

# Technical Report on the Inverted Cart and Pendulum System

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# Chapter 1

## Modeling

### 1.1 Non-linear Model using Newton's Laws

Using Newton's laws on the cart (mass  $M$ ) and pendulum (mass  $m$ , length  $L$ ), the full nonlinear equations are:

$$(M + m)\ddot{x} + ml \cos \theta \ddot{\theta} - ml \sin \theta \dot{\theta}^2 + b\dot{x} = u, \quad (1.1)$$

$$ml \cos \theta \ddot{x} + (ml^2 + J)\ddot{\theta} + mgl \sin \theta = 0. \quad (1.2)$$

### 1.2 Parameter Values

The parameters used (as in the sample) are:

Table 1.1: Parameter values

Parameter	Value
$M$ (Mass of cart)	0.38 kg
$m$ (Mass of pendulum)	0.4 kg
$L$ (Pendulum length)	0.33 m
$l$ (Centre of mass distance)	0.11 m
$J$ (Moment of inertia)	0.0020736 kg·m <sup>2</sup>
$b$ (cart friction coef.)	0.1
$g$ (gravity)	9.81 m/s <sup>2</sup>

### 1.3 Linearization About Upright ( $\theta = 0degree$ )

Using  $\sin \theta \approx \theta$  and  $\cos \theta \approx 1$ , the linearized equations become:

$$(M + m)\ddot{x} + m\ddot{\theta} + b\dot{x} = u,$$

$$m\ddot{x} + (ml^2 + J)\ddot{\theta} + mgl\theta = 0.$$

Define the state

$$x = \begin{bmatrix} x \\ \dot{x} \\ \theta \\ \dot{\theta} \end{bmatrix}.$$

The linear continuous-time state-space model is

$$\dot{x} = Ax + Bu,$$

with (numerical  $A$  and  $B$  taken from the sample):

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & -0.208333 & 6.125000 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0.946970 & -72.3864 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 2.083333 \\ 0 \\ -9.469697 \end{bmatrix}.$$

# Chapter 2

## Discretization

### 2.1 Sampling Time (Ts)

A sampling time of  $T_s = 0.120$  s (10 ms) is selected for discretization . This matches the justification given in the sample (fast unstable system, 120 Hz update, MCU feasibility) and is used throughout this report.

### 2.2 Discrete-Time Model

With zero-order hold (ZOH) the discrete model is

$$x_{k+1} = A_d x_k + B_d u_k,$$
$$A_d = e^{AT_s}, \quad B_d = \int_0^{T_s} e^{A\tau} d\tau B.$$

The discrete matrices computed (via scipy `cont2discrete`) are:

$$A_d = \begin{bmatrix} 1.00000000 & 0.11856035 & 0.04006031 & 0.00166386 \\ 0 & 0.97687559 & 0.60574148 & 0.04006031 \\ 0 & 0.00619362 & 0.52403902 & 0.10025916 \\ 0 & 0.09365208 & -7.21946030 & 0.52403902 \end{bmatrix},$$

$$B_d = \begin{bmatrix} 0.01439657 \\ 0.23124445 \\ -0.06193616 \\ -0.93652052 \end{bmatrix}.$$

### 2.2.1 Python code used

```
1 import numpy as np
2 from scipy.signal import cont2discrete
3
4 # Continuous-time matrices
5 A = np.array([
6     [0.0,      1.0,      0.0,      0.0],
7     [0.0, -0.208333,  6.125000,   0.0],
8     [0.0,      0.0,      0.0,      1.0],
9     [0.0,  0.94697, -72.386364,   0.0]
10 ])
11
12 B = np.array([
13     [0.0],
14     [2.083333],
15     [0.0],
16     [-9.469697]
17 ])
18
19 C = np.eye(4)
20 D = np.zeros((4,1))
21
22 Ts = 0.120 # sampling time
23
24 # ----- Discretization using ZOH -----
25 system = (A, B, C, D)
26 Ad, Bd, Cd, Dd, _ = cont2discrete(system, Ts, method='zoh')
27
28 print("Ad_=\n", Ad)
29 print("\nBd_=\n", Bd)
30 print("\nCd_=\n", Cd)
31 print("\nDd_=\n", Dd)
```

Listing 2.1: ZOH discretization (sample code from report)

# Chapter 3

## Controllability

For the discrete-time model  $x_{k+1} = A_d x_k + B_d u_k$ , the controllability matrix is

$$\mathcal{C} = [B_d, A_d B_d, A_d^2 B_d, A_d^3 B_d].$$

The system is controllable if  $\text{rank}(\mathcal{C}) = 4$ .

