

## Book and Course Evaluation

- Book:

Control System Engineering

Author: Norman Nise

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Control System Engineering

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- Evaluation:

3 quizzes  $3 \times 15 = 45\%$

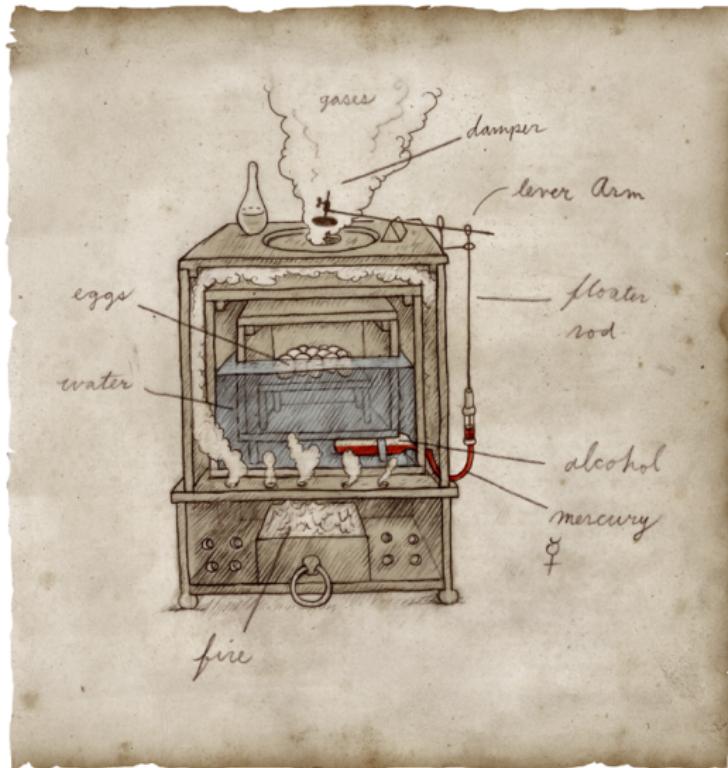
Matlab assignment 5%

End sem 50%

## Cornelis Drebbel (1572-1633)



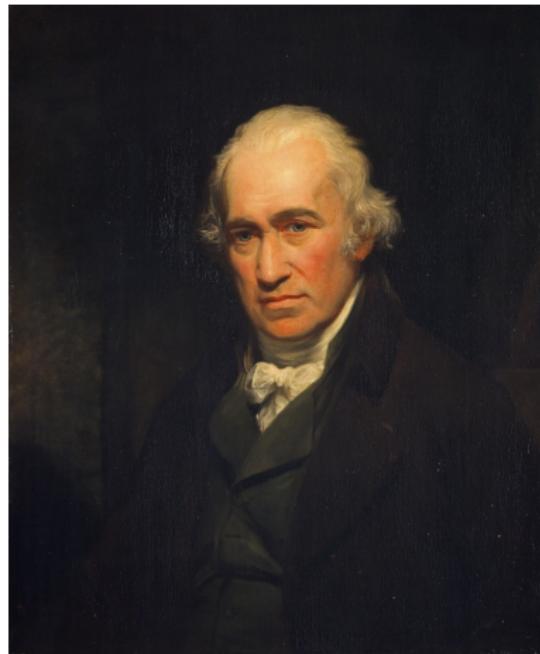
# Drebbel's Constant Temperature Oven



## Christiaan Huygens (1629-1695)



## James Watt (1736-1819)



## Centrifugal Governor in Steam Engine

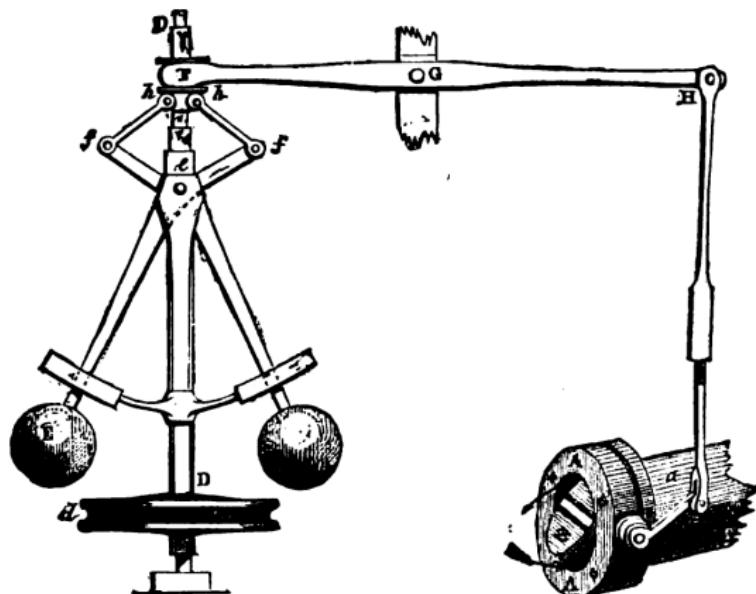


FIG. 4.—Governor and Throttle-Valve.

James Clerk Maxwell (1831-1879)



## James Clerk Maxwell (1831-1879)



- First paper in Control Theory

On governors, *Proceedings of the Royal Society of London*, 1868.

## Negative Feedback Amplifier

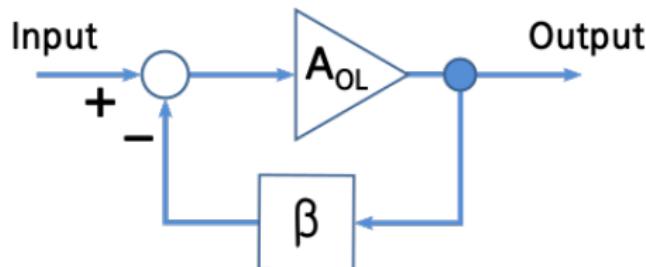
- Year of invention: 1927

Inventor: Harold Black (1898-1983)

# Negative Feedback Amplifier

- Year of invention: 1927

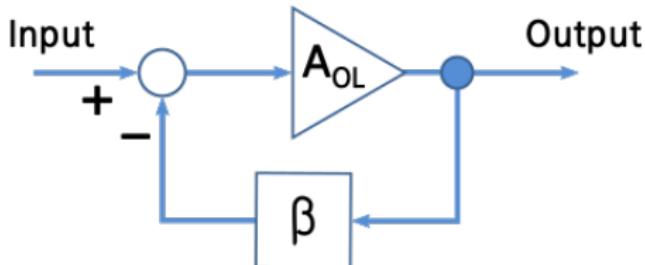
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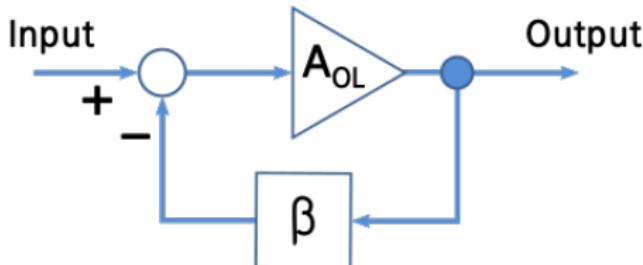
- Feedback gain:

$$A_{FL} = \frac{V_{out}}{V_{in}} = \frac{A_{OL}}{1 + \beta A_{OL}}$$

# Negative Feedback Amplifier

- Year of invention: 1927

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- Feedback gain:

$$A_{FL} = \frac{V_{out}}{V_{in}} = \frac{A_{OL}}{1 + \beta A_{OL}}$$

- If  $A_{OL} \gg 1$ , then  $A_{FL} \approx \frac{1}{\beta}$

## Harry Nyquist (1889-1976)

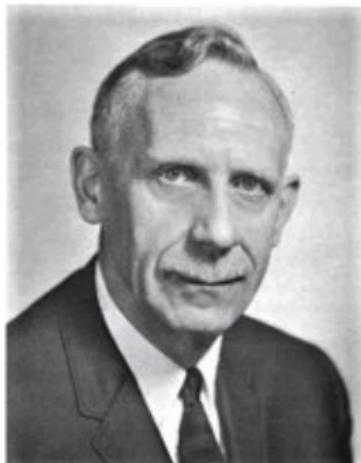


## Harry Nyquist (1889-1976)



- Nyquist stability criteria
- Year: 1932

## Hendrik Bode (1905-1982)



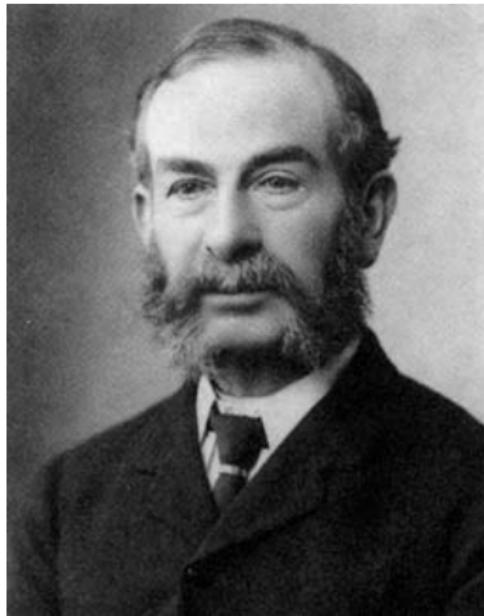
## Hendrik Bode (1905-1982)



- Bode plot
- Year: 1930s

## Routh-Hurwitz Stability Criterion

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Edward Routh

1876



Adolf Hurwitz

1895

Aleksandr Lyapunov (1857-1918)

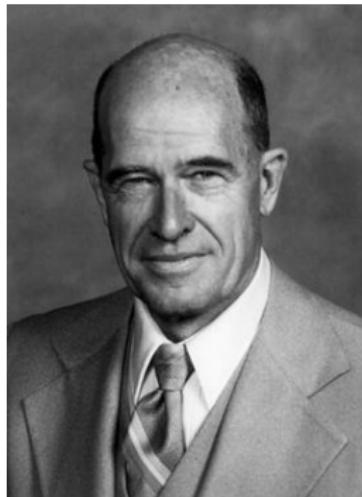


## Aleksandr Lyapunov (1857-1918)

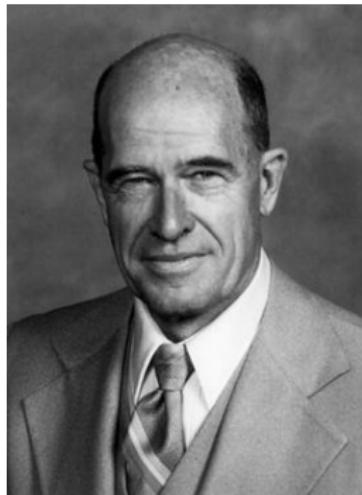


- Lyapunov stability
- Year: 1892

## Walter Evans (1920-1999)



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- Root locus
- Year: 1948

# Rudolf Kalman (1930-2016)



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- Kalman filtering

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- Kalman filtering
- Controllability, Observability, Kalman decomposition
- Optimal Control

The images are sourced from the [Wikipedia](#) website and the book [Control Systems Engineering](#) by Norman Nise. The author extends gratitude to these sources.

