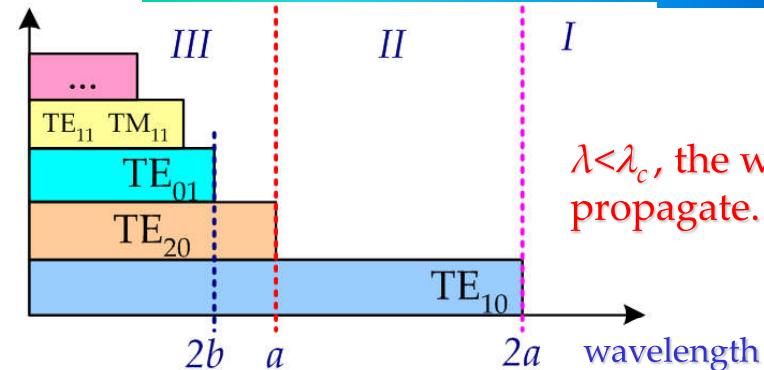
Mode degeneracy: two modes have the same cutoff wavelength.

For example, TE₁₁ and TM₁₁ are the degenerate mode.

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The conditions of single-mode propagation



$\lambda < \lambda_c$, the wave can propagate.

$$\left\{ \begin{array}{l} 2a > \lambda > a \\ \lambda/2 < a < \lambda \quad (a \geq 2b) \end{array} \right.$$

TE₁₀ is the only propagating mode, called the dominant mode.

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4. The dominant mode: TE₁₀

$$\left. \begin{aligned} H_z &= A_o \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_x &= j \frac{\beta}{k_c^2} \frac{m\pi}{a} A_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ H_y &= j \frac{\beta}{k_c^2} \frac{n\pi}{b} A_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_x &= j \frac{\omega\mu}{k_c^2} \frac{n\pi}{b} A_o \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_y &= -j \frac{\omega\mu}{k_c^2} \frac{m\pi}{a} A_o \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{j(\omega t - \beta z)} \\ E_z &= 0 \end{aligned} \right\}$$

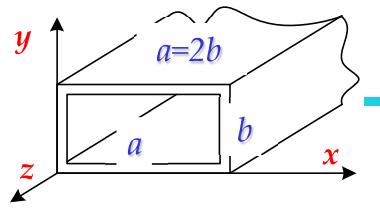
$m=1$

$n=0$



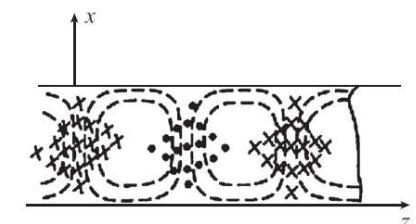
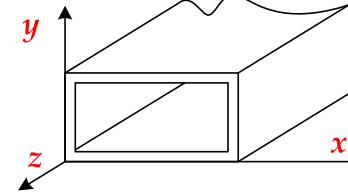
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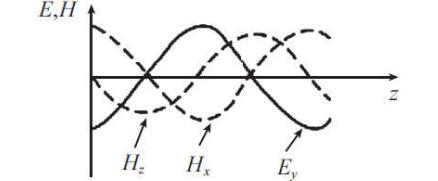


TE₁₀ Mode

$$\left. \begin{aligned} E_y &= -j \frac{\omega \mu \pi \pi}{k_c^2 a} A_o \sin\left(\frac{-x}{a}\right) e^{j(\omega t - \beta z)} \\ H_x &= j \frac{\beta \pi \pi}{k_c^2 a} A_o \sin\left(\frac{-x}{a}\right) e^{j(\omega t - \beta z)} \\ H_z &= A_o \cos\left(\frac{\pi}{a} x\right) e^{j(\omega t - \beta z)} \end{aligned} \right\}$$



$$\left. \begin{aligned} E_y &= -j \frac{\omega \mu \pi \pi}{k_c^2 a} A_o \sin\left(\frac{-x}{a}\right) e^{j(\omega t - \beta z)} \\ H_x &= j \frac{\beta \pi \pi}{k_c^2 a} A_o \sin\left(\frac{-x}{a}\right) e^{j(\omega t - \beta z)} \\ H_z &= A_o \cos\left(\frac{\pi}{a} x\right) e^{j(\omega t - \beta z)} \end{aligned} \right\}$$



