INSTRUMENTATION
AND CONTROL

COEG 304

LECTURE 2



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The process of representation of the dynamics of any physical system with mathematical equations that approximately relates the physical system quantities to the system components is mathematical modeling.



In order to understand the behavior of systems, mathematical models are required.



Mathematical models are equations which describe the relationship between the input and output of a system.



The basis for any mathematical model is provided by the fundamental physical laws that govern the behavior of the system.

Mathematical Model

Most common mathematical models to represent any system are:

Differential equations

Transfer function

State equations

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Mechanical System Building Blocks

Basic building block: **spring**, **dashpots**, and **masses**.

Springs: The reaction force '**f**k' developed due to compression or elongation of the spring is equal to stiffness 'k' and the amount of deformation of the spring. It represent the stiffness of a system.

Dashpots represent the forces opposing motion, for example frictional or damping effects. A **dashpot** is a mechanical device, a damper which resists motion via viscous friction.

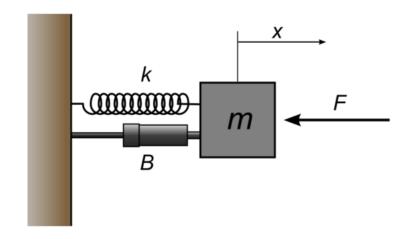
Masses represent the inertia or resistance to acceleration.

Mechanical systems does not have to be really made up of springs, dashpots, and masses but have the properties of stiffness, damping, and inertia.

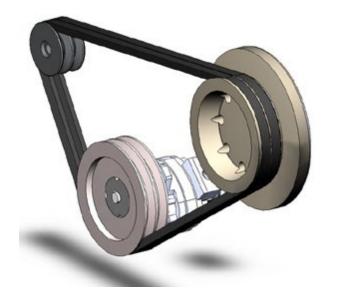
All these building blocks may be considered to have a force as an input and displacement as an output.

Basic Types of Mechanical Systems

- Translational
 - Linear Motion

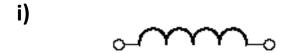


- Rotational
 - Rotational Motion

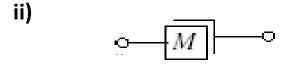


Basic Elements of Translational Mechanical Systems

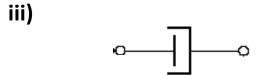
Translational Spring



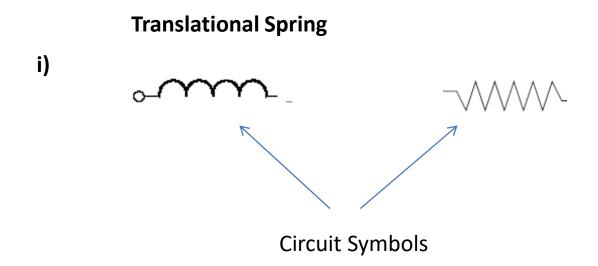
Translational Mass



Translational Damper



 A translational spring is a mechanical element that can be deformed by an external force such that the deformation is directly proportional to the force applied to it.





• If *F* is the applied force

$$x_2 \circ f$$

• Then x_1 is the deformation if $x_2 = 0$



• Or $(x_1 - x_2)$ is the deformation.

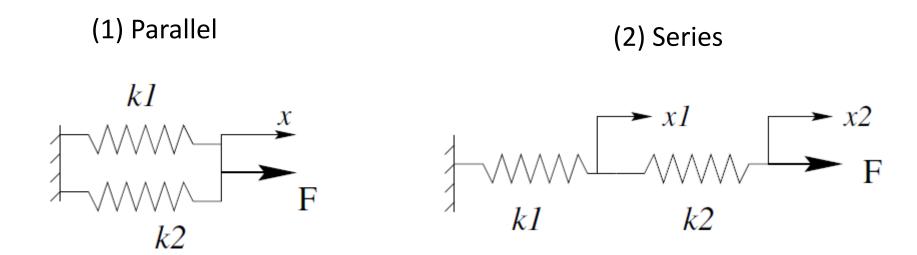


The equation of motion is given as

$$F = k(x_1 - x_2)$$

• Where k is stiffness of spring expressed in N/m

• Given two springs with spring constant k_1 and k_2 , obtain the equivalent spring constant k_{eq} for the two springs connected in:



The two springs have same displacement therefore:

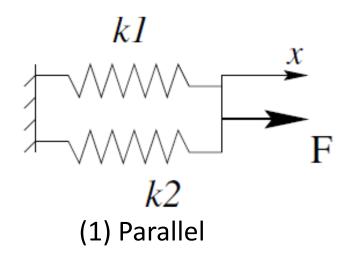
$$k_1x + k_2x = F$$

$$(k_1 + k_2)x = F$$

$$k_{eq}x = F$$

$$k_{eq}x = F$$

$$k_{eq} = k_1 + k_2$$



• If *n* springs are connected in parallel then:

$$k_{eq} = k_1 + k_2 + \dots + k_n$$

• The forces on two springs are same, *F*, however displacements are different therefore:

$$k_1 x_1 = F \text{ and } k_2 (x_2 - x_1) = F$$
 (2) Series
$$k_2 (x_2 - \frac{F}{k_1}) = F$$
 or, $k_2 x_2 = F + \frac{k_2}{k_1} F = \frac{k_1 + k_2}{k_1} F$