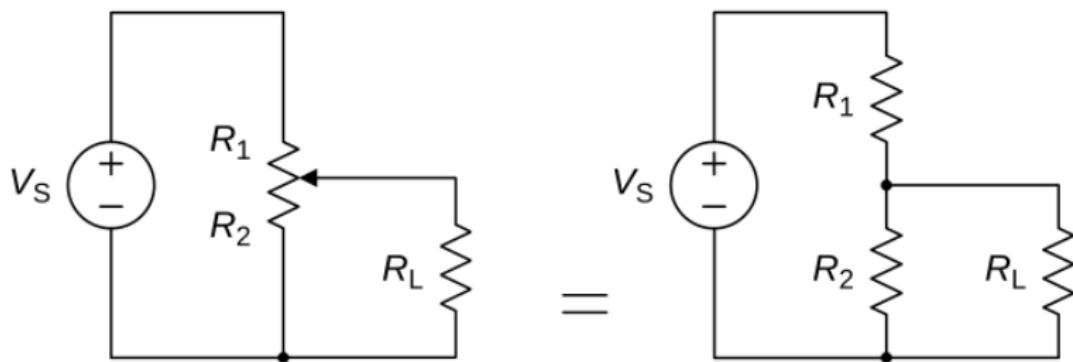
## ISRO Antenna used in Chandrayan Mission



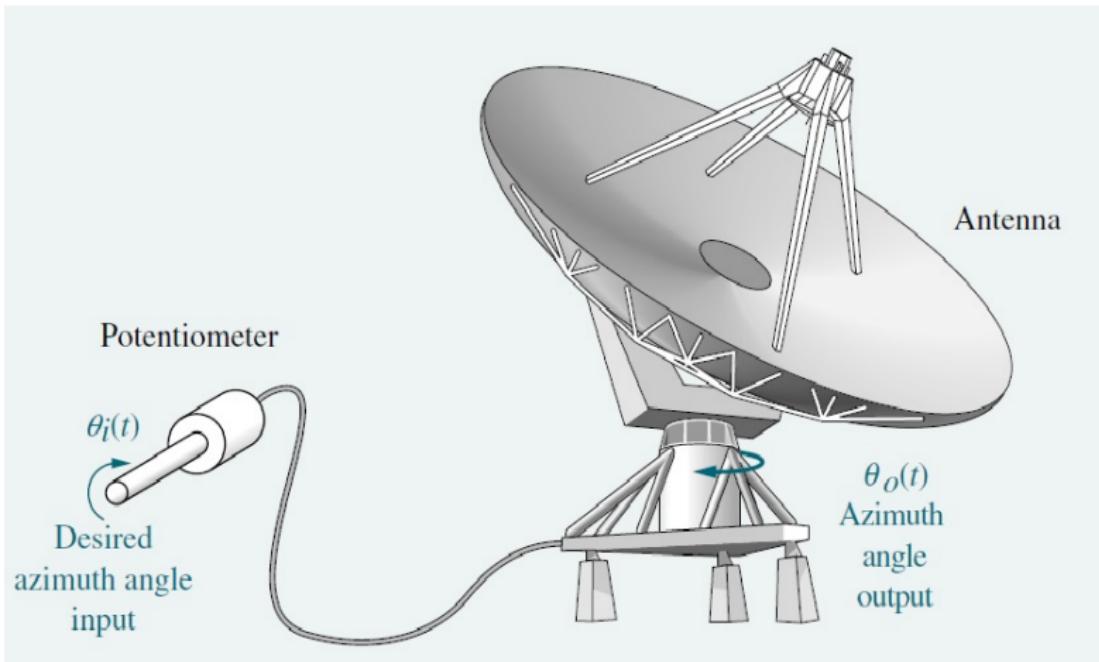
# Potentiometer



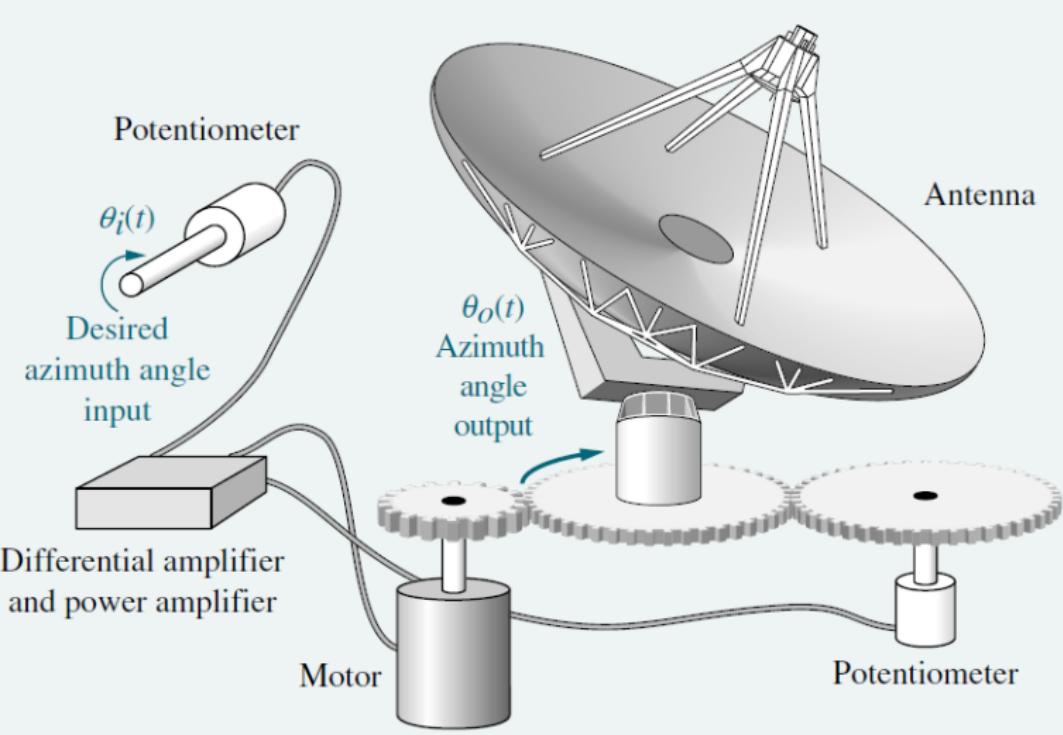
## Potentiometer



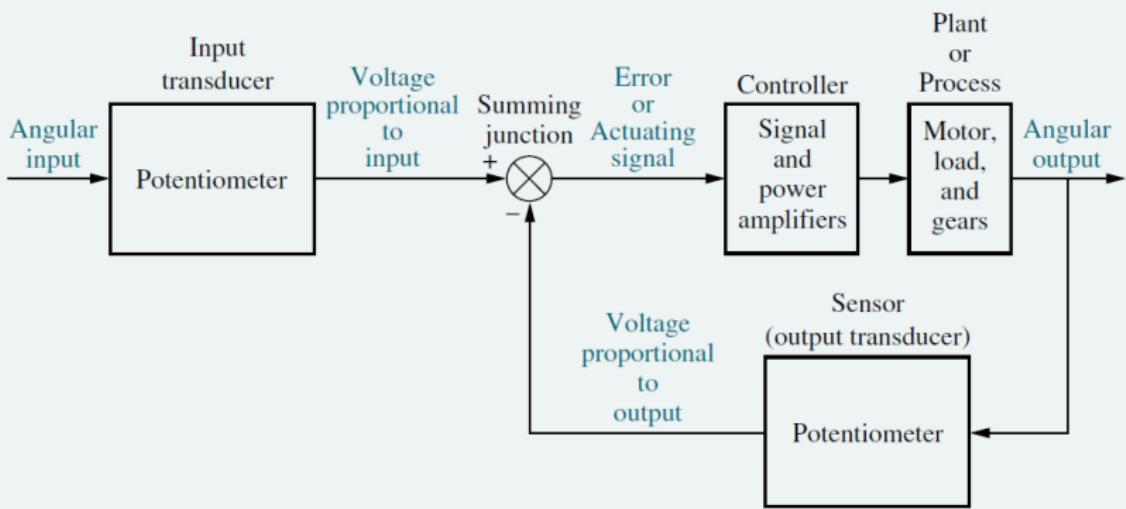
## Potentiometer with Antenna



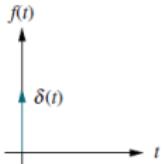
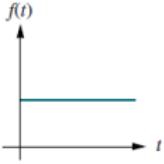
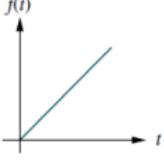
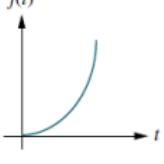
# Antenna Position Control System



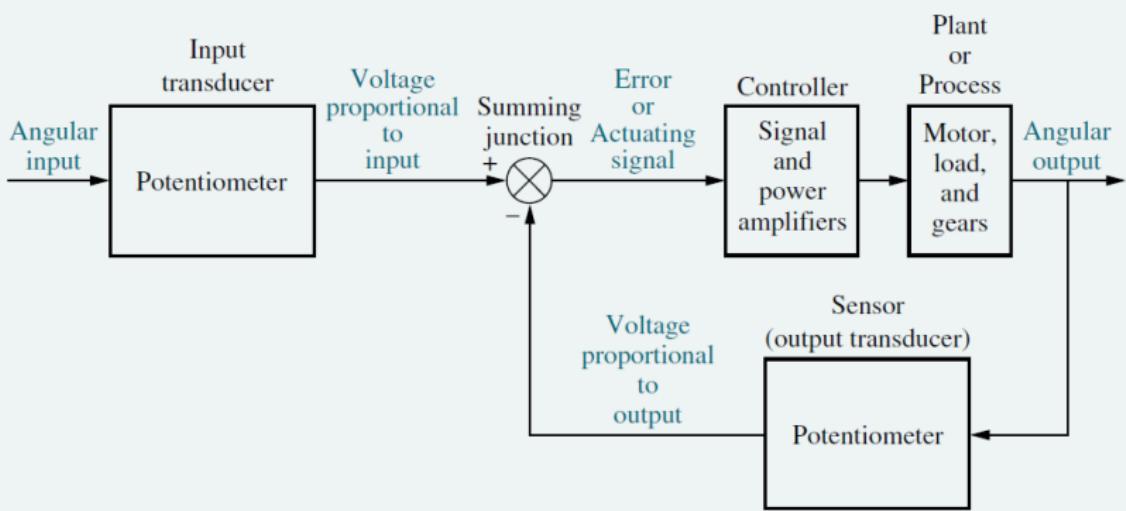
# Block Diagram



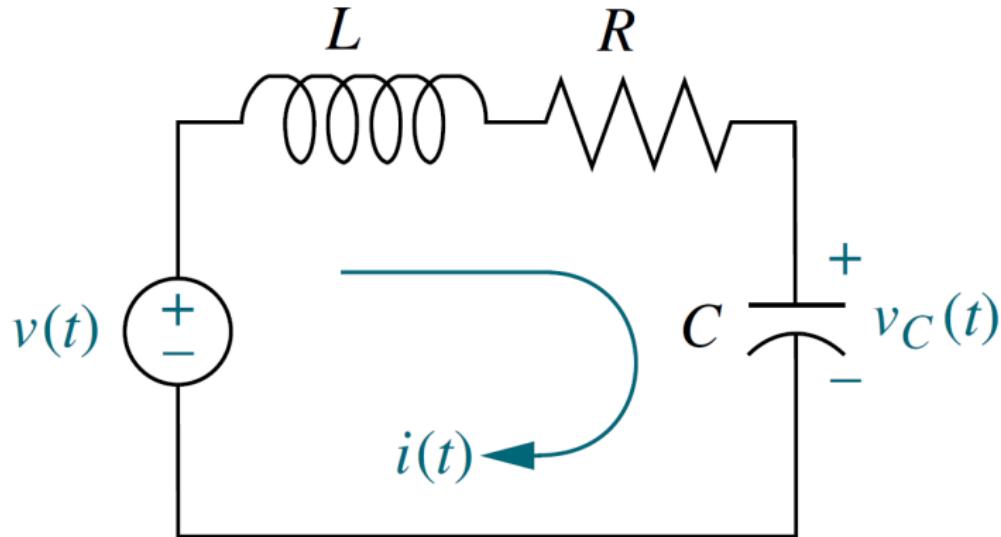
# Test Signals

| Input    | Function             | Description  | Sketch   |
|----------|----------------------|--|--|
| Impulse  | $\delta(t)$          | $\delta(t) = \infty$ for $0- < t < 0+$<br>$= 0$ elsewhere<br>$\int_{0-}^{0+} \delta(t) dt = 1$ |  |
| Step     | $u(t)$               | $u(t) = 1$ for $t > 0$<br>$= 0$ for $t < 0$  |  |
| Ramp     | $tu(t)$              | $tu(t) = t$ for $t \geq 0$<br>$= 0$ elsewhere  |  |
| Parabola | $\frac{1}{2}t^2u(t)$ | $\frac{1}{2}t^2u(t) = \frac{1}{2}t^2$ for $t \geq 0$<br>$= 0$ elsewhere                        |  |

