

# **ANTENNA WAVE PROPAGATION**

## **ELECTRONICS & COMMUNICATION ENGINEERING**

### **HAND NOTES**

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**ANANTAPURAMU**

# Antenna Wave Propagation:

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## Unit - I

### Antenna Basics:

#### \* Introduction:-

▷ Communication:- The process of conveying information (or) intelligence (or) message from one place to another is known as communication.

↳ Radio Communication:- When electromagnetic waves (or) Radio waves used for the communication purpose is so called Radio Comm.

History:- \* → Meaning for "Antenna" in Zoology is "feeler" ie a part of some insects which feel (or) organ of touch.

\* → Plural of "Antenna" is "Antennae"

\* → Where as Antenna (or) Aerial (or) Radiator in radio sense is a device for receiving (or) sending radio waves and plural of Radio Antenna is "Antennas".

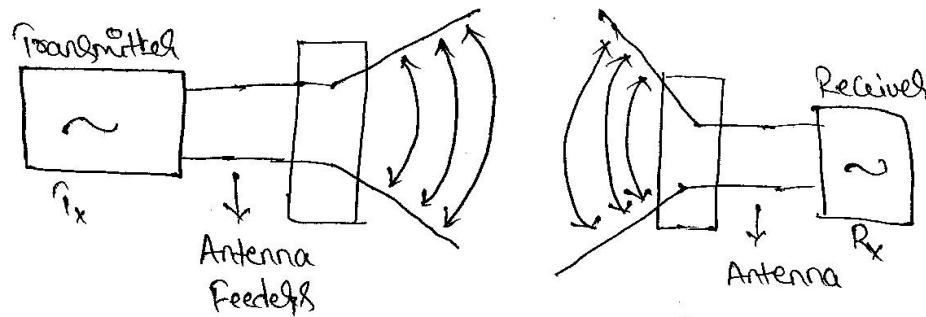
#### Definition of Antenna:-

An antenna is defined as a "metallic device (or) rod (or) wire"

for radiating (or) receiving radio waves (electromagnetic waves).

An Antenna (or) Aerial is a system of evaluated conductors which couples (or) matches the transmitted (or) received to free space.

A transmitting antenna connected to a transmitted by a transmission line (or) cable electromagnetic (radio) waves into free space which travel in space with velocity of light.



(i) Transmission Line :- It is used to carry the Electromagnetic waves

(ii) Antenna Feedbf :- They are used to connect transmitter (or) receiver with the antenna.

Note:- \*) → The source of Electromagnetic fields is the charged particles depends on the availability of charged particles we get the strength of electric and magnetic fields.

\* Maxwell's Equations :-  
which give existence of electric & magnetic field.

Two types of them are :-

(i) Point form (or) Differential form

(ii) Integral form.

These maxwell eqs are based on basic laws Gauss law,  
Faraday's law, Ampere's Circuits law.

(i) Point form (or) Differential form :-

a) Gauss law :- It is defined as the net flux density coming out of closed surface is equal to charge enclosed by that surface.

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from Gauss law:-  $\nabla \cdot D = \rho V$   
 $\nabla \cdot B = 0$

where  $D$  = electric flux density  $C/m^2$

$$E = \frac{F}{Q}$$

$$F = \frac{Q_1 Q_2}{4\pi \epsilon_0 r^2} ; Q_1 = Q_2$$

$$F = \frac{Q^2}{4\pi \epsilon_0 r^2}$$

$$\Rightarrow E = \frac{Q^2}{4\pi \epsilon_0 r^2 Q} = \frac{Q}{4\pi \epsilon_0 r^2}$$

$$\therefore D = \epsilon E$$

$$D = \frac{Q}{4\pi \epsilon_0 r^2} C/m^2$$

$\rho V$  - charge density

$B$  - magnetic flux density  $N/m^2$

$$B = \mu H$$

$\mu$  = permeability of medium

$$\mu_r = \mu_0 \mu_s$$

$$\mu_0 = 4\pi \times 10^{-7} N/A^2$$

$$\mu_s = 1 (\text{air})$$

$$\epsilon_0 = 8.85 \times 10^{-12} F/m^2$$

electric field intensity

b) Faraday's law:- It gives relation between

and magnetic field intensity.

$$\nabla \times E = -\frac{\partial B}{\partial t}$$

$$\nabla \times E = -\mu \cdot \frac{\partial H}{\partial t}$$

blo the current density ( $I$ )

c) Ampere's law:- It gives relation between the electric field intensity

electric to the current density

$$\nabla \times H = J + \frac{\partial D}{\partial t}$$

$$= J + \epsilon \frac{\partial E}{\partial t}$$

$\frac{\partial D}{\partial t}$  = displacement current.

$I_c$  = conduction current density

$$I_c = I/A \text{ A/m}^2$$

(ii) Integral form of Maxwell Eq's:-

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Divergence theorem gives the relation b/w surface integral & volume integral from this theorem.

$$\iint_S D \cdot dS = \iiint_V \epsilon_r \cdot dV \quad \begin{matrix} \text{Stokes law gives relation} \\ \text{b/w L & S} \end{matrix}$$

$$\iint_S B \cdot dS = 0$$

Faraday's law :-

$$\oint_C E \cdot dL = \iint_S -\frac{\partial B}{\partial t} \cdot dS$$

$$\oint_C E \cdot dL = -N \iint_S \frac{\partial H}{\partial t} \cdot dS$$

Ampere's law :-

$$\oint C H \cdot dL = I_{enc}$$

$$\oint C H \cdot dL = \iint_S J + \frac{\partial D}{\partial t}$$

These Maxwell eq are used to find the electric field & magnetic fields from different co-ordinate systems.

\*> Types of Antenna's :-

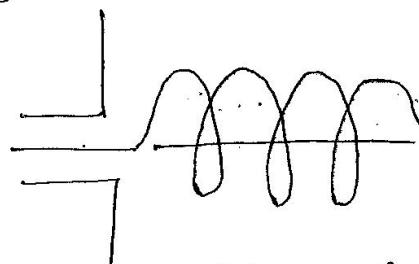
- 1) Isotropic Antenna
- 2) Helical Antenna
- 3) Dipole Antenna
- 4) Dish Antenna
- 5) Loop Antenna
- 6) Two wire Antenna
- 7) Rhombic Antenna

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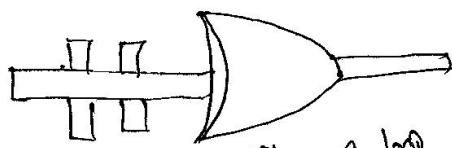
1) Isotropic Antenna :- means it radiates energy to all the directions with equal strength.

