ASEN 3112 Lecture 15: Finite Element Method 3

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Announcements

- Upcoming due dates
 - Homework 6 (energy methods): tomorrow, Friday, March 6
 - Homework 7 (FEM): Friday, March 13
 - Exam 2 (beams, energy methods, FEM): Tuesday, March 17
- Note that the FEM recitation is after HW7 and Exam 2

- My Office Hours (all in AERO 302)
 - Tuesday, March 10, 9:00 10:00 am
 - Thursday, March 12, 11:30 am 12:30 pm
 - Then by appointment

Finite Element Methods Outline

- Last class (Ch. 16 & 17)
 - Member stiffness equations
- * Today (Ch. 17 & 18)
 - Transforming from local to global coordinates
 - Understanding the global stiffness matrix
- ★ Thursday, March 5 (Ch. 18)
 - Assembling the global stiffness matrix
 - Applying boundary conditions to solve
- Tuesday, March 10
 - Examples
 - Exam 2 review?

The Direct Stiffness Method

Breakdown

Disconnection
Localization
Member (Element) Formation

Assembly & Solution

Globalization

Merge

Application of BCs

Solution

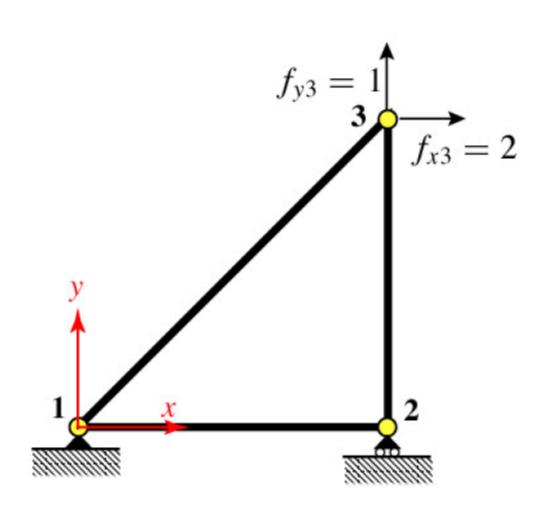
Recovery of Derived Quantities

conceptual steps

processing steps

post-processing steps

Our Example Truss



Member Stiffness Relations

- For each element, but not showing (e) superscript
- In local coordinates:

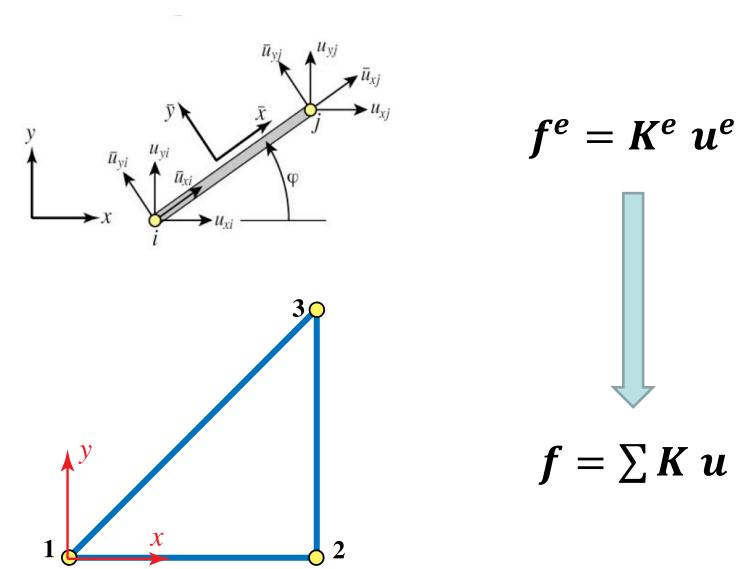
$$\begin{bmatrix} f_{xi} \\ \bar{f}_{yi} \\ \bar{f}_{xj} \\ \bar{f}_{yj} \end{bmatrix} = \overline{K} \begin{bmatrix} \overline{u}_{xi} \\ \overline{u}_{yi} \\ \overline{u}_{xj} \\ \overline{u}_{yj} \end{bmatrix} \quad where \quad \overline{K} = \frac{EA}{L} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

In global coordinates:

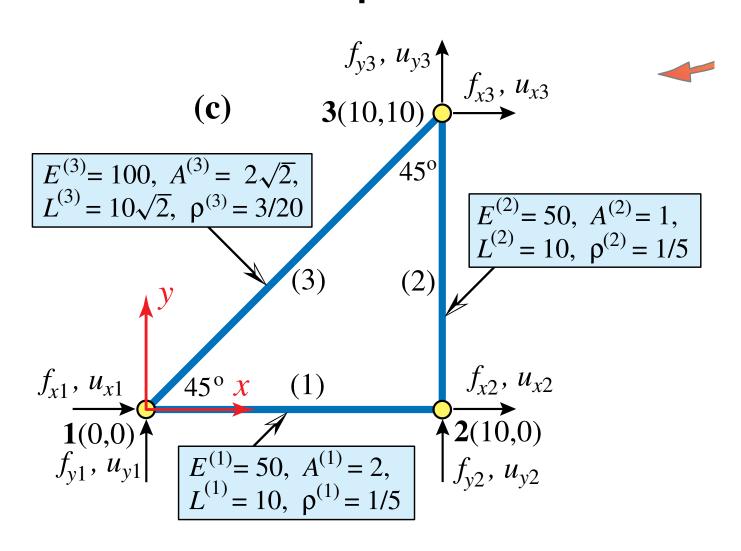
$$\begin{bmatrix} f_{xi} \\ f_{yi} \\ f_{xj} \\ f_{yj} \end{bmatrix} = \mathbf{K} \begin{bmatrix} u_{xi} \\ u_{yi} \\ u_{xj} \\ u_{yj} \end{bmatrix} \quad \text{where} \quad \mathbf{K} = \frac{EA}{L} \begin{bmatrix} c^2 & sc & -c^2 & sc \\ sc & s^2 & sc & -s^2 \\ -c^2 & sc & c^2 & sc \\ sc & -s^2 & sc & s^2 \end{bmatrix}$$

$$or \quad \mathbf{K} = \begin{bmatrix} [\widehat{K}] & [-\widehat{K}] \\ [-\widehat{K}] & [\widehat{K}] \end{bmatrix} \quad \text{where} \quad [\widehat{K}] = \frac{EA}{L} \begin{bmatrix} c^2 & sc \\ sc & s^2 \end{bmatrix}$$

Global Stiffness Relations

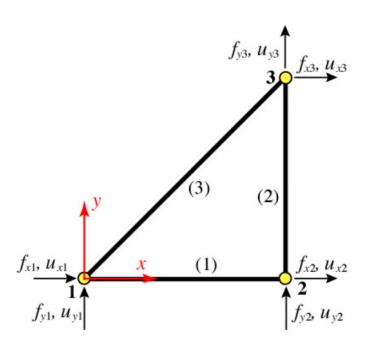


Member Properties in Our Example Truss



Augmented Stiffness Matrices

- Element stiffness equation augmented by "missing" DOFs to yield 6 equations
- Only done for illustration purposes; step not explicitly needed

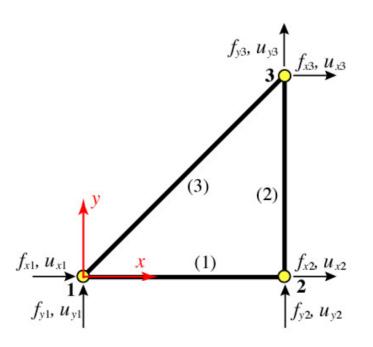


Bar 1:

$$\begin{bmatrix} f_{x1}^{(1)} \\ f_{y1}^{(1)} \\ f_{x2}^{(1)} \\ f_{y2}^{(1)} \end{bmatrix} = 10 \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} u_{x1}^{(1)} \\ u_{y1}^{(1)} \\ u_{y2}^{(1)} \\ u_{y2}^{(1)} \end{bmatrix}$$

Augmented Stiffness Matrices

- Element stiffness equation augmented by "missing" DOFs to yield 6 equations
- Only done for illustration purposes; step not explicitly needed



Bar 1: $f_{y1}^{(1)} \\ f_{x2}^{(1)} \\ f_{x2}^{(1)} \\ f_{y2}^{(1)}$ 0 0 0 0 0 $f_{x3}^{(1)}$ 0

 u_{y2} u_{x3} 0 0 0 0 $f_{y3}^{(1)}$ u_{y3} $\overline{f_{x1}^{(2)}}$ Bar 2: 0 0 0 0 u_{x1}

 u_{x1}

 u_{u1}

 u_{x2}

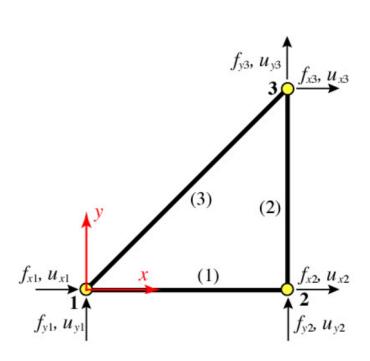
 u_{v1}

0 0 $f_{x2}^{(2)}$ u_{x2} u_{u2} 0 u_{x3} 5 u_{y3}

Bar 3: 10 10 -10-10 u_{x1} £(3) 10 u_{u1} $f_{x2}^{(3)}$ 0 0 u_{x2} $f_{y2}^{(3)}$ 0 u_{y2} $f_{x3}^{(3)}$ 10 10 u_{x3} 10 10 $f_{y3}^{(3)}$ u_{y3}