• The equivalent spring constant k_{eq} for this case is then found as

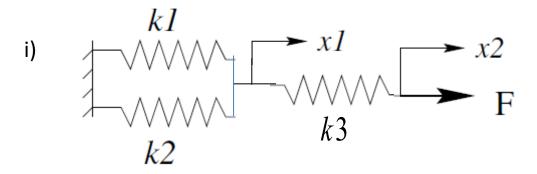
$$k_{eq} = \frac{F}{x_2} = \frac{k_1 k_2}{k_1 + k_2} = \frac{1}{\frac{1}{k_1} + \frac{1}{k_2}}$$

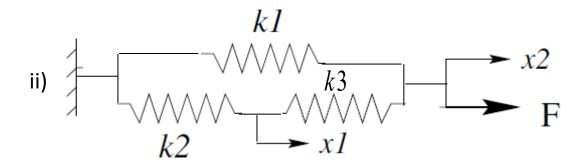
$$k_{eq} = \frac{F}{x_2} = \frac{k_1 k_2}{k_1 + k_2} = \frac{1}{\frac{1}{k_1} + \frac{1}{k_2}}$$

• If *n* springs are connected in series then:

$$k_{eq} = \frac{k_1 k_2 \cdots k_n}{k_1 + k_2 + \cdots + k_n}$$

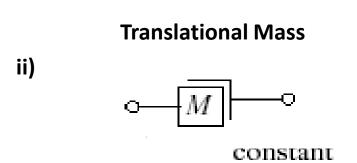
 Exercise: Obtain the equivalent stiffness for the following spring networks.

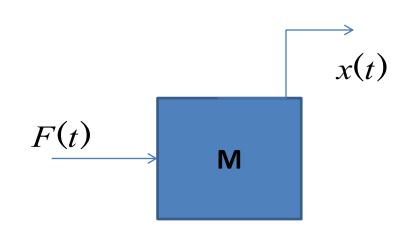




II. Translational Mass

- Translational Mass is an inertia element.
- A mechanical system without mass does not exist.
- If a force *F* is applied to a mass and it is displaced to *x* meters then the relation between force and displacements is given by Newton's law.





$$F = M\ddot{x}$$

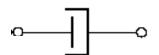
III. Translational Damper

 When the viscosity or drag is not negligible in a system, we often model them with the damping force.

 All the materials exhibit the property of damping to some extent.

 If damping in the system is not enough then extra elements (e.g. Dashpot) are added to increase damping. **Translational Damper**

iii)



Common Uses of Dashpots

Door Stoppers



Bridge Suspension



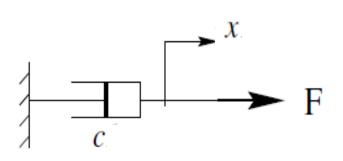
Vehicle Suspension

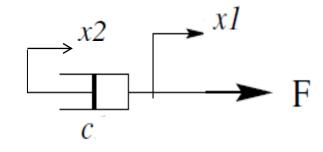


Flyover Suspension



Translational Damper





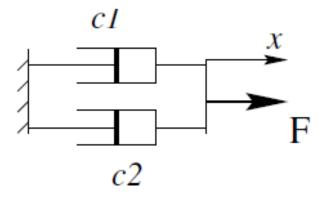
$$F = C\dot{x}$$

$$F = C(\dot{x}_1 - \dot{x}_2)$$

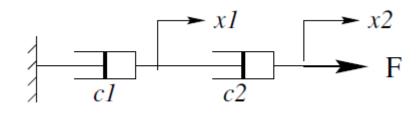
• Where C is damping coefficient (N/ms^{-1}) .

Translational Damper

Translational Dampers in series and parallel.



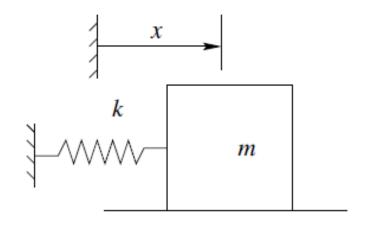
$$C_{eq} = C_1 + C_2$$



$$C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$$

Modelling a simple Translational System

 Example-1: Consider a simple horizontal spring-mass system on a frictionless surface, as shown in figure below.

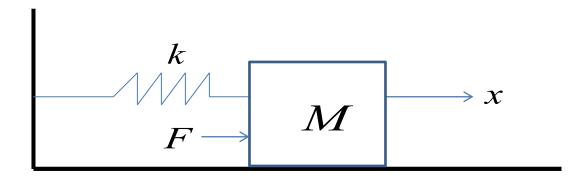


or

$$m\ddot{x} = -kx$$

$$m\ddot{x} + kx = 0$$

Consider the following system (friction is negligible)



Free Body Diagram



• Where f_k and f_M are force applied by the spring and inertial force respectively.



$$F = f_k + f_M$$

• Then the differential equation of the system is:

$$F = M\ddot{x} + kx$$

 Taking the Laplace Transform of both sides and ignoring initial conditions we get