→ It is impractical antenna

2) Helical Antenna :- The structure of antenna is like a helix & couples energy from transmitted to free space & free space to received



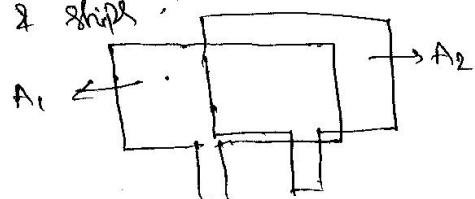
3) Dipole Antenna :- These Antenna are like a bow structure and is used in communication system i.e. to transmission & reception of TV signals



These Antenna are used in

4) Loop Antenna :- Structure is like a loop

aerospace & ships



5) Two Wire Antenna :-

When external voltage  $V_s$  is applied to two wire transmission line as a result electric field is developed b/w the conductors and the charge carriers move towards opposite charges these electric field

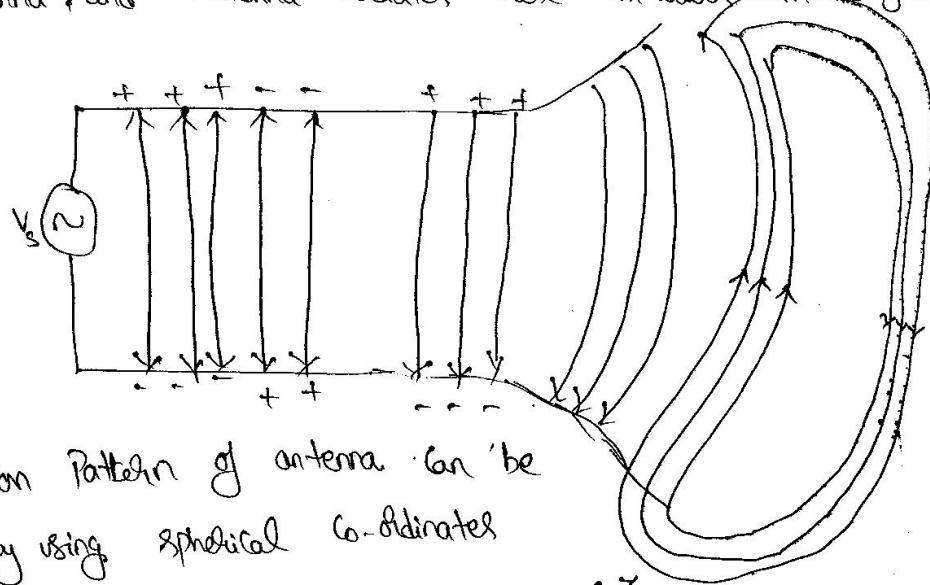
ions are tangent to the applied field.

\* Since the charge carriers are moving as a result magnetic field is developed and which is tangent to generated magnetic field.

these electric and magnetic fields are perpendicular to each other and if the line is terminated with some impedance, the electromagnetic

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Waves are Standing waves will be generated and these are fed to an Antenna, and Antenna radiates these fm wave in to free space

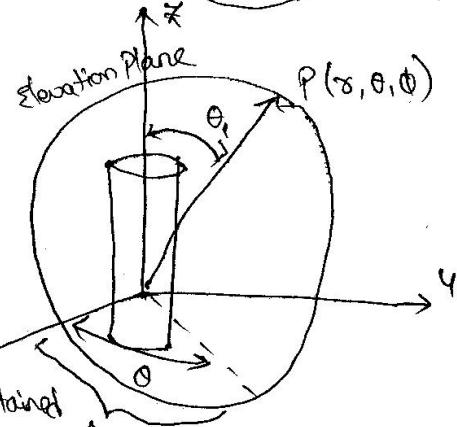


The radiation pattern of antenna can be measured by using spherical co-ordinates

$x, y, z$  are perpendicular to each other  
 $'r'$  is the radial displacement and  
 $\theta, \phi$  are angular displacement

\* where  $\theta_1$  is called elevation angle  
 $\phi$  is the angle b/w radius vector and  $Z$ -axis

\*  $\phi$  is called as azimuthal angle, it is obtained in  $Z=0$  plane by extending radius vector from origin. Then the plane is called azimuthal plane.



Q.

## 2) Isotropic radiation:-

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Isotropic radiator is an ideal antenna radiates energy with equal strength uniformly to all the directions.

\* → In practical no antenna can radiate energy in all direction.

\* → So it is an impractical antenna.

The radiation pattern of isotropic radiator is find by spherical

C-ordinate system.

Let us consider an isotropic radiator which is placed in a spherical C-ordinate system with sphere of radius 'r'.

C-ordinate system with sphere of radius 'r'. By Pointing theorem we can find the amount of energy delivered by isotropic radiator.

Pointing theorem defined as the amount of energy delivered by isotropic radiator.

unit area.

$$\overline{P} = E \times H \text{ W/m}^2$$

$$P = P_s$$

The total Power is given by

$$P_t = \iint_S P \cdot d\mathbf{s}$$

$$= \iint_S P_s \cdot d\mathbf{s}$$

$$P_t = P_s \iint_S d\mathbf{s}$$

$$d\mathbf{s} = A = 4\pi r^2$$

$$\therefore P_t = P_s 4\pi r^2$$

$$P_s = \frac{P_t}{4\pi r^2} \text{ W/m}^2$$

## 3) Dipole Antenna (a) Short electric dipoles:-

It is a short length antenna & takes less time to travel one pole to another pole by charge carriers.

Physical length of dipole antenna is 'x' and is divided

in to 2-halves (or) poles of each length ' $\frac{x}{2}$ '.

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## ~~Electric Potential~~

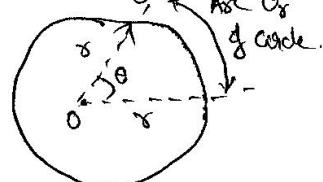
The electric potential at two ends of antenna equals to midpoint potential. The radiation resistance of dipole antenna is given by

$$R_r = 80\pi^2 \left(\frac{dl}{\lambda}\right)^2$$

where  $dl$  is differential length radiation resistance of half wave dipole is

$$R_r = 73\Omega$$

4) Radian :- Radian is used to measure the plane angle and it is nothing but the total angle subtended at the centre of the circle with its vertex.



$$1 \text{ radian} = 57.3 \text{ degrees.}$$

$$\text{The total circumference 'C' of circle with radius 'r' is } C = 2\pi r$$

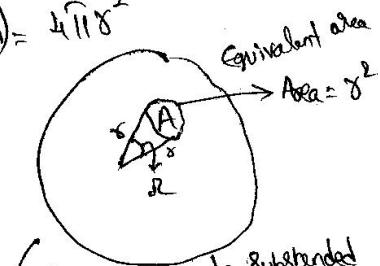
5) Steradian :- It is used to measure the solid angle  $\Omega$  is the total angle subtended at the centre of the sphere. The solid angle is represented by

$$d\Omega = 4\pi \text{ with surface area } A = 4\pi r^2$$

$$1 sr = 1 \text{ rad}^2 = \left(\frac{180}{\pi}\right)^2 \cdot (\text{degree})^2$$

$$= 3282.3 \text{ sq.deg}$$

$$1 sr = \frac{\text{Solid angle}}{4\pi}$$



$$(\Omega = \text{Solid angle subtended by area } A)$$

The infinitesimal area 'ds' on the surface of sphere with radius 'r' is given by

$$ds = r^2 \sin\theta \cdot d\phi \cdot d\theta \text{ m}^2$$

Hence the element of solid angle  $d\Omega$  of a sphere is

$$d\Omega = \frac{ds}{r^2} = \sin\theta \cdot d\phi \cdot d\theta \text{ steradian}$$

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## 6) Antenna Parameters & Antenna Properties :-

- (i) Radiation Pattern
- (ii) Radiation Intensity & Power radiation pattern.
- (iii) Directive gain & Directivity
- (iv) Power gain
- (v) Beam width, beam area & beam efficiency
- (vi) Antenna Apertures
- (vii) Effective height
- (viii) Front to back ratio
- (ix) Antenna Efficiency.

### (i) Radiation Pattern :-

" " (or) Antenna Pattern is defined as a "mathematical function & a graphical representation of the radiation properties of the antenna as a function of space co-ordinates."

