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Development of tilt-rotor unmanned aerial vehicle (UAV): material selection and structural analysis on wing design

M F Saharudin

Jabatan Penyenggaraan Pesawat, Politeknik Banting, Selangor, Malaysia

firdaus.saha@polibanting.edu.my

Abstract. This paper presents the design of a tilting rotor unmanned aerial vehicle (UAV), evaluation of flight loads based on the standard requirement, structural analysis to determine stress and sizing of the wing, and flight test of the UAV. The main objective is to perform structural analysis to size the UAV's wing section. The analysis shows that the structure design of the wing is safe to be used.

1. Introduction

Aeronautic industries have long begun and have been growing over decades with newer inventions, technologies as well as rapid research in this promising field [1]. There are a lot of researches have been made throughout the world including aerial mapping, unmanned aerial vehicle (UAV), etc. The search for an aircraft type with vertical take-off and landing (VTOL) capabilities has triggered the imagination of designers and inventors to produce numerous configurations using a wide variety of lifting and propulsion devices [3]. A summary of some of these configurations is available in the V/STOL (Vertical or Short Take-off and Landing) concepts illustration prepared by the McDonnell Aircraft Company in the 1960s [6]. For various aircraft types considered, one of the key distinguishing features is associated with the device used for providing the vertical lift. The development of VTOL is very important as it has many usage such as in the field of safe and rescue, military application and even some commercial applications [2]. The usage of VTOL cuts the runaway distance, making it easy to take-off and land on aircraft carrier as well as other constrained areas where the paved runaway or space is limited.

Throughout their long history, UAVs have played such an important role whether in warfare or surveillance. The idea of unmanned is to control a machine digitally and replace the needs of human intelligence on-board, saving the human capital for much better use. When compared to manned aerial vehicles, UAVs are believed to provide two vital benefits – they are cost effective and reduce the risk to a pilot's life [4]. However, accident rates in today's UAVs are over 100 times compared manned aircraft. Therefore, improved safety and reliability are still required. The requirement of this research is to design and fabricate a remote controlled aircraft, which is also known as Tilt-Rotor UAV, that can take-off and land vertically. Besides, the study also done to identify the material selection for the UAV and demonstrate the analysis on the wing design of the UAV. In order to achieve the whole benefits and purposes out of Tilt-Rotor UAV, there are a lot of obstacles need to be overcome. Since the rotors can be configured to be more efficient for propulsion (e.g. with root-tip twist) and it avoids a helicopter's issues of retreating blade stall, the tilt-rotor can achieve higher speeds than helicopters. A tilt-rotor aircraft differs from a tilt-wing in that only the rotor pivots rather than the entire wing. This method trades off efficiency in vertical flight for efficiency in STOL/STOVL operations.

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Nevertheless, the scope of this research paper is limited to material selection and structural analysis on the wing design. The primary objectives of this project are to design VTOL of Tilt-Rotor UAV by surveying the material selection and to perform structural analysis to determine the sizing of wing.

2. Materials and methods

This study is focused on the development of multi tilt-rotor UAV by concentrating on the structure and design analysis. The information obtained will guide the UAV to move at tilting concept mechanism towards the respective object of interest. In accomplishing the outlined objectives, several guidelines have been observed: reviewing the previous related VTOL UAV projects and performing a standard structural analysis by several methods in aircraft structural analysis design concept.

2.1. Material selection and conceptual design

In this part, it is basically focused on selecting the suitable material to fabricate the tilt-rotor UAV and adhesive needed for this project. Some reference reading is made based on material selection for the main body such fuselage, wing and tail, type of propeller, type of adhesive and type of motor. Table 1 highlights some of the optional materials that can be selected for the main body of the UAV.

