

Diffusion Approximation

$$\underbrace{\text{leakage} + \text{absorption}}_{\text{loss}} = \underbrace{\text{source} + \text{fission}}_{\text{gain}}$$

$$\Rightarrow \operatorname{div}(\vec{J}(\vec{x})) + \Sigma_a(\vec{x}) \phi(\vec{x}) = S''(\vec{x}) + \gamma \Sigma_f(\vec{x}) \phi(\vec{x})$$

Now, by Fick's law (3D), we have $\vec{J}(\vec{x}) = -D(\vec{x}) \vec{\nabla} \phi(\vec{x})$

\Rightarrow the equation now becomes,

$$\operatorname{div}(-D(\vec{x}) \vec{\nabla} \phi(\vec{x})) + \Sigma_a(\vec{x}) \phi(\vec{x}) = S''(\vec{x}) + \gamma \Sigma_f(\vec{x}) \phi(\vec{x})$$

$$\operatorname{div}(\vec{x}) = \vec{x} \cdot \vec{x}$$

above eqn is written as (as in book)

$$-\vec{x} \cdot D(\vec{x}) \vec{\nabla} \phi(\vec{x}) + \Sigma_a(\vec{x}) \phi(\vec{x}) = S''(\vec{x}) + \gamma \Sigma_f(\vec{x}) \phi(\vec{x})$$

Now as derived previously, $D = \frac{1}{3\Sigma_{fr}}$, $\Sigma_{fr} = \Sigma_f - \bar{\mu} \Sigma_s$.
 averaging diffusion coefficient can be accomplished by hot wire techniques to average Σ_{fr} then $\bar{D} = \frac{1}{3\bar{\Sigma}_{fr}}$.

SOLUTION OF DIFFUSION EQUATION

Diffusion equation.

$$-\vec{x} \cdot D(\vec{x}) \vec{\nabla} \phi(\vec{x}) + \Sigma_a(\vec{x}) \phi(\vec{x}) = S''(\vec{x}) + \gamma \Sigma_f(\vec{x}) \phi(\vec{x})$$

$$-D(\vec{x}) \vec{\nabla} \cdot \vec{\nabla} \phi(\vec{x}) + \Sigma_a(\vec{x}) \phi(\vec{x}) = S''(\vec{x}) + \gamma \Sigma_f(\vec{x}) \phi(\vec{x})$$

$$D(\vec{x}) \vec{\nabla}^2 \phi(\vec{x}) + \Sigma_a(\vec{x}) \phi(\vec{x}) = S''(\vec{x}) + \gamma \Sigma_f(\vec{x}) \phi(\vec{x})$$

$$\vec{\nabla}^2 = \vec{x} \cdot \vec{x} = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$$

DIFFUSION EQUATION FOR NON MULTIPLYING SYSTEMS - PLANE GEOMETRY

First consider case of a uniform medium with no fissionable material i.e. a non multiplying system. $\Sigma_f = 0$ & $D \propto \Sigma_a$ are constants.

Hence the diffusion equation,

$$-D(\vec{x}) \nabla^2 \phi(\vec{x}) + \Sigma_a(\vec{x}) \phi(\vec{x}) = S'''(\vec{x}) + 2\Sigma_f(\vec{x}) \phi(\vec{x})$$

becomes

$$-D \nabla^2 \phi(\vec{x}) + \Sigma_a \phi(\vec{x}) = S'''(\vec{x}) \quad (\because \Sigma_a, D = \text{constant} \quad \Sigma_f = 0)$$

Dividing the equation by D ,

$$-\nabla^2 \phi(\vec{x}) + \frac{\Sigma_a}{D} \phi(\vec{x}) = \frac{S'''(\vec{x})}{D}$$

Let $\frac{D}{\Sigma_a} = L$, $L = \text{diffusion length}$. (magnitude of displacement of neutron before absorption from source)

$$\Rightarrow -\nabla^2 \phi(\vec{x}) + \frac{1}{L^2} \phi(\vec{x}) = \frac{S'''(\vec{x})}{D}$$

Some free example

Consider a simple problem in plane geometry where flux varies so slowly in $y \& z$ direction that it can be ignored, allowing us to eliminate $y \& z$ derivatives. We may also set source = 0

Then now, the diffusion eqn (above) becomes

$$-\frac{d^2}{dx^2} \phi(x) + \frac{1}{L^2} \phi(x) = 0$$

$$\text{or } \frac{d^2}{dx^2} \phi(x) - \frac{1}{L^2} \phi(x) = 0.$$

Second order differential eqn

Homogeneous

MATH SUPPORT

linear second order ODE w/ constant coefficients

$$y'' + Ay' + By = 0 \leftarrow \text{homogeneous}$$

Assume general solⁿ $y = C_1 y_1 + C_2 y_2$

where y_1 & y_2 are solutions

Initial condition are satisfied by choosing C_1, C_2 .

To solve ^{the} ODE, find 2 solutions (independent)

Basic method:

Try $y = e^{rt}$ (t = independent variable, y -dependent)

plug in to above ODE,

$$r^2 e^{rt} + A r e^{rt} + B e^{rt} = 0.$$

$$r^2 + Ar + B = 0.$$

Characteristic equation of system

Case 1: Roots r_1, r_2 (real)

General solution $y = C_1 e^{r_1 t} + C_2 e^{r_2 t}$

Ex

$$y'' + 4y' + 3y = 0. \leftarrow \text{characteristic eqn.}$$

$$r^2 + 4r + 3 = 0$$

$$\Rightarrow (r+3)(r+1) = 0$$

$$\text{SOLN. } y = C_1 e^{-3t} + C_2 e^{-t}$$

Initial conditions: $y(0) = 1; y'(0) = 0$

$$y' = -3C_1 e^{-3t} - C_2 e^{-t} \quad \text{by } y = C_1 e^{-3t} + C_2 e^{-t}$$

$$\Rightarrow 0 = -3C_1 - C_2; 1 = C_1 + C_2 \Rightarrow C_1 = -\frac{1}{2}; C_2 = \frac{3}{2}$$

$$\Rightarrow \text{SOLN. } y = \frac{-1}{2} e^{-3t} + \frac{3}{2} e^{-t}$$

CASE 2 Complex roots

$$z = a \pm bi$$

We get a complex solution

$$y = e^{(at+bt)}$$

Theorem: If $ut+iv$ is a complex solution to a real differential equation to $y'' + Ay' + By = 0$, then $u \& v$ are real solutions.

Proof:

$$(ut+iv)'' + A(ut+iv)' + B(ut+iv) = 0$$

$$\underbrace{u'' + Au' + Bu}_{\text{real part}} + i \underbrace{(v'' + Av' + Bv)}_{\text{imaginary part}} = 0$$

$$\begin{matrix} \parallel & \parallel \\ 0 & 0 \end{matrix}$$

only that would make $v = 0$
that makes $u \& v$ solns.

case 2 SOLⁿ

$$y = e^{at+bt} = e^{at(\cos bt)} \text{ real part}$$

$$e^{at(\sin bt)} \text{ imaginary part}$$

$$\text{SOL}^n: y = e^{at}(C_1 \cos bt + C_2 \sin bt)$$

example

$$y'' + 4y' + 5y = 0$$

char eqn

$$t^2 + 4t + 5 = 0$$

$$\Rightarrow \lambda = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a} = \frac{-4 \pm \sqrt{4}}{2} = -2 \pm i$$

$$\therefore e^{(-2+i)t}$$

$$e^{-2t}(\cos t), e^{-2t}\sin t$$

$$\therefore y = e^{-2t}(C_1 \cos t + C_2 \sin t)$$

18.0

Case 3 Critically damped

$$\zeta^2 + A \zeta \tau B = 0 \quad \text{has 2 equal roots}$$

$$(\zeta + a)^2 = 0$$

$$\Rightarrow \zeta^2 + 2A\zeta + A^2 = 0$$

$$\Rightarrow \text{ODE looks like } y'' + 2Ay' + A^2 y = 0$$

Solⁿ
$$y = e^{-at}$$

Know how to solve $y'' + py' + qy = 0$, then there is another $y = f_1 e^{at}$

unknown f_1 [$y = e^{-at} u$]

$$2a \times [y' = -aue^{-at} + e^{-at} u'$$

$$] \quad y'' = a^2 e^{-at} u - 2ae^{-at} u' + e^{-at} u''$$

$$0 = 0 + 0 + e^{-at} u''$$

$$\Rightarrow e^{-at} u'' = 0$$

$$\Rightarrow u = C_1 t + C_2 \quad (\text{just } t \text{ would be enough})$$

$$y_2 = e^{-at} t$$

$$y_1 = e^{-at}$$

GOING BACK TO OUR EXAMPLE.