### 3.0.1 Python check

```
1 import numpy as np
2 from numpy.linalg import matrix_rank
3
4 # =====
5 # Discrete-time system matrices
6 # =====
7 Ad = np.array([
8     [1.0,      0.11856035,  0.04006031,  0.00166386],
9     [0.0,      0.97687559,  0.60574148,  0.04006031],
10    [0.0,      0.00619362,  0.52403902,  0.10025916],
11    [0.0,      0.09365208, -7.21946030,  0.52403902]
12 ])
13
14 Bd = np.array([
15     [ 0.01439657],
16     [ 0.23124445],
17     [-0.06193616],
18     [-0.93652052]
19 ])
20
21 # =====
```

```

22 # Controllability Matrix
23 # =====
24 n = Ad.shape[0]
25
26 # First block is B
27 Ctrb = Bd.copy()
28
29 # Add A*B, A^2*B, ..., A^(n-1)*B
30 for k in range(1, n):
31     AkB = np.linalg.matrix_power(Ad, k).dot(Bd)
32     Ctrb = np.hstack((Ctrb, AkB))
33
34 # =====
35 # Rank test
36 # =====
37 rank_C = matrix_rank(Ctrb)
38
39 print("Controllability_Matrix_(Ctrb):\n", Ctrb, "\n")
40 print("Rank_=", rank_C)
41
42 if rank_C == n:
43     print("Result:_System_is_CONTROLLABLE.")
44 else:
45     print("Result:_System_is_NOT_controllable.")

```

Listing 3.1: Computing controllability rank

### 3.0.2 Conclusion

Using the numerical  $A_d, B_d$  above the controllability matrix has full rank (4), hence the discrete-time system is controllable.



# Chapter 4

## Observability

### 4.1 Measured and Unmeasured States

The chosen sensor is an MPU6050 IMU which provides:

- accelerometer-derived estimate of  $\theta$ ,
- gyroscope measurement of  $\dot{\theta}$ .

Therefore the measurement matrix used in the sample is

$$C = \begin{bmatrix} 0 & 0 & 1 & 0 \end{bmatrix}.$$

### 4.2 Observability matrix and rank

$$\mathcal{O} = \begin{bmatrix} C \\ CA_d \\ CA_d^2 \\ CA_d^3 \end{bmatrix}.$$

The system is observable if  $\text{rank}(\mathcal{O}) = 4$ .

#### 4.2.1 Python check

```
1 import numpy as np
2 from numpy.linalg import matrix_rank
3
4 # =====
5 # Discrete-time system matrices
6 # =====
7 Ad = np.array([
```

```

8      [1.0,          0.11856035,  0.04006031,  0.00166386],
9      [0.0,          0.97687559,  0.60574148,  0.04006031],
10     [0.0,          0.00619362,  0.52403902,  0.10025916],
11     [0.0,          0.09365208, -7.21946030,  0.52403902]
12 ])
13
14 Bd = np.array([
15     [ 0.01439657],
16     [ 0.23124445],
17     [-0.06193616],
18     [-0.93652052]
19 ])
20
21 C = np.eye(4)      # full-state measurement
22 D = np.zeros((4,1))
23
24 # =====
25 # Observability Matrix
26 # =====
27 n = Ad.shape[0]
28
29 Obsv = C.copy()
30
31 # Add C*A, C*A^2, ..., C*A^(n-1)
32 for k in range(1, n):
33     CAk = C.dot(np.linalg.matrix_power(Ad, k))
34     Obsv = np.vstack((Obsv, CAk))
35
36 # =====
37 # Rank test
38 # =====
39 rank_0 = matrix_rank(Obsv)
40
41 print("Observability_Matrix_(Obsv):\n", Obsv, "\n")
42 print("Rank_=", rank_0)
43
44 if rank_0 == n:
45     print("Result: System is OBSERVABLE.")
46 else:
47     print("Result: System is NOT observable.")