\* ) → Radiation Properties includes Power flux density, radiation intensity, field strength, directivity phase (or) polarization.

\* ) → The Radiation Property of most concern in 2-dimensional & 3-dimensional spatial distribution of radiated energy.

\* ) → A trace of received power at a constant radius is called the Power Pattern. (x)

\* ) → A graph of spatial variation of the electric field along a constant radius is called an amplitude field Pattern ( $E$  volt/meter).

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In practice, the 3-dimensional is measured and recorded in a series of 2-dimensional pattern. where the Co-ordinates system usually used for the same is spherical co-ordinates  $(r, \theta, \phi)$ .

The antenna is assumed to be located at origin of spherical Co-ordinate system and field strength is specified at points on the spherical surface of radius ( $r$ ).

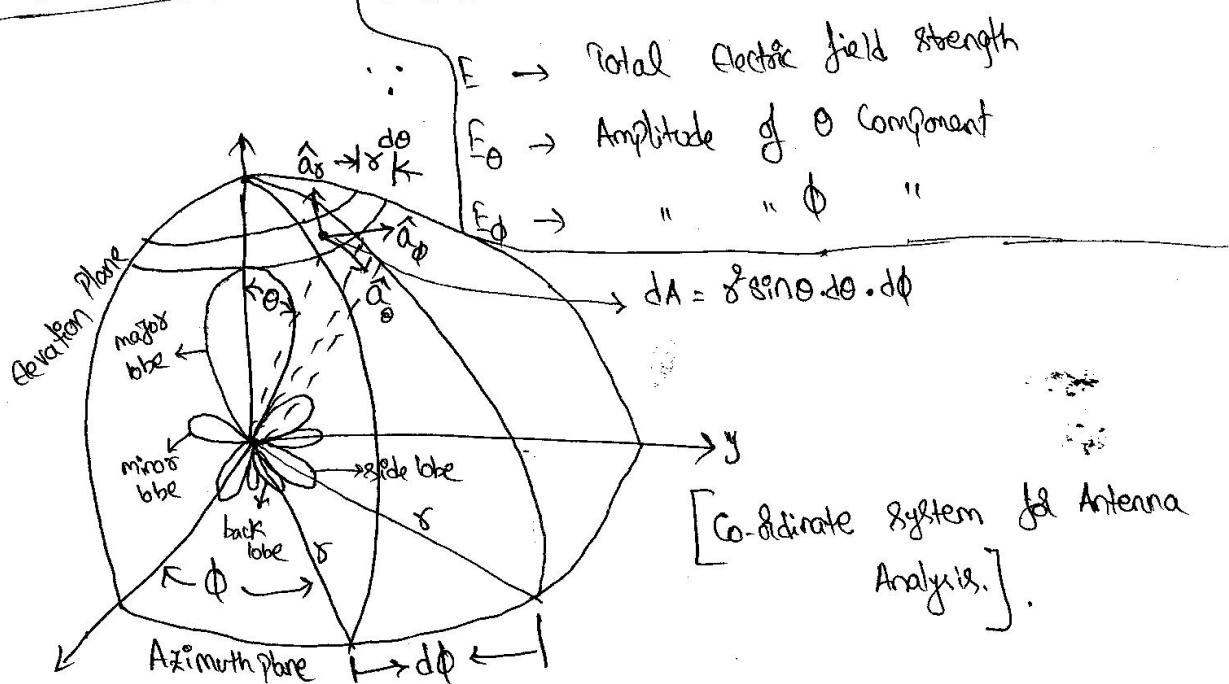
The shape of radiation pattern does not depend on radius ' $r$ '.

$$\text{where } r \gg \lambda \quad \text{The distribution of far field energy } E = \frac{V}{d} \text{ (V/m)}$$

The direction of field strength ( $E$ ) for radiation field is always tangential to spherical surface of imaginary sphere of radius ( $r$ ). For vertical dipole electric field strength  $E$  is in direction ' $\theta$ ' for the horizontal loop in direction of ' $\phi$ '.

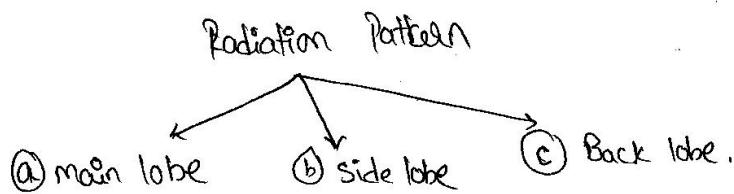
Where the radiation of field strength may have components

$$E_\theta \text{ and } E_\phi \quad \text{where } E = \sqrt{E_\theta^2 + E_\phi^2}$$



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The entire radiation is divided into 3-regions



- (a) Main lobe :- The region where we get maximum energy for an antenna there may be one (or) more main lobes
- (b) Side lobe :- The region where we get minimum & less energy and are adjusted to the main lobes.
- (c) Back lobe :- These are same as side lobes but these regions are adjusted to main lobes.

ii) Radiation intensity (iii) Power Radiation Pattern :-  
 → Radiation intensity is defined as the ratio of differential Power to unit solid angle.

It is represented by 'U'

$$U = \frac{\text{diff Power}}{\text{unit solid angle}}$$

The radiation intensity of an antenna is defined as

$$U(\theta, \phi) = \delta^2 P_d(\theta, \phi)$$

Then the total Power radiated can be expressed in terms of the radiation intensity as

$$P_{\text{rad}} = \int \int P_d(\theta, \phi) d\theta d\phi$$

$$= \int \int P_d(\theta, \phi) [\delta^2 \sin\theta \cdot d\theta \cdot d\phi]$$

$$= \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} [P_d(\theta, \phi) \delta^2] \sin\theta \cdot d\theta \cdot d\phi$$

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Let  $d\Omega = \sin\theta \cdot d\theta \cdot d\phi$  be the differential solid angle in steradian

$$P_{\text{rad}} = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} V(\theta, \phi) \cdot d\Omega$$

Thus the radiation intensity  $V(\theta, \phi)$  is expressed in watt/ $\text{sr}$  (watt/steradian)

It is defined as avg Power per unit solid angle.

The avg of value of radiation intensity is

$$V_{\text{avg}} = \frac{P_{\text{rad}}}{4\pi}$$

Using radiation intensity  $V(\theta, \phi)$  we can also calculate normalized Power Pattern as ratio of radiation intensity  $V(\theta, \phi)$  & its maximum value  $V(\theta, \phi)_{\text{max}}$

$$P_{\text{dn}}(\theta, \phi) = \frac{V(\theta, \phi)}{V(\theta, \phi)_{\text{max}}} \quad 1.$$

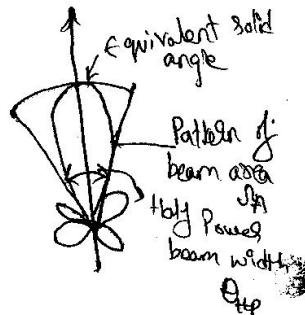
### \* Beam Solid Angle ( $\Omega$ ) Beam Area ( $\Omega_A$ )

Generally Antenna Pattern of Beam Area ( $\Omega$ ) solid angle expressed in steradian. It is defined as integral of normalized Power over a sphere.

$$\Omega_A = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} P_{\text{dn}}(\theta, \phi) \sin\theta \, d\theta \, d\phi$$