Recall

equation was

$$\frac{d^2 \phi(x)}{dx^2} - \frac{1}{L^2} \phi(x) = 0.$$

(stdm & form $\phi(x) = e^{rx}$)

The above is a linear ODE of 2nd order

Characteristic equation is $r^2 - \frac{1}{L^2} = 0$

$$\Rightarrow \left(\frac{r-1}{L}\right)\left(\frac{r+1}{L}\right) = 0$$

$$\Rightarrow r = \pm \frac{1}{L} \rightarrow r_1, r_2$$

Equation has distinct & real roots, hence the solution looks like

$$\begin{aligned} \phi(0) &= C_1 e^{r_1 x} + C_2 e^{r_2 x} \\ \phi(x) &= C_1 e^{x/L} + C_2 e^{-x/L} \end{aligned}$$

Now to find C_1 & C_2 , we need boundary conditions or initial conditions
Initial & Boundary conditions

Here, suppose the domain is semi-infinite i.e. $0 \leq x \leq \infty$

$\phi(0) = \phi_0$ (from left)
No neutrons enter from right as medium is semi-infinite hence each neutron that entered can safely be assumed to be absorbed at the right end i.e. at $\infty \rightarrow \phi(\infty) = 0$.

Now applying boundary conditions, $\phi(0) = \phi_0 ; \phi(\infty) = 0 \rightarrow \phi(x)$

$$\Rightarrow \phi(0) = C_1 e^{0x} + C_2 e^{-0x}$$

$$\Rightarrow \phi_0 = C_1 + C_2$$

Now from
 $C_1 = 0$
 $\Rightarrow C_2 = \phi_0$

$$\begin{aligned} \phi(\infty) &= C_1 e^{0x} + C_2 e^{-\infty x} = 0 \\ \text{because } e^{\infty} &= \infty, e^{-\infty} = 0 \\ \text{This eqn satisfies only if } &C_1 = 0 \end{aligned}$$

Now substituting C_1 & C_2 in eqn.

$$\begin{aligned}\phi(x) &= C_1 e^{-x/L} + C_2 e^{-x/L} \\ &= 0 + C_2 e^{-x/L} \\ \boxed{\phi(x)} &= \phi_0 e^{-x/L}\end{aligned}$$

Uniform source example:

We next examine the case with uniform source $S''(\vec{x}) \rightarrow S_0''$. In plane geometry reduces from

$$-\nabla^2 \phi(\vec{x}) + \frac{1}{L^2} \phi(\vec{x}) = \frac{1}{D} S_0''(\vec{x})$$

$$\frac{-d^2 \phi(x)}{dx^2} + \frac{1}{L^2} \phi(x) = \frac{1}{D} S_0''$$

Non homogeneous 2nd order differential eqn

MATH SUPPORT

2nd order linear ODE means y, y', y''

Sol^m method:

Find 2 independent sol^m - y_1 , y_2 .

Independent means $y_2 \neq c y_1$; $y_1 \neq c' y_2$

Then all sol^m are linear combination with constant coefficients

$$y = C_1 y_1 + C_2 y_2 \quad - \text{WHY?}$$

Q2 why are these all the sol^m?

Q3 why are $C_1 y_1 + C_2 y_2$ sol^m?

Q-1 Superposition principle: y_1, y_2 are soln. $\Rightarrow c_1 y_1 + c_2 y_2$ is also soln.

homogeneous ODE

$\Rightarrow \underbrace{c_1 y_1 + c_2 y_2}_{\text{is a soln.}} \text{ (linear combination of } y_1, y_2)$

Proof: $y'' + py' + qy = 0$

$Dy + pDy + qy = 0 \rightarrow \underbrace{(D^2 + pD + q)y = 0}_{\substack{\text{differentiated} \\ \text{operator}}} \Rightarrow L(y) = 0$

$$\xrightarrow{u(x)} \boxed{L} \xrightarrow{u(x)}$$

Linear operator - $L(u_{(x)} + u_{(x)}) = L(u_{(x)}) + L(u_{(x)})$
 $L(cu_{(x)}) = cL(u_{(x)})$

Ex. D is linear because $D(u_1 + u_2) = Du_1 + Du_2$

Proof of superposition:

ODE $\& Ly = 0$

If L is linear,

$$L(c_1 y_1 + c_2 y_2) = L(c_1 y_1) + L(c_2 y_2)$$

$$= c_1 L(y_1) + c_2 L(y_2)$$

$\stackrel{0}{\parallel}$ as y_1 & y_2 are solutions

$$\Rightarrow L(y_1), L(y_2) = 0$$

$$= 0 + 0$$

$$= 0.$$

Hence $c_1 y_1 + c_2 y_2$ is also a solution.

Q2 Solving the initial value problems (find soln with given initial values at x_0).

Thm: $\{c_1 y_1 + c_2 y_2\}$ is enough to satisfy any initial value

Proof:

$$\begin{aligned} y(x_0) &= a \\ y'(x_0) &= b \end{aligned} \quad \left. \begin{array}{l} \text{initial values} \\ \text{simultaneous linear eqns} \end{array} \right\}$$

$$\begin{aligned} y &= c_1 y_1 + c_2 y_2 \\ y' &= c_1 y'_1 + c_2 y'_2 \end{aligned} \quad \left. \begin{array}{l} \text{plug } x = x_0 \Rightarrow c_1 y_1(x_0) + c_2 y_2(x_0) = a \\ c_1 y'_1(x_0) + c_2 y'_2(x_0) = b \end{array} \right\}$$

c_1 & c_2 are unknown variables \rightarrow needs to find

the system of linear eqns is solvable for c_1 & c_2 , if

$$\begin{vmatrix} y_1 & y_2 \\ y'_1 & y'_2 \end{vmatrix}_{x=x_0} \neq 0. \quad \left. \begin{array}{l} \text{called Wronskian} \\ = W(y_1, y_2) \rightarrow \neq 0 \end{array} \right.$$

Thm: If y_1, y_2 are solutions to ODE (linear, homogeneous, 2nd order), either $W(y_1, y_2) \equiv 0$ (for all values of x) or $W(y_1, y_2) \neq 0$ (for all x)

$\{c_1 y_1 + c_2 y_2\} = \{c_1 u_1 + c_2 u_2\} - u_1, u_2 - \text{any other pair of independent solutions.}$

$$u_1 = \bar{c}_1 y_1 + \bar{c}_2 y_2$$

$$u_2 = \bar{c}_1 y_1 + \bar{c}_2 y_2$$

Finding normalized solutions (at 0) could be x_0

$$Y_1, Y_2$$

$$Y_1: \begin{cases} Y_1(0) = 1 \\ Y_1'(0) = 0 \end{cases}$$

$$Y_2: \begin{cases} Y_2(0) = 0 \\ Y_2'(0) = 1 \end{cases}$$

$$y'' + y = 0$$

$$y_1 = (0) x = Y_1$$

$$y_2 = \sin x = Y_2$$

because it
is 1

$$y'' - y = 0$$

General soln. $c_1 e^x + c_2 e^{-x} = y$, $y' = c_1 e^x - c_2 e^{-x}$

$$y_1 = e^x$$

$$y_2 = e^{-x}$$

$$Y_1: c_1 + c_2 = 1$$

$$c_1 - c_2 = 0$$

$$\Rightarrow c_1 = c_2 = \frac{1}{2}$$

$$Y_1 = \frac{e^x + e^{-x}}{2} = \cos x$$

$$Y_2 = \frac{e^x - e^{-x}}{2} = \sin x$$

y_2 --- put initial conditions

$$y_2 = \frac{e^x - e^{-x}}{2} = \sinh x$$

y_1, y_2 normalized at 0
soln to IVP ODE $y(0)=a$
 $y'(0)=b$

is

$$\boxed{y_0 y_1 + y_0' y_2}$$

Existence & Uniqueness theorem

$y'' + py' + qy = 0$ p, q are continuous for all x
There is one & only one soln satisfying given initial values
such that $y(0)=A, y'(0)=B$

Want all solutions to ODE

Claim $\{c_1 y_1 + c_2 y_2\}$ are all the solutions

Proof

Given soln $u(x), u(0) = u_0, u'(0) = u_0'$ then
 $u_0 y_1 + u_0' y_2$ satisfies the initial values