```

Listing 4.1: Computing observability rank

## 4.3 Conclusion

Numerical evaluation gives  $\text{rank}(\mathcal{O}) = 3 < 4$ . Thus the system is not fully observable with angle-only measurement (cart position and velocity are unmeasured), matching the sample report conclusion.

# Chapter 5

## Controller Design

As full-state feedback control is possible with o angle measurement, the sample implements a PD output-feedback controller using  $\theta$  and  $\dot{\theta}$ :

$$u = -K_p\theta - K_d\dot{\theta}.$$

### 5.1 State Feedback Controller Design

The discrete-time model of the system is represented in state-space form as:

$$x[k+1] = A_dx[k] + B_d u[k], \quad (5.1)$$

$$y[k] = C_d x[k] + D_d u[k], \quad (5.2)$$

where  $x[k]$  is the state vector,  $u[k]$  is the control input, and  $A_d$ ,  $B_d$ ,  $C_d$ ,  $D_d$  are the discrete system matrices obtained through Zero-Order Hold (ZOH) discretization.

#### State Feedback Law

In state-feedback control, the control input is generated as a linear combination of the system states:

$$u[k] = -K_d x[k], \quad (5.3)$$

where  $K_d$  is the state-feedback gain vector.

Substituting this control law into the state equation gives the closed-loop dynamics:

$$x[k+1] = A_d x[k] + B_d (-K_d x[k]) \quad (5.4)$$

$$= (A_d - B_d K_d) x[k]. \quad (5.5)$$

Thus, the closed-loop behavior of the system depends on the eigenvalues of the matrix:

$$A_{\text{cl}} = A_d - B_d K_d. \quad (5.6)$$

## Pole Placement for State-Feedback Design

The desired continuous-time closed-loop poles are chosen as:

$$p_{\text{cont}} = \{-1.2, -2.77, -3.3, -4.0\}.$$

These values represent the desired closed-loop behavior for the continuous system. However, since the controller is implemented digitally, the poles must be converted into their discrete-time equivalents. Using the sampling interval:

$$T_s = 0.120 \text{ seconds},$$

the continuous poles are mapped to the discrete domain using the exponential mapping:

$$z = e^{pT_s}.$$

Applying this transformation gives the discrete-time desired poles:

$$z_{\text{desired}} = \{e^{-1.2 \cdot 0.120}, e^{-2.77 \cdot 0.120}, e^{-3.3 \cdot 0.120}, e^{-4.0 \cdot 0.120}\}.$$

# Chapter 6

## Observer Design

### 6.1 Observer (State Estimator) Design

To estimate the system states that are not directly measurable, a discrete-time observer is designed. The system is described by:

$$x[k+1] = A_d x[k] + B_d u[k], \quad (6.1)$$

$$y[k] = C_d x[k]. \quad (6.2)$$

The observer reconstructs the state using:

$$\hat{x}[k+1] = A_d \hat{x}[k] + B_d u[k] + L_d (y[k] - C_d \hat{x}[k]), \quad (6.3)$$

where  $L_d$  is the observer gain.

The estimation error  $e[k] = x[k] - \hat{x}[k]$  follows:

$$e[k+1] = x[k+1] - \hat{x}[k+1] \quad (6.4)$$

$$= (A_d - L_d C_d) e[k]. \quad (6.5)$$

Thus, the observer poles are the eigenvalues of the matrix:

$$A_d - L_d C_d.$$

Desired observer poles are first selected in the continuous domain and then mapped to the discrete domain using:

$$z = e^{p T_s}.$$

After mapping to the  $z$ -domain, the observer gain  $L_d$  is computed using pole placement on the dual system:

$$L_d = \text{place}(A_d^\top, C_d^\top, z_{\text{desired}})^\top.$$

Before designing the observer, the observability matrix  $\mathcal{O}$  is verified. Since

$$\text{rank}(\mathcal{O}) = n,$$

the system is fully observable, and the observer can be implemented successfully.