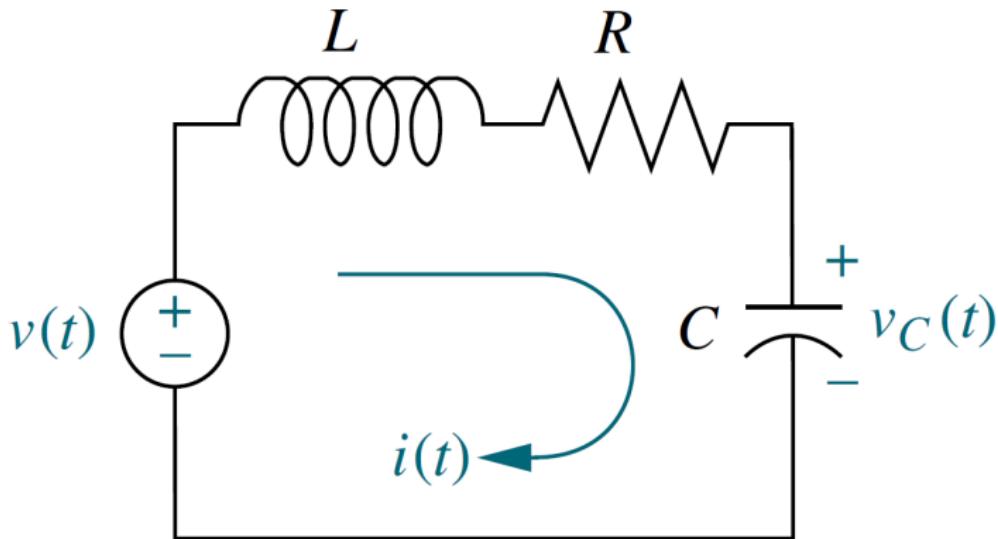
# Block Diagram



RLC

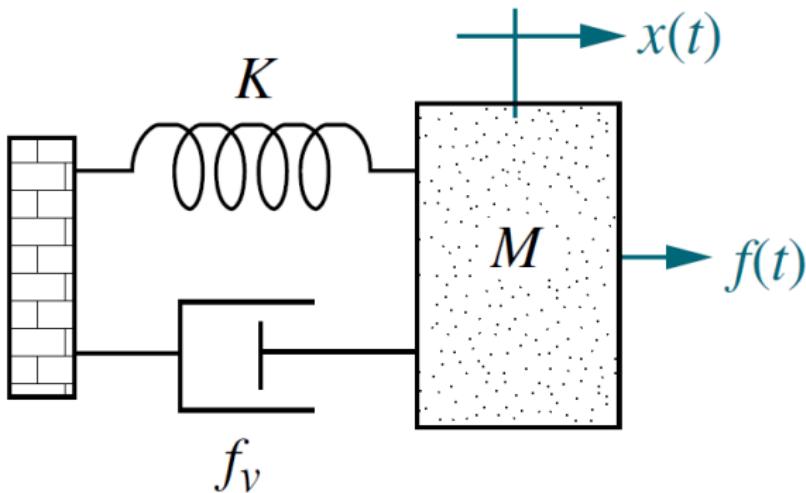


RLC

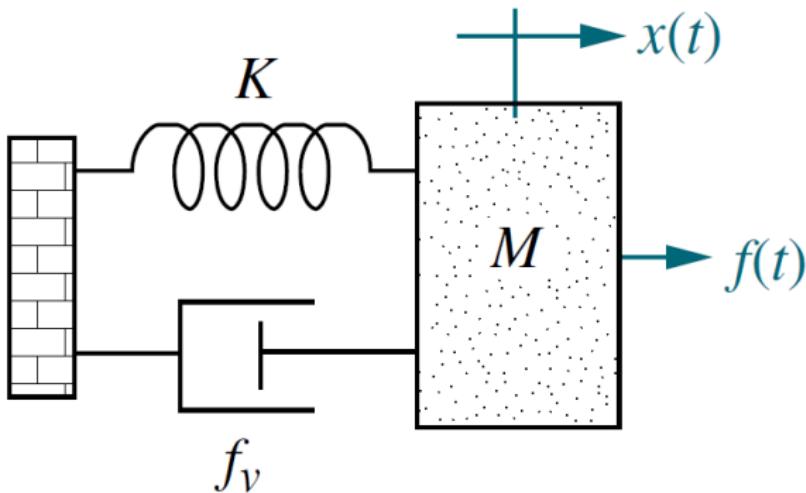


$$LC \frac{d^2 v_c(t)}{dt^2} + RC \frac{dv_c(t)}{dt} + v_c(t) = v(t)$$

## Mass Spring Damper System



## Mass Spring Damper System



$$M \frac{d^2x(t)}{dt^2} + f_v \frac{dx(t)}{dt} + Kx(t) = f(t)$$

## Linear Constant Coefficient Ordinary Differential Equation

$$a_n \frac{d^n y(t)}{dt^n} + a_{n-1} \frac{d^{n-1} y(t)}{dt^{n-1}} + \dots + a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_n \frac{d^n r(t)}{dt^n} + b_{n-1} \frac{d^{n-1} r(t)}{dt^{n-1}} + \dots + b_1 \frac{dr(t)}{dt} + b_0 r(t)$$

## Laplace Transform

$$F(s) := \int_{0^-}^{\infty} f(t) e^{-st} dt$$

$s = \sigma + jw$  : complex variable

$$f(t) = ae^{-bt}$$

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$$F(s)=\frac{a}{s+b}$$

| <b>Item no.</b> | <b><math>f(t)</math></b> | <b><math>F(s)</math></b>        |
|-----------------|--------------------------|---------------------------------|
| 1.              | $\delta(t)$              | 1                               |
| 2.              | $u(t)$                   | $\frac{1}{s}$                   |
| 3.              | $tu(t)$                  | $\frac{1}{s^2}$                 |
| 4.              | $t^n u(t)$               | $\frac{n!}{s^n + 1}$            |
| 5.              | $e^{-at} u(t)$           | $\frac{1}{s + a}$               |
| 6.              | $\sin \omega t u(t)$     | $\frac{\omega}{s^2 + \omega^2}$ |
| 7.              | $\cos \omega t u(t)$     | $\frac{s}{s^2 + \omega^2}$      |

# Properties of Laplace Transform

| Item no. | Theorem  | Name                               |
|----------|--|------------------------------------|
| 1.       | $\mathcal{L}[f(t)] = F(s) = \int_{0-}^{\infty} f(t)e^{-st}dt$                              | Definition                         |
| 2.       | $\mathcal{L}[kf(t)] = kF(s)$   | Linearity theorem                  |
| 3.       | $\mathcal{L}[f_1(t) + f_2(t)] = F_1(s) + F_2(s)$   | Linearity theorem                  |
| 4.       | $\mathcal{L}[e^{-at}f(t)] = F(s+a)$  | Frequency shift theorem            |
| 5.       | $\mathcal{L}[f(t-T)] = e^{-sT}F(s)$  | Time shift theorem                 |
| 6.       | $\mathcal{L}[f(at)] = \frac{1}{a}F\left(\frac{s}{a}\right)$                                | Scaling theorem                    |
| 7.       | $\mathcal{L}\left[\frac{df}{dt}\right] = sF(s) - f(0-)$                                    | Differentiation theorem            |
| 8.       | $\mathcal{L}\left[\frac{d^2f}{dt^2}\right] = s^2F(s) - sf(0-) - f'(0-)$                    | Differentiation theorem            |
| 9.       | $\mathcal{L}\left[\frac{d^n f}{dt^n}\right] = s^n F(s) - \sum_{k=1}^n s^{n-k} f^{k-1}(0-)$ | Differentiation theorem            |
| 10.      | $\mathcal{L}\left[\int_{0-}^t f(\tau)d\tau\right] = \frac{F(s)}{s}$                        | Integration theorem                |
| 11.      | $f(\infty) = \lim_{s \rightarrow 0} sF(s)$   | Final value theorem <sup>1</sup>   |
| 12.      | $f(0+) = \lim_{s \rightarrow \infty} sF(s)$  | Initial value theorem <sup>2</sup> |

## Transfer Function

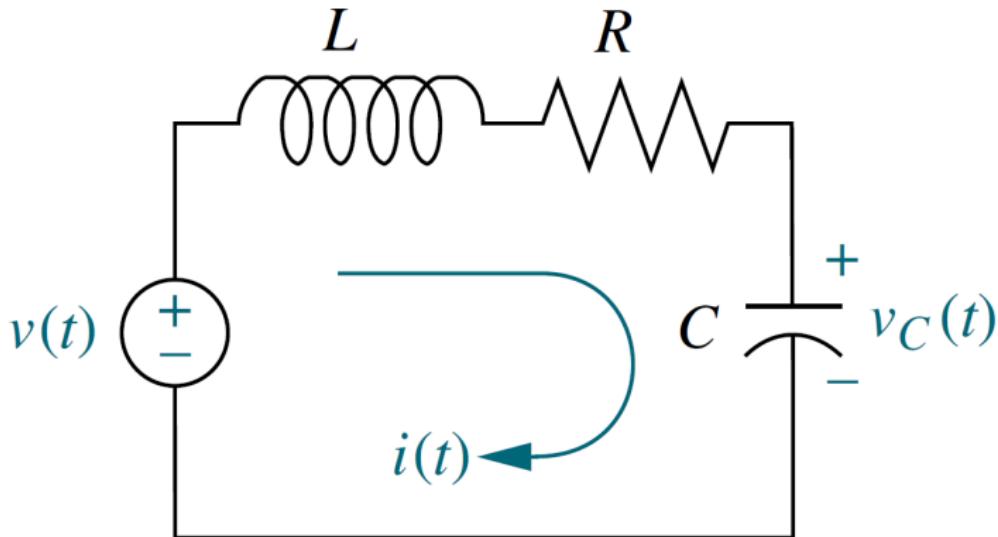
$$\begin{aligned} a_n \frac{d^n y(t)}{dt^n} + a_{n-1} \frac{d^{n-1} y(t)}{dt^{n-1}} + \dots + a_1 \frac{dy(t)}{dt} + a_0 y(t) \\ = \\ b_n \frac{d^n r(t)}{dt^n} + b_{n-1} \frac{d^{n-1} r(t)}{dt^{n-1}} + \dots + b_1 \frac{dr(t)}{dt} + b_0 r(t) \end{aligned}$$

## Transfer Function

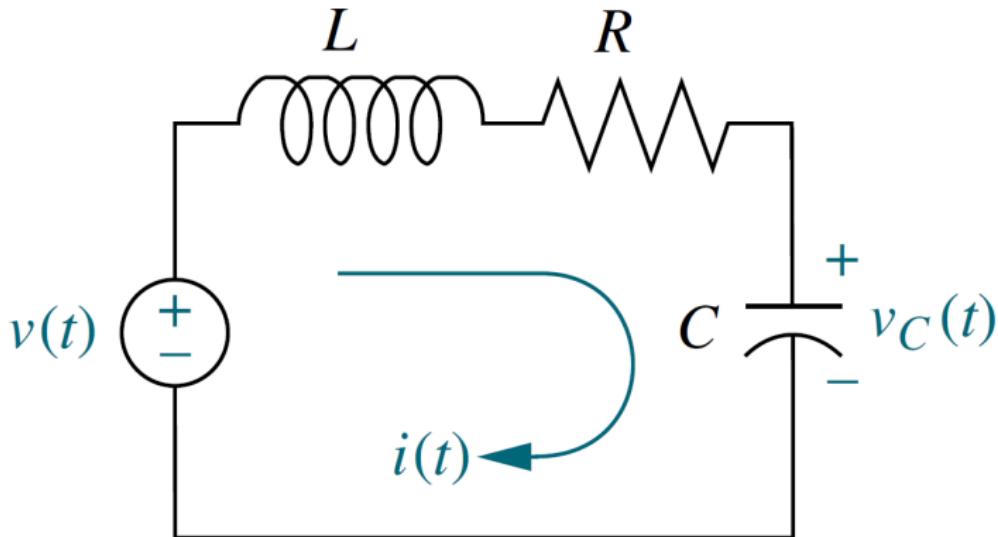
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$$G(s) = \frac{Y(s)}{R(s)} = \frac{b_n s^n + b_{n-1} s^{n-1} + \dots + b_1 s + b_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}$$

