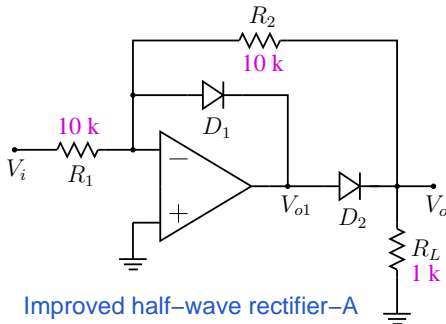
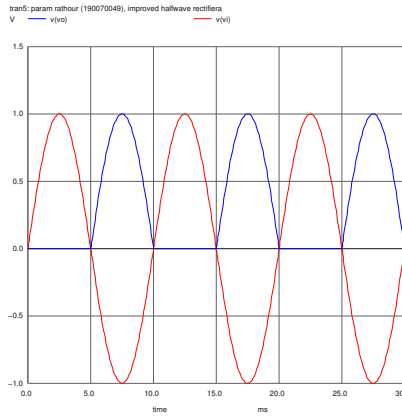
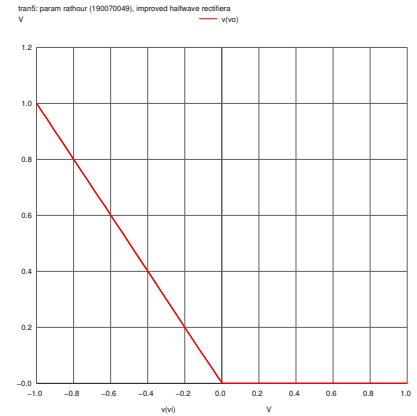


1 Improved Half Wave Rectifier A

1.1 Circuit & Plots



(a) Circuit

(b) V_{in}, V_{out} vs t (c) V_{out} vs V_{in}

1.2 Code

Param Rathour (190070049), Improved Half Wave Rectifier A

```
.include IN914.txt ; Includes Diode Model
.include ua741.txt ; Includes Op-amp Model

Vi Vi gnd sin(0 1 100 0 0) ; Input Voltage
VCCp VCCp gnd 12 ; Supply Voltage
VCCn VCCn gnd -12 ; Supply Voltage
x1 gnd Vn VCCp VCCn Vo1 ua741 ; Operational Amplifier
d1 Vn Vo1 IN914 ; Diode
d2 Vo1 Vo IN914 ; Diode

R1 Vi Vn 10k ; Resistor
R2 Vn Vo 10k ; Resistor
RL Vo gnd 1k ; Resistor

.tran 0.1m 30m ; Transient Analysis
.control ; Control Functions
run
plot V(Vi) V(Vo)
plot V(Vo) vs V(Vi)
.endc
.end
```

1.3 Learnings

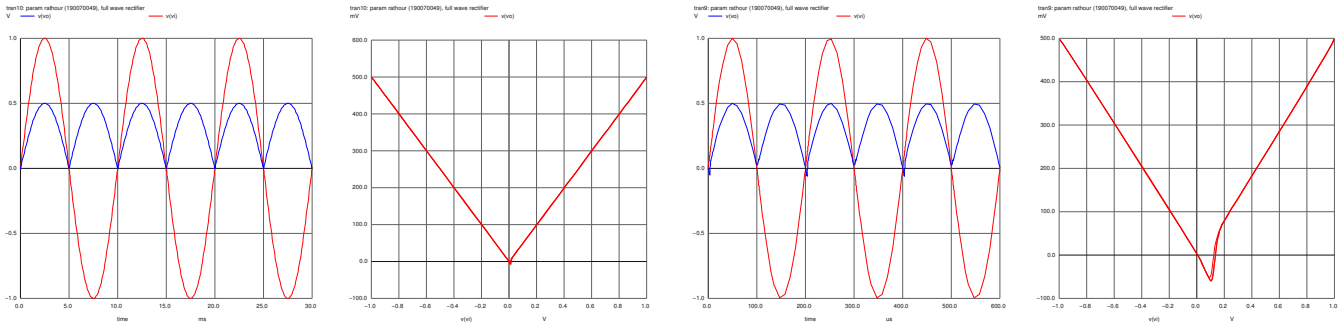
When $V_i > 0$, D_1 conducts and D_2 is off, whereas D_2 conducts and D_1 is off when $V_i < 0$

This rectifier operates in the linear region for both positive and negative values of V_i . Hence, better high-frequency performance compared to precision rectifier circuit.