$$F(s) = Ms^2 X(s) + kX(s)$$

$$F(s) = Ms^2 X(s) + kX(s)$$

The transfer function of the system is

$$\frac{X(s)}{F(s)} = \frac{1}{Ms^2 + k}$$

• if

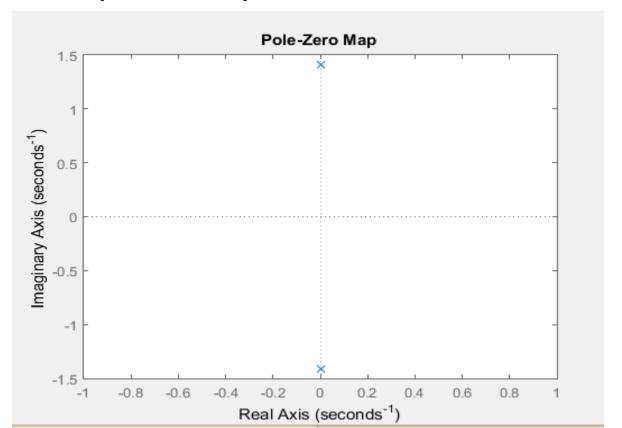
$$M = 1000kg$$
$$k = 2000 Nm^{-1}$$

$$\frac{X(s)}{F(s)} = \frac{0.001}{s^2 + 2}$$

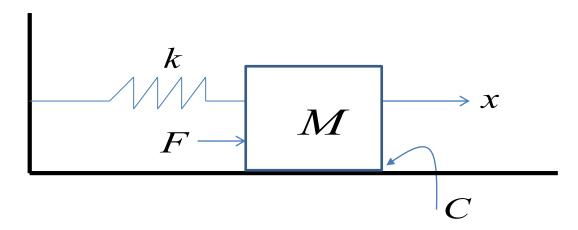
$$\frac{X(s)}{F(s)} = \frac{0.001}{s^2 + 2}$$

$$\int_{0.0000 + 1.4142i}^{0.0000 + 1.4142i}$$

• The pole-zero map of the system is



Consider the following system



Free Body Diagram

$$\begin{array}{c|c}
f_k & & & -f_C \\
F & & -f_M
\end{array}$$

$$F = f_k + f_M + f_C$$

Differential equation of the system is:

$$F = M\ddot{x} + C\dot{x} + kx$$

Taking the Laplace Transform of both sides and ignoring Initial conditions we get

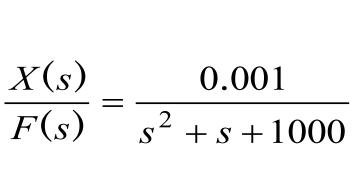
$$F(s) = Ms^2X(s) + CsX(s) + kX(s)$$

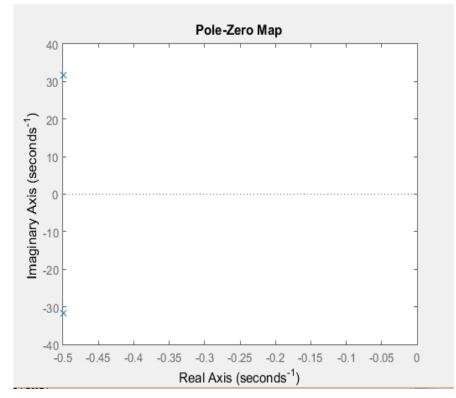
$$\frac{X(s)}{F(s)} = \frac{1}{Ms^2 + Cs + k}$$

$$\frac{X(s)}{F(s)} = \frac{1}{Ms^2 + Cs + k}$$

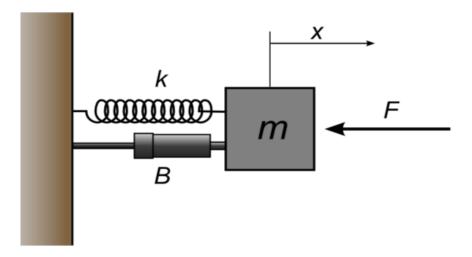
p = -0.5000 +31.6188i -0.5000 -31.6188i

• if





Consider the following system

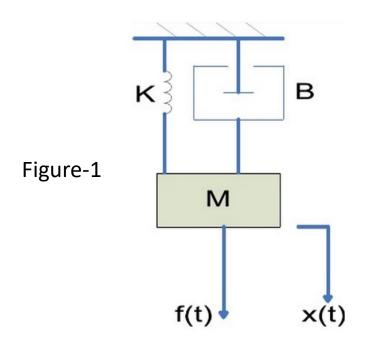


Free Body Diagram (same as example-3)

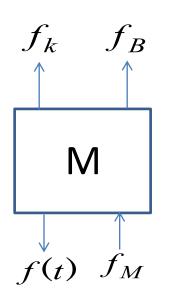
$$F = f_k + f_M + f_B$$

$$\frac{X(s)}{F(s)} = \frac{1}{Ms^2 + Bs + k}$$

• Find the transfer function of the mechanical translational system given in Figure-1.