Global Stiffness Equation

Assembly Process without Augmented Stiffness Matrices



Assembly Process

K =		

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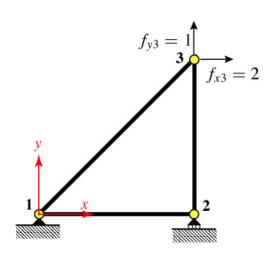
Recovery of Derived Quantities

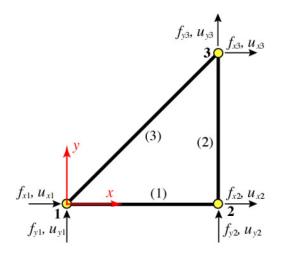
conceptual steps

processing steps

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Applying Boundary Conditions





Displacement BCs:

$$u_{x1} = u_{y1} = u_{y2} = 0$$

Force BCs:

$$f_{x2} = 0$$
, $f_{x3} = 2$, $f_{y3} = 1$

 u_{x1}

 u_{y1}

 u_{x2}

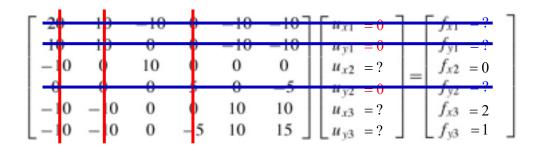
 u_{y2}

 u_{x3}

Global stiffness equation:

$$\begin{bmatrix} f_{x1} \\ f_{y1} \\ f_{x2} \\ f_{y2} \\ f_{x3} \\ f_{y3} \end{bmatrix} = \begin{bmatrix} 20 & 10 & -10 & 0 & -10 & -10 \\ 10 & 10 & 0 & 0 & -10 & -10 \\ -10 & 0 & 10 & 0 & 0 & 0 \\ 0 & 0 & 0 & 5 & 0 & -5 \\ -10 & -10 & 0 & 0 & 10 & 10 \\ -10 & -10 & 0 & -5 & 10 & 15 \end{bmatrix}$$

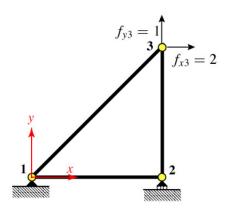
Reduced Global Stiffness Equation



$$\begin{bmatrix} 10 & 0 & 0 \\ 0 & 10 & 10 \\ 0 & 10 & 15 \end{bmatrix} \begin{bmatrix} u_{x2} \\ u_{x3} \\ u_{y3} \end{bmatrix} = \begin{bmatrix} 0 \\ 2 \\ 1 \end{bmatrix}$$

Reduced Global Stiffness Equation (System): $\widetilde{K}\widetilde{u} = \widetilde{f}$

Solution:
$$\begin{bmatrix} u_{x2} \\ u_{x3} \\ u_{y3} \end{bmatrix} = \begin{bmatrix} 0 \\ 0.4 \\ -0.2 \end{bmatrix}$$



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Recovery of Reaction Forces

Complete Displacement Solution:

$$\begin{bmatrix} u_{x2} \\ u_{x3} \\ u_{y3} \end{bmatrix} = \begin{bmatrix} 0 \\ 0.4 \\ -0.2 \end{bmatrix}$$

Displacement BCs:

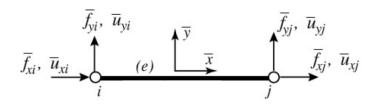
$$u_{x1} = u_{y1} = u_{y2} = 0$$

$$\begin{bmatrix} u_{x1} \\ u_{y1} \\ u_{x2} \\ u_{y2} \\ u_{x3} \\ u_{y3} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0.4 \\ -0.2 \end{bmatrix}$$

Complete Force Vector:

$$\mathbf{f} = \mathbf{K}\mathbf{u} = \begin{bmatrix} 20 & 10 & -10 & 0 & -10 & -10 \\ 10 & 10 & 0 & 0 & -10 & -10 \\ -10 & 0 & 10 & 0 & 0 & 0 \\ 0 & 0 & 0 & 5 & 0 & -5 \\ -10 & -10 & 0 & 0 & 10 & 10 \\ -10 & -10 & 0 & -5 & 10 & 15 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0.4 \\ -0.2 \end{bmatrix} = \begin{bmatrix} -2 \\ -2 \\ 0 \\ 0.4 \\ -0.2 \end{bmatrix} \text{ support reactions recovers applied external forces}$$