Table 1. Justification material selection for the main body [8]

Materials Pros		Cons	
Balsa wood	 Porous Less glue required Lightweight Widely available Stiff Easy to sand 	Varying strengthVery expensive	
Basswood	Won't crushLightweight	Hard to sandNot widely availableMore expensive	
Depron foam	Very lightweightEasy to shapeFlexibleVery cheap	Not very strong	
Plastic	StrongRigid	RigidHard to work withExpensiveRelatively heavy	
Metal	Very strongRigid	Very heavyExpensiveHard to work withNot widely available	
Fibre glass	Very strongVery lightweight	Very expensiveNo previous experienceNot widely available	

Depron foam was chosen as the base frame material due its low cost and easy fabrication properties, despite Fiber Glass having a significant strength to weight advantage. The aluminum box are put in the wing for tilt rotor and the body is covered by fibre glass composite. Table 2 tabulates some of pros and cons of alternatives for the propellers.

APC Blade (Metal)

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Propellers Pros		Cons	
Dual Blade	 Easily available 	Larger diameter	
	 Very efficient 		
	• Easy to use		
	 Fairly cheap 		
Multi Blade	Smaller diameter	Less available	
		 Less efficient 	
Wood Blade	Very rigid	Breaks easily	
	• Efficient	•	
	 Light 		

Table 2. Justification for propeller selection [8]

For this tilt-rotor VTOL UAV, the location of the propeller is placed at the tip of the wing. The thrust must be at the cg location to make it more stable. When the aircraft experience gust load during hover, the tail rotor will produce thrust to make it stable. It was decided to use two-blade propellers as compared to three-bladed system used by the real V-22 Osprey [2]. This is due to increased efficiency of the two-bladed propellers over the three-bladed propellers. Moreover, justification for the adhesive selection can be seen in Table 3.

Don't break as easily

Efficient

Heavy

Table 3. Justification for adhesive selection [8]

Adhesives	Pros	Cons	
Wood Glue	 Easiest to use 	 Poor heat resistance 	
(Urea)	 Low cost 	 Poor moisture resistance 	
	 Light color 	 Bond not very strong 	
Hot Glue	 Quick cooling time 	 Bond not strong 	
	 Relatively easy to use 	 Leaves residue 	
	 Low cost 	 Visible on plane 	
Gorilla	 Very light 	 Hard to work with 	
Glue	 Expands while setting 	 Contains air bubbles 	
	 Best for wood than other 	 Somewhat expensive 	
	materials		
	 Waterproof 		
Pro-bond	 Expands when dry 	 Heavy 	
Glue	 Less glue required 		
	• Cheap		
	 Water-resistant 		
Rubber	 Strong flexible bond 	 Flammable 	
Cement	 Easy to peel off 	 Highly toxic 	
	 Not brittle 	 Expensive 	
Super Glue	 Very strong bond 	 Expensive 	
	 Often used for model aircraft 	 Can become brittle 	
	 Versatile 	 Long cure times 	
	 Water resistant 		

To make the aircraft in stable and solid form, a strong adhesive connection must be used to ensure that the aircraft does not broken during flight or VTOL. On the other hand, some considerations for the motor selection is presented in Table 4.

Motors	Pros	Cons	
Electric	• Cheap	Low power / torque	
	• Easy to run		
	• Clean		
	 Doesn't require gasoline 		
	• Lightweight		
Nitro	Relatively cheap	Special mixture of fuel	
	Wide availability	• Heavy	
	 High torque and power 	•	
Gas	High torque and power	Not as available	
		 Heavy 	
		 Special mixture of fuel 	
		 Expensive 	
Jet	Extreme power	Extremely expensive	
	1	Not as available	

Table 4. Justification for motor selection [8]

Based on the above justification, the main body will be made from depron foam board due its flexibility, easy to shape, price tag and light in weight. For the propeller, the dual propeller is chosen due to its availability, efficiency and price tag. As there are a lot of parts that needs to be mounted, the glue will be the best solution due to the low operating cost and high availability. Last but not least, for the propulsion part, electric motor is chosen as it is very cheap to purchase, environmental friendly and easy to operate.

