

1. Radiation Field:

According to the Figure 1, given in Experiment 4 laboratory paper, there is an image and a source antenna due to the infinite perfect electric conductor.

Source antenna for field characteristic is called as direct component. It can be seen in below,

$$E_{\psi}^d = j\eta \frac{kI_0 l e^{-jkr_1}}{4\pi r_1} \sin\psi \quad (1)$$

Image antenna for field characteristic is called as reflected component. It can also be seen in below,

$$E_{\psi}^r = jR_v \eta \frac{kI_0 l e^{-jkr_2}}{4\pi r_2} \sin\psi$$

Since electric dipole is placed horizontally,

$$E_{\psi}^r = -j\eta \frac{kI_0 l e^{-jkr_2}}{4\pi r_2} \sin\psi \quad (2)$$

$\psi$  angle is measured from the  $y$ -axis to the observation point. Consider this

$$\cos\psi = \hat{a}_y \cdot \hat{a}_r = \hat{a}_y (\hat{a}_x \sin\theta \cos\phi + \hat{a}_y \sin\theta \sin\phi + \hat{a}_z \cos\theta) = \sin\theta \sin\phi$$

Using trigonometric identity,

$$\sin\psi = \sqrt{1 - \cos^2\psi} = \sqrt{1 - \sin^2\theta \sin^2\phi} \quad (3)$$

The approximation for the far-field observations are the ones for phase term

$$r_1 \approx r - h \cos\theta \quad (4a)$$

$$r_2 \approx r + h \cos\theta$$

and the ones for amplitude term

$$r \approx r_1 \approx r_2 \quad (4b)$$

Add the equation (1) and (2) up, (considering equation (3a) and (3b) )

$$\begin{aligned} E_{\psi} &= j\eta \frac{k I_0 L}{4\pi r} \sin\psi (e^{-jk r_1} - e^{-jk r_2}) \\ &= j\eta \frac{k I_0 L}{4\pi r} \sqrt{1 - \sin^2\theta \sin^2\phi} (e^{-jk(r - h\cos\theta)} + e^{-jk(r + h\cos\theta)}) \\ &= j\eta \frac{k I_0 L}{4\pi r} e^{-jkr} \sqrt{1 - \sin^2\theta \sin^2\phi} (e^{+jkh\cos\theta} - e^{-jkh\cos\theta}) \end{aligned}$$

$$E_{\psi} = j\eta \frac{k I_0 L}{4\pi r} e^{-jkr} \underbrace{\sqrt{1 - \sin^2\theta \sin^2\phi}}_{\substack{\sin\psi \\ \text{element factor}}} \underbrace{2j \sinh(kh\cos\theta)}_{\text{array factor}} \quad \because \sinh x = \frac{e^{jx} - e^{-jx}}{2j}$$

## 2. Radiated Power

In order to obtain radiated power, time average power density need to be find.

$$W_{av} = \frac{1}{2\eta} |E_{\psi}|^2 = \frac{(k_0 L)^2 I_0^2 \eta}{32\pi^2 r^2} (1 - \sin^2\theta \sin^2\phi) 4 \sin^2(kh\cos\theta)$$

$$\begin{aligned} P_{rad} &= \int_0^{2\pi} \int_0^{\pi/2} W_{av} r^2 \sin^2\theta d\theta d\phi \\ &= \frac{(k_0 L)^2 I_0^2 \eta}{32\pi^2 r^2} \int_0^{2\pi} \int_0^{\pi/2} (1 - \sin^2\theta \sin^2\phi) 4 \sin^2(kh\cos\theta) d\theta d\phi = \frac{(k_0 L)^2 I_0^2 \eta}{8\pi^2} M \end{aligned}$$

In order to evaluate the integral above, apply change of variable method,

$$\cos\theta = u \Rightarrow -\sin\theta d\theta = du \quad \text{and} \quad \sin^2\theta \triangleq 1 - u^2$$

The boundaries of " $\theta$ " integral must change due to change of variable.

$$\text{lower boundary } \theta = 0^\circ \Rightarrow u = 1$$

$$\text{upper boundary } \theta = 90^\circ \Rightarrow u = 0$$



New form of integral,

$$\begin{aligned}
 M &= \int_0^{2\pi} \int_0^1 (1 - (1-u^2)\sin^2\phi) \sin^2(kh\cos\theta) du d\phi \\
 &= \underbrace{\int_0^{2\pi} \int_0^1 \sin^2(khu) du d\phi}_{A_1} - \underbrace{\int_0^{2\pi} \int_0^1 (1-u^2)\sin^2\phi \sin^2(kh\cos\theta) du d\phi}_{-A_2} = A_1 + (-A_2)
 \end{aligned}$$

$$A_1 = \int_0^{2\pi} d\phi \int_0^1 \sin^2(khu) du = 2\pi \int_0^1 \frac{1 - \cos(2khu)}{2} du \quad \because \sin^2 x \triangleq \frac{1 - \cos 2x}{2}$$

$$= \pi \left[ [u]_0^1 - \left[ \frac{\sin(2khu)}{2kh} \right]_0^1 \right] = \pi \cdot \left( 1 - \frac{\sin 2kh}{2kh} \right)$$

$$-A_2 = - \int_0^{2\pi} \int_0^1 (1-u^2)\sin^2(khu)\sin^2\phi du d\phi = - \int_0^{2\pi} \sin^2\phi d\phi \int_0^1 (1-u^2)\sin^2(khu) du$$

$$= -\pi \cdot \left[ \int_0^1 \sin^2(khu) du - \int_0^1 u^2 \sin^2(khu) du \right]$$

$$= -\pi \left[ \frac{1}{2} - \frac{\sin(2kh)}{4kh} - \underbrace{\int_0^1 u^2 \sin^2(khu) du}_{A_{21}} \right]$$

In order to find  $A_2$ , integration by parts method will be used for  $A_{21}$

$$\int t dv = tv - \int v dt$$

$$A_{21} = \int_0^1 \underbrace{u^2}_t \underbrace{\sin^2(khu)}_{dv} du$$

$$\begin{aligned}
 \Rightarrow \quad t &= u^2 & v &= \frac{u}{2} - \frac{\sin(2khu)}{4kh} \\
 dt &= 2u du & dv &= \sin^2(khu) du
 \end{aligned}$$

Applying integration by parts for the expression,  $A_{21}$ ,

$$\begin{aligned}
 A_{21} &= \int_0^1 \underbrace{u^2}_{\frac{1}{t}} \underbrace{\sin^2(khu)}_{dv} du = t^2 \left( \frac{1}{2} - \frac{\sin(2kht)}{4kh} \right) \Big|_0^1 - \int_0^1 \left[ \frac{t}{2} - \frac{\sin(2kht)}{4kh} \right] 2t dt \\
 &= \frac{1}{2} - \frac{\sin(2kh)}{4kh} - \int_0^1 \left[ t^2 - 2t \frac{\sin(2kht)}{4kh} \right] dt \\
 &= \frac{1}{2} - \frac{\sin(2kh)}{4kh} - \frac{1}{3} + \underbrace{\int_0^1 \frac{2t \sin(2kht)}{4kh} dt}_{A_{211}}
 \end{aligned}$$

Apply integration by parts for the expression  $A_{211}$

$$\begin{aligned}
 A_{211} &= \int_0^1 \underbrace{2t}_{\alpha} \underbrace{\frac{\sin(2kht)}{4kh}}_v dt \Rightarrow \begin{aligned} \alpha &= 2t & v &= \frac{-\cos(2kht)}{8(kh)^2} \\ d\alpha &= 2dt & dv &= \frac{\sin(2kht)}{4kh} dt \end{aligned}
 \end{aligned}$$

$$\begin{aligned}
 &= \frac{-2t \cos(2kht)}{8(kh)^2} \Big|_0^1 - \int_0^1 \frac{-\cos(2kht)}{8(kh)^2} 2dt \\
 &= -\frac{\cos(2kh)}{(2kh)^2} + \left[ \frac{\sin(2kht)}{(2kh)^3} \right]_0^1 = -\frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3}
 \end{aligned}$$

$$A_{21} = \frac{1}{2} - \frac{\sin(2kh)}{4kh} - \frac{1}{3} + \left( -\frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right)$$

$$-A_2 = -\pi \left[ \cancel{\frac{1}{2} - \frac{\sin(2kh)}{4kh}} - \left( \cancel{\frac{1}{2} - \frac{\sin(2kh)}{4kh}} - \frac{1}{3} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right) \right]$$

$$-A_2 = \pi \left( \frac{1}{3} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right)$$

$$M = A_1 + (-A_2) = \pi \left( 1 - \frac{\sin(2kh)}{2kh} \right) + \pi \left( -\frac{1}{3} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right)$$

$$U = \pi \left( \frac{2}{3} - \frac{\sin(2kh)}{2kh} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right)$$