INHOMOGENEOUS ODE e^{nd} order

$$\boxed{y'' + p(x)y' + q(x)y = f(x)}$$

input signal / forcing term / driving term

Solⁿ $y(x)$ called response / output etc

$$y'' + p(x)y' + q(x)y = 0$$

associated homogeneous eqn
aka reduced equation

Solⁿ $y_c = C_1 y_1 + C_2 y_2$

= solution to associated homogeneous equation
aka complementary solution

Example:

$$mx'' + bx' + kx = f(t)$$

$$mx'' = -kx - bx' + f(t)$$

Thm:

$$Ly = f(x)$$

L is a linear operator

$$y'' + p(x)y' + q(x)y = f(x)$$

Solution:

$$y_p + y_c$$

$$\text{ie } y = y_p + y_c = \underbrace{y_p}_{\substack{\text{particular} \\ \text{soln to } Ly = f(x)}} + \underbrace{C_1 y_1 + C_2 y_2}_{\substack{\text{L solutions} \\ \text{of associated homogeneous} \\ \text{equation}}} \quad \text{any one soln}$$

$$y'' + Ay' + By = f(t)$$

$$y = y_p + \underbrace{C_1 y_1 + C_2 y_2}_{\substack{\text{initial conditions}}}$$

Q When does $C_1 y_1 + C_2 y_2 \rightarrow 0$ as $t \rightarrow \infty$ for all C_1, C_2

If this is so, ODE is called stable

$$y = \underbrace{y_p}_{\substack{\text{steady} \\ \text{state} \\ \text{sol}}} + \underbrace{C_1 y_1 + C_2 y_2}_{\substack{\text{transient}}}$$

roots of characteristic eqn	Soln	stability condition
real & distinct	$C_1 e^{\alpha_1 t} + C_2 e^{\alpha_2 t}$	$\alpha_1 < 0, \alpha_2 < 0$
$\alpha_1 = \alpha_2$	$(C_1 + C_2 t) e^{\alpha_1 t}$	$\alpha_1 < 0$
$\alpha = a \pm bi$	$e^{at} (C_1 \cos bt + C_2 \sin bt)$	$a < 0$

ODE is stable if all characteristic roots have $\text{real part} < 0$.

Finding particular solution

$$y'' + Ay' + By = f(x)$$

Find a particular form y_p / ^{complementary} _{sol}

$$\text{General soln } y = y_p + y_c = y_p + C_1 y_1 + C_2 y_2$$

particular soln - anything that satisfies given equation

Back to diffusion theory

Our four source example in a nonmultiplying system

$$S''(\vec{x}) \rightarrow S_0'''$$

In plane geometry, equation reduces to (as shown previously)

$$-\frac{d\phi(x)}{dx^2} + \frac{1}{l^2} \phi(x) = \frac{1}{D} \text{ so}$$

The above equation is 2nd order linear inhomogeneous ODE

The general solution is of the form $y = y_p + y_c$, where y_p is the particular solution and y_c is the solution to related homogeneous eqn.

First finding y_p the particular solution,

First finding y_p , the particular solution,
 Now since source is uniform, the particular solution is a constant. Hence
 its derivative is a constant.

Let ϕ_p be that constant (particular solⁿ)

$$\Rightarrow -\frac{d^2 \phi_p}{dx^2} + \frac{1}{l^2} \phi_p = \frac{1}{D} \sin^2$$

$$\Rightarrow \sigma + \phi_p = \frac{L^2}{D} \sigma_0'' = \frac{D/\epsilon_a}{D} \sigma_0'' = \frac{1}{\epsilon_0} \sigma_0''$$

$$\Rightarrow y_p = \phi_p = \frac{1}{\varepsilon a}^{50''}$$

for y_c ,

for y_c ,
the corresponding homogeneous equation is $\frac{-d^2\phi(x)}{dx^2} + \frac{1}{L^2}\phi(x) = 0$

$$a \frac{d^2 \phi(x)}{dx^2} - \frac{1}{L^2} \phi(x) = 0$$

$$\frac{d^2 \phi(x)}{dx^2} - \frac{1}{L^2} \phi(x) = 0$$

to be $C_1 e^{x/L} + C_2 e^{-x/L}$

We know its solution to be $C_1 e^{-\lambda x} + C_2 e^{\lambda x}$.
 Now to find the constants C_1 & C_2 , we apply boundary conditions
 to the general equation so that $C_1 e^{-\lambda L} + C_2 e^{\lambda L}$

$$y = \phi(x) = Y_p + y_c = \frac{50}{\varepsilon a} + C_1 e^{50x} + C_2 e^{-50x}$$

Suppose current source is distributed throughout a slab extending between $-a \leq x \leq a$, and that we specify boundary conditions as the flux vanishing at the slab i.e. $\phi(±a) = 0$. Hence now applying that boundary condition.

$$\phi(-a) = C_1 e^{-a/L} + C_2 e^{a/L} + \frac{S_0''}{\epsilon a} \quad (1)$$

$$\phi(+a) = C_1 e^{a/L} + C_2 e^{-a/L} + \frac{S_0''}{\epsilon a} \quad (2)$$

Now, the 2 equations are identical & if they are both going to be equal to same number, the equations are equal. So & that gives $C_1 = C_2$ (which is the only condition under which both eqns could be 0)

Hence now using that to solve for C_1 using 2nd eqn.

$$C_1 e^{a/L} + C_1 e^{-a/L} + \frac{S_0''}{\epsilon a} = 0$$

$$C_1 (e^{a/L} + e^{-a/L}) = -\frac{S_0''}{\epsilon a}$$

$$\Rightarrow C_1 = C_2 = -\left(e^{a/L} + e^{-a/L}\right)^{-1} \frac{S_0''}{\epsilon a}$$

$$= -\frac{1}{2} (\cosh a/L)^{-1} \frac{S_0''}{\epsilon a}$$

Now substituting that in one general form,

We have

$$\begin{aligned} \phi(x) &= \frac{S_0''}{\epsilon a} + \frac{-1}{2} \frac{\cosh(a/L)}{\sinh(a/L)} \frac{S_0''}{\epsilon a} e^{ax/L} - \frac{1}{2} \frac{\cosh(a/L)}{\sinh(a/L)} \frac{S_0''}{\epsilon a} e^{-ax/L} \\ &= \frac{S_0''}{\epsilon a} \left(1 - \frac{1}{2} \frac{\cosh(ax/L)}{\sinh(ax/L)} \right) \end{aligned}$$

$$\boxed{\phi(x) = \frac{S_0''}{\epsilon a} \left(1 - \frac{\cosh(ax/L)}{\sinh(ax/L)} \right)}$$

BOUNDARY CONDITIONS

While solving the diffusion equation, which is a differential eqn., the soln. contains 2 arbitrary constants (for 1D). 2 boundary conditions are required to determine these constants. After these boundary conditions accurately represent the physical situation at hand.

A particularly useful concept is that of partial currents:

Recall $J(x)$ = net number of neutrons per cm² per crossing a plane perpendicular to x axis in time \times dm. This may be divided into partial currents, $J_x^+(x) \& J_x^-(x)$ of neutrons travelling in the +ve & -ve x direction.

$$J_x(x) = J_x^+(x) - J_x^-(x).$$

Now as shown before,

$$J_x^\pm(x) = \frac{1}{4} \phi(x) \mp \frac{1}{2} D \frac{d\phi(x)}{dx}$$

VACUUM BOUNDARIES

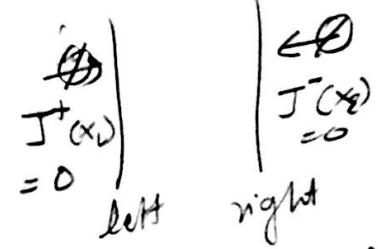
Consider a surface across which no neutrons enter. This would be the case if a vacuum-containing neutron source extended to infinity. Hence we refer to such surfaces at boundaries as vacuum boundaries.

If the boundary is on left, $J_x^+(x_l) = 0$

If the boundary is on right, $J_x^-(x_r) = 0$

The condition on right, using above eqns. may be written as

$$J_x(x_r) = 0 = \frac{1}{4} \phi(x_r) + \frac{1}{2} D \left(\frac{d\phi(x_r)}{dx} \right)_{x_r} = \frac{1}{4} \phi(x_r) - \frac{1}{2} D \left| \frac{d\phi(x)}{dx} \right|_{x_r}$$



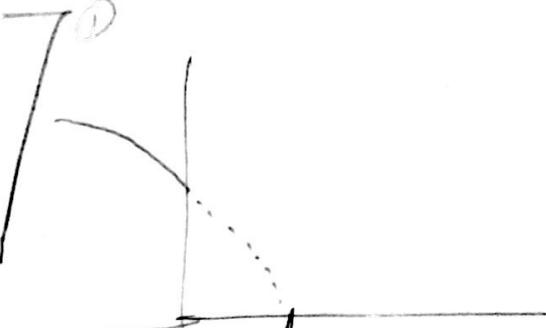
Now, it must be noted that derivative is w.r.t distance as no flux enters

Now, for an isotropic scatter, $D = \frac{1}{3\varepsilon t}$ & $\lambda = mfp = \frac{1}{\varepsilon t}$

$$\text{Hence } 0 = \frac{1}{4} \phi(x_r) - \frac{1}{2} \frac{1}{3\varepsilon t} \left| \frac{d\phi(x)}{dx} \right|_{x_r}$$

$$\Rightarrow \left| \frac{\phi(x_e)}{\frac{d\phi(x)}{dx}} \right|_{x_e} = \frac{2}{3}\lambda = \frac{2}{3}\epsilon_f$$

A visual interpretation of the situation is shown in adjoining figure.