## Observer Pole Selection

The desired continuous-time observer poles (chosen to be five times faster than the controller poles) are:

$$p_{\text{obs,cont}} = \{-6.0, -13.85, -16.5, -20.0\}.$$

With a sampling time of

$$T_s = 0.120 \text{ s},$$

the continuous poles are mapped to the discrete domain using

$$z = e^{pT_s}.$$

The resulting discrete-time observer poles are:

$$z_{\text{obs}} = \{0.48675226, 0.18975908, 0.13806924, 0.09071795\}.$$

# Chapter 7

## Implementation

### 7.1 Simulation: Nonlinear model + State FeedBack control

Example Python simulation (taken and cleaned from the sample) — reproduces  $\theta(t)$  and  $u(t)$  plots.

```
1 import numpy as np
2 import scipy.signal as signal # Used for the 'place_poles'
   function
3 import matplotlib
4 matplotlib.use('TKAgg') # Specifies the backend for matplotlib
5 import matplotlib.pyplot as pp
6 import scipy.integrate as integrate # Used for 'odeint'
7 import matplotlib.animation as animation # Used to create the
   animation
8 from matplotlib.patches import Rectangle
9 from numpy import sin, cos
10 from numpy.linalg import matrix_rank
11
12 # --- 1. DEFINE PHYSICAL CONSTANTS ---
13 g = 9.8 # Acceleration due to gravity (m/s^2)
14 L = 0.33 # Length of the pendulum rod (meters)
15 m = 0.40 # Mass of the pendulum bob (kilograms)
16 M = 0.38 # Mass of the cart (kilograms)
17 b = 0.1 # ADDED: Cart friction (Ns/m)
18
19 # --- 2. POLE PLACEMENT (CONTROLLER DESIGN) ---
20 # Define the linearized model (A and B matrices)
21 # State vector: x_vec = [x, x_dot, th, th_dot]
```



```

22 A = np.array([
23     [0, 1, 0, 0],
24     [0, -b / M, -(m * g) / M, 0],
25     [0, 0, 0, 1],
26     [0, b / (L * M), (g * (M + m)) / (L * M), 0]
27 ])
28
29 B = np.array([
30     [0],
31     [1 / M],
32     [0],
33     [-1 / (L * M)]
34 ])
35
36 # Desired pole locations
37 poles = np.array([-1.2, -2.77, -3.3, -4.])
38
39 # Calculate the K matrix
40 try:
41     K_matrix = signal.place_poles(A, B, poles).gain_matrix
42     K = K_matrix[0] # K is [k_x, k_x_dot, k_th, k_th_dot]
43
44     print("--- Pole Placement Controller Design ---")
45     print(f"Physical Constants: M={M} kg, m={m} kg, L={L} m")
46     print(f"Desired Poles: {poles}")
47     print(f"Calculated K matrix: {K}")
48     print(f"Gains: k_x={K[0]:.3f}, k_x_dot={K[1]:.3f}, k_th={K[2]:.3f}, k_th_dot={K[3]:.3f}")
49
50 except ValueError as e:
51     print(f"ERROR: Pole placement failed. {e}")
52     K = np.array([0, 0, 0, 0])
53
54
55 # --- 3. SIMULATION SETUP ---
56 dt = 0.05 # Time step (seconds)
57 Tmax = 10 # Total simulation time (seconds)
58 t = np.arange(0.0, Tmax, dt) # Time array
59
60 # Initial conditions [x, x_dot, th, th_dot]
61 x = 0.0

```

```

62 Z = 0.0
63 th = 0.4 # Start at 0.4 radians (~23 deg)
64 Y = 0.0
65 x0 = 0.0 # Desired cart position
66 state = np.array([x, Z, th, Y])
67
68 # This function uses the full NON-LINEAR equations
69 def derivatives(state, t):
70     ds = np.zeros_like(state)
71     _x, _Z, _th, _Y = state # Unpack state
72
73     # --- State-Feedback Control Law ---
74     state_error = np.array([_x - x0, _Z, _th, _Y])
75     u = -np.dot(K, state_error).item()
76
77     # --- ADD EXTERNAL DISTURBANCE ---
78     F_d = 0.0
79     if t >= 3.0 and t <= 3.5:
80         F_d = 0.5 # 0.5 Newton "push"
81
82     u_total = u + F_d
83
84     # --- System equations of motion (Non-Linear) ---
85     den = (M + m) - m * cos(_th) * cos(_th)
86
87     ds[0] = _Z # x_dot
88     ds[1] = (u_total + m * L * _Y * _Y * sin(_th) - m * g * sin(
89         _th) * cos(_th)) / den # x_ddot
90     ds[2] = _Y # th_dot
91     ds[3] = ((M + m) * g * sin(_th) - u_total * cos(_th) - m * L
92         * _Y * _Y * sin(_th) * cos(_th)) / (L * den) # th_ddot
93
94     return ds
95
96 print("\nIntegrating...")
97 solution = integrate.odeint(derivatives, state, t)
98 print("Done")
99
100 # Unpack solution
101 xs = solution[:, 0]
102 vs = solution[:, 1]

