

ASEN 3112

Spring 2020

Lecture 1

January 14, 2020

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Stress in 3D

Mechanical Stress in 3D: Concept

Mechanical stress measures *intensity level* of *internal forces* in a material (solid or fluid body) idealized as a mathematical *continuum*. The physical measure of stress is

Force per unit area e.g. N/mm^2 (MPa) or lbs/sq-in (psi)

This measure is convenient to assess the resistance of a material to permanent deformation (yield, creep, slip) and rupture (fracture, cracking). Comparing working and failure stress levels allows engineers to establish *strength safety factors* for structures.

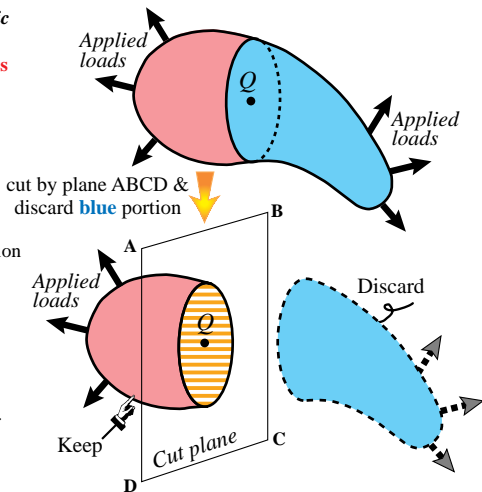
Stresses may vary from point to point. We next consider a solid body (could be a structure or part of one) in 3D.

Cutting a 3D Body



Consider a 3D solid body in *static equilibrium* under applied loads. We want to find the **state of stress** at an arbitrary point Q , which generally will be inside the body.

Cut the body by a *plane* ABCD that passes through Q as shown (How to *orient* the plane is discussed later.) The body is divided into two. Retain one portion (**red** in figure) and discard the other (**blue** in figure)

To *restore equilibrium*, however, we must replace the discarded portion by the *internal forces* it had exerted on the kept portion.



Orienting the Cut Plane

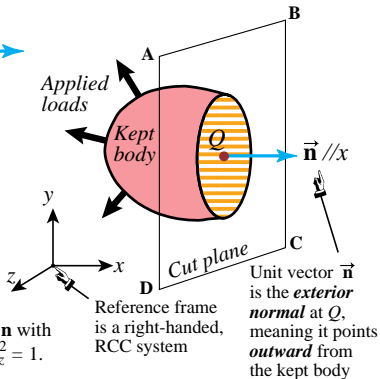
The cut plane ABCD is oriented by its unit normal direction vector \mathbf{n} , or *normal*  for short. By convention we will draw \mathbf{n} as emerging from Q  and pointing *outward* from the kept body. This direction identifies the *exterior normal*.

With respect to the RCC system $\{x, y, z\}$, the normal vector has components

$$\mathbf{n} = \begin{bmatrix} n_x \\ n_y \\ n_z \end{bmatrix}$$

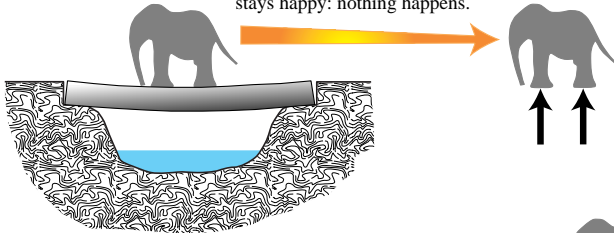
where $\{n_x, n_y, n_z\}$ are the direction cosines of \mathbf{n} with respect to $\{x, y, z\}$. These satisfy $n_x^2 + n_y^2 + n_z^2 = 1$.

In the figure, the cut plane ABCD has been chosen with its exterior normal *parallel* to the $+x$ axis. Consequently $\mathbf{n} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$

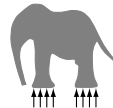


Digression: Action and Reaction (Newton's 3rd Law, from Physics I)

Remove the "bridge" (log) and replace its effect on the elephant by **reaction forces** on the legs. The elephant stays happy: nothing happens.