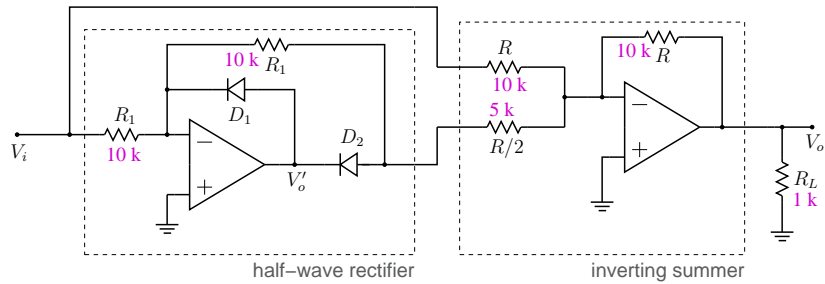
High-frequency performance still isn't much good due to Op-amp's (UA741) poor performance.

2 Full Wave Rectifier

2.1 Circuit & Plots



(a) V_{in}, V_{out} vs t at $f = 100\text{Hz}$ (b) V_{out} vs V_{in} at $f = 100\text{Hz}$ (c) V_{in}, V_{out} vs t at $f = 5\text{kHz}$ (d) V_{out} vs V_{in} at $f = 5\text{kHz}$



Full-wave rectifier

(e) Circuit

2.2 Code

Param Rathour (190070049), Full Wave Rectifier

```
.include IN914.txt ; Includes Diode Model
.include ua741.txt ; Includes Op-amp Model

* Vi Vi gnd dc 0 ac 1 ; Input Voltage
Vi Vi gnd sin(0 1 5000 0 0) ; Input Voltage
VCCp VCCp gnd 12 ; Supply Voltage
VCCn VCCn gnd -12 ; Supply Voltage
x1 gnd Vn1 VCCp VCCn Vo1 ua741 ; Operational Amplifier
x2 gnd Vn2 VCCp VCCn Vo ua741 ; Operational Amplifier
d1 Vo1 Vn1 1N914 ; Diode
d2 Vo2 Vo1 1N914 ; Diode
R1 Vi Vn1 10k ; Resistor
R2 Vn1 Vo2 10k ; Resistor
R3 Vi Vn2 10k ; Resistor
R4 Vo2 Vn2 5k ; Resistor
R5 Vn2 Vo 5k ; Resistor
RL Vo gnd 1k ; Resistor
.tran 0.1m 30m ; Transient Analysis (100Hz)
* .tran 0.02m 0.6m ; Transient Analysis (5kHz)
.control ; Control Functions
run
plot V(Vi) V(Vo)
plot V(Vo) vs V(Vi)
.endc
.end
```

2.3 Learnings

Here, V_o is equal to $|V_i|$. The multiplication of -2 to V_{o2} and -1 to V_i ensures that their summing of gives $|V_i|$. High-frequency performance still isn't much good due to Op-amp's (UA741) poor performance.

3 Single-pole Active Low-pass Filter

3.1 Analysis

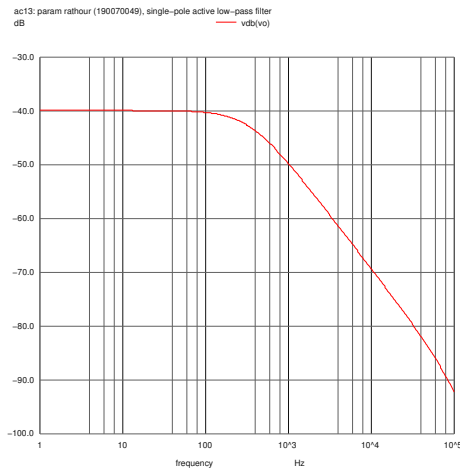
Theoretical Values

$$f_c = \frac{1}{2\pi R_A C_A} = \frac{1}{2\pi} \approx 338.63 \text{ Hz} \quad \text{Roll-off Frequency} = -20 \text{ dB/decade}$$

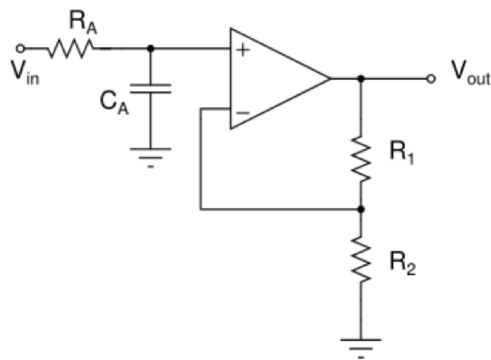
Simulation Values

$$f_c = f \text{ when } V_{\text{out}} = \frac{V_{\text{max}}}{\sqrt{2}} \Rightarrow V_{\text{out}_{\text{dB}}} = V_{\text{max}_{\text{dB}}} - 3 \Rightarrow f_c = 3.378190 \cdot 10^2 \text{ Hz} \quad \text{Roll-off Frequency} = -1.95728 \cdot 10^1 \text{ dB/decade}$$