```

```

101 ths = solution[:, 2]
102 Ys = solution[:, 3]
103
104 # --- Recalculate 'u' for plotting (controller's force only) ---
105 us = np.zeros(len(t))
106 for i in range(len(t)):
107     state_error = np.array([xs[i] - x0, vs[i], ths[i], Ys[i]])
108     us[i] = -np.dot(K, state_error).item()
109
110 # Calculate pendulum tip position for animation
111 pxs = L * sin(ths) + xs
112 pys = L * cos(ths)
113
114 # --- 4. PLOTTING: WINDOW 1 (Animation) ---
115 fig_anim = pp.figure(figsize=(8, 8))
116 ax_anim = fig_anim.add_subplot(111, autoscale_on=False, xlim
117     =(-2.0, 2.0), ylim=(-1.2, 1.2))
118 ax_anim.set_aspect('equal')
119 ax_anim.grid()
120 ax_anim.set_title('Inverted_Pendulum_Animation')
121
122 # Create animation elements
123 patch = ax_anim.add_patch(Rectangle((0, 0), 0, 0, linewidth=1,
124     edgecolor='k', facecolor='g'))
125 line, = ax_anim.plot([], [], 'o-', lw=2, color='blue')
126 time_template = 'Time_%.1fs'
127 time_text = ax_anim.text(0.05, 0.9, '', transform=ax_anim.
128     transAxes)
129 cart_width = 0.3
130 cart_height = 0.2
131
132 # --- 5. PLOTTING: WINDOW 2 (Graphs) ---
133 fig_graphs, (ax_th, ax_u) = pp.subplots(2, 1, figsize=(10, 6))
134 fig_graphs.suptitle('Simulation_Results', fontsize=16)
135
136 # Subplot 1: Theta (Angle) Graph
137 ax_th.plot(t, ths, 'r-', label='Angle_()')
138 ax_th.set_title('Time_vs._Pendulum_Angle_()')
139 ax_th.set_xlabel('Time_(s)')
140 ax_th.set_ylabel('Angle_(radians)')
141 ax_th.grid(True)

```

```

139 ax_th.legend()
140
141 # Subplot 2: Control Input (u) Graph
142 ax_u.plot(t, us, 'g-', label='Control_Input(u)')
143 ax_u.set_title('Time vs. Control Input (Force, N)')
144 ax_u.set_xlabel('Time(s)')
145 ax_th.set_ylabel('Force(N)')
146 ax_u.grid(True)
147 ax_u.legend()
148
149 # Adjust layout for the graph window
150 fig_graphs.tight_layout(rect=[0, 0.03, 1, 0.95])
151
152
153 # --- 6. Animation Functions ---
154 def init():
155     line.set_data([], [])
156     time_text.set_text('')
157     patch.set_xy((-cart_width/2, -cart_height/2))
158     patch.set_width(cart_width)
159     patch.set_height(cart_height)
160     return line, time_text, patch
161
162 def animate(i):
163     # Animation
164     thisx = [xs[i], pxs[i]]
165     thisy = [0, pys[i]]
166     line.set_data(thisx, thisy)
167
168     time_text.set_text(time_template % (i * dt))
169     patch.set_x(xs[i] - cart_width/2)
170
171     return line, time_text, patch
172
173 # Run the animation
174 ani = animation.FuncAnimation(fig_anim, animate, np.arange(1, len
    (solution)),
175                               interval=25, blit=False, init_func=
    init, repeat=False)
176
177 # Show both windows