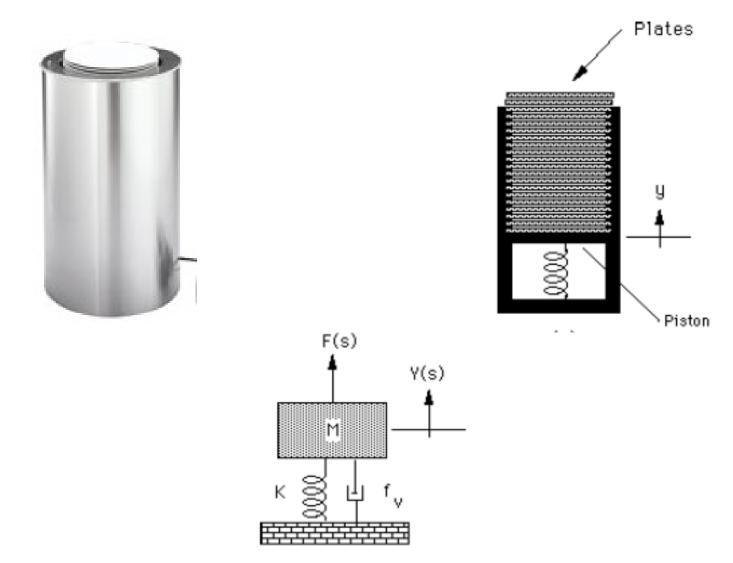
Free Body Diagram



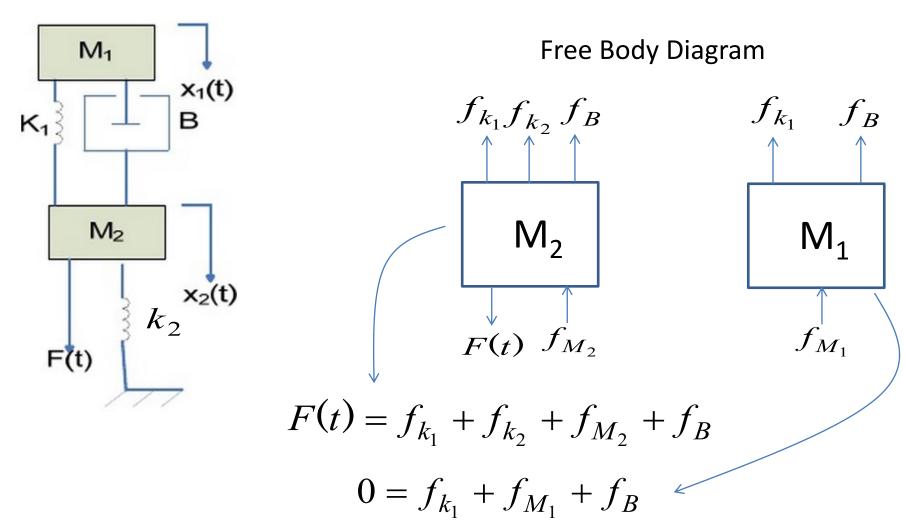
$$f(t) = f_k + f_M + f_B$$

$$\frac{X(s)}{F(s)} = \frac{1}{Ms^2 + Bs + k}$$

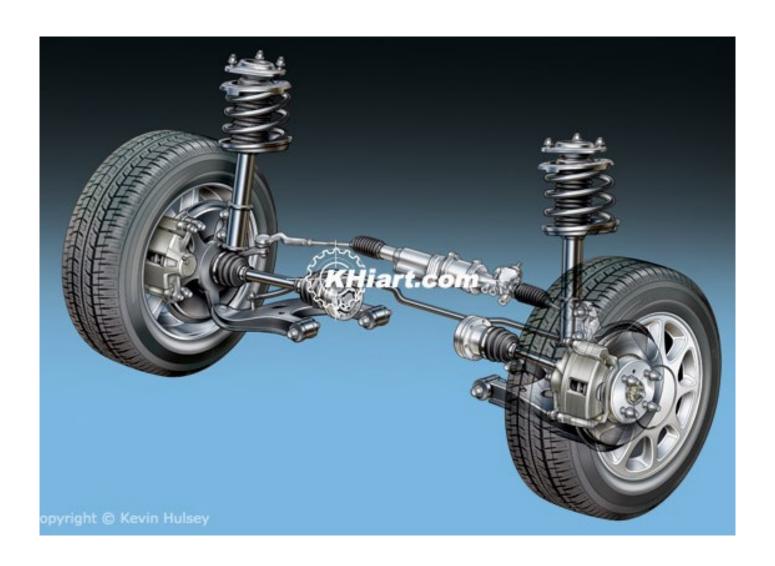
• Restaurant plate dispenser



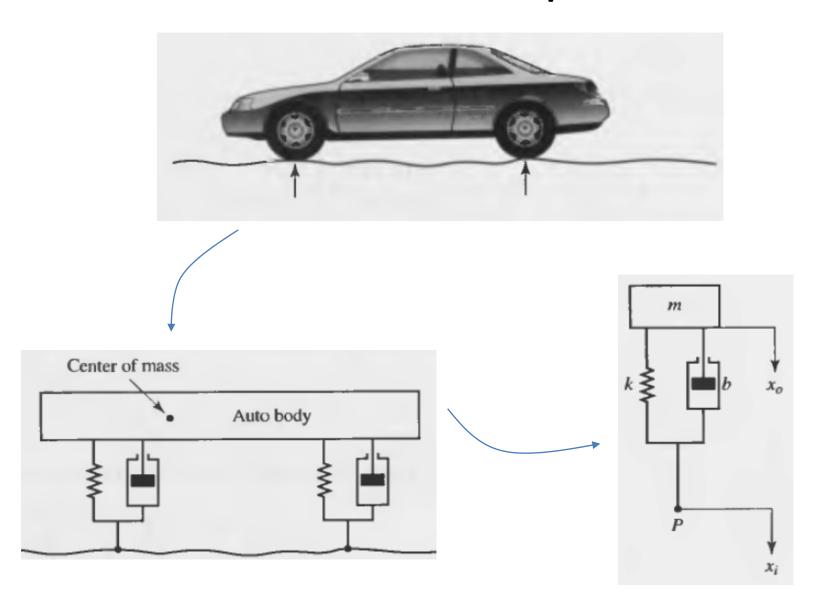
• Find the transfer function $X_2(s)/F(s)$ of the following system.