Now, extrapolating flux linearly, flux goes to 0 when it is $\frac{2}{3}\lambda$ outside boundary

Thus $\frac{2}{3}\lambda$ is referred to as extrapolation distance

$$\frac{\phi(x) - \phi(0)}{x_e - x_0} = \frac{d\phi(x)}{dx} = \frac{3}{2\lambda} \phi(x_e) \quad (\text{by } ①)$$

\downarrow
Extrapolation distance

$$\rightarrow \frac{\phi(x_e)}{x_e - x_0} = \frac{3}{2\lambda} \phi(x_e) \rightarrow \frac{2\lambda}{3} = x_e - x_0$$

Hence x_0 is $\frac{2\lambda}{3}$ units to the right of x_e as shown in figure

When a vacuum boundary is encountered, simply adjust the dimensions & vary another boundary condition or move straight forward. Thus far problem with left & right vacuum boundaries

$$\boxed{x_e: \phi(x_e - \frac{2\lambda}{3}) = 0 = \phi(\tilde{x}_e)} \\ x_e: \phi(x_e + \frac{2\lambda}{3}) = 0 = \phi(\tilde{x}_e)}$$

$$(x_e - \frac{2\lambda}{3} = \tilde{x}_e) \\ (x_e + \frac{2\lambda}{3} = \tilde{x}_e)$$

FOR VACUUM BOUNDARIES

at λ is too small

$$\boxed{\phi(x_e) \approx 0; \phi(x_tilde_e) \approx 0}$$

REFLECTED BOUNDARIES

REFLECTED BOUNDARIES

If the net current I_x is known at a boundary, it may be used as a condition. Current conditions appear most frequently as a result of problem symmetry.

Hence the net number of neutrons crossing boundary vanishes

$$J_x(0) = -D \frac{d}{dx} \left. (Ax(x)) \right|_{x=0} = 0$$

$$\frac{d}{dx} \Phi(m) \Big|_{m=0} = 0$$

SURFACE SOURCES AND ALBEDOS

SURFACE SOURCES AND FLUXES

Partial currents are particularly useful in specifying boundary conditions in situations where surfaces are bounded by neutrons. To illustrate this consider a source free cm^{-3} . For this sort to hold, neutrons must be being supplied from left. We can relate the boundary flux to a surface source of $s'' \text{ neutrons/cm}^2\text{s}$ noting that no neutrons enter from left.

$$J(x) = \frac{Dd}{dx} \Phi^{(n)}$$

$$J^+(0) = s''$$

Now, we know that $J_x^+(x) = \frac{1}{4} \phi(x) - \frac{1}{2} \frac{Dd\phi}{dx}(x)$

$$\propto \phi(u) = \phi_0 e^{-\alpha u}$$

$$\text{Now, } \quad \text{Substitute}$$

$$R \phi(x) = \phi_0 e^{-x/L} \quad \leftarrow$$

$$\Rightarrow \frac{d}{dx} \phi(x) = -\frac{1}{L} \phi_0 e^{-x/L}$$

$$\Rightarrow J_x(x) = \frac{1}{4} \phi_0 e^{-x/L} - \frac{1}{2(L)} D_0 e^{-x/L}$$

$$\phi_B e^{-x/L} \left(\frac{1}{4} + \frac{D}{2L} \right)$$

Now we know that $\exists x \phi = \exists^{\prime \prime}$

$$\rightarrow J_x^+(0) = S^{10} = \left(\frac{1}{4} + \frac{D}{2L}\right) \Phi_0 e^{0i\kappa}$$

$$\rightarrow \frac{s^{11}}{1 + \frac{D}{ZL}} = \phi_0$$

$$d(x) = \frac{s''}{\left(\frac{1}{4} + \frac{D}{2L}\right)} e^{-x/L}$$

ALBEDO

The ratio of exiting to entering neutrons is termed albedo It may be expressed in terms of partial currents as

$$\alpha = \frac{J_x^-(0)}{J_x^+(0)}$$

thus,

We know that

$$J_x^+(0) = \left(\frac{1}{4} + \frac{D}{2L}\right) \Phi_0 e^{-x/L}$$

similarly

$$J_x^-(0) = \left(\frac{1}{4} - \frac{D}{2L}\right) \Phi_0 e^{-x/L}$$

$$\therefore \alpha = \frac{J_x^-(0)}{J_x^+(0)} = \frac{\text{outgoing } J_x^-}{\text{incoming } J_x^+} = \frac{\frac{1}{4} - \frac{D}{2L}}{\frac{1}{4} + \frac{D}{2L}}$$

$$= \boxed{\frac{1 - \frac{2D}{L}}{1 + \frac{2D}{L}}}$$

Thus in a semiinfinite medium α 's " neutrons/cm² will be reemitted from the surface, while remaining $(1-\alpha)$'s " neutrons will be absorbed within the medium.

INTERFACE CONDITIONS

If more than 1 region is present, with different Cs, the diffusion equation solution will have 2 arbitrary constants for each region. Thus 2 conditions are required for each region. Thus 2 conditions are required at each interface.

The conditions are - both current and flux are continuous
Hence for an interface at x_0 .

$$\boxed{\phi(x_{0-}) = \phi(x_{0+})}$$

$$\& \boxed{D(x_{0-}) \frac{d\phi(x)}{dx} \Big|_{x_{0-}} = D(x_{0+}) \frac{d\phi(x)}{dx} \Big|_{x_{0+}}}$$

where x_{0-} & x_{0+} indicate evaluation immediately to left & right of x_0 .
For option ii if there is a localized source present. If an intensity s_{pi} source emits s_{pi}' neutrons/cm²/s along the interface, neutron balance at interface is

$$J(x_{0-}) + s_{pi}' = J(x_{0+}) \&$$

$$\boxed{-D(x_{0-}) \frac{d\phi(x)}{dx} \Big|_{x_{0-}} + s_{pi}' = -D(x_{0+}) \frac{d\phi(x)}{dx} \Big|_{x_{0+}}}$$

BOUNDARY CONDITIONS IN OTHER GEOMETRIES /

The boundary conditions are applicable in cylindrical and spherical as well as cartesian geometries: $\vec{x} \parallel$ simply replaced by the direction normal to surface.

In spherical or cylindrical geometries, boundary conditions at the origin or centre line must be treated differently.

For a point source emitting s^p neutrons/s at center of sphere, s^p
 $s^p = \lim_{r \rightarrow 0} (4\pi r^2 J_e(r))$ for a line source emitting s^l neutrons/cm/s
 along centreline of a cylinder. $s^l = \lim_{r \rightarrow 0} (2\pi r J_e(r))$

If there are no sources present, it is required that flux be finite at $r=0$.

NON MULTIPLYING SYSTEMS - SPHERICAL GEOMETRY

- Consider a spherical geometry problem with a source at center of sphere in infinite medium

Recall the diffusion eqn

$$\nabla^2 \phi(\vec{r}) + \frac{1}{D} \phi(\vec{r}) = \frac{1}{D} S''(r)$$

Now, replace ∇^2 by 1D spherical term,

$$\frac{-1}{r^2} \frac{d}{dr} r^2 \frac{d}{dr} \phi(r) + \frac{1}{D} \phi(r) = \frac{1}{D} S''(r)$$

POINT SOURCE EXAMPLE

Consider a point source of strength s^p concentrated at the origin of an infinite medium extending from $r=0$ to $r=\infty$.

For $r > 0$, $S''(r) = 0$.

