

# Analysis of Channel Impairments in Quadrature Demodulation Systems

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## 1 Introduction

Quadrature Amplitude Modulation (QAM) is foundational to modern communication systems, allowing two independent signals,  $x_I(t)$  and  $x_Q(t)$ , to be sent on the same carrier frequency,  $f_c$ . This is achieved by using two carriers in quadrature (90° out of phase). This report analyzes the mathematical principles of quadrature modulation and the impact of several real-world channel impairments.

## 2 Quadrature Modulator Principle

The project first asks to prove the complex-number representation of the quadrature modulator output. The modulator diagram shows the output  $x_{bp}(t)$  as:

$$x_{bp}(t) = x_I(t) \cos(2\pi f_c t) - x_Q(t) \sin(2\pi f_c t)$$

We must prove this is equivalent to  $x_{bp}(t) = \text{Re}\{[x_I(t) + jx_Q(t)]e^{j2\pi f_c t}\}$ .

### Proof

We start with the complex expression and use Euler's formula,  $e^{j\theta} = \cos(\theta) + j \sin(\theta)$ :

$$y(t) = \text{Re}\{[x_I(t) + jx_Q(t)] \cdot [\cos(2\pi f_c t) + j \sin(2\pi f_c t)]\}$$

We expand the multiplication:

$$y(t) = \text{Re}\{[x_I(t) \cos(2\pi f_c t) + jx_I(t) \sin(2\pi f_c t) + jx_Q(t) \cos(2\pi f_c t) + j^2 x_Q(t) \sin(2\pi f_c t)]\}$$

Using  $j^2 = -1$  and grouping real and imaginary parts:

$$y(t) = \text{Re}\{\underbrace{[x_I(t) \cos(2\pi f_c t) - x_Q(t) \sin(2\pi f_c t)]}_{\text{Real Part}} + j[x_I(t) \sin(2\pi f_c t) + x_Q(t) \cos(2\pi f_c t)]\}$$

Taking the real part,  $\text{Re}\{\dots\}$ , leaves:

$$y(t) = x_I(t) \cos(2\pi f_c t) - x_Q(t) \sin(2\pi f_c t)$$

This matches  $x_{bp}(t)$ , completing the proof.

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### 3 Analysis of Channel with Phase Error (Noise-Free)

This section analyzes the effect of a channel that introduces an attenuation  $\alpha$  and a phase shift  $\phi$ , but no noise. The received signal is:

$$y(t) = \text{Re}\{\alpha x_I(t) e^{j\phi} e^{j2\pi f_c t}\}$$

Using the angle-addition identity  $\cos(A + B) = \cos A \cos B - \sin A \sin B$ , we can write  $y(t)$  in real terms:

$$y(t) = \text{Re}\{\alpha x_I(t) e^{j(2\pi f_c t + \phi)}\} = \alpha x_I(t) \cos(2\pi f_c t + \phi)$$

This signal enters an ideal quadrature demodulator.

#### I-Channel (Top Path) Recovery

The signal  $y(t)$  is multiplied by  $\cos(2\pi f_c t)$ :

$$v_1(t) = y(t) \cdot \cos(2\pi f_c t) = \alpha x_I(t) \cos(2\pi f_c t + \phi) \cos(2\pi f_c t)$$

Using the identity  $\cos A \cos B = \frac{1}{2}[\cos(A - B) + \cos(A + B)]$ :

$$v_1(t) = \frac{\alpha x_I(t)}{2} [\cos(\phi) + \cos(4\pi f_c t + \phi)]$$

The Low-Pass Filter (LPF) removes the high-frequency  $2f_c$  term, leaving:

$$y_1(t) = \frac{\alpha x_I(t)}{2} \cos(\phi)$$

#### Q-Channel (Bottom Path) Recovery

The signal  $y(t)$  is multiplied by  $-\sin(2\pi f_c t)$ :

$$v_2(t) = y(t) \cdot [-\sin(2\pi f_c t)] = -\alpha x_I(t) \cos(2\pi f_c t + \phi) \sin(2\pi f_c t)$$