Example-11: Automobile Suspension



Automobile Suspension



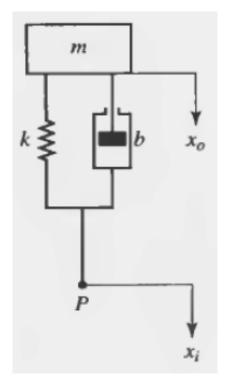
Automobile Suspension

$$m\ddot{x}_o + b(\dot{x}_o - \dot{x}_i) + k(x_o - x_i) = 0$$
 (eq.1)

$$m\ddot{x}_o + b\dot{x}_o + kx_o = b\dot{x}_i + kx_i$$

eq. 2

Taking Laplace Transform of the equation (2)



$$ms^{2}X_{o}(s) + bsX_{o}(s) + kX_{o}(s) = bsX_{i}(s) + kX_{i}(s)$$

$$\frac{X_o(s)}{X_i(s)} = \frac{bs + k}{ms^2 + bs + k}$$

Electrical System Building Blocks

The basic building blocks of electrical systems are resistance, inductance and capacitance.

Resistor:
$$v = iR$$
; $P = i^2R$

Inductor:
$$i = \frac{1}{L} \int v dt$$
; $E = \frac{1}{2} Li^2$

Capacitor:
$$i = C \frac{dv}{dt}$$
; $E = \frac{1}{2}Cv^2$

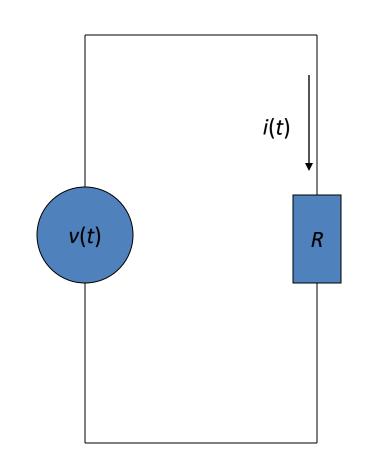
Resistance, R (ohm)

Appied voltage v(t)

Current i(t)

$$v(t) = Ri(t)$$

$$i(t) = \frac{1}{R}v(t)$$



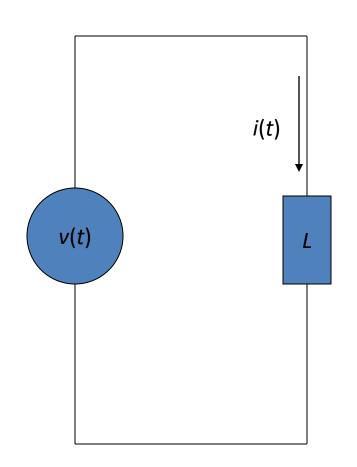
Inductance, L (H)

Appied voltage v(t)

Current i(t)

$$v(t) = L \frac{di(t)}{dt}$$

$$i(t) = \frac{1}{L} \int_{t_0}^{t} v(t)dt$$



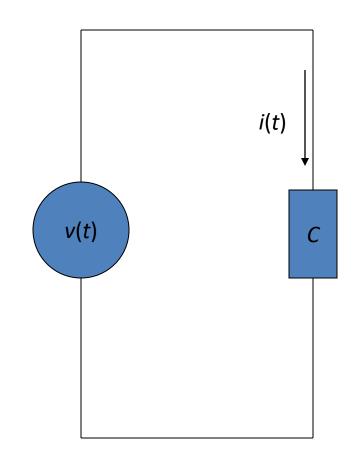
Capacitance, C (F)

Appied voltage v(t)

Current i(t)

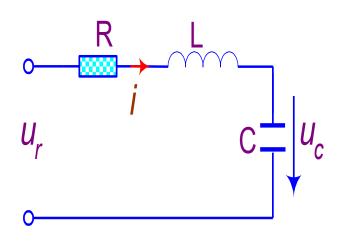
$$v(t) = \frac{1}{C} \int_{t_0}^{t} i(t)dt$$

$$i(t) = C \frac{dv(t)}{dt}$$



Example 13

A passive circuit



define: input $\rightarrow u_r$ output $\rightarrow u_{c_s}$ we have:

$$C = U_{c}$$

$$Ri + L \frac{di}{dt} + u_{c} = u_{r} \quad i = C \frac{du_{c}}{dt}$$

$$\downarrow \downarrow$$

$$LC \frac{d^{2}u_{c}}{dt^{2}} + RC \frac{du_{c}}{dt} + u_{c} = u_{r}$$

make:
$$RC = T_1$$
 $\frac{L}{R} = T_2$ \Rightarrow $T_1T_2 \frac{d^2u_c}{dt^2} + T_1 \frac{du_c}{dt} + u_c = u_r$

Modelling of Electric Systems:

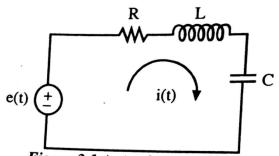


Figure 3.1 A simple RLC circuit

The differential equations describing the dynamics of the circuit are

$$e(t) = Ri(t) + L\frac{di}{dt} + \frac{1}{C}\int i(t)d(t)$$

Taking Laplace transform of the above equation with all initial conditions set to zero, we get

$$E(s) = RI(s) + sLI(s) + \frac{1}{sC}I(s)$$

The transfer function of the given system is given by the ratio of current I(s) in the circuit to the emf E(s) in the circuit.

$$\therefore \frac{I(s)}{E(s)} = \frac{sC}{s^2LC + sRC + 1}$$

Phase Lag Network

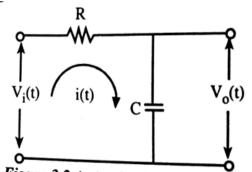


Figure 3.2 A simple phase lag network

Applying KVL across input, we get

$$V_i(t) = Ri(t) + \frac{1}{C} \int i(t)d(t)$$

Taking Laplace Transform of the above equation, we get

$$V_i(s) = \frac{1}{sC}I(s) + RI(s)$$
(3.5)

