ASEN 3112 "Lecture" 16: Finite Element Method Examples

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Announcements

- Talk to Dr. Johnson about
 - Homework 7 (FEM): due Friday, March 13
 - Exam 2 (beams, energy methods, FEM): Tuesday, March 17
 - Lab 2: due Thursday, April 2
- ANSYS Tutorial Recitations on Thursday (March 12)
 - Thursday's recitations are for going through the ANSYS Tutorial
 - Section 011
 - Last names A to M: 8:30 am to 9:20 am.
 - Last names N to Z: 9:30 10:20 am
 - Section 012
 - Last names A to K: 2:30 3:20 pm
 - Last names L to Z: 3:30 4:20 pm
- Next week's recitations (Thursday, March 19) will be open office hours focused on Lab 2

Exam 2 Announcements

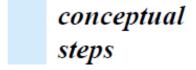
- Exam policies
 - Will have 1 hour and 15 minutes for the exam
 - 4 problems
 - Closed-book
 - Your crib sheet can be one 8.5" x 11" piece of paper with writing on both sides
 - Non-internet-enabled calculators are allow (no phones, laptops)
- Past exams will be posted ASAP

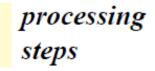
Exam 2 Announcements

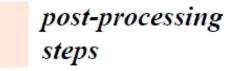
- Did you watch the review videos I posted for Exam 1?
 - a) Yes 42
 - b) No 30
- Do you think you'll come to Monday's office hours (4–6 pm in AERO N240)?
 - a) Definitely yes! 3
 - b) Probably yes 16
 - c) Probably no 77
 - d) Definitely no 75

The Direct Stiffness Method

Disconnection Breakdown Member (Element) Formation Globalization Assembly & Merge Solution **Application of BCs** Solution - unknown displacements **Recovery of Derived Quantities**







Member Stiffness Relations

- For each element, but not showing (e) superscript
- In local coordinates:

$$\begin{bmatrix} f_{xi} \\ \bar{f}_{yi} \\ \bar{f}_{xj} \\ \bar{f}_{yi} \end{bmatrix} = \bar{K} \begin{bmatrix} \bar{u}_{xi} \\ \bar{u}_{yi} \\ \bar{u}_{xj} \\ \bar{u}_{yj} \end{bmatrix} \quad where \quad \bar{K} = \frac{EA}{L} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

In global coordinates:

$$\begin{bmatrix} f_{xi} \\ f_{yi} \\ f_{xj} \\ f_{yj} \end{bmatrix} = \mathbf{K} \begin{bmatrix} u_{xi} \\ u_{yi} \\ u_{xj} \\ u_{yj} \end{bmatrix} \quad \text{where} \quad \mathbf{K} = \frac{EA}{L} \begin{bmatrix} c^2 & sc & -c^2 & -sc \\ sc & s^2 & -sc & -s^2 \\ -c^2 & -sc & c^2 & sc \\ -sc & -s^2 & sc & s^2 \end{bmatrix}$$

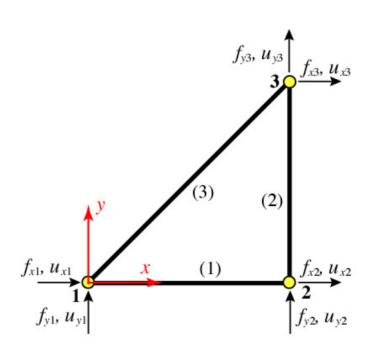
$$or \quad \mathbf{K} = \begin{bmatrix} [\widehat{K}] & [-\widehat{K}] \\ [-\widehat{K}] & [\widehat{K}] \end{bmatrix} \quad \text{where} \quad [\widehat{K}] = \frac{EA}{L} \begin{bmatrix} c^2 & sc \\ sc & s^2 \end{bmatrix}$$

Assembly Process

- Assemble the $[\widehat{K}]$ matrices for each member into the global stiffness matrix.
- Remember our rules!
 - 1. Only have sums of $+[\widehat{K}]$ s on the diagonal.
 - 2. Only have lone $-[\widehat{K}]$ s off the diagonal.
 - 3. The number of $[\widehat{K}]$ s in a diagonal cell shows the number of members at that node
 - 4. All diagonal cells must be filled
 - 5. A cell off the diagonal =0 means those two nodes aren't connected.

Assembly Process without Augmented Stiffness Matrices

$$\begin{bmatrix} \hat{K}^{(e)} \end{bmatrix} = \frac{EA}{L} \begin{bmatrix} c^2 & sc \\ sc & s^2 \end{bmatrix}$$



$$K^{(i)} = \begin{bmatrix} \begin{bmatrix} \hat{k}^{(i)} \end{bmatrix} \begin{bmatrix} -\hat{k}^{(i)} \end{bmatrix} \\ \begin{bmatrix} -\hat{k}^{(i)} \end{bmatrix} \begin{bmatrix} -\hat{k}^{(i)} \end{bmatrix} \end{bmatrix} \begin{bmatrix} \hat{k}^{(i)} \end{bmatrix}$$