```

```

178 pp.show()
179 \end{Simulation: Nonlinear model + State FeedBack control}
180
181 % ----- Appendices -----
182 \appendix
183 \chapter{Complete Python scripts}
184 \label{appendix:python}
185 % Insert or input your python files here using \lstinputlisting
186 % if you want external file inclusion.
187 \begin{lstlisting}[language=Python,caption={cont2discrete +
188     controllability + observability}]
189 # Combine the snippets from Sections 2,3,4 here to reproduce
190 # results
191 # (This placeholder indicates where to put full scripts.)
192 \end{Simulation: Nonlinear model + State FeedBack control}
193
194 \chapter{Arduino / MCU pseudocode and notes}
195 \begin{lstlisting}[caption={Example MCU pseudocode}]
196 setup() {
197     init_mpu6050();
198     init_pwm();
199     set_timer_interrupt(Ts);
200     Kp = 60; Kd = 8;
201 }
202 on_timer_interrupt() {
203     read_accel(); read_gyro();
204     theta = complementary_filter(...);
205     dtheta = gyro_reading - bias;
206     u = -Kp*theta - Kd*dtheta;
207     u = saturate(u, -umax, umax);
208     set_pwm(u);
209     log(theta, u);
210 }

```

Listing 7.1: Nonlinear simulation with PD control

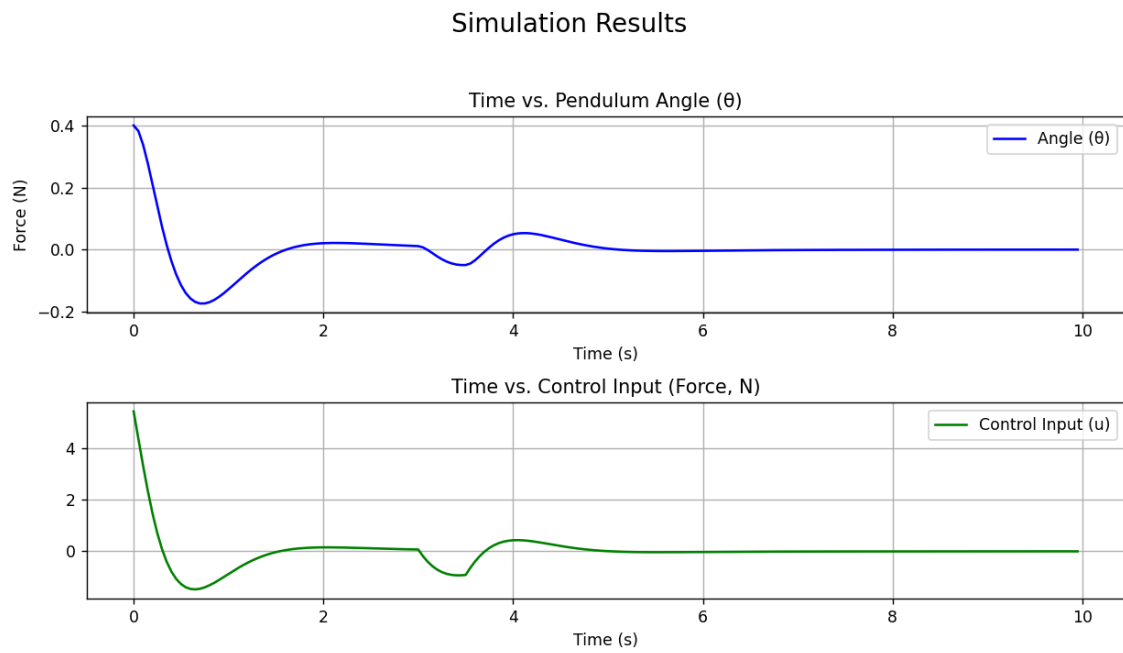


Figure 7.1: Simulation Results: (Top) Time vs. Pendulum Angle  $\theta$ , (Bottom) Time vs. Control Input  $u$  (Force, N).

