# ASEN 3112 Lecture 8: Beam Differential Equations

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#### Exam 1 Announcements

- Syllabus has been updated with new exam make up policy
- In class next Tuesday, Feb. 11
- Covers Ch. 1-9 of textbook
- If you have an accommodation, respond to my e-mail or send me an e-mail if you didn't get one

#### Exam 1 Announcements

- Exam policies
  - Will have 1 hour and 15 minutes for the exam
  - 3-4 problems?
  - Closed-book
  - Your crib sheet can be one 8.5" x 11" piece of paper with writing
     on both sides
  - Non-internet-enabled calculators are allow (no phones, laptops)
- Past exams posted
- Will post a review video ASAP

#### Announcements

- Lecture capture videos are posted to Canvas
  - We trust that you won't just skip class
- Lab 1 video and the associated individual quiz will be posted later today
- Homework 2 is graded and posted to Canvas and Gradescope
- Pre-exam office hours
  - Monday, 4:00 6:00 pm in AERO N240
  - Tuesday, 9:00 10:00 am in AERO 302

#### This Week's Outline

- Applying beam bending differential equations (Ch. 11)
  - Finding deflection with 2<sup>nd</sup> and 4<sup>th</sup> order ODEs
  - Boundary conditions
  - Matching conditions
  - Solving statically indeterminate problems with superposition
- Note: Ch. 12 is not covered in this course.

## Beam Notation & Sign Conventions

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Quantity	Symbol	Sign convention(s)
Problem specific load	varies	You pick'em
Generic load for ODE work	p(x)	+ if up
Transverse shear force	$V_{y}\left( x\right)$	+ if up on +x face
Bending moment	$M_z(x)$	+ if it produces compression on top face
Slope of deflection curve	dv(x)/dx = v'(x)	+ if positive slope, or cross-section rotates CCW
Deflection curve	v(x)	+ if beam cross-section moves upward

Note 1: Some textbooks (e.g. Vable and Beer-Johnson-DeWolf) use  $V = -V_y$  as alternative transverse shear force symbol. This has the advantage of eliminating the minus sign in two of the ODEs listed on the next slide. V will only be used occsionally in this course.

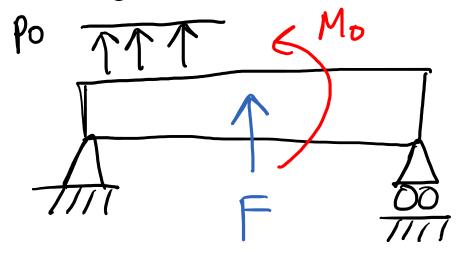
Note 2. In our beam model, the slope v'(x) = dv(x)/dx is equal to the rotation  $\theta(x)$  of the cross section

#### **Beam Differential Equations**

Connected quantities	Ordinary Differential Equations (ODEs)
From load to transverse shear force	$\frac{dV_y}{dx} = -p  \text{or } p = -V_y' = V'$
From transverse shear to bending moment	$\frac{dM_z}{dx} = -V_y  \text{or } M_z' = -V_y = V$
From bending moment to deflection	$E I_{zz}v'' = M_z  or  v'' = \frac{M_z}{E I_{zz}}$
From load to moment	$M_z^{"}=p$
From load to deflection	$E I_{zz} v^{IV} = p$

## **Ungraded Clicker Question**

 Right now, I am confident that I could find V(x), M(x), and the max bending stress for this beam?



- a) Strongly agree
- b) Agree
- c) Disagree
- d) Strongly disagree

$$p(x) \quad \nabla(x) \quad M(x) \quad \theta(x) \quad \nabla(x)$$

$$-p(x) = \nabla'(x) \qquad M(x) = EIB'(x) \quad \theta(x) = \nabla'(x)$$

$$-\nabla(x) = M'(x) \qquad ||(z)|$$
We defined  $K = \frac{\partial \theta}{\partial s_0} = \frac{\partial \theta}{\partial x} = \theta'(x) = \nabla''(x)$ 
We also defined  $M = EIK$ 

$$M(x) = EI_{v''(x)}$$
 $V(x) = -EI_{v'''(x)}$ 
 $p(x) = EI_{v'''(x)}$ 

Typically 
$$p(x)$$
 known
$$\int p(x) \Rightarrow -\nabla(x)$$

$$\int p(x) \Rightarrow M(x)$$

$$\int p(x) \Rightarrow M(x)$$

$$\int p(x) \Rightarrow \nabla(x)$$

$$\int p(x) \Rightarrow \nabla(x)$$

$$\sigma = \frac{My}{T}$$

TAM for statically det. beams  $\neq S(EI)$  Ex. | Given po, L, E, I TTTTPO Find v(x) X=D ODE method p(x)= Po = EIv"(x)  $p_{\delta} \times + C_{1} = E I \sigma''(x) = T T(x)$  $\frac{1}{2}\rho_{\delta}x^{2} + C_{1}x + C_{2} = E I v''(x) = M(x) \leftarrow$ 1/6 ρ<sub>8</sub> x 3 + 2 C, x 2 + C<sub>2</sub> x + (3 = E I v '(x)) 1/24 Pox 4 + = C1x 3 + = (2x2+(3x+(4=EIV(x)