## RLC: Transfer function

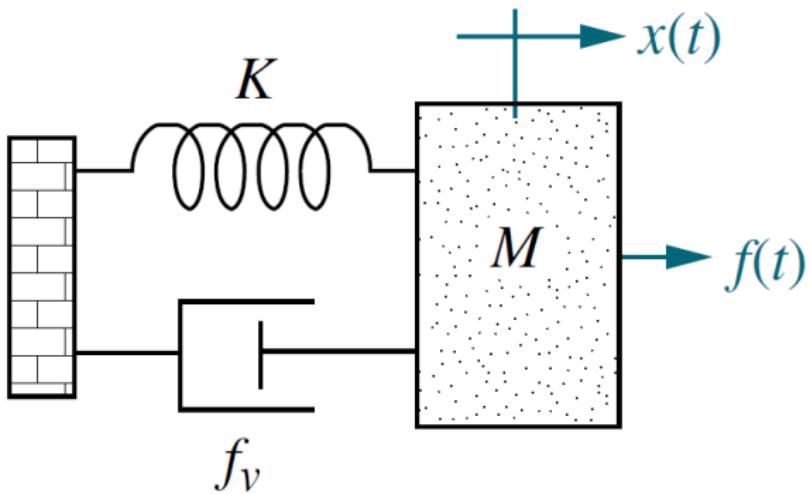


## RLC: Transfer function

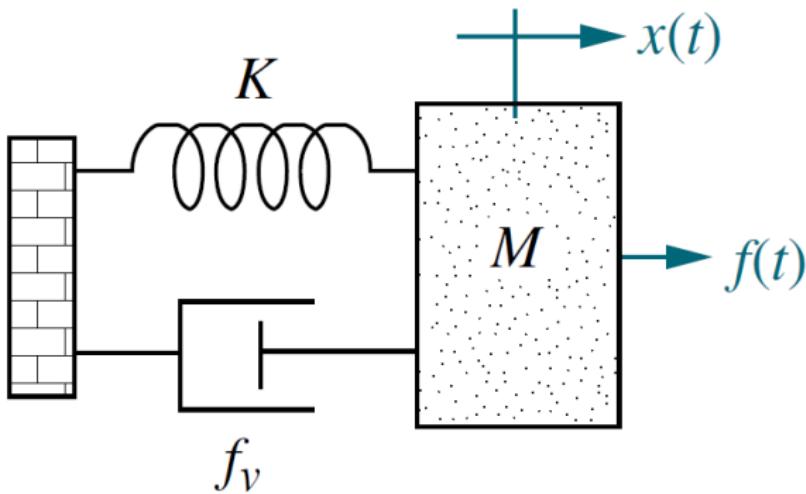


$$G(s) = \frac{V_c(s)}{V(s)} = \frac{1}{LCs^2 + RCs + 1}$$

## Mass Spring Damper: Transfer Function



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$$G(s) = \frac{X(s)}{F(s)} = \frac{1}{Ms^2 + f_v s + K}$$

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$$G(s) := \frac{Y(s)}{R(s)} = \frac{32}{s^2 + 12s + 32} =$$

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$$G(s) := \frac{Y(s)}{R(s)} = \frac{32}{s^2 + 12s + 32} = \frac{32}{(s+4)(s+8)}$$

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Step Response:

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$$Y(s) = \frac{32}{s(s+4)(s+8)}$$

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$$y(t) = A_1 u(t) + A_2 e^{-4t} u(t) + A_3 e^{-8t} u(t)$$

## Computation of $A_1$ , $A_2$ and $A_3$

$$\frac{32}{s(s+4)(s+8)} = \frac{A_1}{s} + \frac{A_2}{s+4} + \frac{A_3}{s+8} \quad (1)$$

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i) Multiply Equation (1) with  $s$

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$$A_1 = 1$$

## Computation of $A_1$ , $A_2$ and $A_3$

$$\frac{32}{s(s+4)(s+8)} = \frac{A_1}{s} + \frac{A_2}{s+4} + \frac{A_3}{s+8} \quad (3)$$

### 2) Computation of $A_2$

i) Multiply Equation (3) with  $(s+4)$

## Computation of $A_1$ , $A_2$ and $A_3$

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$$A_2 = -2$$

$$A_1 = 1 \quad A_2 = -2 \quad A_3 = 1$$

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$$Y(s) = \frac{32}{s(s+4)(s+8)} = \frac{1}{s} - \frac{2}{s+4} + \frac{1}{s+8} \quad (5)$$

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$$\frac{Y(s)}{R(s)} = \frac{32}{(s+4)(s+8)}$$

## Denominator With Real Repeated Roots

$$G(s) = \frac{Y(s)}{R(s)} = \frac{2}{(s+1)(s+2)^2}$$

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$$\boxed{A_1 = \frac{1}{2} \qquad A_2 = -2 \qquad A_4 = 1}$$

## Computation of $A_3$

$$\frac{2}{s(s+1)(s+2)^2} = \frac{A_1}{s} + \frac{A_2}{s+1} + \frac{A_3}{s+2} + \frac{A_4}{(s+2)^2} \quad (6)$$

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## Complex Roots in Denominator

$$G(s) = \frac{Y(s)}{R(s)} = \frac{3}{s^2 + 2s + 5}$$

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$$Y(s) = \frac{3}{s(s^2 + 2s + 5)} = \frac{A_1 s^2 + 2A_1 s + 5A_1 + A_2 s^2 + A_3 s}{s(s^2 + 2s + 5)}$$

$$3 = (A_1 + A_2)s^2 + (2A_1 + A_3)s + 5A_1$$

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## Property of Laplace Transform

$$\begin{array}{ccc} f(t) & \iff & F(s) \\ e^{-at}f(t) & \iff & F(s+a) \end{array}$$

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$$\begin{array}{ccc} f(t) = \sin(2t) & \iff & F(s) = \frac{2}{s^2+4} \\ e^{-t}\sin(2t) & \iff & \frac{2}{(s+1)^2+4} = \frac{2}{s^2+2s+5} \end{array}$$

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## Transfer Function

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$$G(s) = \frac{Y(s)}{R(s)} = \frac{s+2}{s+5}$$

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## Relation between Poles and Form of Response

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$$y(t) = A_1 u(t) + A_2 e^{-4t} u(t) + A_3 e^{-8t} u(t)$$

## First Order System

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$$G(s) = \frac{a}{s+a}$$

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$$y(t) \Big|_{t=\frac{1}{a}} = 1 - \frac{1}{e} = 0.63$$

## Transient Specifications of First Order System

$$\text{Time Constant} = \frac{1}{a}$$

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**Rise Time:** Time taken by  $y(t)$  to rise from  $y(t) = 0.1$  to  $y(t) = 0.9$

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$$\boxed{\text{Rise Time} = T_r = \frac{2.31}{a} - \frac{0.11}{a} = \frac{2.2}{a}}$$

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**Settling Time:** Time taken by  $y(t)$  to reach and remain within 2% of final value, which is 1

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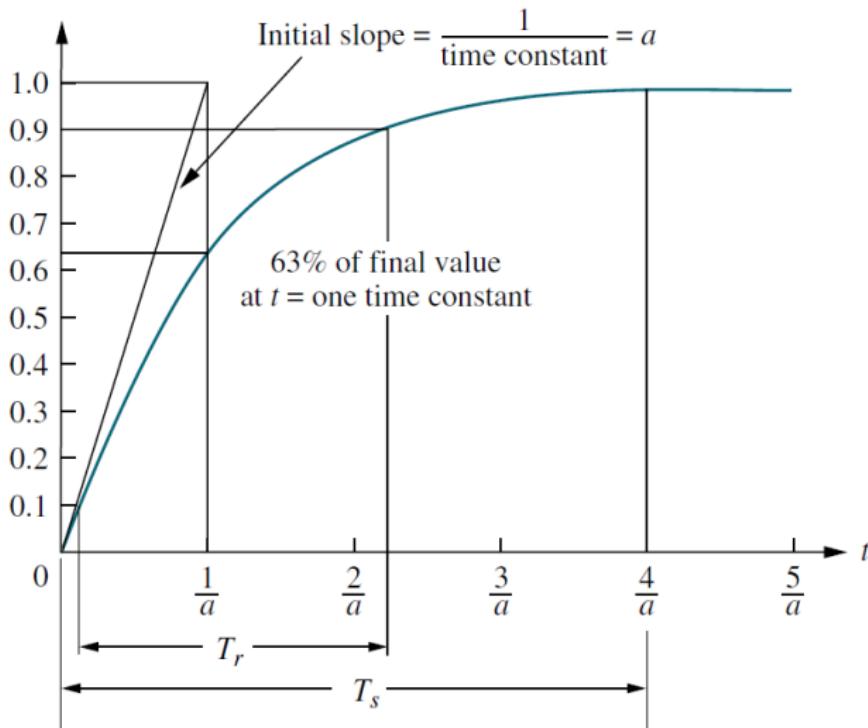
## Transient Specifications of First Order System

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$$y(T_s) = (1 - e^{-aT_s}) = 0.98$$

$$T_s = \frac{4}{a}$$

## Transient Specifications of First Order System



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$$y(t) = \frac{K}{a} (1 - e^{-at}) u(t)$$

## Second Order System

$$G(s) = \frac{b}{s^2 + as + b}$$

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Poles:  $\sigma_{1,2} = -\zeta w_n \pm w_n \sqrt{\zeta^2 - 1}$

$$\zeta > 1$$

Poles are Real

$$\sigma_1 = -\zeta w_n - w_n \sqrt{\zeta^2 - 1}$$

$$\sigma_2 = -\zeta w_n + w_n \sqrt{\zeta^2 - 1}$$

$$\zeta > 1$$

Poles are Real

$$\sigma_1 = -\zeta w_n - w_n \sqrt{\zeta^2 - 1}$$

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$$\zeta w_n > w_n \sqrt{\zeta^2 - 1}$$

$$\zeta > 1$$

Poles are Real

$$\sigma_1 = -\zeta w_n - w_n \sqrt{\zeta^2 - 1}$$

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$$\zeta w_n > w_n \sqrt{\zeta^2 - 1}$$

$$\sigma_1 < 0$$

$$\sigma_2 < 0$$

$$\zeta > 1$$

$$G(s) = \frac{Y(s)}{R(s)} = \frac{w_n^2}{(s - \sigma_1)(s - \sigma_2)}$$

$$\zeta > 1$$

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$$Y(s) = \frac{w_n^2}{s(s - \sigma_1)(s - \sigma_2)} = \frac{A_1}{s} + \frac{A_2}{s - \sigma_1} + \frac{A_3}{s - \sigma_2}$$

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$$y(t) = (A_1 + A_2 e^{-\sigma_1 t} + A_3 e^{-\sigma_2 t}) u(t)$$

$$\zeta > 1$$

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OVERDAMPED system

$$\zeta = 1$$

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Poles are **real** and **repeated**

$$\sigma_1 = \sigma_2 = -w_n$$

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Poles are **real** and **repeated**

$$\sigma_1 = \sigma_2 = -w_n$$

$$G(s) = \frac{Y(s)}{R(s)} = \frac{w_n^2}{(s + w_n)^2}$$

$$\zeta = 1$$

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$$G(s) = \frac{Y(s)}{R(s)} = \frac{w_n^2}{(s + w_n)^2}$$

$$Y(s) = \frac{w_n^2}{s(s + w_n)^2} = \frac{1}{s} + \frac{A_1}{s + w_n} + \frac{A_2}{(s + w_n)^2}$$