2.2. Conceptual design of tilt-rotor UAV

Aircraft design is basically a combination of science and art together in producing a beautiful machine. In the design phase, whether for normal configuration like the common civilian transport aircraft or for new configuration, there are few steps that need to be followed in order to design and build an aircraft. These design phases are in chronological order: conceptual design, preliminary design, detail design. In conceptual design phase, it basically starts by setting a few specifications for the new aircraft. Every designer has their own approach in developing their conceptual design. However, there are some basic guidelines that are vital and significant for conceptual design. They are design requirement, estimation of the weight of aircraft, identification of some critical performance parameters, type of configuration, performance analysis and optimization. For this study, the mission specifications of the tilt-rotor UAV are presented in Table 5. Some initial conceptual design estimations are then presented in Table 6.

Mission Specifications Mission Profile $V_{max} = 30 \text{ m/s}$ CRUISE $V_{climb} = 49 \text{ ft/s}$ 3 2 Rate of climb = 10 ft/s $V_{stall} = 39 \text{ ft/s}$ LOITTER CLIMB $V_{cruise} = 69 \text{ ft/s}$ Range = 10000 ftAltitude = 1000 ftEndurance = 20 minLANDING Rho (sls) = $0.00238 \text{ slug/ft}^3$ TAKE/OFF Rho (cruise) = $0.002308 \text{ slug/ft}^3$

Table 5. Preliminary mission specifications of the present UAV [7-8]

Table 6. Design calculations

	FORMULA/DESIGN	CALCULATION VALUE
MAXIMUM TAKE OFF	STALL: $\frac{W}{S} \ll \frac{1}{2} \cdot \rho \cdot Vstall^2 \cdot C_{lmax}$	STALL: $\frac{W}{s} \ll 1.79 lb/ft2$
WEIGHT	TAKE-OFF: $\frac{w}{s} \ll TOP. \sigma. C_{lTO}. \frac{Hp}{w}$	TAKE-OFF: $\frac{w}{s} \ll 1.411 lb/ft2$
	CLIMB:	CLIMB: $\frac{W}{s} = 39.896 lb/ft2$
	$\frac{w}{s} = \frac{\left(\frac{T}{W} - G\right) \pm \sqrt{\left(\frac{T}{W} - G\right)^2 - \left(\frac{4Cdo}{\pi e}\right)}}{2/q\pi Ae}$	CRUISE: $\frac{w}{s} = 1.582 lb/ft2$
	CRUISE: $\frac{W}{S} = q\sqrt{\pi AeCdo}$	
WING LOADING	The lowest wing loading is the one to be selected.	$\frac{W}{S} = 1.411 lb/ft2$ $L = 2.31 ft = 700 mm$
FUSELAGE SIZING	$L = aWo^{c}$ Figure 1. Fuselage sizing	L = 2.31 ft = 700 mm
WING	Figure 1. Pusetage Sizing	$\frac{Wo}{s} = 1.411, s = \frac{Wo}{1.411} = 1.79 ft2$
SIZING	Figure 2. Wing Sizing	$b = \sqrt{A \times S} = 3.3 ft$ $Cr = \frac{2S}{b(1+\lambda)} = 0.54$ $\bar{c} = \frac{2}{3} \cdot \text{Cr.} \left(\frac{1+\lambda+\lambda^2}{1+\lambda}\right) = 0.54$ $Ct = \lambda Cr = 0.54 ft,$ $\bar{y} = \frac{b}{6} \left(\frac{1+2\lambda}{1+\lambda}\right) = 0.82$
TAIL		<u>VERTICAL TAIL</u>
SIZING	Total State of the	$Svt = \frac{Cvtnew \cdot bw \cdot sw}{Lvt} = 0.162ft$ $Svt = \frac{60}{100}L = 1.386ft$ $b = \sqrt{A \times S} = 0.44ft$ $Cr = \frac{2S}{b(1+\lambda)} = 0.368ft$ $ct = \lambda Cr = 0.368ft$ $\bar{c} = \frac{2}{3} \cdot Cr \cdot \left(\frac{1+\lambda+\lambda^2}{1+\lambda}\right) = 0.368ft$
	Figure 3 . Tail Sizing	,
		$\bar{y} = \frac{b}{6} \left(\frac{1+2\lambda}{1+\lambda} \right) = 0.11 ft$