Assembly Process of 2x2

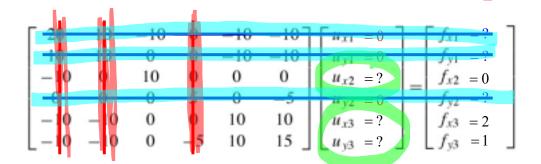
f 2×2 matrices

3×3 matrix

$$K = \begin{bmatrix} \begin{bmatrix} \hat{k}^{(1)} \end{bmatrix} + \begin{bmatrix} \hat{k}^{(2)} \end{bmatrix} \\ \begin{bmatrix} -\hat{k}^{(2)} \end{bmatrix} \end{bmatrix} \begin{bmatrix} -\hat{k}^{(2)} \end{bmatrix} \begin{bmatrix} -\hat{k}^{(2)} \end{bmatrix}$$

$$\begin{bmatrix} -\hat{k}^{(2)} \end{bmatrix} + \begin{bmatrix} \hat{k}^{(2)} \end{bmatrix} + \begin{bmatrix} \hat{k}^{(2)} \end{bmatrix}$$

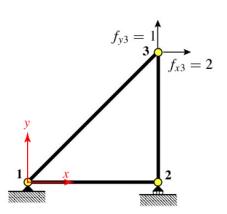
Reduced Global Stiffness Equation



$$\begin{bmatrix} 10 & 0 & 0 \\ 0 & 10 & 10 \\ 0 & 10 & 15 \end{bmatrix} \begin{bmatrix} u_{x2} \\ u_{x3} \\ u_{y3} \end{bmatrix} = \begin{bmatrix} 0 \\ 2 \\ 1 \end{bmatrix}$$

Reduced Global Stiffness Equation (System): $\widetilde{K}\widetilde{u} = \widetilde{f}$

Solution:
$$\begin{bmatrix} u_{x2} \\ u_{x3} \\ u_{u3} \end{bmatrix} = \begin{bmatrix} 0 \\ 0.4 \\ -0.2 \end{bmatrix}$$



Recovery of Reaction Forces & Internal Force/Stress

Small angle approx

$$COSP \approx 1$$
 $COSP \approx 1$
 $COSP \approx 1$

Force Equilibrium at Nodes

Over all node)

$$f_{y3}^{(3)} = f_{y3}^{(2)} + f_{$$

Recovery of Internal Force Through Forces

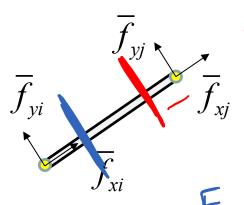
Recovery of Internal Force Through Forces exercal forces

Element Stiffness Equation in global CS:

$$\mathbf{f}^e = \mathbf{K}^e \mathbf{u}^e$$

Transformation from global to local CS:

$$\begin{bmatrix}
\overline{f}_{xi} \\
\overline{f}_{yi} \\
\overline{f}_{xj} \\
\overline{f}_{yj}
\end{bmatrix} = \begin{bmatrix}
c & s & 0 & 0 \\
-s & c & 0 & 0 \\
0 & 0 & c & s \\
0 & 0 & -s & c
\end{bmatrix} \begin{bmatrix}
f_{xi} \\
f_{yi} \\
f_{xj} \\
f_{yj}
\end{bmatrix}$$



Note: for bar element

$$\overline{f}_{yi} = \overline{f}_{yj} = 0$$

internal force

$$F = -\frac{1}{3}xi \times$$

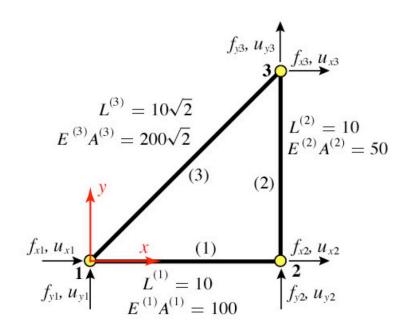
$$F = -f_{xi} = -(cos y f_{xi} + sin y f_{yi})$$

$$F = +f_{xi} = cos y f_{xi} + sin y f_{xi}$$

Example with Example Truss

Example: Bar 2 Using nodal solution for Bar 2:

$$\mathbf{f}^{e} = \mathbf{K}^{e} \mathbf{u}^{e} \begin{bmatrix} 0.0 \\ 1.0 \\ 0.0 \\ -1.0 \end{bmatrix} = 5 \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 \\ 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0.0 \\ 0.0 \\ 0.4 \\ -0.2 \end{bmatrix}$$



$$F = -\overline{f}_{xi} = -\left(c \ f_{xi} + s \ f_{yi}\right) \quad or \quad F = \overline{f}_{xj} = \left(c \ f_{xj} + s \ f_{yj}\right)$$

for $\cos 90 = 0 \quad \sin 90 = 1$

$$F = -\overline{f}_{xi} = -(0 \cdot 0 + 1 \cdot 1) = -1$$
 or $F = \overline{f}_{xi} = (0 \cdot 0 + 1 \cdot -1) = -1$

Calculate U 1. Calculate force of nodes it jon bor (e) f (e) = K (e) u (e) 2. Then do translation to local coord. $F_{int} = -\frac{1}{5}(e) = -\left(\cos \varphi f_{xi}^{(e)} + \sin \varphi f_{yi}^{(e)}\right)$ $F_{int} + f_{xj}^{(e)} = \cos \varphi f_{xj}^{(e)} + \sin \varphi f_{y,i}^{(e)}$ 3. $\sigma = \frac{F_{int}}{\Delta}$