3.2 Circuit & Plots



(a) Filter Response for $f = 1$ to $100k$ Hz



(b) Circuit

3.3 Code

```
Param Rathour (190070049), Single-pole Active Low-pass Filter
.include ua741.txt
Vi Vi gnd dc 0 ac 1m
VCCp VCCp gnd 12
VCCn VCCn gnd -12
x1 Vp Vn VCCp VCCn Vo ua741
RA Vi Vp 4.7k
CA Vp gnd 0.1u
R1 Vn Vo 9.1k
R2 Vn gnd 1k
.ac DEC 100 1 100k
.control
run
meas ac Vdbmax max vdb(Vo)
let Vdbreq = Vdbmax-3
meas ac fC when vdb(Vo) = Vdbreq fall = 1
meas ac V1 find Vdb(Vo) at = 1000
meas ac V2 find Vdb(Vo) at = 10000
let RollOff = V2 - V1
print fC RollOff
.endc
.end
```

; Includes Op-amp Model
; Input Voltage
; Supply Voltage
; Supply Voltage
; Operational Amplifier
; Resistor
; Capacitor
; Resistor
; Resistor
; AC Analysis
; Control Functions

3.4 Learnings

The theoretical results match well with simulation results for cutoff and roll-off frequency.

4 Sallen-Key (2-pole) Active High-pass Filter

4.1 Analysis

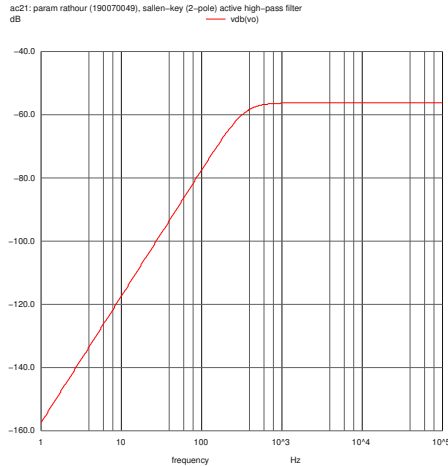
Theoretical Values

$$f_c = \frac{1}{2\pi R_A C_A} = \frac{1}{2\pi} \approx 338.63 \text{ Hz} \quad \text{Roll-off Frequency} = 40 \text{ dB/decade}$$

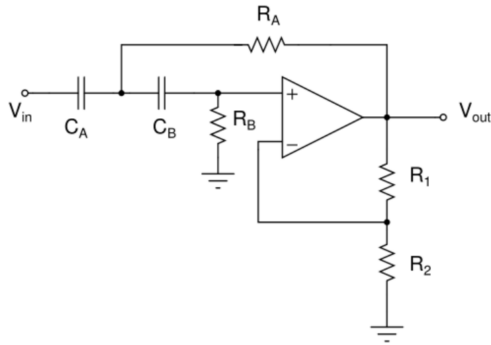
Simulation Values

$$f_c = f \text{ when } V_{\text{out}} = \frac{V_{\text{max}}}{\sqrt{2}} \Rightarrow V_{\text{out}_{\text{dB}}} = V_{\text{max}_{\text{dB}}} - 3 \Rightarrow f_c = 3.487332 \cdot 10^2 \text{ Hz} \quad \text{Roll-off Frequency} = 3.992473 \cdot 10^1 \text{ dB/decade}$$

4.2 Circuit & Plots



(a) Filter Response for $f = 1$ to $100k$ Hz



(b) Circuit

4.3 Code

```
Param Rathour (190070049), Sallen-Key (2-pole) Active High-pass Filter
.include ua741.txt                                     ; Includes Op-amp Model
Vi Vi gnd dc 0 ac 1m                                  ; Input Voltage
VCCp VCCp gnd 12                                       ; Supply Voltage
VCCn VCCn gnd -12                                      ; Supply Voltage
x1 Vp Vn VCCp VCCn Vo ua741                           ; Operational Amplifier
RA mid Vo 4.7k                                         ; Resistor
CA Vi mid 0.1u                                         ; Capacitor
RB Vp gnd 4.7k                                         ; Resistor
CB mid Vp 0.1u                                         ; Capacitor
R1 Vn Vo 9.1k                                          ; Resistor
R2 Vn gnd 1k                                           ; Resistor
.ac DEC 100 1 100k                                    ; AC Analysis
.control                                               ; Control Functions
run
plot Vdb(Vo)
meas ac Vdbmax max vdb(Vo)
let Vdbreq = Vdbmax-3
meas ac fC when vdb(Vo) = Vdbreq rise = 1
meas ac V1 find Vdb(Vo) at = 10
meas ac V2 find Vdb(Vo) at = 100
let RollOff = V2 - V1
print fC RollOff
.endc
.end
```

4.4 Learnings

The theoretical results match well with simulation results for cutoff and roll-off frequency. For very high frequencies, output will again decrease due to Op-amp's (UA741) poor performance.