Applying KVL across output, we get

$$V_0(t) = \frac{1}{C} \int i(t)dt$$

Taking Laplace Transform of the above equation, we get

$$V_0(s) = \frac{1}{sC}I(s)$$
 (3.6)

Thus, the transfer function of the phase lag network is the ratio of output voltage $V_0(s)$ to the input voltage $V_i(s)$

$$\therefore \frac{V_0(s)}{V_i(s)} = \frac{1}{1 + sCR}$$

Phase Lead Network

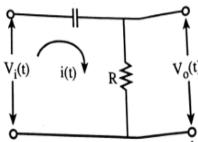


Figure 3.3 A phase lead network

Applying KVL across input, we get

$$V_i(t) = \frac{1}{C} \int i(t).dt + R.i(t)$$

Taking Laplace transform of the above equation, we get

$$V_i(s) = \frac{1}{sC}I(s) + RI(s)$$

Applying KVL across output, we get

$$V_0(t) = Ri(t)$$

Taking Laplace Transform of the above equation, we get

$$V_0(s) = RI(s) \tag{3.8}$$

Thus, the transfer function of the phase lead network is the ratio of output voltage $V_o(s)$ to the input voltage V(s)

$$\therefore \frac{V_0(s)}{V_i(s)} = \frac{sCR}{1 + sCR}$$

Analogy between Mechanical and Electrical System

SN	Mechanical Translational System	Electrical System	
		Voltage Analogy	Current Analogy
1.	Force, $F(t)$	Voltage, e(t)	Current, i(t)
2.	Mass, M	Inductance, L	Capacitance, C
3.	Stiffness, K	Reciprocal of	Reciprocal of
		capacitance, 1/C	inductance, I/L
4.	Damping Coefficient, B	Resistance, R	Reciprocal of
			resistance, I/R
5.	Displacement, $x(t)$	Charge, q(t)	Flux Linkage, $\varphi(t)$

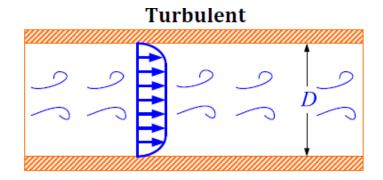
Laminar *vs* Turbulent Flow

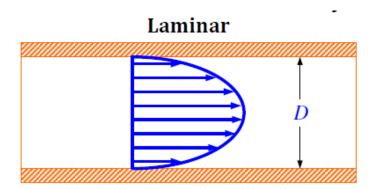
Laminar Flow

-Laminar flow or streamline flow occurs when a fluid flows in parallel layers, with no disruption between the layers. At low velocities, the fluid tends to flow without lateral mixing.

Turbulent Flow

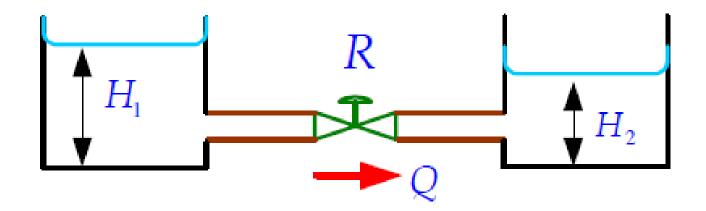
 When inertia forces dominate, the flow is called turbulent flow and is characterized by an irregular motion of the fluid.





Resistance of Liquid-Level Systems

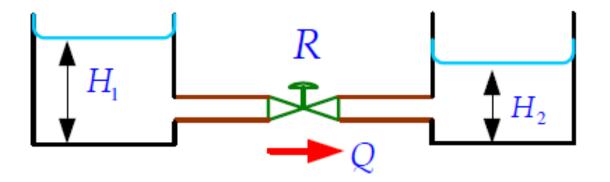
 Consider the flow through a short pipe connecting two tanks as shown in Figure.



• Where H_1 is the height (or level) of first tank, H_2 is the height of second tank, R is the resistance in flow of liquid and Q is the flow rate.

Resistance of Liquid-Level Systems

 The resistance for liquid flow in such a pipe is defined as the change in the level difference necessary to cause a unit change inflow rate.



Resistance =
$$\frac{\text{change in level difference}}{\text{change in flow rate}} = \frac{m}{m^3 / s}$$

$$R = \frac{\Delta(H_1 - H_2)}{\Delta Q} = \frac{m}{m^3 / s}$$

Resistance in Laminar Flow

 For laminar flow, the relationship between the steady-state flow rate and steady state height at the restriction is given by:

$$Q = k_l H$$

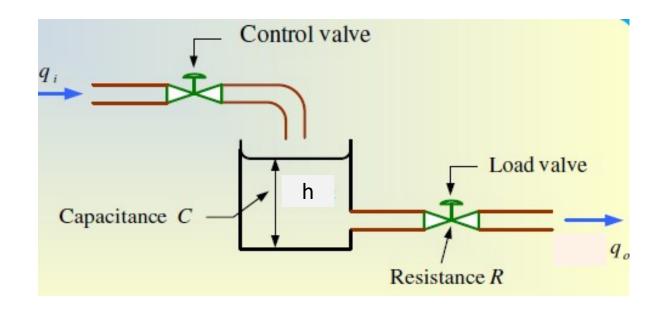
- Where Q = steady-state liquid flow rate in m^3/s
- $K_1 = constant in m^2/s$
- and H = steady-state height in m.
- The resistance R_{ℓ} is

$$R_l = \frac{dH}{dQ}$$
 $R = \frac{\text{change in level difference, m}}{\text{change in flow rate, m}^3/\text{sec}}$