Table 6.	Design	calculation	is (continued)
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	FORMULA/DESIGN	CALCULATION VALUE
TAIL		HORIZONTAL TAIL
SIZING		Chtnew = 0.95(0.5) = 0.475
		$Sht = \frac{Chtnew.Cw.sw}{Lvt} = 0.361ft$ $Lvt = \frac{30}{100}L = 0.693ft$
		$Lvt = \frac{100}{100}L = 0.693ft$
		$b = \sqrt{A \times S} = 1.46ft$
		$Cr = \frac{2S}{b(1+\lambda)} = 0.38ft$
		$Ct = \lambda Cr = 0.114ft$
		$\bar{c} = \frac{2}{3} \cdot Cr \cdot \left(\frac{1+\lambda+\lambda^2}{1+\lambda}\right) = 0.27ft$
		$\bar{y} = \frac{b}{6} \left(\frac{1+2\lambda}{1+\lambda} \right) = 0.27 ft$
CENTRE		Weight distribution:
OF	CENTER OF GRAVITY (CG)	Wo= 2.52 lb, Wwing= 0.25 kg,
GRAVITY	Xwing	Wengine= 0.20 kg , Wpl = 0.4 kg , Wtail= 0.25 kg
	Xcg	$\sum_{m} Mcg = \sum_{m} Mle$
		without wing:
	Figure 4. Centre of gravity	$x = \frac{0.20(0.9) + 0.4(0.3) + 0.25(2)}{0.2 + 0.4 + 0.25}$
		$x = \frac{0.2 + 0.4 + 0.25}{0.941 ft}$
		with wing:
		Xcg = 0.97 ft
		$Xcg = 0.97ft \simeq 296 mm$
		$static margin = \frac{(Xn - Xcg)}{c} = 0.1$
		$0.1 = \frac{Xn - 0.97}{0.54} = Xn = 1.024$
-		Xac = Xn - Xvt = 0.794 ft

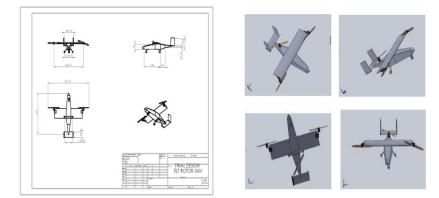


Figure 5. Layout and 3D view of the UAV design after achieved the design requirements

3. Results and discussion

Before the structure of the wing can be designed, there is a need to determine the loads that will be imposed on the aircraft's wing. This section deals with the general issue of aircraft loads and how they are predicted in the early stages of the design process. The load factor is the multiplier used on limit load to determine the design load. In this case, since there are specific requirements for the factor of safety, 4.5 will be used as the factor of safety as obtained from the STANAG USAR requirement [14]. The safety factor, N_z from the STANAG requirement is calculated as follows, taking the weight to be 1.3 kg or 2.866 lb:

$$Nz = 2.1 + (\frac{10900}{W + 4536}) = 2.1 + (\frac{10900}{2.866 + 4536}) = 4.5$$

3.1. Structural analysis of wing design

In this section, the structural analysis is mainly about investigation of shear force and bending moment at the wing of the tilt rotor UAV. This theory will be applied at the calculation part for the tilt-rotor UAV project.

Table 7. Justification for structural analysis of wing design

ITEM ANALYSIS	RESULT	FIGURE
Load Factor	Nz = 4.5	
Shear force		†×
Va (aerodynamic shear force)	Va = 0.2088 N	
Vp (propeller shear force)	Va = 7.505N	b/2 ×
V(Total)	V = 7.7138N	y 5/2
Bending moment		†¥ da
Ma (aerodynamic moment)	Ma = 0.02724 N.m	
Mp (propeller moment)	Mp = 1.3133 N. m	y ×
M(Total)	M = 1.34054 N. m	b/2
Moment of Inertia	$I = 2.62083 \times 10^{-9}$	
Shear Stress	τ = 344.91 <i>KPa</i>	0.0125m
Bending stress	$\sigma = 4.260 MPa$	$\sigma_{x} = -\frac{M_{z}y}{I_{zz}} + \frac{M_{y}z}{I_{yy}}$