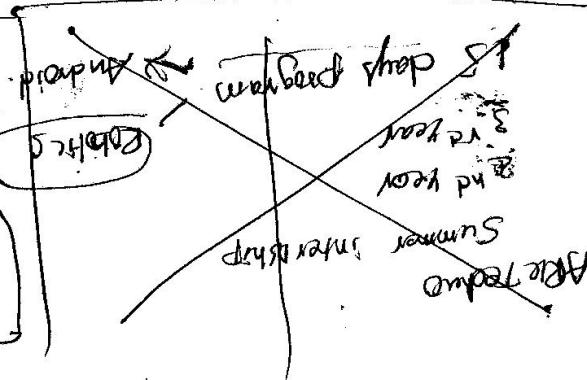
$$\text{but } d\Omega = \sin\theta \cdot d\theta \cdot d\phi$$

$$\therefore \Omega_A = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} P_{\text{dn}}(\theta, \phi) \cdot d\Omega \text{ steradian}$$



many times Beam area is denoted as angle subtended by half Power Points of main lobe.

$$\text{Beam area} = \Omega_A = \Theta_{\text{HP}} \cdot \Phi_{\text{HP}} \text{ steradian}$$



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iii) Gain :- It is defined as the ratio of maximum Radiation intensity from subject & test antenna. to the average radiation intensity of reference antenna.

$$\text{Gain (G)} = \frac{\text{Max R.I. of test antenna}}{\text{Avg R.I. of reference Antenna}}$$

$$G = \frac{U_t}{U_r}$$

iv) Directive Gain ( $G_d$ ) :-

It is defined as a ratio of radiation intensity of an antenna in a direction to the avg radiation intensity of standard Antenna in that direction.

$$G_d = \frac{\text{R.I. of an Antenna in a direction}}{\text{Avg R.I. of standard antenna in that direction}}$$

$$G_d = \frac{V(\theta, \phi)}{V_{\text{avg}}(\theta, \phi)} = \frac{V(\theta, \phi)}{\omega_s / 4\pi}$$

$$G_d = \frac{4\pi V(\theta, \phi)}{\omega_s}$$

$$G_d (\text{db}) = 10 \log G_d$$

$$G_d (\text{db}) = 10 \log G_d$$

It depends on radiation intensity ( $R$ ) radiated Power but does not depend on S.P. Power.

### v) Power gain:- ( $G_p$ )

Is a ratio of two Power densities of an antenna in a direction to avg power density of standard antenna in that direction

$$G_p = \frac{\text{Power density of an Antenna in direction}}{\text{Avg Power density of Standard Antenna}}$$

$$G_p = \eta_r G_d \quad (\because \eta_r = \text{Efficiency of Antenna})$$

$$G_p = G_d \quad G_p = \frac{\phi(\theta, \phi)}{W_r} \quad (\because W_r = W_{tr} + W_e = \text{Total Power})$$

$$G_p = \boxed{\frac{\phi(\theta, \phi)}{W_r}}$$

In terms of Power  $\phi_p$  & Power gain. in 'dB'

$$\boxed{G_p = 10 \log_{10}(\phi_p)}$$

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### vi) Directivity (D) :-

The maximum directive gain is called Directivity (D) of an antenna.

Defined as ratio of Maximum radiation intensity to its average radiation intensity i.e.,

$$\text{Directivity } (D) = \frac{\text{Max Radiation Intensity to test antenna}}{\text{Avg Radiation Intensity of test Antenna.}}$$

$$D = \frac{U(\theta, \phi)_{\max}}{\Phi_{av}} \text{ both of test antenna}$$

### Directivity of antenna for isotropic Antenna :-

$$\text{Directivity } (D) = \frac{\text{Max Radiation Intensity of Subject (S) test Antenna}}{\text{Radiation Intensity of isotropic Antenna}}$$

$$D = \frac{U(\theta, \phi)_{\max} \text{ (test antenna)}}{\Phi_0 \cdot \text{ (isotropic Antenna)}}$$

### vii) Radiation Efficiency (δ) Antenna Efficiency :- ( $\eta$ )

The efficiency of an Antenna is defined as the ratio of Power radiated to the total Q.H.P power supplied to the antenna and denoted as  $\eta$  ( $\delta$ ) K.

$$\begin{aligned} \text{Antenna Efficiency } \eta &= \frac{\text{Power Radiated}}{\text{Total Q.H.P Power}} \\ \eta &= \frac{W_R}{W_T} = \frac{W_R}{W_S + W_R} \\ &= \frac{W_R}{W_T} \times \frac{4\pi U(\theta, \phi)}{4\pi U(\theta, \phi)} \end{aligned}$$

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$$= \frac{4\pi I_0 U(\theta, \phi)}{W_t} \cdot \frac{W_b}{4\pi I_0(\theta, \phi)}$$

$$\eta_b = G_p \cdot \frac{1}{G_d} = \frac{G_p}{G_d} = \frac{W_b}{W_b + W_t}$$

$W_b$  = Power radiated

$W_t$  = ohmic loss

If current flowing in antenna is  $I$  then

$$\eta_b = \frac{I^2 R_s}{I^2 (R_s + R_d)}$$

$$\eta \% = \frac{R_s}{R_s + R_d} \times 100$$

$R_s \rightarrow$  Radiation resistance

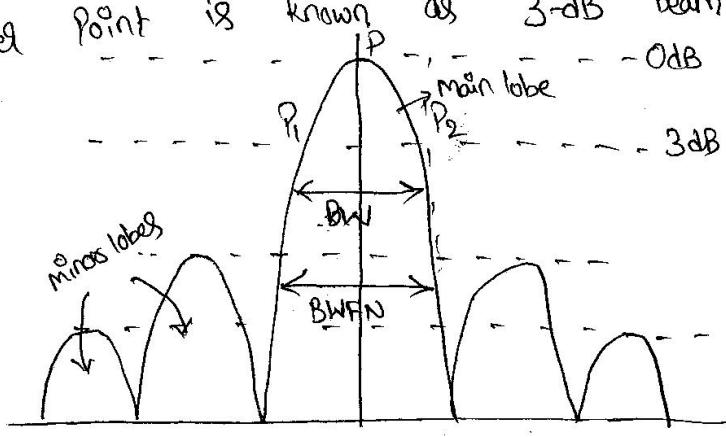
$R_d \rightarrow$  ohmic loss resistance  
of antenna conductor

### VIII) Antenna Beam width :-

Antenna Beam width is a measure of directivity of the antenna. The Antenna beam width is an angular width in degrees. It is measured on a radiation pattern major lobe.