The laminar flow resistance is constant and is analogous to the electrical resistance

Capacitance of Liquid-Level Systems

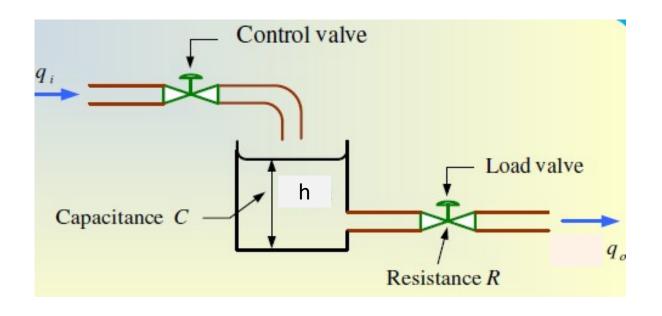
 The capacitance of a tank is defined to be the change in quantity of stored liquid necessary to cause a unity change in the height.



Capacitance =
$$\frac{change\ in\ liquid\ stored}{change\ in\ height} = \frac{m^3}{m}\ or\ m^2$$

Capacitance (C) is cross sectional area (A) of the tank.

Capacitance of Liquid-Level Systems

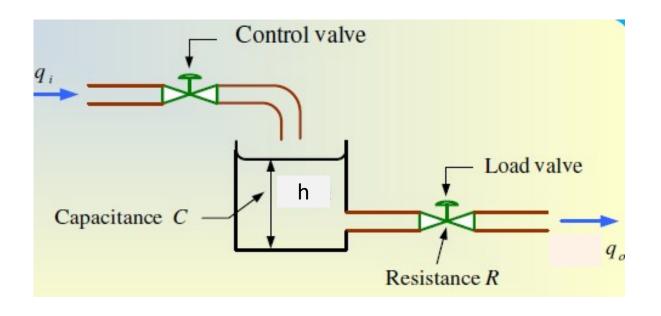


Rate of change of fluid volume in the tank = flow in - flow out

$$\frac{dV}{dt} = q_i - q_o$$

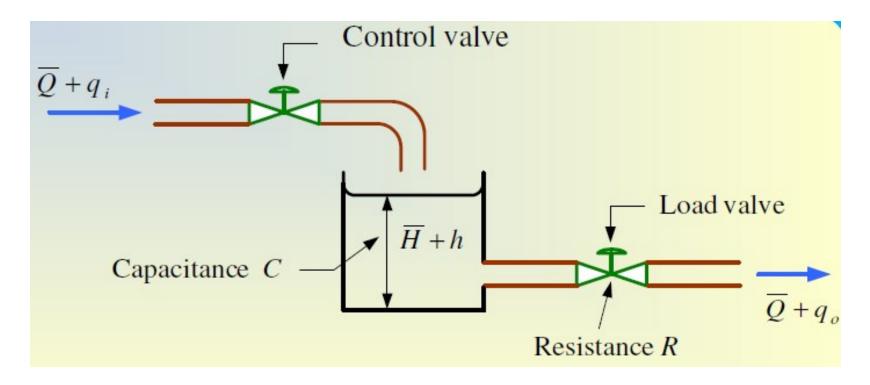
$$\frac{d(A \times h)}{dt} = q_i - q_o$$

Capacitance of Liquid-Level Systems



$$A\frac{dh}{dt} = q_i - q_o$$

$$C\frac{dh}{dt} = q_i - q_o$$



 \overline{H} = steady-state head (before any change has occurred), m.

h = small deviation of head from its steady-state value, m.

 \overline{Q} = steady-state flow rate (before any change has occurred), m³/s.

 q_i = small deviation of inflow rate from its steady-state value, m³/s.

 q_o = small deviation of outflow rate from its steady-state value, m³/s.

 The rate of change in liquid stored in the tank is equal to the flow in minus flow out.

$$C\frac{dh}{dt} = q_i - q_o \qquad (1)$$

• The resistance R may be written as

$$R = \frac{dH}{dQ} = \frac{h}{q_0} \qquad ----- \qquad (2)$$

Rearranging equation (2)

$$q_0 = \frac{h}{R} \qquad ----- \qquad (3)$$

$$C\frac{dh}{dt} = q_i - q_o \qquad ----- \qquad (1) \qquad q_0 = \frac{h}{R} \qquad ----- \qquad (3)$$

• Substitute q_o in equation (3) to equation (1)