2nd order ODE method Find M(x) by cuts. 1. Global FBD  $P_{0} \times R_{A} = \frac{1}{2} p_{0} L \qquad R_{B} = \frac{1}{2} p_{0} L$   $P_{0} \times R_{A} = \frac{1}{2} p_{0} L \qquad R_{B} = \frac{1}{2} p_{0} L$  $\frac{1}{z}\rho_{\delta}L$   $M(x) = \frac{1}{z}\rho_{\delta}x^{2} - \frac{1}{z}\rho_{\delta}Lx$  $M(x) = \frac{1}{z} \rho_0 x^2 - \frac{1}{z} \rho_0 L x = E \mathbf{T} r''(x)$  $\frac{1}{6}\rho_{6} \times^{3} - \frac{1}{4}\rho_{0}L \times^{2} + C_{3} = EIv'(x)$ 1/24 Pox 4 - 1/2 po Lx3+ C3x + C4 = EIV(x)

2nd order Conditions Boun dary (r(L)=D V(0)=0 M(L) = 0 M(0)20 i @ B ath ode Planed Jointe A Do we easily know Joint Image Pinned/ Roller Clamped Free

M(L) = 0  $EF \Rightarrow V(L) = 0$   $EM \Rightarrow M(L) = M_0$   $V(L) = M_0$ 

Assume so small  $(\partial x \rightarrow 0)$  p(x) has no effect forces don't cause moments

$$EI_{V(x)} = \frac{1}{2u} \rho_{0} x^{4} - \frac{1}{12} \rho_{0} l x^{3} + l_{3} x + l_{7} y$$

$$0 = 0 + 0 + 0 = l_{7} y$$

$$2 v(l) = 0 = \frac{1}{2u} \rho_{0} l^{4} - \frac{1}{12} \rho_{0} l^{4}$$

$$+ l_{3} l + 0$$

$$(3 = \frac{1}{2u} \rho_{0} l^{3})$$

Ex. 2 Critical points Force 1. External 2. External moment 3\_ Change in p(x) At critical points, me have a plecewisi function INTEGRATE EACH PIECE  $(x) = \begin{cases} \rho_1(x) & 0 \leq x \leq \frac{1}{2} \\ \rho_2(x) & \frac{1}{2} \leq x \leq L \end{cases}$ 2005×57

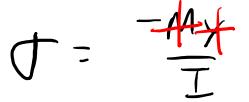
Matching Conditions PLX) doesn't Mi( $\frac{1}{z}$ ) Mo S | Moments

Moments

Moments

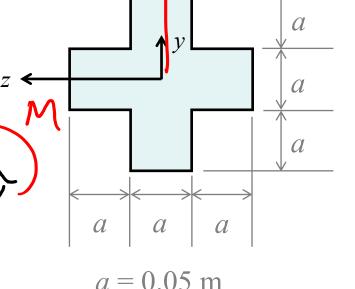
Ti( $\frac{1}{z}$ ) =  $V_2(\frac{1}{z})$ 2Fy=0= V2(2)-V,(2)+F  $\nabla_{z}(\frac{1}{z}) - \nabla_{z}(\frac{1}{z}) = -F - M_{o}$   $\leq M = D - M_{z}(\frac{1}{z}) - M_{z}(\frac{1}{z}) + M_{o} M_{z}(\frac{1}{z}) - M_{z}(\frac{1}{z})^{z}$ 

## Question 1



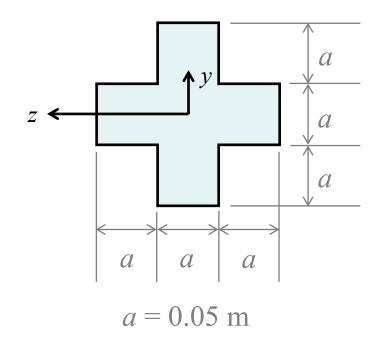
• A beam has the following cross-section. The centroid of the cross-section is right in the middle. At this particular point along the length of the beam, the shear force across the cross-section is V = -40 kN and the bending moment is  $M = +\frac{100}{3} = +33.\overline{3}$  kN-m.

- Is the top of the beam in tension or compression?
  - a) Tension
  - b) Compression



### Question 2

- A beam has the following cross-section. The centroid of the cross-section is right in the middle. At this particular point along the length of the beam, the shear force across the cross-section is V = -40 kN and the bending moment is  $M = + \frac{100}{3} = +33.\overline{3}$  kN-m.
- What is the relationship between the maximum tensile and maximum compressive bending stresses?
  - a) Tensile is larger
  - b) Compressive is larger
  - c) They are the same



## Question 4

O= My

 A cantilever (fixed) beam is loaded with a point load P. If we know the material will fail in COMPRESSION, which point is more likely to fail first:

