

Warming up RBC (McKay) Analytics

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1 Problem

Assume that preferences are given by:

$$\mathbb{E} \sum_{t=0}^{\infty} \beta^t \frac{C_t^{1-\gamma}}{1-\gamma} \quad (1)$$

while

$$Y_t = Z_t K_{t-1}^{\alpha} \bar{L}^{1-\alpha} \quad (2)$$

Production Function

$$Y_t = C_t + I_t \quad (3)$$

Resource Constraint

$$K_t = (1 - \delta)K_{t-1} + I_t \quad (4)$$

Law of Motion of Capital

$$\log Z_t = \rho \log Z_{t-1} + \epsilon_t \quad (5)$$

Productivity Shock process

Combining (3) and (4) we get:

$$Y_t = K_t - (1 - \delta)K_{t-1} + C_t \quad (6)$$

So, now the problem states as ¹:

$$L = \mathbb{E} \sum_{t=0}^{\infty} \beta^t \left\{ \frac{C_t^{1-\gamma}}{1-\gamma} + \lambda_t [Z_t K_{t-1}^{\alpha} \bar{L}^{1-\alpha} + (1 - \delta)K_{t-1} - K_t - C_t] \right\} \quad (7)$$

¹we could omit \bar{L} (as we do next) since labor supply is exogenously given

FOC

C_t :

$$\beta^t(C_t^{-\gamma} - \lambda_t) = 0 \rightarrow \lambda_t = C_t^{-\gamma} \quad (8)$$

K_t :

$$\begin{aligned} \beta^t(-\lambda_t) + \beta^{t+1}\mathbb{E}\{\lambda_{t+1}(\alpha Z_{t+1}K_t^{\alpha-1}\bar{L}^{1-\alpha} + 1 - \delta)\} &= 0 \\ \lambda_t &= \beta\mathbb{E}\{\lambda_{t+1}(\alpha Z_{t+1}K_t^{\alpha-1}\bar{L}^{\alpha-1} + 1 - \delta)\} \end{aligned} \quad (9)$$

Combining (8) and (9) we get:

$$C_t^{-\gamma} = \beta\mathbb{E}\{C_{t+1}^{-\gamma}(\alpha Z_{t+1}K_t^{\alpha-1}\bar{L}^{1-\alpha} + 1 - \delta)\} \quad (10)$$

Denoting the gross real interest rate as $R_{t+1} = \alpha Z_{t+1}K_t^{\alpha-1}\bar{L}^{1-\alpha} + 1 - \delta$, we get:

$$\boxed{C_t^{-\gamma} = \beta\mathbb{E}[R_{t+1}C_{t+1}^{-\gamma}]} \quad (11)$$

Euler for Consumption

Equilibrium

We have a system of 5 equations on 5 unknowns $\{C_t, R_t, K_t, Y_t, Z_t\}$

$$C_t^{-\gamma} = \beta \mathbb{E}(R_{t+1} C_{t+1}^{-\gamma}) \quad (12)$$

$$R_t = \alpha Z_t K_{t-1}^{\alpha-1} \bar{L}^{1-\alpha} + 1 - \delta \quad (13)$$

$$K_t = (1 - \delta) K_{t-1} + Y_t - C_t \quad (14)$$

$$Y_t = Z_t K_{t-1}^{\alpha} \bar{L}^{1-\alpha} \quad (15)$$

$$\log Z_t = \rho \log Z_{t-1} + \epsilon_t \quad (16)$$

Steady State

Equation (12) becomes:

$$\begin{aligned} C^{-\gamma} &= \beta R C^{-\gamma} \\ R &= \frac{1}{\beta} \end{aligned} \quad (17)$$

Equation (13) becomes:

$$\begin{aligned} R &= \alpha Z K^{\alpha-1} \bar{L}^{1-\alpha} + (1 - \delta) \\ K &= \left[\frac{R - 1 + \delta}{\alpha} \right]^{\frac{1}{\alpha-1}} \end{aligned} \quad (18)$$

Equation (14) becomes:

$$C = Y - \delta K \quad (19)$$

Equation (15) becomes:

$$Y = K^{\alpha} \quad (20)$$

Equation (16) becomes:

$$Z = 1 \quad (21)$$

Log-Linearization

Let's start by loglinearizing equation (12):

$$C_t^{-\gamma} = \beta \mathbb{E}[R_{t+1} C_{t+1}^{-\gamma}]$$

Taking logs on both sides

$$-\gamma \log(C_t) = \log(\beta) + \log(R_{t+1}) - \gamma \log(C_{t+1})$$

Taking a First Order Taylor Expansion (FOTE):

$$\begin{aligned} -\gamma \log(C) - \gamma \frac{1}{C} (C_t - C) = \\ \log(\beta) + \log(R) + \frac{1}{R} (R_{t+1} - R) - \gamma \log(C) - \frac{\gamma}{C} (C_{t+1} - C) \end{aligned}$$

We know that in SS:

$$\log(R) = -\log(\beta)$$

so, we have that:

$$\begin{aligned} \frac{-\gamma}{C} (C_t - C) &= \frac{1}{R} (R_{t+1} - R) - \frac{\gamma}{C} (C_{t+1} - C) \\ -\gamma \tilde{c}_t &= \tilde{r}_{t+1} - \gamma \tilde{c}_{t+1} \\ \boxed{\tilde{c}_{t+1} - \tilde{c}_t &= \frac{1}{\gamma} \tilde{r}_{t+1}} \end{aligned} \tag{22}$$

This is the log-linearized Euler for Consumption.

Now let's log-linearize (15)

$$Y_t = Z_t K_{t-1}^\alpha \bar{L}^{1-\alpha}$$

Following the same steps as before we get:

$$\begin{aligned} \log(Y) + \frac{1}{Y} (Y_t - Y) &= \log(Z) + \frac{1}{Z} (Z_t - Z) + \alpha \log(K) + \frac{\alpha}{K} (K_{t-1} - K) \\ \frac{1}{Y} (Y_t - Y) &= \frac{1}{Z} (Z_t - Z) + \frac{\alpha}{K} (K_{t-1} - K) \end{aligned}$$

$$\boxed{\tilde{y}_t = \zeta_t + \alpha \tilde{k}_{t-1}} \tag{23}$$

This is the log-linearized Production Function.

Note that ζ_t is the $\log(Z_t)$ since $\log(\frac{Z_t}{Z}) = \log(Z_t)$ because $\log(Z) = 0$

Let's log-linearize (14)

$$K_t = (1 - \delta)K_{t-1} + Y_t - C_t$$

$$\log(K) + \frac{1}{K}(K_t - K) = \log[(1 - \delta)K + Y - C] + \frac{1(1-\delta)}{(1-\delta)K+Y-C}(K_{t-1} - K) + \frac{1}{(1-\delta)K+Y-C}(Y_t - Y) - \frac{1}{(1-\delta)K+Y-C}(C_t - C)$$

$$\frac{1}{K}(K_t - K) = \frac{1-\delta}{(1-\delta)K+Y-C}(K_{t-1} - K) + \frac{1}{(1-\delta)K+Y-C}(Y_t - Y) - \frac{1}{(1-\delta)K+Y-C}(C_t - C)$$

$$\frac{1}{K}(K_t - K) = \frac{1-\delta}{K}(K_{t-1} - K) + \frac{1}{K}(Y_t - Y) - \frac{1}{K}(C_t - C)$$

where we have used that in SS: $K = (1 - \delta)K + Y - C$

Now, we multiply and divide by Y,C where appropriate

$$\tilde{k}_t = (1 - \delta)\tilde{k}_{t-1} + \frac{Y}{K} \frac{(Y_t - Y)}{Y} - \frac{C}{K} \frac{(C_t - C)}{C}$$

$$\tilde{k}_t = (1 - \delta)\tilde{k}_{t-1} + \frac{Y}{K} \tilde{y}_t - \frac{C}{K} \tilde{c}_t$$

If you check the equilibrium conditions: $\frac{Y}{K} = \frac{R-1+\delta}{\alpha}$ and $\frac{C}{K} = \frac{R-1+\delta(1-\alpha)}{\alpha}$

so, we get

$$\boxed{\tilde{k}_t = (1 - \delta)\tilde{k}_{t-1} + \left(\frac{R-1+\delta}{\alpha}\right) \tilde{y}_t - \left(\frac{R-1+\delta(1-\alpha)}{\alpha}\right) \tilde{c}_t} \quad (24)$$

This is the log-linearized capital accumulation equation.

Let's loglinearize (13)

$$R_t = \alpha Z_t K_{t-1}^{\alpha-1} + 1 - \delta \longrightarrow R_t = \alpha \frac{Y_t}{K_{t-1}} + 1 - \delta$$

$$\log(R) + \frac{1}{R}(R_t - R) = \log\left(\alpha \frac{Y}{K} + 1 - \delta\right) + \frac{\frac{\alpha}{K}}{\alpha \frac{Y}{K} + 1 - \delta}(Y_t - Y) - \frac{\alpha(\frac{Y}{K^2})}{\alpha \frac{Y}{K} + 1 - \delta}(K_{t-1} - K)$$

We multiply and divide by Y,K when appropriate

$$\log(R) + \frac{1}{R}(R_t - R) = \log\left(\alpha \frac{Y}{K} + 1 - \delta\right) + \frac{\frac{\alpha}{K}}{\alpha \frac{Y}{K} + 1 - \delta} Y \frac{(Y_t - Y)}{Y} - \frac{\alpha(\frac{Y}{K^2})}{\alpha \frac{Y}{K} + 1 - \delta} K \frac{(K_{t-1} - K)}{K}$$

$$\log(R) + \frac{1}{R}(R_t - R) = \log\left(\alpha \frac{Y}{K} + 1 - \delta\right) + \frac{\alpha \frac{Y}{K}}{\alpha \frac{Y}{K} + 1 - \delta} \tilde{y}_t - \frac{\alpha \frac{Y}{K}}{\alpha \frac{Y}{K} + 1 - \delta} \tilde{k}_{t-1}$$

From the SS conditions we can see that

$$\alpha \frac{Y}{K} = R - 1 + \delta$$

Also, in SS

$$\log(R) = \left(\alpha \frac{Y}{K} + 1 - \delta\right)$$

so

$$\frac{1}{R}(R_t - R) = \frac{R-1+\delta}{R}(\tilde{y}_t - \tilde{k}_{t-1})$$

$$\boxed{\tilde{r}_t = \frac{R-1+\delta}{R}(\tilde{y}_t - \tilde{k}_{t-1})} \quad (25)$$

Now we are just left with the shock process, which takes the form:

$$\boxed{\zeta_t = \rho_z \zeta_{t-1} + \epsilon_t} \quad (26)$$

Let's rewrite the log-linearized equations for clarity:

$$\tilde{c}_{t+1} - \tilde{c}_t = \frac{1}{\gamma} \tilde{r}_{t+1} \quad (27)$$

$$\tilde{y}_t = \zeta_t + \alpha \tilde{k}_{t-1} \quad (28)$$

$$\tilde{k}_t = (1 - \delta) \tilde{k}_{t-1} + \left(\frac{R - 1 + \delta}{\alpha} \right) \tilde{y}_t - \left(\frac{R - 1 + \delta(1 - \alpha)}{\alpha} \right) \tilde{c}_t \quad (29)$$

$$\tilde{r}_t = \frac{R - 1 + \delta}{R} (\tilde{y}_t - \tilde{k}_{t-1}) \quad (30)$$

$$\zeta_t = \rho_z \zeta_{t-1} + \epsilon_t \quad (31)$$

System Reduction

Substituting (30) into (27)

$$\tilde{c}_{t+1} - \tilde{c}_t = \frac{1}{\gamma} \left(\frac{R - 1 + \delta}{R} \right) \tilde{y}_{t+1} - \frac{1}{\gamma} \left(\frac{R - 1 + \delta}{R} \right) \tilde{k}_t \quad (32)$$

So, we have eliminated the equation for the real interest rate (30)