$$C\frac{dh}{dt} = q_i - \frac{h}{R}$$

After simplifying above equation

$$RC\frac{dh}{dt} + h = Rq_i$$

• Taking Laplace transform considering initial conditions to zero

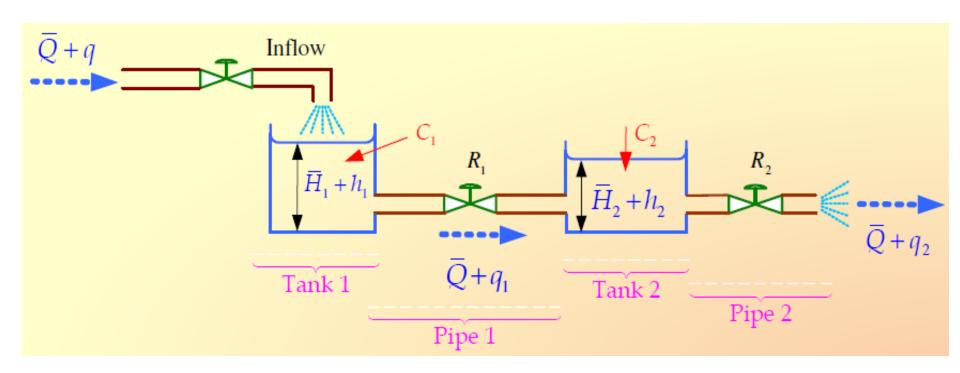
$$RCsH(s) + H(s) = RQ_i(s)$$

$$RCsH(s) + H(s) = RQ_i(s)$$

• The transfer function can be obtained as

$$\frac{H(s)}{Q_i(s)} = \frac{R}{(RCs+1)}$$

• Consider the liquid level system shown in following Figure. In this system, two tanks interact. Find transfer function $Q_2(s)/Q(s)$.

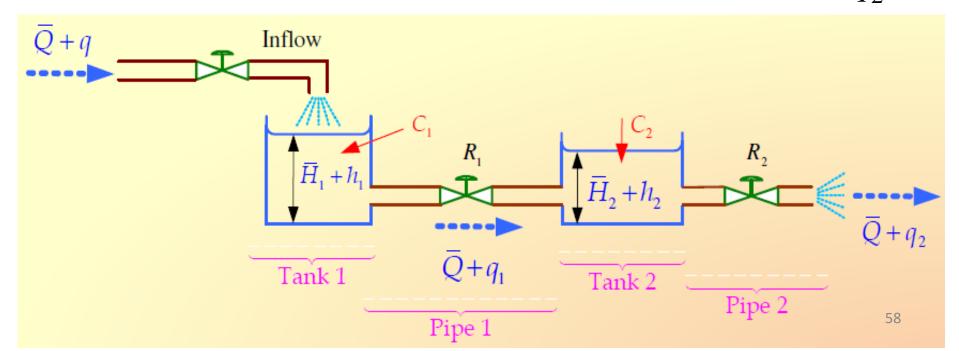


• Tank 1
$$C_1 \frac{dh_1}{dt} = q - q_1$$

Pipe 1
$$R_1 = \frac{h_1 - h_2}{q_1}$$

• Tank 2
$$C_2 \frac{dh_2}{dt} = q_1 - q_2$$

Pipe 2
$$R_2 = \frac{h_2}{q_2}$$



• Tank 1
$$C_1 \frac{dh_1}{dt} = q - \frac{h_1 - h_2}{R_1}$$

Pipe 1
$$q_1 = \frac{h_1 - h_2}{R_1}$$

• Tank 2
$$C_2 \frac{dh_2}{dt} = \frac{h_1 - h_2}{R_1} - \frac{h_2}{R_2}$$

Pipe 2
$$q_2 = \frac{h_2}{R_2}$$

Re-arranging above equation

$$C_1 \frac{dh_1}{dt} + \frac{h_1}{R_1} = q + \frac{h_2}{R_1}$$

$$C_2 \frac{dh_2}{dt} + \frac{h_2}{R_1} + \frac{h_2}{R_2} = \frac{h_1}{R_1}$$

$$C_1 \frac{dh_1}{dt} + \frac{h_1}{R_1} = q + \frac{h_2}{R_1}$$

$$C_2 \frac{dh_2}{dt} + \frac{h_2}{R_1} + \frac{h_2}{R_2} = \frac{h_1}{R_1}$$

• Taking LT of both equations considering initial conditions to zero [i.e. $h_1(0)=h_2(0)=0$].

$$\left(C_{1}s + \frac{1}{R_{1}}\right)H_{1}(s) = Q(s) + \frac{1}{R_{1}}H_{2}(s) \tag{1}$$

$$\left(C_2 s + \frac{1}{R_1} + \frac{1}{R_2}\right) H_2(s) = \frac{1}{R_1} H_1(s) \tag{2}$$

$$\left(C_{1}s + \frac{1}{R_{1}}\right)H_{1}(s) = Q(s) + \frac{1}{R_{1}}H_{2}(s) \quad (1) \qquad \left(C_{2}s + \frac{1}{R_{1}} + \frac{1}{R_{2}}\right)H_{2}(s) = \frac{1}{R_{1}}H_{1}(s) \quad (2)$$

• From Equation (1)

$$H_1(s) = \frac{R_1 Q(s) + H_2(s)}{R_1 C_1 s + 1}$$

• Substitute the expression of $H_1(s)$ into Equation (2), we get

$$\left(C_2 s + \frac{1}{R_1} + \frac{1}{R_2}\right) H_2(s) = \frac{1}{R_1} \left(\frac{R_1 Q(s) + H_2(s)}{R_1 C_1 s + 1}\right)$$

$$\left(C_2 s + \frac{1}{R_1} + \frac{1}{R_2}\right) H_2(s) = \frac{1}{R_1} \left(\frac{R_1 Q(s) + H_2(s)}{R_1 C_1 s + 1}\right)$$

• Using $H_2(s) = R_2Q_2(s)$ in the above equation

$$[(R_2C_2S+1)(R_1C_1S+1)+R_2C_1S]Q_2(S)=Q(S)$$

$$\frac{Q_2(s)}{Q(s)} = \frac{1}{R_2 C_1 R_1 C_2 s^2 + (R_1 C_1 + R_2 C_2 + R_2 C_1) s + 1}$$

Assignment Modelling Example#3

• Write down the system differential equations.