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$$y(t) = (1 + A_1 e^{-w_n t} + A_2 t e^{-w_n t}) u(t)$$

**CRITICALLY DAMPED system**

$$\zeta = 0$$

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Poles are imaginary

$$\sigma_1 = j\omega_n \quad \sigma_2 = -j\omega_n$$

$$\zeta = 0$$

Poles are imaginary

$$\sigma_1 = j\omega_n \quad \sigma_2 = -j\omega_n$$

$$G(s) = \frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + \omega_n^2}$$

$$\zeta = 0$$

Poles are imaginary

$$\sigma_1 = j\omega_n \quad \sigma_2 = -j\omega_n$$

$$G(s) = \frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + \omega_n^2}$$

$$Y(s) = \frac{\omega_n^2}{s(s^2 + \omega_n^2)} = \frac{1}{s} - \frac{s}{s^2 + \omega_n^2}$$

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Poles are imaginary

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$$Y(s) = \frac{\omega_n^2}{s(s^2 + \omega_n^2)} = \frac{1}{s} - \frac{s}{s^2 + \omega_n^2}$$

$$y(t) = \left(1 - \cos(\omega_n t)\right) u(t)$$

$$\zeta = 0$$

Poles are **imaginary**

$$\sigma_1 = j\omega_n \quad \sigma_2 = -j\omega_n$$

$$G(s) = \frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + \omega_n^2}$$

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$$y(t) = \left(1 - \cos(\omega_n t)\right) u(t)$$

**UNDAMPED** system

$$0 < \zeta < 1$$

$$0 < \zeta < 1$$

Poles are **complex**

$$\sigma_1 = -\zeta w_n - jw_n \sqrt{1 - \zeta^2}$$

$$\sigma_2 = -\zeta w_n + jw_n \sqrt{1 - \zeta^2}$$

$$0 < \zeta < 1$$

Poles are **complex**

$$\sigma_1 = -\zeta w_n - jw_n \sqrt{1 - \zeta^2}$$

$$\sigma_2 = -\zeta w_n + jw_n \sqrt{1 - \zeta^2}$$

$$G(s) = \frac{Y(s)}{R(s)} = \frac{w_n^2}{s^2 + 2\zeta w_n s + w_n^2}$$

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$$Y(s) = \frac{w_n^2}{s(s^2 + 2\zeta w_n s + w_n^2)} = \frac{A_1}{s} + \frac{A_2 s + A_3}{s^2 + 2\zeta w_n s + w_n^2}$$

$$Y(s) = \frac{w_n^2}{s(s^2 + 2\zeta w_n s + w_n^2)} = \frac{A_1(s^2 + 2\zeta w_n s + w_n^2) + A_2 s^2 + A_3 s}{s(s^2 + 2\zeta w_n s + w_n^2)}$$

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# Step Response of Second Order System

| $\zeta$         | Poles  | Step response  |
|-----------------|--|--|
| 0               | <p>s-plane<br/>Poles: <math>j\omega_n</math>, <math>-j\omega_n</math></p>  | <p><math>c(t)</math><br/>t<br/>Undamped</p>          |
| $0 < \zeta < 1$ | <p>s-plane<br/>Poles: <math>-\zeta\omega_n</math>, <math>-j\omega_n\sqrt{1-\zeta^2}</math></p>   | <p><math>c(t)</math><br/>t<br/>Underdamped</p>       |
| $\zeta = 1$     | <p>s-plane<br/>Pole: <math>-\zeta\omega_n</math></p>   | <p><math>c(t)</math><br/>t<br/>Critically damped</p> |
| $\zeta > 1$     | <p>s-plane<br/>Poles: <math>-\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1}</math>, <math>-\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}</math></p> | <p><math>c(t)</math><br/>t<br/>Overdamped</p>        |

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Time instant at which  $y(t)$  reaches its first peak

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$$\frac{dy(t)}{dt} = e^{-\zeta w_n t} w_d \sin(w_d t) - \zeta w_n e^{-\zeta w_n t} \cos(w_d t) + \\ \zeta w_n e^{-\zeta w_n t} \cos(w_d t) + \frac{\zeta^2 w_n e^{-\zeta w_n t}}{\sqrt{1-\zeta^2}} \sin(w_d t)$$

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## Transient Specifications

- Peak Time  $T_p$ :

$$T_p = \frac{\pi}{w_d} = \frac{\pi}{w_n \sqrt{1 - \zeta^2}}$$

- % Overshoot:

$$\% \text{ Overshoot} = e^{\frac{-\zeta \pi}{\sqrt{1 - \zeta^2}}} \times 100$$

- Rise Time:

$$T_r = \frac{\pi - \theta}{w_d} = \frac{\pi - \theta}{w_n \sqrt{1 - \zeta^2}} \quad \theta = \arctan\left(\frac{\sqrt{1 - \zeta^2}}{\zeta}\right)$$

$$y(t) = u(t) - e^{-\zeta w_n t} \left( \cos(w_d t) + \frac{\zeta}{\sqrt{1-\zeta^2}} \sin(w_d t) \right) u(t)$$

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$$T_r = \frac{\pi - \theta}{w_d} \qquad \qquad \theta = \arctan \left( \frac{\sqrt{1-\zeta^2}}{\zeta} \right)$$

## Settling Time

Settling Time  $T_s$ : Time taken by  $y(t)$  to reach and stay within 2% of final value, i.e., 1

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$$\frac{e^{-\zeta w_n t}}{\sqrt{1-\zeta^2}} = 0.02$$

$$T_s = \frac{-\ln(0.02\sqrt{1-\zeta^2})}{\zeta w_n}$$

$$T_s \, = \, \frac{-\ln \left( 0.02 \sqrt{1-\zeta^2} \right)}{\zeta w_n}$$

$$T_s \, = \, \frac{4}{\zeta w_n}$$

## Relation between Peak Time and Pole Location

Poles:

$$\sigma_1 = -\zeta w_n - jw_n \sqrt{1 - \zeta^2}$$

$$\sigma_2 = -\zeta w_n + jw_n \sqrt{1 - \zeta^2}$$

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Peak Time:

$$T_p = \frac{\pi}{w_d} = \frac{\pi}{w_n \sqrt{1 - \zeta^2}} = \frac{\pi}{|\text{Imaginary part of pole}|}$$

## Relation between Settling Time and Pole Location

Poles:

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## Relation between Settling Time and Pole Location

Poles:

$$\sigma_1 = -\zeta w_n - jw_n \sqrt{1 - \zeta^2}$$

$$\sigma_2 = -\zeta w_n + jw_n \sqrt{1 - \zeta^2}$$

Settling Time:

$$T_s = \frac{4}{\zeta w_n} = \frac{4}{|\text{Real part of pole}|}$$

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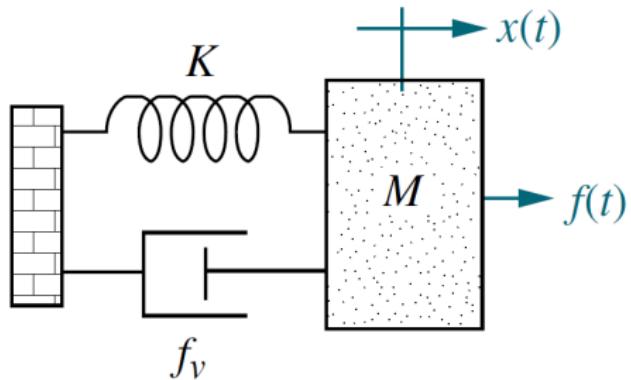
Poles:

$$\sigma_1 = -\zeta w_n - jw_n \sqrt{1 - \zeta^2}$$

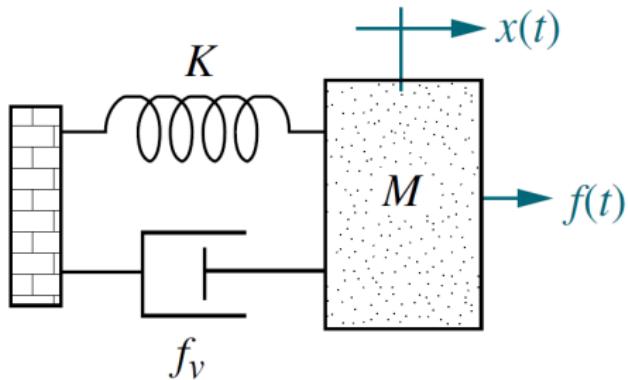
$$\sigma_2 = -\zeta w_n + jw_n \sqrt{1 - \zeta^2}$$

$$\cos \theta = \zeta$$

## Mass Spring Damper

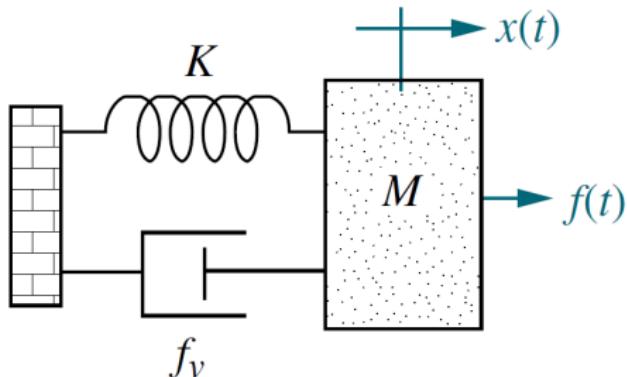


## Mass Spring Damper



$$G(s) = \frac{X(s)}{F(s)} = \frac{1}{Ms^2 + f_v s + K}$$

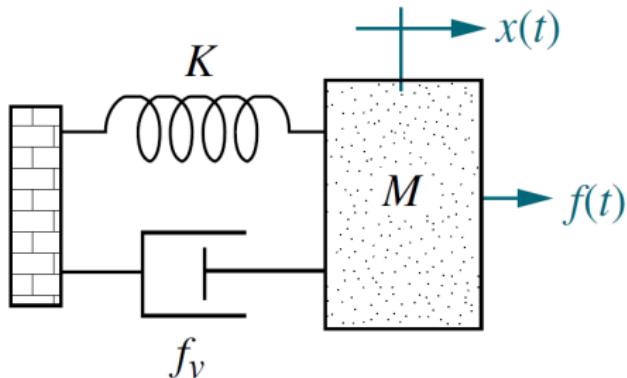
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**Problem:** Take  $K = 5$ . Find  $M$  and  $f_v$  which results in settling time 2 sec and overshoot 20%

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**Problem:** Take  $K = 5$ . Find  $M$  and  $f_v$  which results in settling time 2 sec and overshoot 20%  
 $M = 0.26$  and  $f_v = 1.04$

## Second Order System with Additional Pole

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$$G(s) = \frac{w_n^2}{(s^2 + 2\zeta w_n s + w_n^2)}$$

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$$G(s) = \frac{w_n^2}{(s^2 + 2\zeta w_n s + w_n^2)} \frac{\alpha_r}{(s + \alpha_r)}$$

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$$y(t) = A_1 u(t) + A_2 e^{-\zeta w_n t} \left( A_2 \cos(w_d t) + A_3 \sin(w_d t) \right) + A_4 e^{-\alpha_r t}$$

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$$A_1 = 1$$

$$A_2 = \frac{\alpha_r a - \alpha_r^2}{\alpha_r^2 + b - \alpha_r a}$$

$$A_3 = \frac{\alpha_r a^2 - \alpha_r^2 a - b \alpha_r}{\alpha_r^2 + b - \alpha_r a}$$