Strictly speaking, reaction forces are ***distributed*** over the elephant leg contact areas. They are replaced above by equivalent point forces, a.k.a. ***resultants***, for visualization convenience

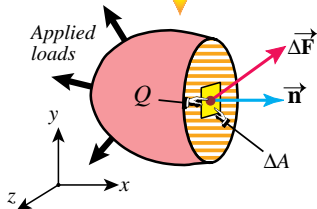
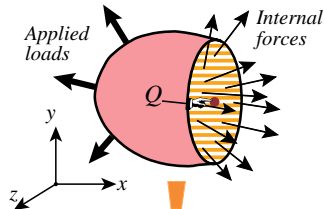


Internal Forces on Cut Plane

Those internal forces generally will form a system of ***distributed forces per unit of area***, which, being vectors, generally will vary in magnitude and direction as we move from point to point of the cut plane, as pictured.

Next, we focus our attention on point Q ●. Pick an ***elemental area*** ΔA around Q that lies on the cut plane. Call $\Delta \mathbf{F}$ the ***resultant*** of the internal forces that act on ΔA . Draw that vector  with origin at Q , as pictured. Don't forget the normal 

The use of the increment symbol Δ suggests a pass to the limit. This will be done later to define the stresses at Q



Arrows are placed over $\Delta \mathbf{F}$ and \mathbf{n} to remind you that they are ***vectors***

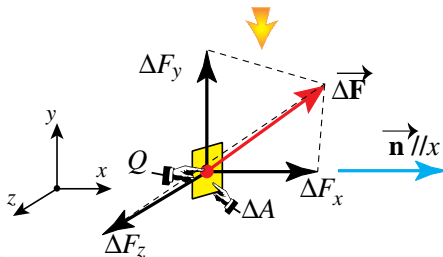
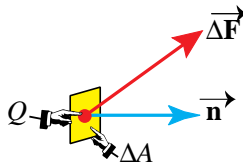
Internal Force Components

Zoom on the elemental area about Q , omitting the kept-body and applied loads for clarity:

Project vector $\Delta \mathbf{F}$ on axes x , y and z to get its components ΔF_x , ΔF_y and ΔF_z , respectively. See bottom figure.

Note that component ΔF_x is aligned with the cut-plane normal, because \mathbf{n} is parallel to x . It is called the **normal internal force** component.

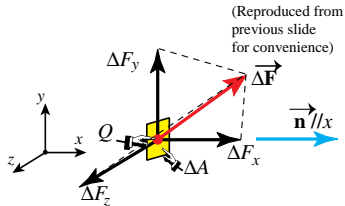
Components ΔF_y and ΔF_z lie on the cut plane. They are called **tangential internal force** components.



We are now ready to define stresses.

Stress Components at a Point: x Cut

Define the **x -stress components** at point Q by taking the limits of internal-force-over-area ratios as the elemental area shrinks to zero:



$$\sigma_{xx} \stackrel{\text{def}}{=} \lim_{\Delta A \rightarrow 0} \frac{\Delta F_x}{\Delta A} \quad \tau_{xy} \stackrel{\text{def}}{=} \lim_{\Delta A \rightarrow 0} \frac{\Delta F_y}{\Delta A} \quad \tau_{xz} \stackrel{\text{def}}{=} \lim_{\Delta A \rightarrow 0} \frac{\Delta F_z}{\Delta A}$$

σ_{xx} is called a **normal stress**, whereas τ_{xy} and τ_{xz} are **shear stresses**.

Stress Components at a Point: y and z Cuts

It turns out we need *nine* stress components in 3D to fully characterize the stress state at a point. So far we got only three. Six more are obtained by repeating the same take-the-limit procedure with *two other cut planes*. The obvious choice is to pick planes normal to the other two axes: y and z.

Taking \mathbf{n}/y we get three more components, one normal and two shear:

$$\sigma_{yy} \quad \tau_{yx} \quad \tau_{yz}$$

These are called *y-stress components*.

Taking \mathbf{n}/z we get three more components, one normal and two shear:

$$\sigma_{zz} \quad \tau_{zx} \quad \tau_{zy}$$

These are called *z-stress components*.

Together with the three *y-stress components* found before, this makes up a total of nine, as required.