Using the identity  $\cos A \sin B = \frac{1}{2}[\sin(A + B) - \sin(A - B)]$ :

$$v_2(t) = -\frac{\alpha x_I(t)}{2} [\sin(4\pi f_c t + \phi) - \sin(\phi)] = \frac{\alpha x_I(t)}{2} \sin(\phi) - \dots \text{High Freq}$$

The LPF removes the high-frequency term, leaving:

$$y_2(t) = \frac{\alpha x_I(t)}{2} \sin(\phi)$$

This shows that a phase error  $\phi$  causes the desired signal in the I-channel to be attenuated by  $\cos(\phi)$ , while "crosstalk" (an unwanted copy of the I-channel signal) leaks into the Q-channel, scaled by  $\sin(\phi)$ .

### 4 Analysis of Channel with Differential Delay

This section analyzes a different impairment model where the channel introduces a base delay  $t_a$  to both paths, but an additional \*differential delay\*  $t_d$  to the Q-path only. The received signal  $y(t)$  is:

$$y(t) = \alpha x_I(t - t_a) \cos(2\pi f_c t) - \alpha x_Q(t - t_a - t_d) \sin(2\pi f_c t)$$

This signal enters an ideal demodulator.

### I-Channel Recovery

$$v_1(t) = y(t) \cdot \cos(2\pi f_c t)$$

$$v_1(t) = \alpha x_I(t - t_a) \cos^2(2\pi f_c t) - \alpha x_Q(t - t_a - t_d) \sin(2\pi f_c t) \cos(2\pi f_c t)$$

After applying trigonometric identities and low-pass filtering, the high-frequency terms are removed:

$$y_1(t) = \frac{\alpha}{2} x_I(t - t_a)$$

### Q-Channel Recovery

$$v_2(t) = y(t) \cdot [-\sin(2\pi f_c t)]$$

$$v_2(t) = -\alpha x_I(t - t_a) \cos(2\pi f_c t) \sin(2\pi f_c t) + \alpha x_Q(t - t_a - t_d) \sin^2(2\pi f_c t)$$

After filtering, the output is:

$$y_2(t) = \frac{\alpha}{2} x_Q(t - t_a - t_d)$$

This shows that the I-signal is recovered correctly (with delay  $t_a$ ), but the Q-signal is recovered with an additional delay  $t_d$ , misaligning it with the I-signal.

## 5 BER Analysis with Attenuation and Phase Error

This section analyzes a Binary PAM system ( $x_I = \pm A$ ,  $x_Q = 0$ ) with attenuation  $\alpha$ , phase error  $\phi$ , and Complex White Gaussian Noise  $n(t) \sim CN(0, 2\sigma^2)$ .

### 5.1 Demodulator Model with Impairments

The received signal  $r(t)$  includes the attenuated signal and noise:

$$r(t) = [\alpha x_I(t) + n_I(t)] \cos(2\pi f_c t) - n_Q(t) \sin(2\pi f_c t)$$

The receiver's local oscillator has a phase error  $\phi$ , so the I-path LO is  $\cos(2\pi f_c t + \phi)$ . The output of the I-path LPF is the decision variable  $Y_1$ :

$$Y_1 = \underbrace{\frac{\alpha x_I}{2} \cos(\phi)}_{\text{Signal Part}} + \underbrace{\frac{1}{2} n_I \cos(\phi) + \frac{1}{2} n_Q \sin(\phi)}_{\text{Noise Part } n'}$$

### 5.2 Noise and Error Probability Derivation

The noise  $n(t) \sim CN(0, 2\sigma^2)$  means the total variance is  $2\sigma^2$ , so the independent components  $n_I$  and  $n_Q$  each have a variance of  $\sigma^2$ .

$$\text{Var}[n_I] = \sigma^2 \quad \text{and} \quad \text{Var}[n_Q] = \sigma^2$$

The variance of the noise at the decision point,  $\sigma_{n'}^2$ , is:

$$\sigma_{n'}^2 = \text{Var} \left[ \frac{1}{2} n_I \cos(\phi) \right] + \text{Var} \left[ \frac{1}{2} n_Q \sin(\phi) \right]$$

$$\sigma_{n'}^2 = \frac{1}{4} \cos^2(\phi) \text{Var}[n_I] + \frac{1}{4} \sin^2(\phi) \text{Var}[n_Q]$$

$$\sigma_{n'}^2 = \frac{1}{4} \cos^2(\phi)(\sigma^2) + \frac{1}{4} \sin^2(\phi)(\sigma^2) = \frac{\sigma^2}{4} (\cos^2(\phi) + \sin^2(\phi)) = \frac{\sigma^2}{4}$$

The standard deviation of the noise is  $\sigma_{n'} = \sqrt{\sigma^2/4} = \frac{\sigma}{2}$ .