Hence,

$$\frac{1}{r^2} \frac{d}{dr} r^2 \frac{d}{dr} \phi(r) - \frac{1}{D} \phi(r) = 0$$

Now, let $\phi(r) = \frac{1}{r} \Phi(r)$ a singular flux

$$\therefore \frac{1}{x^2} \frac{d}{dx} x^2 \frac{d}{dx} \phi(x) - \frac{1}{x^2} \phi(x) = 0 \text{ becomes}$$

$$\frac{1}{x^2} \frac{d}{dx} x^2 \frac{d}{dx} \frac{1}{x} \phi(x) - \frac{1}{x^2} \frac{\phi(x)}{x} = 0 \text{ which simplifies to}$$

$$\frac{d^2 \phi(x)}{dx^2} - \frac{1}{x^2} \phi(x) = 0.$$

Above is a 2nd order linear differential equation with a general soln that looks like $y = C_1 y_1 + C_2 y_2$ where $y_1 = e^{x/L}$ and $y_2 = e^{-x/L}$.

$$\text{The characteristic eqn is } x^2 - \frac{1}{L^2} = 0 \Rightarrow (x + \frac{1}{L})(x - \frac{1}{L}) = 0.$$

$$\Rightarrow R_{1/2} = \pm \frac{1}{L},$$

$$\Rightarrow y = C_1 e^{x/L} + C_2 e^{-x/L} = \phi(x)$$

$$\text{Now, } \phi(x) = \phi(r) r$$

$$\Rightarrow \phi(r) = C_1 e^{r/L} + C_2 e^{-r/L}$$

$$\Rightarrow \boxed{\phi(r) = C_1 e^{r/L} + C_2 e^{-r/L}}$$

Now, we shall employ boundary conditions to determine C_1, C_2 . At $r = 0$, $\phi(0) = \phi(\infty) = 0$. The second boundary condition is at the

origin. In the limit as $r \rightarrow 0$, the current

$I_e(r) = -D \frac{d\phi(r)}{dr}$ emerging from a small sphere with total area $= 4\pi r^2$ must be equal to source strength

$$S_p = \lim_{r \rightarrow 0} 4\pi r^2 I_e(r)$$

total
area

currents
from unit
area

Now from the 1st boundary condition,

$$\phi(\infty) = 0, \text{ we find that } C_2 e^{-r/L} = 0 \Rightarrow C_2 = 0 \text{ as } \phi(\infty) \neq 0 \text{ otherwise}$$

$$\phi(r) = \frac{C_1}{r} e^{r/L}$$

$\phi(r) = \frac{C_2}{r} e^{-\frac{r}{L}}$
 Now to find C_2 , apply boundary condition at origin
 $S_p = \lim_{r \rightarrow 0} 4\pi r^2 J_e(r) = \lim_{r \rightarrow 0} 4\pi r^2 \left(-D \frac{d}{dr} \phi(r) \right)$
 $= -D \lim_{r \rightarrow 0} 4\pi r^2 \frac{d}{dr} \phi(r)$
 Now $\phi(r) = \frac{C_2}{r} e^{-\frac{r}{L}}$ substitute
 $\Rightarrow S_p = -D \lim_{r \rightarrow 0} \frac{4\pi r^2}{r} \left(C_2 e^{-\frac{r}{L}} \right)$ substitute
 $\frac{d}{dr} \frac{C_2}{r} e^{-\frac{r}{L}} = C_2 \left[\frac{-1}{r^2} e^{-\frac{r}{L}} - \frac{1}{r} e^{-\frac{r}{L}} \right]$
 $\Rightarrow S_p = -D (4\pi) \lim_{r \rightarrow 0} r^2 \left[-C_2 \left(\frac{1}{r^2} e^{-\frac{r}{L}} - \frac{1}{r} e^{-\frac{r}{L}} \right) \right]$
 $\Rightarrow S_p = 4\pi C_2 D \lim_{r \rightarrow 0} \left(\frac{r}{L} e^{-\frac{r}{L}} + e^{-\frac{r}{L}} \right)$
 $\Rightarrow S_p = 4\pi C_2 D (0 + 1)$
 $\Rightarrow S_p = 4\pi C_2 D$
 $\Rightarrow C_2 = \frac{S_p}{4\pi D}$
 $\phi(r) = \frac{S_p}{4\pi D r} e^{-\frac{r}{L}}$

PH neutrons produced by point source must be absorbed in infinite medium.
 Taking an incremental volume as $dV = 4\pi r^2 dr$, we show that
 $\int_{\text{all space}} \phi(r) dV = S_p$.

TWO REGION EXAMPLE

In this problem, we shall consider 2 regions and a distributed source. It illustrates the treatment of boundary condition at origin as well as interface conditions.

① Consider a sphere of radius R with material properties $D \times \epsilon_a$ contains a uniform source S_0'' .

② The sphere is surrounded by a second source free medium with properties $D \times \epsilon_a$, it extends to $r = \infty$. Our objective is to determine $\phi(r)$.

For ① region, the diffusion eqn takes the form

$$-\frac{1}{r^2} \frac{d}{dr} r^2 \frac{d\phi(r)}{dr} + \frac{1}{L^2} \phi(r) = \frac{1}{D} S_0'' \quad 0 \leq r \leq R$$

$$\text{For ② region, diffusion eqn is of form} \\ -\frac{1}{r^2} \frac{d}{dr} r^2 \frac{d\phi(r)}{dr} + \frac{1}{L^2} \phi(r) = 0 \quad R < r \leq \infty$$

For region ①,

$$\phi(r) = \phi_p(r) + \phi_e(r)$$

$$\text{For a uniform source } \frac{d}{dr} \phi(r) = 0$$

$$\Rightarrow \frac{1}{L^2} \phi_p(r) = \frac{1}{D} S_0'' \Rightarrow \phi_p(r) = \frac{L^2}{D} S_0'' = \frac{S_0''}{\epsilon_a}$$

$\phi_e(r) = 10^{10}$ to corresponding homogeneous soln which was previously seen to be $\phi_e(r) = C_1 e^{2IL} + C_2 e^{-2IL}$

$$\Rightarrow \text{General soln. } \phi(r) = \phi_p(r) + \phi_e(r)$$

$$\phi(r) = \frac{S_0''}{\epsilon_a} + C_1 e^{2IL} + C_2 e^{-2IL} \quad (0 \leq r \leq R)$$

②

For the 2nd region, as solved previously, solution is at the form.

$$\boxed{\phi(r) = C_1 e^{r/L} + C_2 e^{-r/L}} \quad (R < r \leq \infty)$$

Now, to solve for the arbitrary constants, we apply boundary conditions

- 1) $0 \leq \phi(0) < \infty$ - which means we have a finite flux at origin (since no point source at origin)

This condition is applicable to eqn ①

Applying it to

$$\phi(r) = \frac{S_0''}{\epsilon a} + \frac{C_1}{r} e^{+r/L} + \frac{C_2}{r} e^{-r/L}$$

Now apply boundary condition

$$\phi(0) = \lim_{r \rightarrow 0} \left(\frac{S_0''}{\epsilon a} + \frac{(C_1) e^{+r/L}}{r} + \frac{(C_2) e^{-r/L}}{r} \right) = e^{+0/L} = e^{0/L}$$

Now we see the 2 terms have r in denominator that would make solⁱⁿ ∞ as $r \rightarrow 0$. So we need them to cancel each other out (ie C_1 should cancel C_2) for that $C_1 = -C_2$ or $C_2 = -C_1$.

$$\boxed{C_2 = -C_1} \Rightarrow \boxed{\phi(r) = \frac{2C_1}{r} \sinh(r/L) + \frac{S_0''}{\epsilon a} \quad (0 \leq r \leq R)} \quad -3$$

- 2) $\phi(\infty) = 0$. - which means, flux eventually goes to 0 at ∞ . This boundary condition must be applied to the ② eqn

$$\phi(0) = C_1 e^{+r/L} + C_2 e^{-r/L} = 0$$

$$\Rightarrow C_1 e^{+0/L} + C_2 e^{-0/L} = 0$$

$$\Rightarrow C_1 e^{+0/L} + 0 = 0$$

$\Rightarrow C_1$ must be 0 to balance $e^{+\infty/L}$ term

$$\Rightarrow \boxed{C_1 = 0} \quad \text{II}$$

$$\Rightarrow \boxed{\phi(r) = C_2 e^{-r/L} \quad (R < r \leq \infty)} \quad -4$$