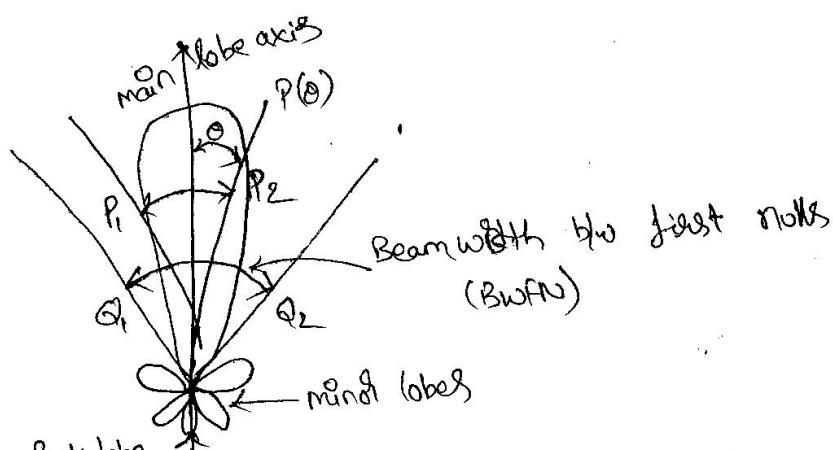
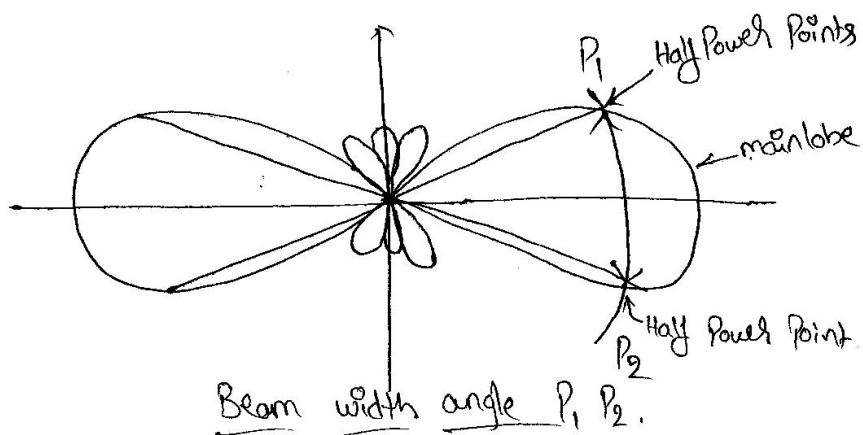
The antenna beamwidth is defined as the angular width in degree bw the two points in a major lobe of a radiation pattern where the radiated power decreased to half of the maximum value. This is called Beam width. Its half Power (BW)

Half Power Point is known as 3-dB beam width.



Antenna Pattern  
on rectangular  
Co-ordinates  
(a)  
Logarithmic Scale

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Antenna Power Pattern in Polar Co-ordinates.

The beam width is also called as Half Power Beam Width (HPBW) because it is measured b/w two points on main lobe where power is half of its maximum power. The two points  $P_1$  &  $P_2$  is nothing but antenna the angular width between Points  $P_1$  &  $P_2$  is called beamwidth ( $\delta$ ) Half Power beamwidth (HPBW).

It is clear Power is maximum at Point 'P' but at Points  $P_1$  &  $P_2$  the Power is 3dB down the maximum power.

Many times Radiation Pattern of antenna is described as in term of angular beamwidth b/w first nulls ( $\delta$ ) first Side lobes. Then such an angular beamwidth is called Beamwidth b/w First Nulls (BwFN).

The directivity ( $D$ ) of antenna is related with beam solid angle  $(\Omega_A)$  & beam area ' $B$ ' through expression (18)

$$D = \frac{4\pi}{\cdot \Omega_A} = \frac{4\pi}{B}$$

$B$  = Beam Area

$B = (\text{HPBW}) \text{ in horizontal plane} \times (\text{HPBW}) \text{ in vertical plane}$

$= (\text{HPBW}) \text{ in E-Plane} \times (\text{HPBW}) \text{ in H-Plane}$

$$(a) \\ B = \theta_e \times \theta_h$$

$$\therefore D = \frac{4\pi}{\theta_e \theta_h} \dots \text{if } \theta_e \text{ and } \theta_h \text{ are in radians}$$

Then

$$D = \frac{4\pi (1 \text{ radian})^2}{\theta_e^\circ \theta_h^\circ} = \frac{4\pi (57.3)^2}{\theta_e^\circ \theta_h^\circ} = \frac{41257}{\theta_e^\circ \theta_h^\circ}$$

### (ix) Antenna Beam Efficiency :- (BE)

Antenna beam efficiency is the parameter that is frequency used to judge the quality of transmitting and receiving antennas for the antenna with major lobe coincident with  $Z$ -axis

the beam efficiency is given as

Power transmitted ( $\phi$ ) received with in cone angle  $\theta_1$

$BE = \frac{\text{Power transmitted } (\phi) \text{ received by antenna}}{\text{Power transmitted } (\phi) \text{ received by antenna}}$

$\theta_1 \rightarrow$  half angle of the cone within Percentage of total Power is.

$$\int_{\phi=0}^{2\pi} \int_{\theta=0}^{\theta_1} U(\theta, \phi) \cdot \sin \theta \cdot d\theta \cdot d\phi$$

$$\text{Mathematically Beam Efficiency (BE)} = \frac{\int_{\phi=0}^{2\pi} \int_{\theta=0}^{\theta_1} U(\theta, \phi) \cdot \sin \theta \cdot d\theta \cdot d\phi}{\int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} U(\theta, \phi) \cdot \sin \theta \cdot d\theta \cdot d\phi}$$

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If  $\theta_1$  is chosen as angle where first nulls (8) minimum occurs  
the beam efficiency expressed as in terms ( $S_{Lm}$ ) and beam area ( $S_{LA}$ )

Beam efficiency can be defined as ratio of main beam area to  
total beam area denoted as ( $E_M$ )

$$\text{Bf (8)} \quad E_M = \frac{S_{Lm}}{S_{LA}} = \frac{\text{Main beam area}}{\text{Total beam area}}$$

Total beam area consists of main beam area ( $S_{Lm}$ ) and  
minor lobe area (8) solid angle  $S_{Lm}$  i.e

$$S_{LA} = S_{Lm} + S_{Lm}$$

Total beam area = Main beam area + Minor lobe area.

$$1 = \frac{S_{Lm}}{S_{LA}} + \frac{S_{Lm}}{S_{LA}}$$

$$1 = E_M + E_m$$

where

$$E_m = \frac{S_{Lm}}{S_{LA}} = \text{Stagn Factor} = \frac{\text{Minor lobe area}}{\text{Total beam area}}$$

$$E_M = \frac{S_{Lm}}{S_{LA}} = \text{Beam Efficiency.}$$

(X) Front to Back Ratio (FBR):-

FBR = Front power radiated / Back power radiated  
is the ratio of Power radiated in desired direction to  
the Power radiated in the opposite direction.

$$FBR = \frac{\text{Power radiated in desired direction}}{\text{Power radiated in opposite direction.}}$$

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ON the frequency of radiation. FBR is depended, so when frequency of an antenna changes, the FBR also changes. Similarly the FBR depends on the spacing b/w the antenna elements. If spacing b/w antenna elements increased the FBR decreases. The FBR also depends on electrical length & parasitic elements of the antenna.

The FBR can be varied by deviating the gain of backward direction response of antenna to the front (F) forward (F) desired direction by adjusting the length of parasitic elements. The method of adjusting the electrical length of the parasitic element is called tuning.