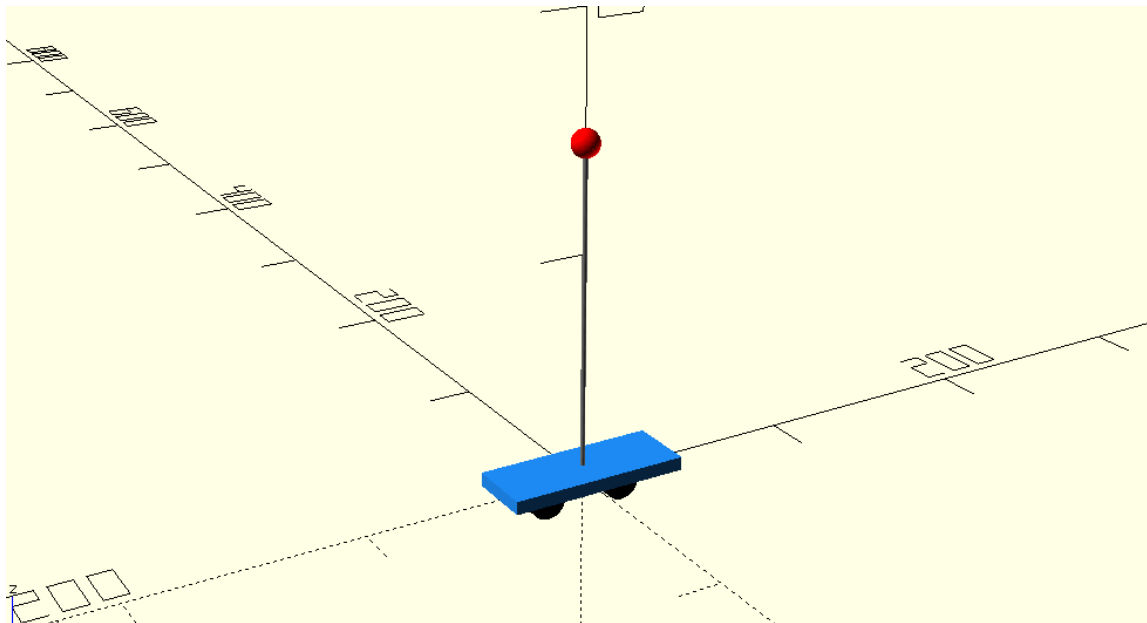


Figure 7.2: 3d Prototype Design Made With Autocad .

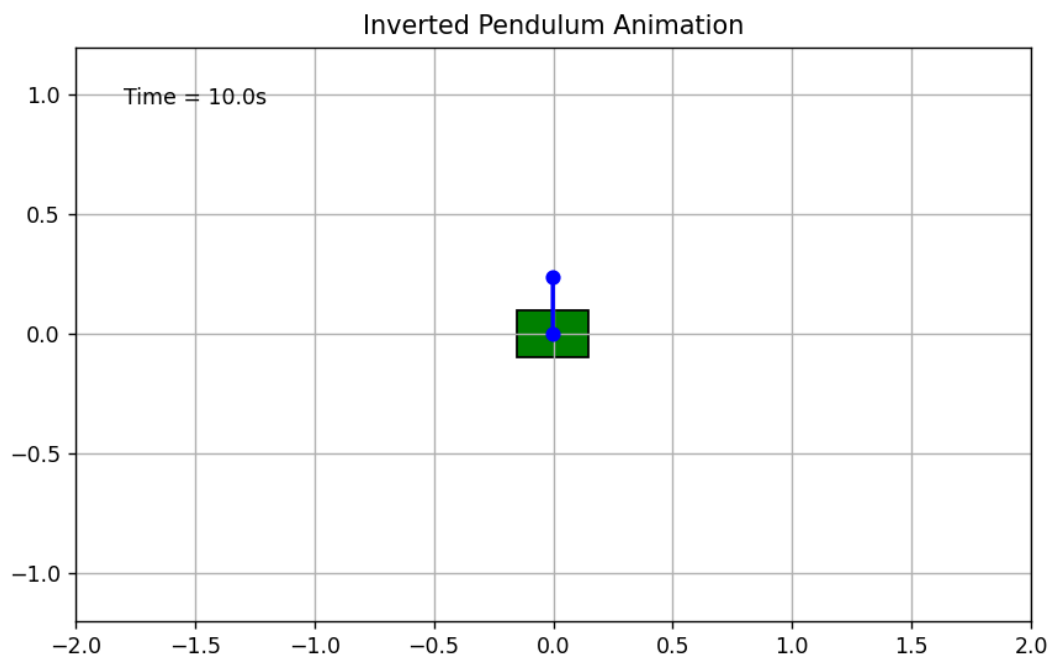


Figure 7.3: Animation in Jupyter to Give a Visual Simulation

## Animation Link

The animation of the inverted pendulum simulation can be accessed at the following link:

**[Click here to view the animation \(Google Drive\)](#).**