The general probability of error  $P_e$  (assuming  $x_I = A$  was sent) is:

$$P_e = P(Y_1 < 0) = Q\left(\frac{\text{Signal Part}}{\text{Noise Std Dev}}\right) = Q\left(\frac{\frac{\alpha A}{2} \cos(\phi)}{\frac{\sigma}{2}}\right)$$

$$P_e = Q\left(\frac{\alpha A \cos(\phi)}{\sigma}\right)$$

### 5.3 Comparison of Ideal vs. Impaired BER

The project asks to find the error probability for two cases.

#### 1. Probability of Error WITHOUT Channel Effect

This is the ideal case, where  $\alpha = 1$  (no attenuation) and  $\phi = 0$  (no phase error).

$$P_e(\text{ideal}) = Q\left(\frac{1 \cdot A \cdot \cos(0)}{\sigma}\right) = Q\left(\frac{A}{\sigma}\right)$$

#### 2. Probability of Error WITH Channel Effect

Here, we use the given parameters  $\alpha = 0.2$  and  $\phi = \pi/4$ .

$$P_e(\text{channel}) = Q\left(\frac{0.2 \cdot A \cdot \cos(\pi/4)}{\sigma}\right)$$

Since  $\cos(\pi/4) = 1/\sqrt{2}$ :

$$P_e(\text{channel}) = Q\left(\frac{0.2 \cdot A \cdot (1/\sqrt{2})}{\sigma}\right) = Q\left(\frac{0.2A}{\sqrt{2}\sigma}\right) \approx Q\left(\frac{0.1414A}{\sigma}\right)$$

The channel impairments significantly reduce the argument of the Q-function, which will dramatically increase the bit error rate.

## 6 Analysis of the 3D Error Surface

The 3D surface plot visualizes the general  $P_e$  formula,  $P_e = Q\left(\frac{\alpha A \cos(\phi)}{\sigma}\right)$ , by plotting  $\log_{10}(P_e)$  as a function of  $\alpha$  and  $\phi$ . The resulting plot confirms the theory:

- **Best Performance (Blue Valley):** The error is lowest (Z-axis is most negative) when  $\alpha$  is close to 1 (low attenuation) and  $\phi$  is 0 or  $2\pi$ . Here,  $\cos(\phi) = 1$ , maximizing the signal component.
- **Catastrophic Error (Yellow Ridges):** The error is highest (Z-axis close to 0) in two scenarios:

1. **Phase Quadrature** ( $\phi = \pi/2, 3\pi/2$ ): Here,  $\cos(\phi) = 0$ . The signal component becomes zero, and the receiver is just guessing based on noise. This leads to  $P_e = Q(0) = 0.5$ , so  $\log_{10}(P_e) \approx -0.3$ .
  2. **Phase Inversion** ( $\phi = \pi$ ): Here,  $\cos(\phi) = -1$ . The signal is inverted, causing the receiver to make the wrong decision on nearly every bit. This leads to  $P_e \approx 1$ , so  $\log_{10}(P_e) = 0$ .
- **Effect of Attenuation** ( $\alpha$ ): As  $\alpha$  approaches 0, the argument of the Q-function goes to zero for all  $\phi$ . This causes  $P_e$  to approach 0.5 (random guessing). The plot correctly shows the entire surface rising to the yellow region as  $\alpha \rightarrow 0$ .

## 7 Conclusion

This report successfully modeled several key principles and impairments in a quadrature communication system. The derivations showed how the complex-number notation represents the modulator, how phase error creates crosstalk, how differential delay de-synchronizes the I and Q channels, and how attenuation and phase error jointly impact the bit error rate. The final 3D plot provided a clear visualization of this relationship.