Now, substituting (28) into (32), and (28) into (29)

$$\tilde{c}_{t+1} - \tilde{c}_t = \frac{1}{\gamma} \left(\frac{R - 1 + \delta}{R} \right) \zeta_{t+1} + \frac{\alpha - 1}{\gamma} \left(\frac{R - 1 + \delta}{R} \right) \tilde{k}_t \quad (33)$$

and

$$\tilde{k}_t = R \tilde{k}_{t-1} + \left(\frac{R - 1 + \delta}{\alpha} \right) \zeta_t - \left(\frac{R - 1 + \delta(1 - \alpha)}{\alpha} \right) \tilde{c}_t \quad (34)$$

Thus, we have eliminated the equation for the production function (28)

In the (unlikely) event that we have no mistakes, our final system consists of:

$$\boxed{\tilde{c}_{t+1} - \tilde{c}_t = \frac{1}{\gamma} \left(\frac{R-1+\delta}{R} \right) \zeta_{t+1} + \frac{\alpha-1}{\gamma} \left(\frac{R-1+\delta}{R} \right) \tilde{k}_t} \quad (35)$$

$$\boxed{\tilde{k}_t = R\tilde{k}_{t-1} + \left(\frac{R-1+\delta}{\alpha} \right) \zeta_t - \left(\frac{R-1+\delta(1-\alpha)}{\alpha} \right) \tilde{c}_t} \quad (36)$$

$$\boxed{\zeta_t = \rho_z \zeta_{t-1} + \epsilon_t} \quad (37)$$

Bringing everything on the LHS:

$$\boxed{\tilde{c}_{t+1} - \tilde{c}_t - \frac{1}{\gamma} \left(\frac{R-1+\delta}{R} \right) \zeta_{t+1} - \frac{\alpha-1}{\gamma} \left(\frac{R-1+\delta}{R} \right) \tilde{k}_t = 0} \quad (38)$$

$$\boxed{\tilde{k}_t - R\tilde{k}_{t-1} - \left(\frac{R-1+\delta}{\alpha} \right) \zeta_t + \left(\frac{R-1+\delta(1-\alpha)}{\alpha} \right) \tilde{c}_t = 0} \quad (39)$$

$$\boxed{\zeta_t - \rho_z \zeta_{t-1} + \epsilon_t = 0} \quad (40)$$

Now, we are asked to express the system in the form

$$A\mathbb{E}X_{t+1} + BX_t + CX_{t-1} + \varepsilon\epsilon_t = 0$$

So, we have that:

$$A = \begin{bmatrix} 1 & 0 & -(\frac{1}{\gamma}) \left(\frac{R-1+\delta}{R} \right) \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad (41)$$

$$X_{t+1} = \begin{bmatrix} \tilde{c}_{t+1} \\ \tilde{k}_{t+1} \\ \zeta_{t+1} \end{bmatrix} \quad (42)$$

$$B = \begin{bmatrix} -1 & -\left(\frac{\alpha-1}{\gamma}\right)\left(\frac{R-1+\delta}{R}\right) & 0 \\ \left(\frac{R-1+\delta(1-\alpha)}{\alpha}\right) & 1 & -\left(\frac{R-1+\delta}{\alpha}\right) \\ 0 & 0 & 1 \end{bmatrix} \quad (43)$$

$$X_t = \begin{bmatrix} \tilde{c}_t \\ \tilde{k}_t \\ \zeta_t \end{bmatrix} \quad (44)$$

$$C = \begin{bmatrix} 0 & 0 & 0 \\ 0 & -R & 0 \\ 0 & 0 & -\rho_z \end{bmatrix} \quad (45)$$

$$X_{t-1} = \begin{bmatrix} \tilde{c}_{t-1} \\ \tilde{k}_{t-1} \\ \zeta_{t-1} \end{bmatrix} \quad (46)$$

$$\varepsilon = \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix} \quad (47)$$

ATTENTION: capital is an (endogenous) state variable so its coefficients should not appear in the A matrix, which contains only the coefficients of the forward-looking (control variables). Instead they will appear in X_{t-1} which contains the coefficients of the backward-looking (state) variables (here capital and prod.).