(b) Distribution of the electric and magnetic field for TE₁₀ wave in the xOz plane

Field plots

Parameters of TE₁₀ Mode



The cutoff wavelength:

$$\lambda_c = \frac{2}{\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}} = 2a$$

The cutoff frequency:

$$f_c = \frac{\nu}{\lambda_c} = \frac{1}{2a} \frac{c}{\sqrt{\epsilon_r \mu_r}}$$

The phase constant:

$$\beta = k \sqrt{1 - (\lambda / \lambda_c)^2} = k \sqrt{1 - (\lambda / 2a)^2}$$

The waveguide wavelength:

$$\lambda_g = \frac{2\pi}{\beta} = \frac{\lambda}{\sqrt{1 - (\lambda / 2a)^2}}$$

The phase velocity:

$$v_p = \frac{\omega}{\beta} = \frac{\nu}{\sqrt{1 - (\lambda / 2a)^2}}$$



The group velocity:

$$v_g = \nu \sqrt{1 - (\lambda / \lambda_c)^2} = \nu \sqrt{1 - (\lambda / 2a)^2}$$

The wave impedance:

$$Z_{W(TE)} = \frac{\eta}{\sqrt{1 - (\lambda / \lambda_c)^2}} = \frac{\eta}{\sqrt{1 - (\lambda / 2a)^2}}$$



$$P = \dots = \frac{1}{2 \cdot Z} \int_S |\vec{E}|^2 dS$$

$$TE_{10} \quad |E_y| = \dots = \omega \mu \cdot \left(\frac{a}{\pi} \right) \cdot H_{zm} \cdot \left| \sin \left(\frac{\pi}{a} \cdot x \right) \right|^2$$

$$P_{TE_{10}} = \frac{1}{2 \cdot Z_{TE}} \int_S |\vec{E}|^2 dS = \frac{ab}{4 \cdot Z_{TE}} \left(\omega \mu \cdot \left(\frac{a}{\pi} \right) \cdot H_{zm} \right)^2$$



Exercises 10.1, 10.4, 10.6, 10.7

例 若内充空气的矩形波导尺寸为 $\lambda < a < 2\lambda$ ，工作频率为 3GHz。如果要求工作频率至少高于主模 TE_{10} 波的截止频率的 20%，且至少低于 TE_{01} 波的截止频率的 20%。试求：① 波导尺寸 a 及 b ；② 根据所设计的波导，计算工作波长，相速，波导波长及波阻抗。

解 ① TE_{10} 波的截止波长 $\lambda_c = 2a$

对应的截止频率 $f_c = c/\lambda_c = c/2a$ 。

TE_{01} 波的截止波长 $\lambda_c = 2b$ ，

对应的截止频率 $f_c = c/2b$ ，

$$3 \times 10^9 \geq c/2a \times 1.2 \quad 3 \times 10^9 \leq c/2b \times 0.8$$

$$\rightarrow a \geq 0.06m \quad b \leq 0.04m$$

$$\text{取 } a = 0.06m \quad b = 0.04m$$

② 工作波长，相速，波导波长及波阻抗分别

$$\lambda = c/f = 0.1m$$

$$v_p = \frac{c}{\sqrt{1 - \left(\frac{\lambda}{2a} \right)^2}} = 5.42 \times 10^3$$

$$\lambda_g = \frac{\lambda}{\sqrt{1 - \left(\frac{\lambda}{2a} \right)^2}} = 0.182$$

$$Z_{TE_{10}} = \frac{Z}{\sqrt{1 - \left(\frac{\lambda}{2a} \right)^2}} = 682(\Omega)$$