Finally radiated power can be calculated such that,

$$\begin{aligned} P_{\text{rad}} &= \frac{k_0^2 L^2 I_0^2}{8\pi^2} \eta \cdot \pi \left( \frac{2}{3} - \frac{\sin(2kh)}{2kh} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right) \\ &= \frac{(2\pi)^2}{\lambda^2} \frac{L^2 I_0^2}{8\pi^2} \eta \pi (\dots) \\ &= \eta \frac{\pi}{2} \left( \frac{LI_0}{\lambda} \right)^2 \left( \frac{2}{3} - \frac{\sin(2kh)}{2kh} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right) \end{aligned}$$

### 3- Radiation Resistance

Radiation resistance is derived from radiated power so

$$R_{\text{rad}} = \frac{2 P_{\text{rad}}}{|I_0|^2}$$

$$R_{\text{rad}} = \eta \pi \left( \frac{L}{\lambda} \right)^2 \left( \frac{2}{3} - \frac{\sin(2kh)}{2kh} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right)$$

Using the expansions of the sine & cosine functions, when  $kh$  approaches to zero, radiation resistance becomes

$$R_{\text{rad}} = \eta \pi \left( \frac{L}{\lambda} \right)^2 \left[ \frac{2}{3} - \frac{2}{3} + \frac{8}{15} \left( \frac{2kh}{\lambda} \right)^2 \right] = \eta \frac{32\pi^3}{15} \left( \frac{L}{\lambda} \right)^2 \left( \frac{h}{\lambda} \right)^2$$

### 4- Radiation Intensity & Directivity

The radiation intensity is given by

$$U \approx \frac{r^2}{2\eta} |E_\phi|^2 = \frac{\eta}{2} \left| \frac{I_0 L}{\lambda} \right|^2 (1 - \sin^2 \theta \sin^2 \phi) \sin^2(kh \cos \theta)$$

The maximum value of radiation intensity depends on the value of  $kh$  (whether  $kh \leq \frac{\pi}{2}$ ,  $h \leq \frac{\lambda}{4}$ ;  $kh > \frac{\pi}{2}$ ,  $h > \frac{\lambda}{4}$ ). It can be shown that the maximum of radiation intensity, considering the conditions mentioned above,



$$U_{\max} = \begin{cases} \frac{\eta}{2} \left| \frac{I_0 L}{\lambda} \right|^2 \sin^2(kh) & kh \leq \frac{\pi}{2} \quad (h \leq \lambda/4) \\ \frac{\eta}{2} \left| \frac{I_0 L}{\lambda} \right|^2 & kh > \frac{\pi}{2} \quad (h > \lambda/4) \end{cases}$$

( $\theta = 0^\circ$ )

[  $\theta = 0^\circ$  and  $\sin(kh \cos \theta_{\max}) = 1$   
or  $\theta_{\max} = \cos^{-1}(\frac{\pi}{2kh})$  ]

Directivity formula can be found from the equation,

$$D_0 = \frac{4\pi U_{\max}}{P_{\text{rad}}}$$

where

$$P_{\text{rad}} = \frac{1}{2} |I_0|^2 R_{\text{rad}} \rightarrow$$

The conditions which are used in the calculation of  $U_{\max}$  are still valid for directivity.

Consider the case where  $kh \leq \frac{\pi}{2}$  and  $h \leq \lambda/4$

$$D_{0_1} = \frac{4\pi \frac{\eta}{2} \frac{I_0^2 L^2}{\lambda^2} \sin^2 kh}{\frac{1}{2} |I_0|^2 R_{\text{rad}}} = \frac{4\pi \eta \sin^2(kh) \frac{L^2}{\lambda^2}}{\eta \left( \frac{L}{\lambda} \right)^2 R(kh)} = \frac{4 \sin^2(kh)}{R(kh)}$$

and  $kh > \frac{\pi}{2}$  ( $h > \lambda/4$ ) case

$$D_{0_2} = \frac{4\pi \frac{\eta}{2} \frac{I_0^2 L^2}{\lambda^2}}{\frac{1}{2} |I_0|^2 R_{\text{rad}}} = \frac{4\pi \eta \frac{L^2}{\lambda^2}}{\eta \left( \frac{L}{\lambda} \right)^2 R(kh)} = \frac{4}{R(kh)}$$

As a result

$$D_0 = \begin{cases} \frac{4 \sin^2(kh)}{R(kh)} & kh \leq \frac{\pi}{2} \quad (h \leq \lambda/4) \\ \frac{4}{R(kh)} & kh > \frac{\pi}{2} \quad (h > \lambda/4) \end{cases}$$