### (XII) Antenna Temperature ( $T_A$ ):-

Antenna Radiation Pattern is affected by temperature with its radiation resistance and it does not depends on location (F) direction of antenna. In general temperature and power are related as

$$P \propto T_A \quad P \rightarrow \text{Noise Power per unit BW W/Hz}$$

$$K \rightarrow \text{Boltzmann Constant} = 1.38 \times 10^{-23} \text{ J/K}$$

$$P = K A T_A \quad T_A \rightarrow \text{Absolute temp of Antenna in K.}$$

Let an antenna placed at environmental temperature and the radiation pattern depends on physical size of antenna. due to environmental temperature the noise power is

$$P = S \cdot A_p \cdot B \rightarrow ②$$

(21)

$P \rightarrow$  Noise Power ;  $B \rightarrow$  Bandwidth

$S \rightarrow$  Power density (or) Power spectral density

$A_e \rightarrow$  Effective aperture of antenna

from eq ① & ② The flux density of antenna is

$$K \tilde{r}_A B = S \cdot A_e B$$

$$S = \frac{K \tilde{r}_A}{A_e} \text{ W/m}^2 \text{ Hz} \rightarrow ③$$

∴ Temperature of Antenna is written as

from above eq

$$\tilde{r}_A = \frac{S \cdot A_e}{K} ^\circ K$$

If the source is small compared to the beam solid angle ' $\Omega_A$ ' then the source temperature can be given.

$$\tilde{r}_s = \frac{\Omega_A \tilde{r}_A}{\Omega_s} ^\circ K$$

$\Omega_A$  = Beam solid angle in steradian

$\Omega_s$  = Source solid angle in steradian //,

(xi) Effective Aperture (or) Effective Area ( $A_e$ ) :-

A transmitting antenna transmits electromagnetic waves

and receiving antenna receives a fraction of the same.

On consideration on antenna to have effective area

(or) aperture over which it absorbs electromagnetic energy

from travelling electromagnetic waves.

(22)

The ratio of Power received at the antenna load terminal to the Poynting vector of average Power density.

$$A_e = \frac{P_{\text{Received}}}{P_{\text{Avg}}} \text{ m}^2 \rightarrow 1$$

Power received is denoted as ( $P_r$ ) measured in Watts

Power density measured in watts/m<sup>2</sup>.

$$(a) A_e = \frac{W}{P} = A \rightarrow 2$$

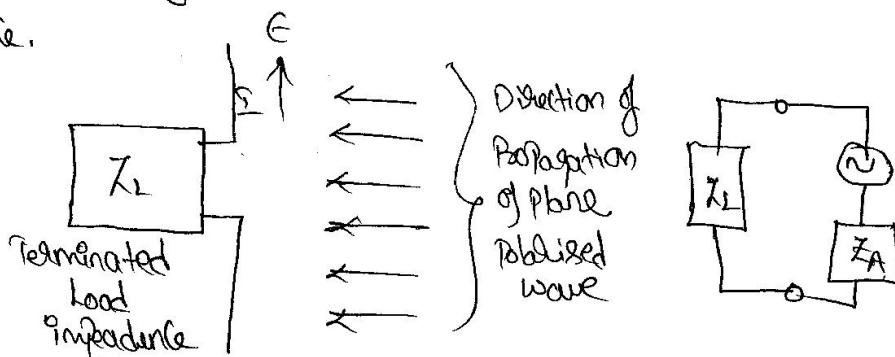
$$W = PA$$

$W$  = Power received in Watts

$P$  = Poynting avg Power density

$A$  = Effective (or) Capture area (or) effective aperture in m<sup>2</sup>.

Let a receiving antenna be placed in the field of plane polarised travelling waves in having an effective area  $A$  and the receiving antenna (dipole) is terminated at load impedance.



$I \rightarrow$  terminal current, then Received Power

$$W = I_{\text{avg}}^2 R_L \rightarrow 3$$

$R_L \rightarrow$  load resistance in  $\Omega$ .

$I_{\text{avg}} \rightarrow$  terminal avg Current

$$A = \frac{W}{P} = \frac{\Gamma_{\text{one}}^2 R_L}{P} \rightarrow (4) \quad (23)$$

Since the antenna extracts energy from incident electromagnetic waves, delivers the same to terminated load impedance  $Z_L$  and power flowing per square meter (a) Poynting vector  $P \text{ W/m}^2$ . and entire system replaced by equivalent circuit of

$V$  = Equivalent Thvenin Voltage  
 $Z_A$  = Equivalent Impedance

$$\Gamma_{\text{one}} = \frac{\text{Equivalent voltage}}{\text{Equivalent Impedance}} = \frac{V}{Z_L + Z_A} \text{ Amp} \rightarrow (5)$$

where  $Z_A = R_A + jX_A$  (Complex antenna impedance)

$$Z_L = R_L + jX_L$$

Now -  $\Gamma_{\text{one}} = \frac{V}{Z_A + Z_L} = \frac{V}{Z_T} \rightarrow (6)$

$$\Gamma_{\text{one}} = \frac{V}{(R_A + jX_A) + (R_L + jX_L)}$$

$$|\Gamma_{\text{one}}| = \sqrt{(R_A + jX_A)^2 + (R_L + jX_L)^2}$$

Squaring on Both Sides

$$|\Gamma_{\text{one}}|^2 = \frac{V^2}{(R_A + R_L)^2 + (X_A + X_L)^2} \rightarrow (7)$$

$$\therefore W = \frac{\Gamma_{\text{one}}^2 R_L}{P} = \frac{V^2 R_L}{(R_A + R_L)^2 + (X_A + X_L)^2} \rightarrow (8)$$

$$A_e = \frac{W}{P} = \frac{V^2 R_L}{P(R_A + R_L)}$$

$$A_e = \frac{V^2 R_L}{P(R_A + R_L) + P(X_A + X_L)^2} \rightarrow (9)$$

According to maximum power transfer theorem,

(24)

$$X_L = -X_A$$

$$R_L = R_A \Rightarrow (R_A + R_L)$$

$$R_L = R_A \text{ if } R_L = 0$$

from Eq (9)

$$A_e = \frac{V^2 R_L}{P[(2R_L)^2 + 0]}$$

$$A_e = \frac{V^2 R_L}{4 P R_L^2} = \frac{V^2}{4 P R_L}$$

$$\therefore A_e = \boxed{\frac{V^2}{4 P R_L}}$$

(xiii) Effective Length :-

It represents effectiveness of antenna as radiator (or) Electromagnetic wave energy.

It is defined as ratio of incident (or) open circuit voltage to incident (or) field strength.

$$l_{eff} = \frac{\text{Open Ckt Voltage}}{\text{Incident field Strength}}$$

$$l_{eff(\text{received})} = \frac{V}{E} \rightarrow (1)$$

We know that

$$V^2 R_L$$

$$A_e = \frac{V^2 R_L}{P[(R_A + R_L)^2 + (X_A + X_L)^2]}$$

$$V^2 = \frac{Ae P \left\{ (R_A + R_L)^2 + (x_A + x_L)^2 \right\}}{R_L} \quad (25)$$

$$V = \sqrt{\frac{Ae P \left\{ (R_A + R_L)^2 + (x_A + x_L)^2 \right\}}{R_L}} \rightarrow (2)$$

$$P = \frac{E^2}{Z}$$

$$V = \sqrt{\frac{Ae E^2 \left[ (R_A + R_L)^2 + (x_A + x_L)^2 \right]}{Z R_L}}$$

$$I_e = \frac{V}{E} = \sqrt{\frac{Ae (R_A + R_L)^2 + (x_A + x_L)^2}{Z R_L}}$$

By maximum Power theorem

$$x_A = -x_L ; R_A = R_L$$

$$I_{eff} = \frac{V}{E} = \sqrt{\frac{Ae \left( \frac{1}{2} R_L \right)^2}{Z R_L}}$$

$$I_{eff} = \sqrt{\frac{4 Ae R_L}{Z}}$$

$$I_{eff} = 2 \sqrt{\frac{Ae R_L}{Z}}$$

$$I_{eff} = 2 \sqrt{\frac{Ae (R_A + R_L)}{Z}}$$

$$\therefore I_{eff} = 2 \sqrt{\frac{Ae R_A}{Z}}$$

## \*> Fields from Oscillating Dipole :-

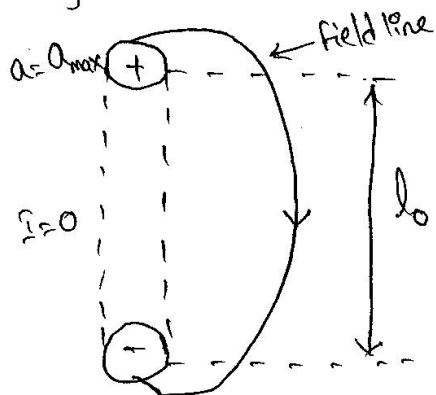
(26)

In this we discuss the radiation mechanism of an oscillating charge which moves back and forth in simple harmonic motion along a dipole.