3) $\Phi(R-) = \Phi(R_+)$ This is also called the interface condition which means flux to left at $R = \text{flux to right at } R$

$$\Rightarrow \textcircled{I} = \textcircled{II} \text{ at } R$$

$$\Rightarrow \frac{2C_1}{R} \sinh(Rl_C) + \frac{so''}{\epsilon a} = \frac{C_2'}{R} e^{(Rl_C)} \text{ at } R = \infty$$

$$\Rightarrow \boxed{\frac{2C_1}{R} \sinh(Rl_C) + \frac{so''}{\epsilon a} = \frac{C_2'}{R} e^{-Rl_C}} \quad \textcircled{III}$$

$$4) D \frac{d}{dr} \Phi(r) \Big|_{R-} = D \frac{d}{dr} \Phi(r) \Big|_{R+} \quad \text{as const} \quad \begin{aligned} & \text{Another interface} \\ & \text{condition employs} \\ & \text{equal partial currents} \\ & \text{at } R. \end{aligned}$$

$$\Rightarrow D \frac{d}{dr} \left(\frac{2C_1}{R} \sinh(Rl_C) + \frac{so''}{\epsilon a} \right)$$

$$= D \frac{d}{dr} \left(\frac{C_2'}{R} e^{-Rl_C} \right)$$

$$\Rightarrow 2D C_1 \left[\frac{d}{dr} \frac{1}{R} \sinh(Rl_C) \right] = DC_2' \left[\frac{d}{dr} \frac{1}{R} e^{-Rl_C} \right]$$

$$\Rightarrow \boxed{2DC_1 \left[\frac{1}{Rl_C} \cosh(Rl_C) - \frac{1}{R^2} \sin(Rl_C) \right] = -DC_2' \left(\frac{1}{R^2} + \frac{1}{R^2} \right) e^{-Rl_C}} \quad \textcircled{IV}$$

Solving \textcircled{III} & \textcircled{IV} for C_1 & C_2' and inserting these results

in $\textcircled{3,4,5}$ results in so''

$$\Phi(r) = \left[1 - \left(\frac{R \sinh(Rl_C)}{e \sinh(Rl_C)} \right) \frac{so''}{\epsilon a} \right]$$

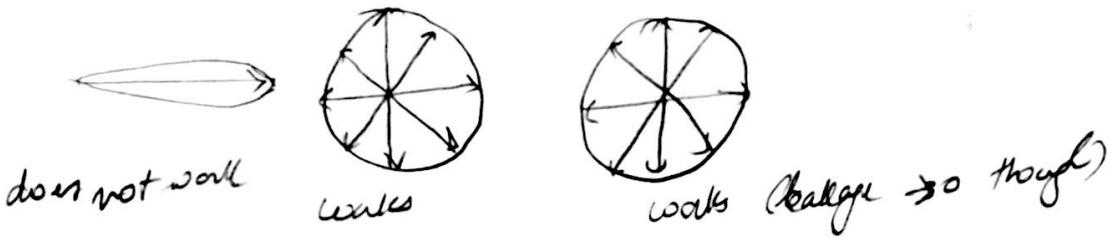
$$0 \leq r \leq R$$

$$-(r-R)/l_C \quad R < r \leq \infty$$

$$d\Phi = (1-C) \frac{so''}{\epsilon a} \frac{1}{r} e$$

$$C = \left[1 + \frac{D}{B} \frac{(Rl_C) \coth(Rl_C) - 1}{Rl_C} \right]^+$$

THE VALIDITY OF DIFFUSION APPROXIMATION



DIFFUSION LENGTH

The physical interpretation of diffusion can be gained by examining mean squared distance that neutron attains between birth and death to do this.

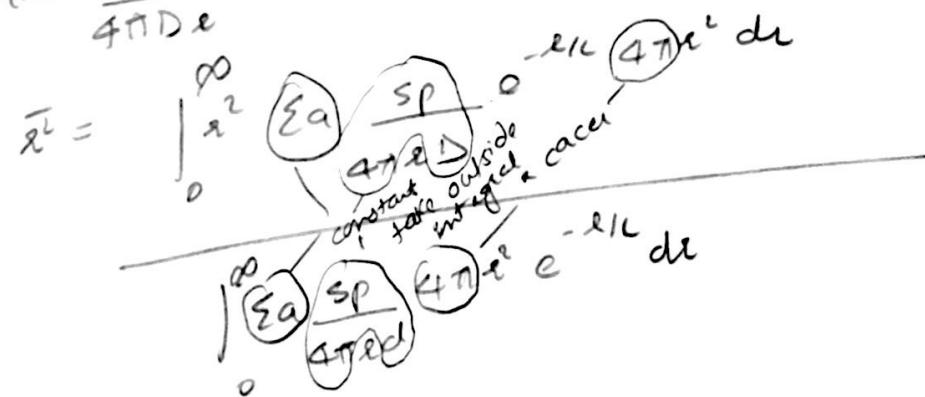
assume neutron was born at $r = 0$ & calculate the mean squared distance weighed by absorption rate.

$$\bar{r}^2 = \frac{\int r^2 \Sigma_a \phi(r) dr}{\int \Sigma_a \phi(r) dr}$$

Now, recall flux distribution of a point source S at the origin

$$r dr = 4\pi r^2 dr$$

$$\phi(r) = \frac{Sp}{4\pi D r} e^{-\frac{r}{L}}$$



$$\Rightarrow \bar{r}^2 = \frac{\int_0^\infty r^3 e^{-2r/L} dr}{\int_0^\infty r^2 e^{-2r/L} dr} = L^2$$

$$\Rightarrow L = \frac{1}{\sqrt{2}} \sqrt{\bar{r}^2} = 0.408 \sqrt{\bar{r}^2}$$

Thus diffusion length λ is proportional to rms distance diffused by neutron b/w birth & absorption

Now recall that $\lambda = \frac{1}{\Sigma}$ is the mean free path and average distance b/w scatter collisions.

$$\text{for isotropic scatter, } D = \frac{1}{3\Sigma_t} = \frac{1}{3\Sigma_f} = \frac{2}{3}$$

$$c = \frac{\Sigma_s}{\Sigma_t} = \frac{\Sigma_s}{\Sigma_s + \Sigma_a}$$

$$\Rightarrow c(\Sigma_s + \Sigma_a) = \Sigma_s$$

$$\Rightarrow \Sigma_a = \frac{(1-c)\Sigma_s}{c} = \frac{(1-c)\Sigma_s}{\frac{\Sigma_s}{\Sigma_t}} = (1-c)\Sigma_t$$

$$\Rightarrow \boxed{\Sigma_a = (1-c)\Sigma_t = \frac{(1-c)}{c}}$$

$$\text{we know that } L = \sqrt{\frac{D}{\Sigma_a}}$$

$$= \left[\frac{D}{(1-c)} \right]^{\frac{1}{2}} = \left[\frac{2/3}{(1-c)} \right]^{\frac{1}{2}} = \left[\frac{\lambda^2}{3(1-c)} \right]^{\frac{1}{2}}$$

$$\boxed{L = \frac{\lambda}{\sqrt{3(1-c)}}}$$

(valid if $c > 0.7$)

UNCOLLODED FLUX REVISITED

Further insights on validity of diffusion equation may be gained by comparing uncollided flux from point source to total (ie collided + uncollided) flux attributable to the source.

From Ch. 2, the uncollided flux at a pt source is

$$\Phi_{u0} = \frac{Sp}{4\pi c^2} e^{-\Sigma_L} = \frac{Sp}{4\pi c^2} e^{-2\lambda}, \text{ Now compare it with diffusion eqn at pt source}$$

$$\Phi(c) = \frac{Sp}{4\pi D_s} e^{-\Sigma_L c}$$

$c = \text{mtrs}$

Regardless of cross-section, the uncollided flux drops off as $\frac{1}{x^2}$, while total flux drops only at $\frac{1}{x}$.

While ntp appears in exponential of the uncollided flux, while diffusion length - which is larger - appears in diffusion length of total flux. Thus total flux decays more slowly with distance.

2nd point of comparison b/w uncollided and diffusing neutrons per cm² distance to first collision & absorption, respectively To obtain mean distance travelled by uncollided neutrons, we again consider pt. source at origin but employ first collision rate as weight instead of absorption rate.

$$\overline{x_u^2} = \frac{\int x^2 \epsilon_i \phi_u(x) dx}{\int \epsilon_i \phi_u(x) dx}$$

$$\text{sub. } \phi_u = \frac{sp}{4\pi x^2} e^{-\lambda x}$$

$$\begin{aligned} \overline{x_u^2} &= \frac{\int_0^\infty x^2 \epsilon_i \frac{sp}{4\pi x^2} e^{-\lambda x} 4\pi x^2 dx}{\int_0^\infty \epsilon_i \frac{sp}{4\pi x^2} e^{-\lambda x} 4\pi x^2 dx} \\ &= \frac{\int_0^\infty x^2 e^{-\lambda x} dx}{\int_0^\infty e^{-\lambda x} dx} \end{aligned}$$

$$\Rightarrow \overline{x_u^2} = \lambda^{-2} \Rightarrow \lambda = 0.107 \sqrt{\overline{x_u^2}}$$

\Rightarrow meaning collision. not ntp proportional to units before making 1st FRT
The ratio of 2 rms distances.

$$\frac{\overline{x^2}}{\overline{x_u^2}} = \frac{6L^2}{8\lambda^2} \cdot \frac{3L^2}{\lambda^2} = \frac{3\lambda^2}{3(1-c)\lambda^2} = \frac{1}{1-c}$$

$$\Rightarrow \boxed{\frac{\overline{x^2}}{\overline{x_u^2}} = \frac{1}{1-c}}$$

As the distance from source increases, importance of uncollided source rapidly diminishes provided that c , the ratio of scattering to total cross section, is sufficiently close to 1.