Recovery of Internal Stress Through Displacements



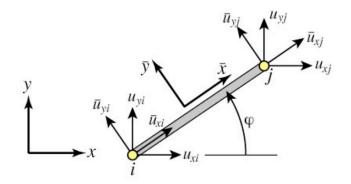
Transformation from global to local CS:

$$\begin{bmatrix}
\overline{u}_{xi} \\
\overline{u}_{yi} \\
\overline{u}_{xj} \\
\overline{u}_{yj}
\end{bmatrix} = \begin{bmatrix}
c & s & 0 & 0 \\
-s & c & 0 & 0 \\
0 & 0 & c & s \\
0 & 0 & -s & c
\end{bmatrix} \begin{bmatrix}
u_{xi} \\
u_{yi} \\
u_{xj} \\
u_{yj}
\end{bmatrix}$$

$$\overline{\mathbf{u}}^{e}$$

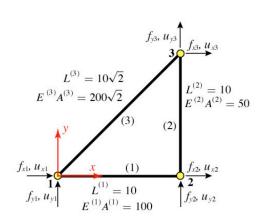
$$\mathbf{T}^{e}$$

$$\mathbf{u}^{e}$$



Recovery of Internal Stress Through Displacements

Example: Bar 2



$$\begin{bmatrix} \bar{u}_{x2} \\ \bar{u}_{y2} \\ \bar{u}_{x3} \\ \bar{u}_{y3} \end{bmatrix} = \begin{bmatrix} \cos 90^{\circ} & \sin 90^{\circ} & 0 & 0 \\ -\sin 90^{\circ} & \cos 90^{\circ} & 0 & 0 \\ 0 & 0 & \cos 90^{\circ} & \sin 90^{\circ} \\ 0 & 0 & -\sin 90^{\circ} & \cos 90^{\circ} \end{bmatrix} \begin{bmatrix} u_{x2} \\ u_{y2} \\ u_{x3} \\ u_{y3} \end{bmatrix}$$

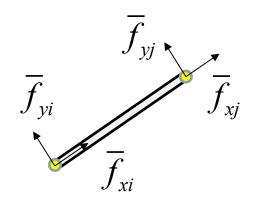
$$\Delta L^{(3)} = \overline{u}_{x3} - \overline{u}_{x2} = -0.2$$

$$F^{(3)} = \frac{\left(EA\right)^{(3)}}{L^{(3)}} \Delta L^{(3)} = -\frac{50}{10} 0.2 = -1$$

Recovery of Internal Stress Through Forces

Element Stiffness Equation in global CS:

$$\mathbf{f}^e = \mathbf{K}^e \mathbf{u}^e$$



Note: for bar element

$$\overline{f}_{yi} = \overline{f}_{yj} = 0$$

Transformation from global to local CS:

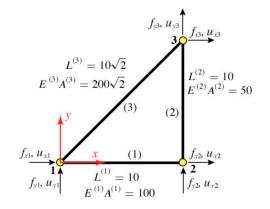
$$\begin{bmatrix}
\overline{f}_{xi} \\
\overline{f}_{yi} \\
\overline{f}_{xj} \\
\overline{f}_{yj}
\end{bmatrix} = \begin{bmatrix}
c & s & 0 & 0 \\
-s & c & 0 & 0 \\
0 & 0 & c & s \\
0 & 0 & -s & c
\end{bmatrix} \begin{bmatrix}
f_{xi} \\
f_{yi} \\
f_{xj} \\
f_{yj}
\end{bmatrix}$$

$$\mathbf{T}^{e}$$

Recovery of Internal Stress Through Forces

Example: Bar 2 Using nodal solution for Bar 2:

$$\mathbf{f}^e = \mathbf{K}^e \mathbf{u}^e \qquad \begin{vmatrix} 0.0 \\ 1.0 \\ 0.0 \\ -1.0 \end{vmatrix} = 5 \begin{vmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 \\ 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \end{vmatrix} \begin{vmatrix} 0.0 \\ 0.0 \\ 0.4 \\ -0.2 \end{vmatrix}$$



$$F = -\overline{f}_{xi} = -\left(c \ f_{xi} + s \ f_{yi}\right) \quad or \quad F = \overline{f}_{xj} = \left(c \ f_{xj} + s \ f_{yj}\right)$$

for $\cos 90 = 0 \quad \sin 90 = 1$

$$F = -\overline{f}_{xi} = -(0 \cdot 0 + 1 \cdot 1) = -1$$
 or $F = \overline{f}_{xj} = (0 \cdot 0 + 1 \cdot -1) = -1$

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