Aluminium 2014-T6 was used as the reference, which $\sigma y = 414$ MPa. To compare it:

$$\sigma = 4.260 MPa < \frac{414}{1.5} \rightarrow \sigma = 4.260 MPa < 276 MPa$$

where σ is 4.260 MPa. This shows that the wing bending stress is less than bending stress yield, even though it is very small but may increase the weight later. For the shear stress:

$$\tau = \frac{VQ}{It} = 344.91 \, KPa$$

 $\tau = \frac{VQ}{It} = 344.91 \ KPa$ where τ is 344.91 kPa, V is 7.7138 N , Q is 2.34375X10⁻⁷, I is 2.62083 \times 10⁻⁹ and t is 0.002. In aircraft structure design, one of the most important factors is load factor. Each design of aircraft has its own *V-n* diagram. Here the *V-n* diagram is the same as RV-9 [8]. Since the airspeed is no more than 25 kts, a load factor of 1.5 is given, so the maximum stress is 276 MPa. For aluminum, the stress strain curve is shown in Figure 6. According to the calculation, the maximum stress is 4.118 MPa, which is far smaller than the upper yield point for aluminum, hence aluminum is safe to use.

3.2. Wing design simulation analysis

After the theoretical structural analysis has been performed by proving design requirement calculation and mechanical structure on wing parts, Solidworks and Catia V5 software have been used to design and simulation for this research. The load distribution is assume to be elliptical and the fixed support is at the edge of the wing, as shown in Figure 7. The wing is arranged as high wing location. The load distribution pressure is 7.784 N/m² as calculated by using area under the elliptical graph at the wing. The material of the wing is fixed foam, which has tensile strength of 7 lbs/sq.in. The properties of the material are 1.2 lb/ft³ of the weight and the density of the foam is 1.2 lbs/cu.ft.

Mesh analysis on the wing is done to get the grid solid region on the wing and to justify structural wing design for doing further element structural analysis. This is shown in Figure 8. Figure 9 shows that the value of bending stress of the wing using this software simulation is 5.42 MPa. The diagram shows that the structure is safe because most region of the wing is blue, which not in critical condition. The wing is safe to use in the UAV after doing structural analysis. The UAV wing span is 1.96 ft and the chord length is 0.54 ft. After doing simulation by using Solidworks 2014 software, it shows that the bending stress is 5.42 MPa. From manual calculation, the theoretical bending stress is found to be 4.26 MPa. There is a small difference with approximately 10% between both values.

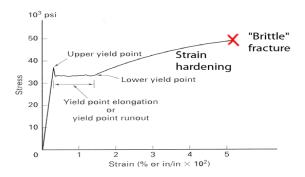


Figure 6. Stress-strain curve diagram [8]

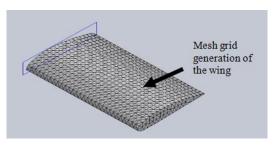


Figure 8. Mesh generation for wing

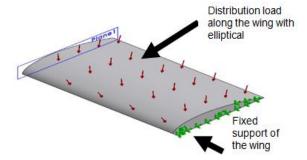


Figure 7. Load distribution applied along the wing

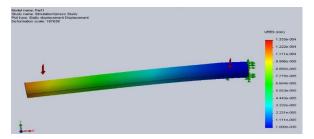


Figure 9. Von Mises stress analysis for wing

4. Conclusion

In this paper, the details of design, material selection and structural analysis on the wing of rotor UAV platform have been outlined. The designed Tiltrotor UAV is economical, moderately functional and an excellent platform for academic research purpose. By performing the structural analysis of the model, the results show that the design is safe for use. All in all, the objective of this project is achieved and it is ready to be fabricated for a flight test.

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