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$$A_1 = 1$$

$$A_2 = -1$$

$$A_3 = -a$$

$$A_4 = 0$$

## Second Order System With Additional Zero

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## Pole Zero Cancellation

$$G(s) = \frac{k(s + z)}{(s + p)(s^2 + as + b)}$$

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$$G(s) = \frac{k(s + z)}{(s + p)(s^2 + as + b)}$$

$$G(s) = \frac{A_1}{s + p} + \frac{A_2 s + A_3}{s^2 + as + b}$$

## Examples

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$$G_1(s) = \frac{26.25(s+4)}{(s+3.5)(s+5)(s+6)}$$

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$$G_1(s) = \frac{26.25(s+4)}{(s+3.5)(s+5)(s+6)}$$

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$$G_2(s) = \frac{26.25(s+4)}{(s+4.01)(s+5)(s+6)}$$

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$$Y_2(s) = \frac{26.25(s+4)}{s(s+4.01)(s+5)(s+6)} = \frac{0.87}{s} + \frac{0.033}{s+4.01} - \frac{5.3}{s+5} + \frac{4.4}{s+6}$$

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## Feedback Loop

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- Transfer function:

$$T(s) := \frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)}$$

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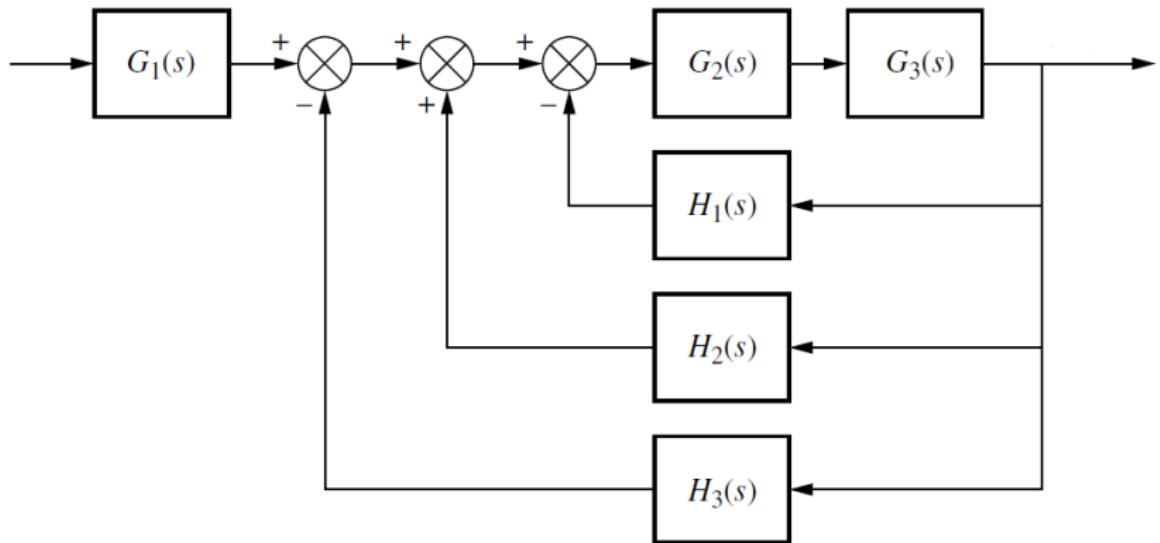
- Closed loop transfer function

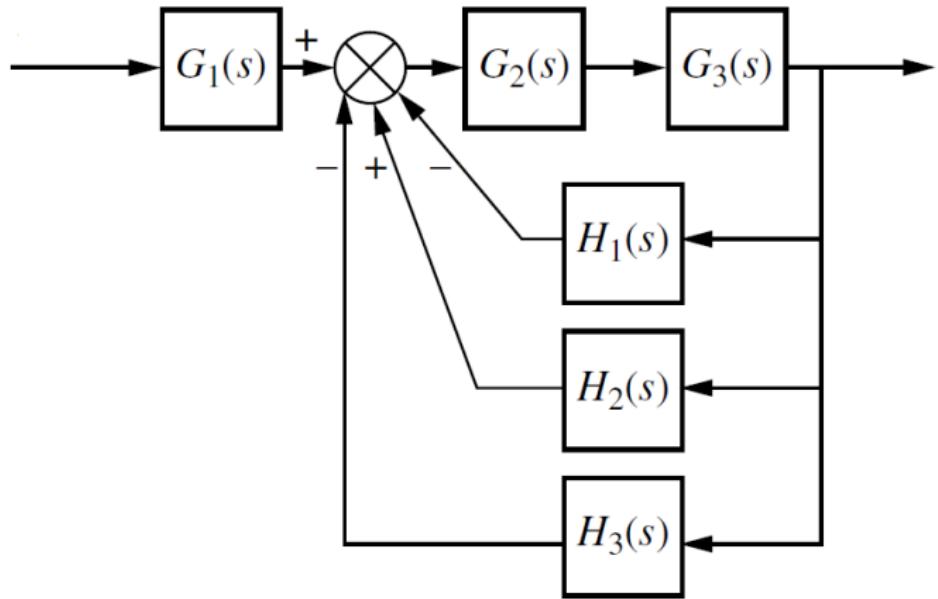
## Feedback Loop

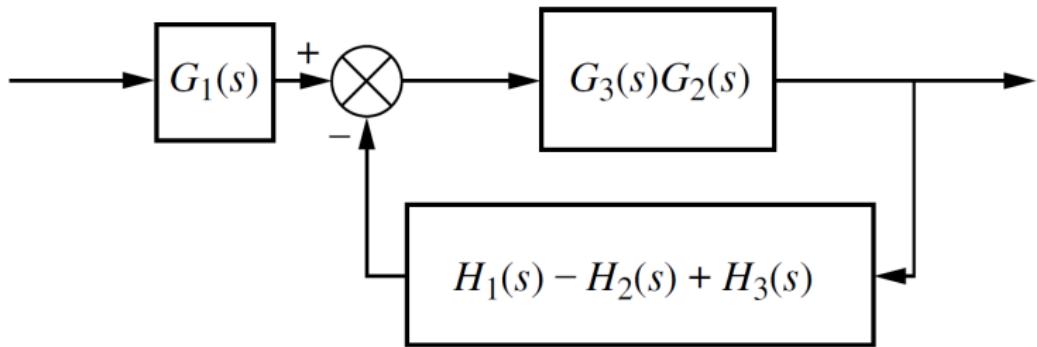
- Transfer function:

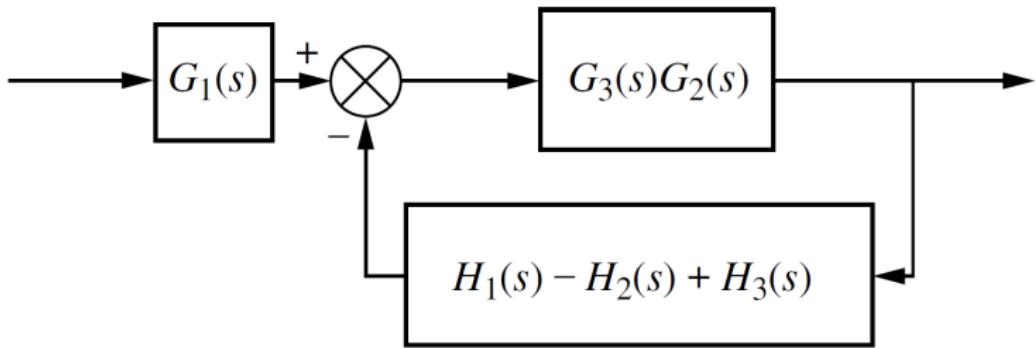
$$T(s) := \frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)}$$

- Closed loop transfer function
- $G(s)H(s)$ : Loop Gain or Open-Loop transfer function





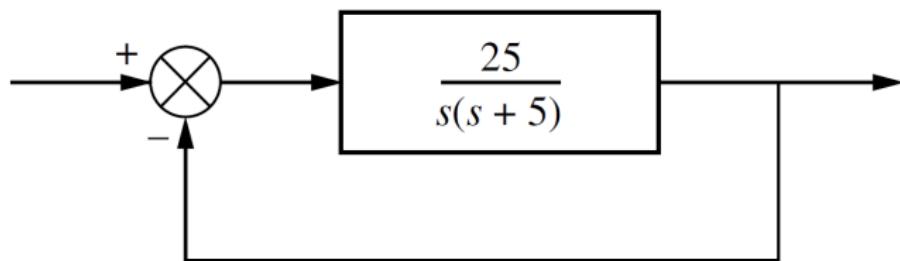




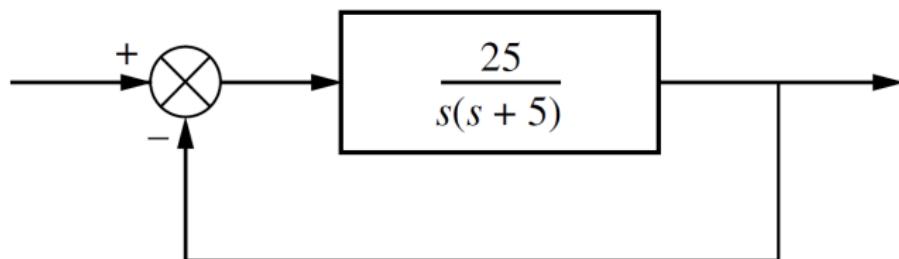
$$T(s) = \frac{G_3(s)G_2(s)G_1(s)}{1 + G_3(s)G_2(s)(H_1(s) - H_2(s) + H_3(s))}$$

## Unity Feedback

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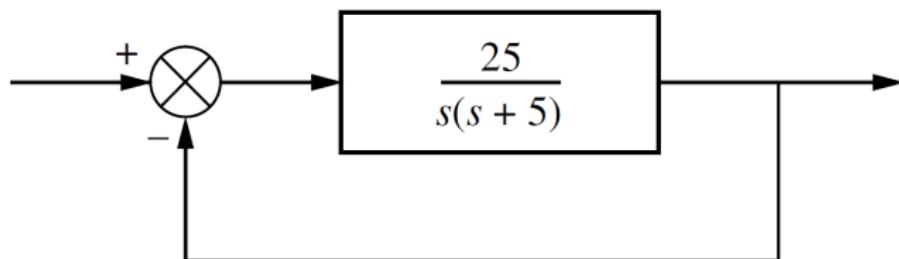


## Unity Feedback



$$T(s) = \frac{25}{s^2 + 5s + 25}$$

## Unity Feedback



$$T(s) = \frac{25}{s^2 + 5s + 25}$$

$$\zeta = 0.5$$

$$w_n = 5$$

## Specifications of Control Systems

- Transient response
- Stability
- Steady state response

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Bounded-Input Bounded-Output (BIBO) Stability

## Bounded Signal

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- Definition: A signal  $x(t)$  is said to be a **bounded** signal if

$$|x(t)| \leq M_x < \infty, \quad \forall t \geq 0$$

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- Examples: Unit Step Signal

Sine / Cosine Signal

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$$|r(t)| \leq M_r < \infty \quad \forall t \geq 0$$



$$|y(t)| \leq M_y < \infty \quad \forall t \geq 0$$

## Impulse Response

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$$G(s) = \frac{Y(s)}{R(s)}$$

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$$Y(s) = G(s)$$

Impulse Response  $h(t) := \mathcal{L}^{-1}(G(s))$



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$$\mathcal{L}^{-1}\left(Y(s)\right) = \mathcal{L}^{-1}\left(G(s)\right) * \mathcal{L}^{-1}\left(R(s)\right)$$

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\* Convolution

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\* Convolution

$$y(t) = h(t) * r(t)$$

## Convolution Integral

$$y(t) = \int_0^{\infty} r(t - \tau) h(\tau) d\tau$$

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$$|y(t)| \leq \int_0^\infty |r(t - \tau)| |h(\tau)| d\tau$$

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$$|y(t)| \leq \int_0^{\infty} M_r |h(\tau)| d\tau$$

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$$|y(t)| \leq \int_0^{\infty} M_r |h(\tau)| d\tau = M_r \int_0^{\infty} |h(\tau)| d\tau$$

$$|y(t)| \leq \int_0^{\infty} |r(t - \tau)| |h(\tau)| d\tau$$

$$|y(t)| \leq \int_0^{\infty} M_r |h(\tau)| d\tau = M_r \int_0^{\infty} |h(\tau)| d\tau$$

If  $\int_0^{\infty} |h(\tau)| d\tau \leq M_h < \infty$

$$|y(t)| \leq \int_0^{\infty} |r(t - \tau)| |h(\tau)| d\tau$$

$$|y(t)| \leq \int_0^{\infty} M_r |h(\tau)| d\tau = M_r \int_0^{\infty} |h(\tau)| d\tau$$

If  $\int_0^{\infty} |h(\tau)| d\tau \leq M_h < \infty$

$$|y(t)| \leq M_r M_h < \infty$$

## LTI System

$$\int_0^{\infty} |h(\tau)| d\tau \leq M_h < \infty \quad h(t) \text{ is absolutely integrable}$$

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BIBO Stable

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BIBO Stable  $\implies$   $h(t)$  is absolutely integrable ????