If not, then average the neutrals will not make enough scatter before absorption for the distortion app to be valid

Examining angular distributions of neutrinos further illuminates the distinction between uncollided and diffused neutrinos. The uncollided neutrinos at a pt. come from a point source and travel in straight lines, radially outward, while diffused neutrinos will be dispersed at an angle.

Hence for diffusion to give a reasonable accuracy, only a small fraction of neutrino population at a point can remain uncollided. This condition typically exists only in situations where $\Sigma \epsilon_f / \epsilon_t > 0.7$.

MULTIPLYING SYSTEMS

- fission term present

SUBCRITICAL ASSEMBLIES

spherical geometry
in a multiplying system, $\nabla \epsilon_f > 0$ because fissile material is present.

For a uniform system, with a uniform source S_0^{in} , ϵ_s is space independent

the macrodiffusion equation

$$-D \nabla^2 \phi(\vec{r}) + \epsilon_a(\vec{r}) \phi(\vec{r}) = S_0^{\text{in}}(\vec{r}) + \nabla \epsilon_f(\vec{r}) \phi(\vec{r})$$

$$\downarrow \\ -D \nabla^2 \phi(\vec{r}) + \frac{1}{D} \epsilon_a(\vec{r}) \phi(\vec{r}) = \frac{S_0^{\text{in}}(\vec{r})}{D} + \frac{1}{D} \nabla \epsilon_f(\vec{r}) \phi(\vec{r})$$

↓ 2D spherical geometry becomes

$$-\frac{1}{r^2} \frac{d}{dr} r^2 \frac{d}{dr} \phi(r) + \frac{1}{D} \epsilon_a \phi(r) = \frac{S_0^{\text{in}}}{D} + \frac{1}{D} \nabla \epsilon_f \phi(r)$$

$$\frac{\nabla \epsilon_f}{\epsilon_a} = K_{\infty} \quad \text{as } D = L^2 \epsilon_a \Rightarrow \frac{\nabla \epsilon_f}{D} = \frac{\nabla \epsilon_f}{L^2 \epsilon_a} = \frac{K_{\infty}}{L^2}$$

↓

$$-\frac{1}{r^2} \frac{d}{dr} r^2 \frac{d}{dr} \phi(r) + \frac{1}{L^2} \epsilon_a \phi(r) = \frac{S_0^{\text{in}}}{D} + \frac{1}{L^2} K_{\infty} \phi(r)$$

$$\left[\frac{-1}{x^2} \frac{d}{dx} \frac{d^2 \phi(x)}{dx^2} + \frac{1}{L^2} (1 - k_{\infty}) \phi(x) = \frac{g_0}{D} \right] \quad (2)$$

The above is a 2nd order, linear differential ODE of degree 2.

Its soln is of the form

$$y = y_p + y_c \quad \text{Hence } \phi(x) = \phi_p(x) + \phi_c(x)$$

y_c = soln to corresponding homogeneous eqn i.e.

$$\left[\frac{-1}{x^2} \frac{d}{dx} \frac{d^2 \phi(x)}{dx^2} + \frac{1}{L^2} (1 - k_{\infty}) \phi(x) = 0 \right] \quad (1)$$

As before,

$$\text{let } \phi_c(x) = \frac{1}{x} \psi(x)$$

∴ eqn 1 becomes

$$\frac{d^2 \psi(x)}{dx^2} - \frac{1}{L^2} (1 - k_{\infty}) \psi(x) = 0.$$

The above eqn has a characteristic eqn.

$$s^2 - \frac{1}{L^2} (1 - k_{\infty}) = 0$$

$$\Rightarrow \left(s + \frac{\sqrt{1 - k_{\infty}}}{L} \right) \left(s - \frac{\sqrt{1 - k_{\infty}}}{L} \right) = 0$$

$$\Rightarrow s_{1,2} = \pm \frac{1}{L} \sqrt{1 - k_{\infty}}$$

→ The soln of homogeneous eqn looks like

$$\psi_c(x) = C_1 e^{\frac{1}{L} \sqrt{1 - k_{\infty}} x} + C_2 e^{-\frac{1}{L} \sqrt{1 - k_{\infty}} x} \quad \therefore \phi_c(x) = \frac{\psi_c(x)}{x}$$

$$\Rightarrow \phi_c(x) = \frac{C_1 e^{\frac{1}{L} \sqrt{1 - k_{\infty}} x}}{x} + \frac{C_2 e^{-\frac{1}{L} \sqrt{1 - k_{\infty}} x}}{x} \quad (2)$$

Solve for particular solⁿ.

For a uniform source, particular solⁿ is a constant. Hence derivative term in eqn ① vanishes

$$\text{R so } \frac{1}{L^2} (1 - k_{\infty}) \Phi_p(x) = \frac{S_0'''}{D}$$

$$\Rightarrow \boxed{\Phi_p(x) = \frac{S_0''' L^2}{D(1 - k_{\infty})} = \frac{S_0''' D / \epsilon_a}{D(1 - k_{\infty})} = \frac{S_0'''}{\epsilon_a(1 - k_{\infty})}}$$

Now

$$\Phi(x) = \Phi_c(x) + \Phi_p(x)$$

$$\rightarrow \boxed{\Phi(x) = \frac{C_1}{x} e^{+2/L \sqrt{1-k_{\infty}}} + \frac{C_2}{x} e^{-2/L \sqrt{1-k_{\infty}}} + \frac{S_0'''}{\epsilon_a(1 - k_{\infty})}}$$

We must apply boundary conditions to solve for C₁ & C₂

Now since we have a uniform source & no point source, we have
finite flux at the origin.

i.e. $\Phi(0) \rightarrow \text{finite}$
This is possible only if $C_2 = -C_1$

(exponential terms go to 1
& for Φ to be finite $1/x$
terms must cancel out)

$$\begin{aligned} \Rightarrow \Phi(x) &= \frac{C_1}{x} e^{+2/L \sqrt{1-k_{\infty}}} - \frac{C_1}{x} e^{-2/L \sqrt{1-k_{\infty}}} + \frac{S_0'''}{\epsilon_a(1 - k_{\infty})} \\ &= \frac{C_1}{x} \left[\left(e^{+2/L \sqrt{1-k_{\infty}}} - e^{-2/L \sqrt{1-k_{\infty}}} \right) \right] + \frac{S_0'''}{\epsilon_a(1 - k_{\infty})} \\ &\quad - \frac{2C_1}{x} \sinh\left(\frac{2\sqrt{1-k_{\infty}}}{L}\right) + \frac{S_0'''}{\epsilon_a(1 - k_{\infty})} \end{aligned}$$

①

Take R as extrapolated radius of sphere when $b \rightarrow 0$

$$\Rightarrow \Phi(R) = 0$$

Hence from eqn ①

$$\phi(R) = 0 = \frac{2C_1}{R} \sinh\left(\frac{\tilde{R}\sqrt{1-K_{\infty}}}{L}\right) + \frac{S_0''}{\sinh(1-K_{\infty})}$$

Now solving for C_1 ,

$$C_1 = -\frac{\tilde{R} S_0''}{L \sinh(1-K_{\infty})}$$

$$\downarrow \text{Substitute in eqn ② general soln}$$

$$\boxed{\phi(x) = \frac{S_0''}{\sinh(1-K_{\infty})} \left[1 - \frac{\tilde{R} \sinh(x \sqrt{1-K_{\infty}} / L)}{\sinh(\tilde{R} \sqrt{1-K_{\infty}} / L)} \right]}$$

For $K_{\infty} \leq 1$ system must be subcritical even if there were no mass leaving out of sphere. (particular & general soln cgs remain the same)