Let us consider a dipole antenna with two equal and opposite charges oscillating up and down with simple harmonic motion.

Consider  $l_0$  be the maximum separation b/w two equal and opposite charges while  $l$  be an instantaneous separation b/w charges.

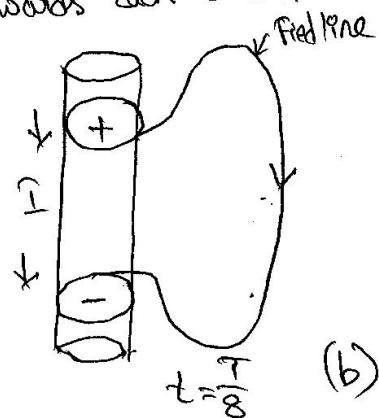
Let us analyze the electric field by taking into account a single electric field line.



\*) The equal and opposite charges are at maximum separation of ' $l_0$ ',  $t=0$ .

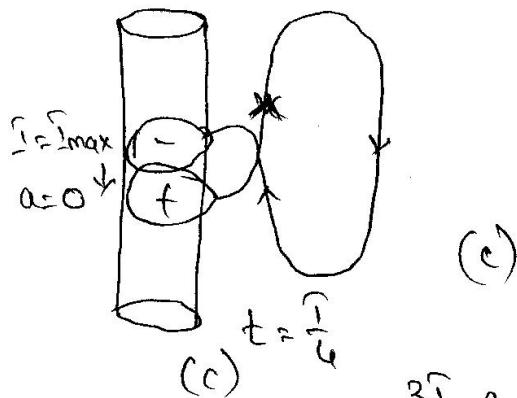
$\Rightarrow$  Here the acceleration of charges is maximum i.e.  $a_{max}$  as seen in direction of current ( $I=0$ ).

Let ' $T$ ' be the period of oscillation. Then after period  $t = \frac{T}{8}$  the charges move towards each other.

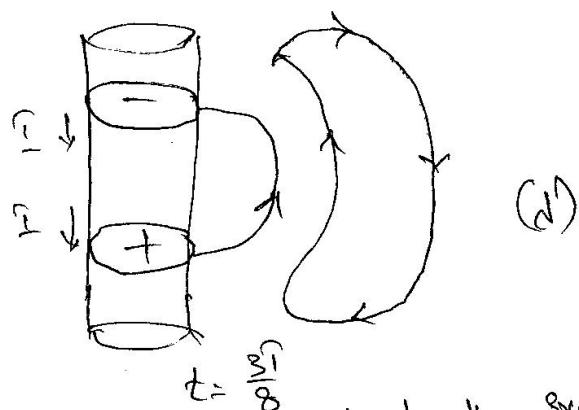


27

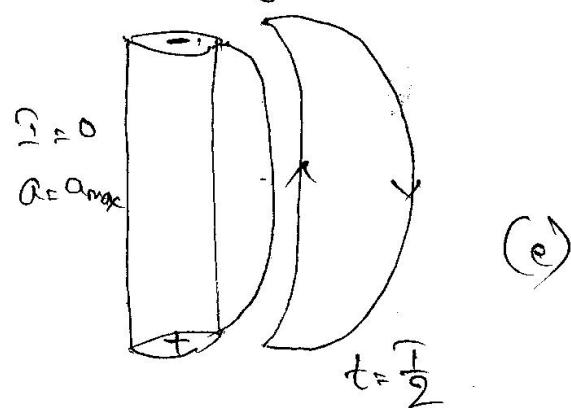
After a time period  $t = \frac{1}{4}$  the charges reach at Mid Point of  $\alpha$  axis of the dipole. At this instant the acceleration of charge becomes zero ( $a=0$ ) with current of maximum value ( $I=I_{\max}$ )



After a time period  $t = \frac{3}{8}$  a field line is completely detached and released from dipole. After detachment of field line new field line starts developing.



After  $t = \frac{1}{2}$  instant the charges reach to the exactly opposite ends of dipole as shown below. Again the charges gain maximum acceleration ( $a=a_{\max}$ ) with current being zero ( $I=0$ )



\*> Relation Between Max. Aperture and Gain (or) Directivity:-

The radiation pattern is same for transmitting and receiving antennas.

By virtue of Reciprocity theorem and hence the idea of directivity which itself is related with shape of radiation pattern is extended for receiving antennas also.

In practice that the directivity of receiving antennas are directly proportional to maximum effective apertures.

Let there be two Antenna A and B whose directivities and maximum effective apertures are denoted by  $D_a, D_b$ , and  $(A_{ea})_{max}$  and  $(A_{eb})_{max}$

$$\therefore D_a \propto (A_{ea})_{max}$$

$$D_b \propto (A_{eb})_{max}$$

$$\therefore \frac{D_a}{D_b} = \frac{(A_{ea})_{max}}{(A_{eb})_{max}}$$

For antenna with loss, gain will be less than directivity by a factor which corresponds to efficiency. The directivity and gain given as

$G_o \rightarrow$  Gain of transmitting (or) receiving antenna  
 $G_o = kD$

$k \rightarrow$  Efficiency factor

$D \rightarrow$  Directivity

If now the losses of efficiency both  $k$  and mismatch are included, the  $k$  can be replaced by effectiveness ratio  $\alpha$  i.e.

$$G_o \propto D$$

29

Let us now assume that  $G_{ra}$ ,  $\alpha_a$ ,  $D_a$  being the gain, effectiveness ratio and directivity of antenna A and  $G_{rb}$ ,  $\alpha_b$ ,  $D_b$  the corresponding quantities for antenna B, then

$$\begin{aligned} G_{ra} &= \alpha_a D_a \dots \text{for Antenna A} \\ G_{rb} &= \alpha_b D_b \dots \text{for " B} \end{aligned}$$

$$\frac{G_{ra}}{G_{rb}} = \frac{\alpha_a D_a}{\alpha_b D_b} = \frac{\alpha_a (A_{ra})_{\max}}{\alpha_b (A_{rb})_{\max}} \rightarrow (3)$$

$$\text{from Def. } \alpha_a = \frac{A_{ra}}{(A_{ra})_{\max}} \rightarrow (4)$$

$$\begin{aligned} (4) (A_{ra}) &= \alpha_a (A_{ra})_{\max} \\ (A_{rb}) &= \alpha_b (A_{rb})_{\max} \end{aligned} \rightarrow (5)$$

from eq (3)

$$\frac{G_{ra}}{G_{rb}} = \frac{A_{ra}}{A_{rb}}$$

when  $A_{ra}$  and  $A_{rb}$  are the effectiveness apertures A & B

let us assume that Antenna A is an isotropic antenna

then its directivity  $D_a = 1$

now from eq (1).

$$\frac{D_a}{D_b} = \frac{1}{D_b} = \frac{(A_{ra})_{\max}}{(A_{rb})_{\max}}$$

(30)

(a)

$$(A_{ea})_{max} = \frac{(A_{eb})_{max}}{D_b}$$

This above Eq suggests that if the maximum effective aperture and directivity of antenna B ( $D_b$ ) any antenna are known the ratio of two will give the maximum effective aperture of an isotropic antenna.