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BIBO Stable

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BIBO Stable  $\iff$   $h(t)$  is absolutely integrable

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$$\int_0^{\infty} |h(\tau)| d\tau \leq M_h < \infty$$

$$a > 0, b > 0$$

Both Poles in LHP of complex plane

$$G(s) = \frac{1}{s}$$

$$G(s) = \frac{1}{s} \quad h(t) = u(t)$$

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Take  $r(t) = u(t)$   $R(s) = \frac{1}{s}$

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$$Y(s) = G(s)R(s) = \frac{1}{s^2}$$

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      Not Bounded

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$$y(t) = tu(t) \quad \text{Not Bounded}$$

System is NOT BIBO stable

$$G(s) = \frac{1}{s^2 + 1}$$

$$G(s) = \frac{1}{s^2 + 1} \quad h(t) = \sin(t)u(t)$$

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$$G(s) = \frac{1}{s^2 + 1} \quad h(t) = \sin(t)u(t)$$

Take  $r(t) = \sin(t)u(t)$   $R(s) = \frac{1}{s^2 + 1}$

$$Y(s) = G(s)R(s) = \frac{1}{(s^2 + 1)^2}$$

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$$Y(s) = G(s)R(s) = \frac{1}{(s^2 + 1)^2}$$

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System is NOT BIBO stable

## BIBO stability

$h(t)$  is **absolutely** integrable

≡

BIBO stability

≡

**All** Poles of  $G(s)$  in **LHP** of complex plane

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**All** Poles of  $G(s)$  in **LHP** of complex plane

$$T(s) = \frac{N(s)}{D(s)}$$

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**Definition:** If all roots of polynomial  $D(s)$  are in LHP, then  $D(s)$  is called as the **hurwitz** polynomial

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$$T(s) \text{ is BIBO stable} \iff D(s) \text{ is hurwitz}$$

## Routh-Hurwitz Stability Criterion

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Edward Routh

1876



Adolf Hurwitz

1895

## Polynomial with Degree 1

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$$D(s) = a_1 s + a_0$$

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$$D(s) = a_1 s + a_0$$

$$D_1(s) = s + \frac{a_0}{a_1} = s + a$$

$D(s)$  is Hurwitz  $\iff$   $a_1 \neq 0$ ,  $a_0 \neq 0$ , and  
 $a_1$  and  $a_0$  have same sign

## Polynomial with Degree 2

$$D(s) = a_2 s^2 + a_1 s + a_0$$

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## Polynomial with Degree 2

3)  $a_2 < 0, \quad a_1 > 0 \quad \text{and} \quad a_0 > 0$

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4)  $a_2 > 0, \quad a_1 > 0 \quad \text{and} \quad a_0 > 0$

$\implies$  Both roots of  $D(s)$  lie in LHP

## Polynomial with Degree 2

3)  $a_2 < 0, \quad a_1 > 0 \quad \text{and} \quad a_0 > 0$

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4)  $a_2 > 0, \quad a_1 > 0 \quad \text{and} \quad a_0 > 0$

$\implies$  Both roots of  $D(s)$  lie in LHP

$D(s)$  is Hurwitz  $\iff$   $a_2 \neq 0, \quad a_1 \neq 0, \quad a_0 \neq 0,$   
 $a_2, \quad a_1 \text{ and } a_0 \text{ have same sign}$

## Routh Table

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$$D(s) = a_4 s^4 + a_3 s^3 + a_2 s^2 + a_1 s_1 + a_0$$

## Routh Table

$$D(s) = a_4 s^4 + a_3 s^3 + a_2 s^2 + a_1 s_1 + a_0$$

|       |       |       |       |
|-------|-------|-------|-------|
| $s^4$ | $a_4$ | $a_2$ | $a_0$ |
| $s^3$ | $a_3$ | $a_1$ | 0     |
| $s^2$ |       |       |       |
| $s^1$ |       |       |       |
| $s^0$ |       |       |       |

## Routh Table

|       |   |   |   |
|-------|---|---|---|
| $s^4$ | $a_4$   | $a_2$   | $a_0$   |
| $s^3$ | $a_3$   | $a_1$   | 0   |
| $s^2$ | $\frac{-\begin{vmatrix} a_4 & a_2 \\ a_3 & a_1 \end{vmatrix}}{a_3} = b_1$ | $\frac{-\begin{vmatrix} a_4 & a_0 \\ a_3 & 0 \end{vmatrix}}{a_3} = b_2$ | $\frac{-\begin{vmatrix} a_4 & 0 \\ a_3 & 0 \end{vmatrix}}{a_3} = 0$ |
| $s^1$ | $\frac{-\begin{vmatrix} a_3 & a_1 \\ b_1 & b_2 \end{vmatrix}}{b_1} = c_1$ | $\frac{-\begin{vmatrix} a_3 & 0 \\ b_1 & 0 \end{vmatrix}}{b_1} = 0$     | $\frac{-\begin{vmatrix} a_3 & 0 \\ b_1 & 0 \end{vmatrix}}{b_1} = 0$ |
| $s^0$ | $\frac{-\begin{vmatrix} b_1 & b_2 \\ c_1 & 0 \end{vmatrix}}{c_1} = d_1$   | $\frac{-\begin{vmatrix} b_1 & 0 \\ c_1 & 0 \end{vmatrix}}{c_1} = 0$     | $\frac{-\begin{vmatrix} b_1 & 0 \\ c_1 & 0 \end{vmatrix}}{c_1} = 0$ |

## Routh Stability Criteria

$D(s)$  is Hurwitz

if and only if

- 1) All coefficients of  $D(s)$  are non-zero and of same sign
- 2) All elements in the first column of Routh table are non-zero
- 3) No sign changes in the first column of Routh table

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Number of sign changes in first column

=

Number of roots of  $D(s)$  in RHP

## Example

$$D(s) = s^3 + 10s^2 + 31s + 1030$$

## Example

$$D(s) = s^3 + 10s^2 + 31s + 1030$$

$s^3$

1

31

0

$s^2$

-10 -1

1030 103

0

$s^1$

$$\frac{-\begin{vmatrix} 1 & 31 \\ 1 & 103 \end{vmatrix}}{1} = -72$$

$$\frac{-\begin{vmatrix} 1 & 0 \\ 0 & 0 \end{vmatrix}}{1} = 0$$

$$\frac{-\begin{vmatrix} 1 & 0 \\ 1 & 0 \end{vmatrix}}{1} = 0$$

$s^0$

$$\frac{-\begin{vmatrix} 1 & 103 \\ -72 & 0 \end{vmatrix}}{-72} = 103$$

$$\frac{-\begin{vmatrix} 1 & 0 \\ -72 & 0 \end{vmatrix}}{-72} = 0$$

$$\frac{-\begin{vmatrix} 1 & 0 \\ -72 & 0 \end{vmatrix}}{-72} = 0$$

## Example

$$D(s) = s^3 + 10s^2 + 31s + 1030$$

$s^3$

1

31

0

$s^2$

-10 -1

-1030 -103

0

$s^1$

$$\frac{-\begin{vmatrix} 1 & 31 \\ 1 & 103 \end{vmatrix}}{1} = -72$$

$$\frac{-\begin{vmatrix} 1 & 0 \\ 0 & 0 \end{vmatrix}}{1} = 0$$

$$\frac{-\begin{vmatrix} 1 & 0 \\ 1 & 0 \end{vmatrix}}{1} = 0$$

$s^0$

$$\frac{-\begin{vmatrix} 1 & 103 \\ -72 & 0 \end{vmatrix}}{-72} = 103$$

$$\frac{-\begin{vmatrix} 1 & 0 \\ -72 & 0 \end{vmatrix}}{-72} = 0$$

$$\frac{-\begin{vmatrix} 1 & 0 \\ -72 & 0 \end{vmatrix}}{-72} = 0$$

Two roots in RHP

$$D(s) = s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3$$

$$D(s) = s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3$$

|       |   |               |   |
|-------|---|---------------|---|
| $s^5$ | 1   | 3             | 5 |
| $s^4$ | 2   | 6             | 3 |
| $s^3$ | $-\theta - \epsilon$                                    | $\frac{7}{2}$ | 0 |
| $s^2$ | $\frac{6\epsilon - 7}{\epsilon}$                        | 3             | 0 |
| $s^1$ | $\frac{42\epsilon - 49 - 6\epsilon^2}{12\epsilon - 14}$ | 0             | 0 |
| $s^0$ | 3   | 0             | 0 |

| <b>Label</b> | <b>First column</b>                                     | $\epsilon = +$ | $\epsilon = -$ |
|--------------|---|----------------|----------------|
| $s^5$        | 1   | +              | +              |
| $s^4$        | 2   | +              | +              |
| $s^3$        | $-\theta \quad \epsilon$                                | +              | -              |
| $s^2$        | $\frac{6\epsilon - 7}{\epsilon}$                        | -              | +              |
| $s^1$        | $\frac{42\epsilon - 49 - 6\epsilon^2}{12\epsilon - 14}$ | +              | +              |
| $s^0$        | 3   | +              | +              |

## Routh Stability Criteria

$D(s)$  is Hurwitz

if and only if

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## Routh Stability Criteria

$D(s)$  is Hurwitz

if and only if

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- 3) No sign changes in the first column of Routh table

Number of sign changes in first column

=

Number of roots of  $D(s)$  in RHP

## Routh Stability Criteria

Special case *I*:                    0 in first column of Routh table

## Routh Stability Criteria

Special case 1: 0 in first column of Routh table

Number of sign changes in first column

=

Number of roots of  $D(s)$  in RHP

## Example 1

$$D(s) = s^3 - 14s^2 + 49s - 36$$

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$$D(s) = s^3 - 14s^2 + 49s - 36$$

$$\begin{array}{cccc} s^3 & 1 & 49 & 0 \end{array}$$

$$\begin{array}{cccc} s^2 & -14 & -36 & 0 \end{array}$$

$$\begin{array}{cccc} s & 46.43 & 0 & 0 \end{array}$$

$$\begin{array}{cccc} s^0 & -36 & 0 & 0 \end{array}$$

## Example 1

$$D(s) = s^3 - 14s^2 + 49s - 36$$

|       |   |    |   |
|-------|---|----|---|
| $s^3$ | 1 | 49 | 0 |
|-------|---|----|---|

|       |     |     |   |
|-------|-----|-----|---|
| $s^2$ | -14 | -36 | 0 |
|-------|-----|-----|---|

|     |       |   |   |
|-----|-------|---|---|
| $s$ | 46.43 | 0 | 0 |
|-----|-------|---|---|

|       |     |   |   |
|-------|-----|---|---|
| $s^0$ | -36 | 0 | 0 |
|-------|-----|---|---|