Now for $\boxed{K_{\infty} > 1}$ corresponding homogeneous eqn ②

$$\frac{d^2}{dx^2} \phi(x) - \frac{1}{L^2} (1-K_{\infty}) \phi(x) = 0$$

$$\text{Now } K_{\infty} > 1$$

$$\Rightarrow \frac{d^2}{dx^2} \phi(x) + \frac{1}{L^2} (K_{\infty} - 1) \phi(x) = 0$$

Hence characteristic eqn takes form

$$r^2 + \frac{K_{\infty} - 1}{L^2} = 0$$

$$\Rightarrow r_{1,2} = \pm \sqrt{\frac{K_{\infty} - 1}{L^2}}$$

$$\text{Let } \frac{K_{\infty} - 1}{L^2} = B$$

$$\Rightarrow r_{1,2} = B^{1/2}$$

We know that for complex roots of characteristic eqn $a \pm bi$, solⁿ of the form $e^{at} (C_1 \sin bt + C_2 \cos bt)$

$$\text{Hence } \lambda_{12} = 0 \pm Bi$$

\Rightarrow solⁿ is of the form $e^{0t} (C_1 \sin Bx + C_2 \cos Bx)$

$$\Rightarrow \boxed{\psi(x) = C_1 \sin Bx + C_2 \cos Bx} \quad (B = \frac{\sqrt{K\alpha^2 - 1}}{L})$$

$$\text{Now, } \frac{\psi(x)}{e} = \phi(x)$$

$$\Rightarrow \phi_c(x) = \frac{C_1 \sin Bx}{e} + \frac{C_2 \cos Bx}{e}$$

$$= \frac{C_1}{e} \sin \left(\frac{\sqrt{K\alpha^2 - 1}}{L} x \right) + \frac{C_2}{e} \cos \left(\frac{\sqrt{K\alpha^2 - 1}}{L} x \right)$$

Solving for particular solⁿ,

For uniform source particular solⁿ is a constant

\Rightarrow derivative term goes to 0.

$$\Rightarrow 0 + \frac{1}{L} (K\alpha^2 - 1) \phi_p(x) = - \frac{S_0''}{D}$$

$$\Rightarrow \phi_p(x) = - \frac{S_0''}{K\alpha^2 - 1} \frac{x^2}{D} = - \frac{S_0''}{\epsilon_a (K\alpha^2 - 1)}$$

Hence $\phi(x)$'s general solⁿ is

$$\phi(x) = \phi_p(x) + \phi_c(x)$$

$$\phi(x) = - \frac{S_0''}{\epsilon_a (K\alpha^2 - 1)} + \frac{C_1}{e} \sin \left(\frac{\sqrt{K\alpha^2 - 1}}{L} x \right) + \frac{C_2}{e} \cos \left(\frac{\sqrt{K\alpha^2 - 1}}{L} x \right)$$

To solve for C_1 & C_2 , apply boundary conditions.

D $\phi(r)$ must be finite.

$$\Rightarrow \lim_{r \rightarrow 0} \phi(r) = \lim_{r \rightarrow 0} \left[\frac{S_0'''}{\epsilon_a(K\omega^{-1})} r + \frac{C_1 \sin(Br)}{r} + \frac{C_2 \cos(Br)}{r} \right] \text{ is finite}$$
$$= -\frac{S_0'''}{\epsilon_a(K\omega^{-1})} + \lim_{r \rightarrow 0} \frac{C_1}{r} \sin(Br) + \lim_{r \rightarrow 0} \frac{C_2}{r} \cos(Br)$$

$$\lim_{r \rightarrow 0} \frac{\sin Br}{r} = B, \quad \lim_{r \rightarrow 0} \frac{C_2}{r} \cos Br = \infty \quad \text{as } \cos Br \rightarrow 1 \text{ at } r \rightarrow 0$$

\Rightarrow for sum to be finite, $C_2 = 0$.

$$\Rightarrow C_2 = 0$$

$$\boxed{\phi(r) = -\frac{S_0'''}{\epsilon_a(K\omega^{-1})} + \frac{C_1}{r} \sin(Br)}$$

We determine C_1 by requiring the above eqn to meet $\phi(\tilde{R}) = 0$

$$\therefore \phi(\tilde{R}) = -\frac{S_0'''}{\epsilon_a(K\omega^{-1})} + \frac{C_1}{\tilde{R}} \sin(B\tilde{R}) = 0$$

Substitute.

$$\Rightarrow \frac{C_1}{\tilde{R}} \sin(B\tilde{R}) = \frac{S_0'''}{\epsilon_a(K\omega^{-1})}$$

$$\Rightarrow C_1 = \frac{S_0''' \tilde{R}}{\sin(B\tilde{R}) \epsilon_a(K\omega^{-1})}$$

$$\phi(r) = \frac{\frac{S_0''' \tilde{R}}{\epsilon_a(K\omega^{-1})} \sin Br}{\sin(B\tilde{R}) \epsilon_a(K\omega^{-1})} - \frac{S_0'''}{\epsilon_a(K\omega^{-1})}$$

$$\boxed{\phi(r) = \frac{S_0'''}{\epsilon_a(K\omega^{-1})} \left[\frac{\frac{\tilde{R}}{\epsilon_a(K\omega^{-1})} \sin(Br)}{\sin(B\tilde{R})} - 1 \right]}$$

$$\left(B = \sqrt{\frac{K\omega^{-1}}{\epsilon_a}} \right)$$

Similar analysis can be done for different geometries where.

Geometry	Dim.	Bg^e	<u>Area</u>
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Infinite slab	thickness α	$(\frac{\pi}{\alpha})^2$	Area $(\frac{\pi}{\alpha})$
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2D Rectangle	$a \times b \times c$	$(\frac{\pi}{a})^2 + (\frac{\pi}{b})^2 + (\frac{\pi}{c})^2$
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3D Cylinder	radius R	$(\frac{2 \cdot 405}{R})^2$
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Finite cylinder	radius R height H	$(\frac{2 \cdot 405}{R})^2 + (\frac{\pi}{H})^2$
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Sphere	radius R	$(\frac{\pi}{R})^2$
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Reactor is critical when $\beta_m = \underline{\beta_g}$.

If reactor is smaller than critical size for a given material

$\beta_g > \beta_m \rightarrow$ reactor is subcritical.

If $\beta_g < \beta_m \rightarrow$ reactor is critical.

Numerical criticality search.

$$-\frac{\partial}{\partial x} D \frac{\partial \phi}{\partial x} + \epsilon_a \phi = \frac{\nu \epsilon_f}{K} \phi.$$

6) $M\phi = \frac{1}{K} F\phi$

If ϕ is assumed to be known, & if we let
 $S = F\phi$,
↓
power iteration

$$M\phi = \frac{S}{K} \Rightarrow \boxed{M\phi^{(n)} = \frac{S^{(n)}}{K^n}}$$

looks just like our steady state eqn
which we can solve by discrete numerically -
FD / FEM etc.

- sum
- ① Discretize domain
 - ② find matrix M , F & vector ϕ .
 - ③ Start iteration Assume $\phi^{(0)}$,
 $K^{(0)} \rightarrow$ get $S^{(0)}$
(generating t , $\phi^{(n)}$, $K^{(n)}$, $S^{(n)}$)

5

$$M\phi^{(1)} = S^{(0)} \xrightarrow{\text{iterative}} M\phi^{(n+1)}$$

(4) Solve for $\phi^{(1)}$: $\phi^{(1)} = M^{-1} \frac{S^{(0)}}{k^{(0)}}$

(5) \Rightarrow generalize to $\boxed{\phi^{(n+1)} = M^{-1} \frac{S^{(n)}}{k^{(n)}}}$

(5) Calculate $k^{(n)}$ \rightarrow generalize to b^n .

Eqn: $M\phi = \frac{1}{k} S$.

M is a matrix, ϕ is a vector, S is a vector.
 s is a scalar.

To find k , we integrate eqn over space

$$\int dx M\phi = \frac{1}{k} \int dx S$$

$$\therefore k \approx \frac{\int dx S}{\int dx M\phi} \Rightarrow k^{n+1} = \frac{\int dx S^{n+1}}{\int dx M\phi^{n+1}}$$

Moreover, by iteration eqn.

$$M\phi^{n+1} = \frac{1}{k} S^{(n)}$$

$$\therefore k^{(n+1)} = \frac{\int dx S^{(n+1)}}{\int dx M\phi^{(n+1)}}$$

Now that we know k^{n+1} ,

(3) Update $\frac{s^{n+1}}{k^{n+1}}$ & find ϕ^{n+1} ... go back
to (4).

check for convergence in $\| \cdot \|_2$ ϕ .

If not converged, go back to (4).

Final

Show Code.