Roots: 1, 4, 9

$$D(s) = a_4 s^4 + a_3 s^3 + a_2 s^2 + a_1 s + a_0$$

$$D(s) = a_4 s^4 + a_3 s^3 + a_2 s^2 + a_1 s + a_0 = 0$$

$$D(s) = a_4 s^4 + a_3 s^3 + a_2 s^2 + a_1 s + a_0 = 0$$

Substitute:  $s = \frac{1}{r}$

$$D(s) = a_4 s^4 + a_3 s^3 + a_2 s^2 + a_1 s + a_0 = 0$$

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$$Q_1(r) = a_4 \left(\frac{1}{r}\right)^4 + a_3 \left(\frac{1}{r}\right)^3 + a_2 \left(\frac{1}{r}\right)^2 + a_1 \left(\frac{1}{r}\right) + a_0 = 0$$

$$D(s) = a_4 s^4 + a_3 s^3 + a_2 s^2 + a_1 s + a_0 = 0$$

Substitute:  $s = \frac{1}{r}$

$$Q_1(r) = a_4 \left(\frac{1}{r}\right)^4 + a_3 \left(\frac{1}{r}\right)^3 + a_2 \left(\frac{1}{r}\right)^2 + a_1 \left(\frac{1}{r}\right) + a_0 = 0$$

$$Q_2(r) = a_0 r^4 + a_1 r^3 + a_2 r^2 + a_3 r + a_4 = 0$$

## Example 2

$$D(s) = s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3$$

|       |   |               |   |
|-------|---|---------------|---|
| $s^5$ | 1   | 3             | 5 |
| $s^4$ | 2   | 6             | 3 |
| $s^3$ | $-\theta - \epsilon$                                    | $\frac{7}{2}$ | 0 |
| $s^2$ | $\frac{6\epsilon - 7}{\epsilon}$                        | 3             | 0 |
| $s^1$ | $\frac{42\epsilon - 49 - 6\epsilon^2}{12\epsilon - 14}$ | 0             | 0 |
| $s^0$ | 3   | 0             | 0 |

$$D(s) = s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3$$

$$D(s) = s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3$$

$$Q_2(r) = 3r^5 + 5r^4 + 6r^3 + 3r^2 + 2r + 1$$

$$D(s) = s^5 + 2s^4 + 3s^3 + 6s^2 + 5s + 3$$

$$Q_2(r) = 3r^5 + 5r^4 + 6r^3 + 3r^2 + 2r + 1$$

|       |       |     |   |
|-------|-------|-----|---|
| $s^5$ | 3     | 6   | 2 |
| $s^4$ | 5     | 3   | 1 |
| $s^3$ | 4.2   | 1.4 |   |
| $s^2$ | 1.33  | 1   |   |
| $s^1$ | -1.75 |     |   |
| $s^0$ | 1     |     |   |

## Example 3

$$D(s) = s^5 + 7s^4 + 6s^3 + 42s^2 + 8s + 56$$

## Example 3

$$D(s) = s^5 + 7s^4 + 6s^3 + 42s^2 + 8s + 56$$

|       |   |   |   |
|-------|---|---|---|
| $s^5$ | 1 | 6 | 6 |
|-------|---|---|---|

|       |   |    |    |
|-------|---|----|----|
| $s^4$ | 7 | 42 | 56 |
|-------|---|----|----|

|       |   |   |   |
|-------|---|---|---|
| $s^3$ | 0 | 0 | 0 |
|-------|---|---|---|

## Even/Odd Polynomial

Even Polynomial:  $D(-s) = D(s)$

## Even/Odd Polynomial

Even Polynomial:  $D(-s) = D(s)$

$$D(s) = s^2 + 1$$

## Even/Odd Polynomial

Even Polynomial:  $D(-s) = D(s)$

$$D(s) = s^2 + 1$$

$$D(s) = s^8 + 2s^6 + 1$$

## Even/Odd Polynomial

Even Polynomial:  $D(-s) = D(s)$

$$D(s) = s^2 + 1$$

$$D(s) = s^8 + 2s^6 + 1$$

Odd Polynomial:  $D(-s) = -D(s)$

## Even/Odd Polynomial

Even Polynomial:  $D(-s) = D(s)$

$$D(s) = s^2 + 1$$

$$D(s) = s^8 + 2s^6 + 1$$

Odd Polynomial:  $D(-s) = -D(s)$

$$D(s) = s^5 + 2s^3 + s = s(s^4 + 2s^2 + 1)$$

$$D(s) = s^5 + 7s^4 + 6s^3 + 42s^2 + 8s + 56$$

$$D(s) = s^5 + 7s^4 + 6s^3 + 42s^2 + 8s + 56$$

|       |   |   |   |
|-------|---|---|---|
| $s^5$ | 1 | 6 | 6 |
|-------|---|---|---|

|       |   |    |    |
|-------|---|----|----|
| $s^4$ | 7 | 42 | 56 |
|-------|---|----|----|

|       |   |   |   |
|-------|---|---|---|
| $s^3$ | 0 | 0 | 0 |
|-------|---|---|---|

$$D(s) = s^5 + 7s^4 + 6s^3 + 42s^2 + 8s + 56$$

|       |   |   |   |
|-------|---|---|---|
| $s^5$ | 1 | 6 | 6 |
|-------|---|---|---|

|       |   |    |    |
|-------|---|----|----|
| $s^4$ | 7 | 42 | 56 |
|-------|---|----|----|

|       |   |   |   |
|-------|---|---|---|
| $s^3$ | 0 | 0 | 0 |
|-------|---|---|---|

$$D_1(s) = s^4 + 6s^2 + 8$$

$$D(s) = s^5 + 7s^4 + 6s^3 + 42s^2 + 8s + 56$$

$$s^5 \quad 1 \quad 6 \quad 6$$

$$s^4 \quad 7 \quad 42 \quad 56$$

$$s^3 \quad 0 \quad 0 \quad 0$$

$$D_1(s) = s^4 + 6s^2 + 8$$

$$\frac{dD_1(s)}{ds} = 4s^3 + 12s$$

|       |   |   |               |    |    |    |   |
|-------|---|---|---------------|----|----|----|---|
| $s^5$ |   | 1 |               | 6  |    | 8  |   |
| $s^4$ |   | 7 | 1             | 42 | 6  | 56 | 8 |
| $s^3$ | 0 | 4 | 1             | 0  | 12 | 3  | 0 |
| $s^2$ |   |   | 3             |    | 8  |    | 0 |
| $s^1$ |   |   | $\frac{1}{3}$ |    | 0  |    | 0 |
| $s^0$ |   |   | 8             |    | 0  |    | 0 |

|       |    |    |               |     |    |    |   |
|-------|----|----|---------------|-----|----|----|---|
| $s^5$ |    | 1  |               | 6   |    | 8  |   |
| $s^4$ | -7 | 1  | 42            | 6   | 56 | 8  |   |
| $s^3$ | -8 | -4 | 1             | -12 | 3  | -8 | 0 |
| $s^2$ |    |    | 3             |     | 8  |    | 0 |
| $s^1$ |    |    | $\frac{1}{3}$ |     | 0  |    | 0 |
| $s^0$ |    | 8  |               | 0   |    | 0  |   |

Roots:  $-7, \pm 2i, \pm \sqrt{2}i$

### Example 3

$$D(s) = s^8 + s^7 + 12s^6 + 22s^5 + 39s^4 + 59s^3 + 48s^2 + 38s + 20$$

### Example 3

$$D(s) = s^8 + s^7 + 12s^6 + 22s^5 + 39s^4 + 59s^3 + 48s^2 + 38s + 20$$

|       |                 |         |         |      |    |
|-------|-----------------|---------|---------|------|----|
| $s^8$ | 1               | 12      | 39      | 48   | 20 |
| $s^7$ | 1               | 22      | 59      | 38   | 0  |
| $s^6$ | -10 -1          | -20 -2  | 40 1    | 20 2 | 0  |
| $s^5$ | -20 1           | -60 3   | 40 2    | 0    | 0  |
| $s^4$ | 1               | 3       | 2       | 0    | 0  |
| $s^3$ | -0 -4 2         | -0 -6 3 | -0 -0 0 | 0    | 0  |
| $s^2$ | $\frac{3}{2}$ 3 | -2 4    | 0       | 0    | 0  |
| $s^1$ | $\frac{1}{3}$   | 0       | 0       | 0    | 0  |
| $s^0$ | 4               | 0       | 0       | 0    | 0  |

$$D_1(s) = s^4 + 3s^2 + 2$$

$$D_1(s) = s^4 + 3s^2 + 2$$

All 4 roots of  $D_1(s)$  are on the imaginary axis

$$D_1(s) = s^4 + 3s^2 + 2$$

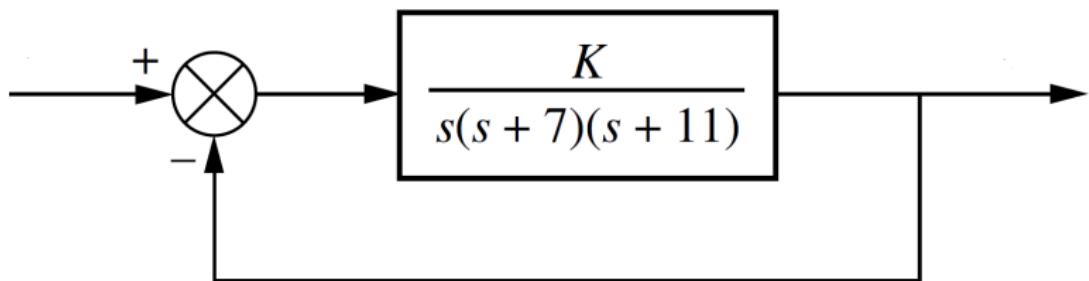
All 4 roots of  $D_1(s)$  are on the imaginary axis

Out of remaining 4 roots of  $D(s)$ :

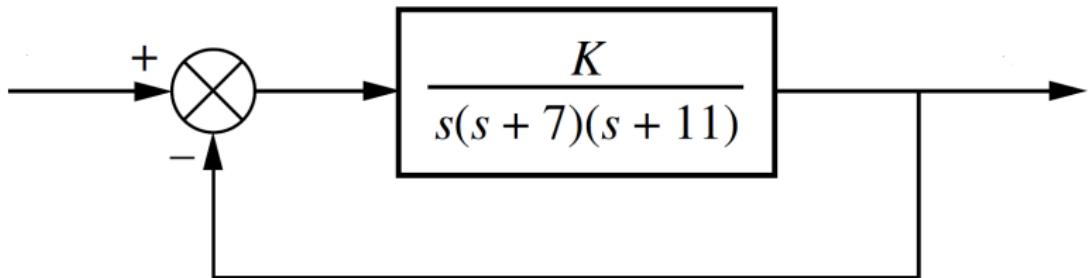
2 roots in RHP

2 roots in LHP

## Design Using Routh Hurwitz



## Design Using Routh Hurwitz



$$T(s) = \frac{K}{s^3 + 18s^2 + 77s + K}$$

$$\begin{array}{lll} s^3 & 1 & 77 \\ s^2 & 18 & K \\ \hline s^1 & \frac{1386 - K}{18} & \\ s^0 & K & \end{array}$$

$$\begin{array}{lll} s^3 & 1 & 77 \\ s^2 & 18 & K \\ \hline s^1 & \frac{1386 - K}{18} & \\ s^0 & K & \end{array}$$

$K < 1386$       All roots in LHP

$$\begin{array}{ccc}
 s^3 & 1 & 77 \\
 s^2 & 18 & K \\
 s^1 & \frac{1386 - K}{18} & \\
 s^0 & K &
 \end{array}$$

$K < 1386$       All roots in LHP

$K > 1386$       1 roots in LHP and 2 roots in RHP

$$\begin{array}{lll}
 s^3 & 1 & 77 \\
 s^2 & 18 & K \\
 s^1 & \frac{1386 - K}{18} & \\
 s^0 & K &
 \end{array}$$

$K < 1386$  All roots in LHP

$K > 1386$  1 roots in LHP and 2 roots in RHP

$K = 1386$  2 roots on imaginary axis  $\pm\sqrt{77}i$   
1 roots in LHP