The directivity of any antenna can be calculated by

$$D_b = \frac{(A_{eb})_{max}}{(A_{ea})_{max}}$$

(31)

## Reciprocity Theorem:-

Statement :- If an emf is applied to the terminals of an antenna 1 and the current measured at the terminals of another antenna 2, then an equal current both in amplitude and phase will be obtained at the terminals of antenna no 1 if the same emf is applied to the terminals of antenna 2.

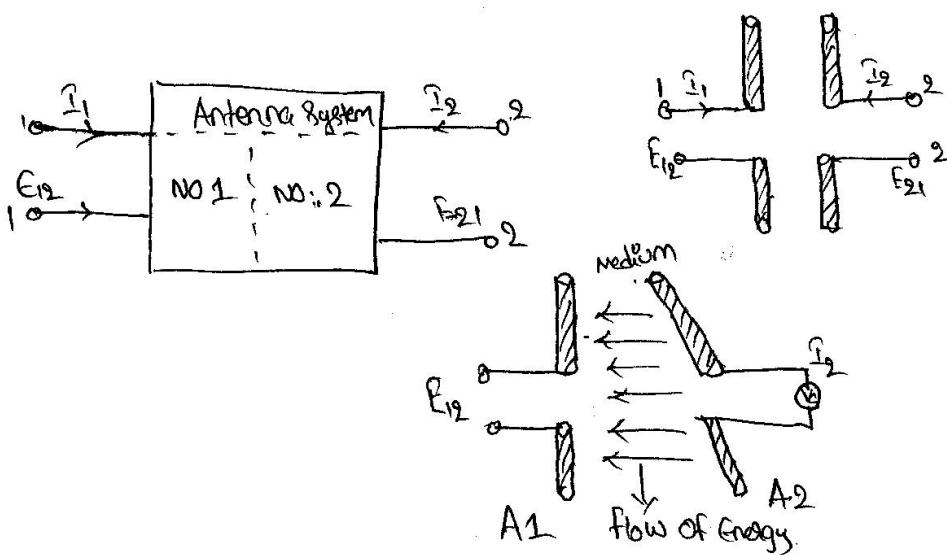
(a)  
If a current  $I_1$  at the terminals of Antenna 1 induces an emf  $E_{21}$  at open terminals of antenna 2 and current  $I_2$  at the terminals of Antenna 2 induces emf of  $E_{12}$  at the open ~~closed~~ terminals of Antenna 1 then  $E_{12} = E_{21}$

### Assumptions :-

- Emf are in same frequency
- Medium b/w the two Antenna are linear, passive and isotropic.
- Generator producing emf and Ammeter for measuring the current have zero impedance.

### Explanation :-

A transmitter of frequency 'f' and zero impedance be connected to the terminals of Antenna 2 which is generating a current  $I_2$  and inducing emf  $E_{12}$  at the open terminals of Antenna 1.



(32)

② Now the same transmitter is transferred to Antenna 1 which is generating a current  $I_1$  and inducing a voltage  $E_{21}$  at the open terminals of Antenna 2.

Thus A/c statement of reciprocity theorem

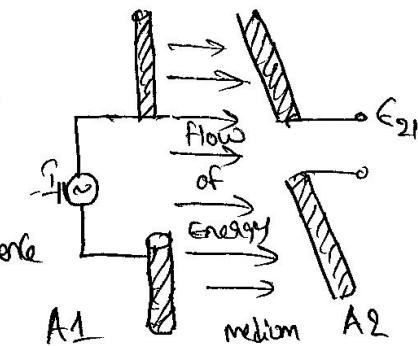
$$I_1 = I_2 \text{ Provided } E_{12} = E_{21}$$

$\therefore$  The ratio of emf to current is an impedance

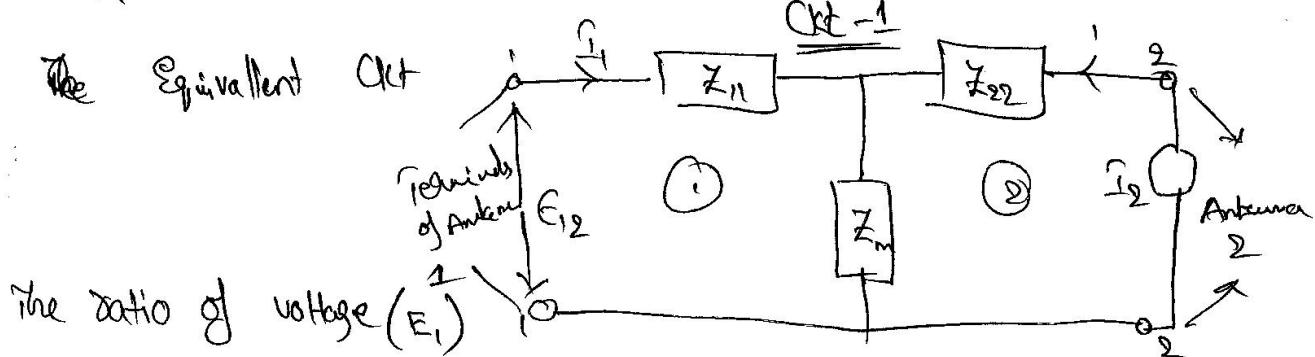
therefore the ratio  $\frac{E_{12}}{I_2}$  is given as

Transfer Impedance  $Z_{12}$  as in Case I, and so also the ratio

$\frac{E_{21}}{I_1}$  as Transferred Impedance  $Z_{21}$  as in II Case.



The Equivalent Ckt



The ratio of voltage ( $E_1$ )

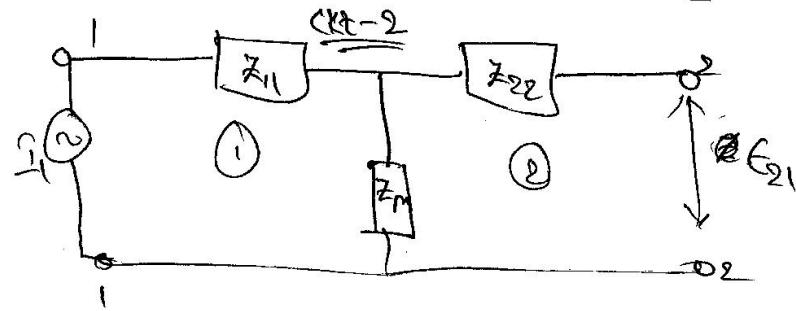
of 1 ckt to current  $I_2$

In second ckt is defined as

transfer impedance

$Z_T$  (or)  $Z_{12}$  i.e

$$Z_T = Z_{12} = \frac{E_1}{I_2} \rightarrow ①$$



That from the reciprocity it follows that the two ratios i.e two impedance are equal i.e

$$Z_{12} = Z_{21} \rightarrow ②$$

Where the mutual impedance ( $Z_m$ ) b/w two antennas is

$$Z_m = Z_{12} = Z_{21} = \frac{E_{12}}{I_2} = \frac{E_{21}}{I_1} \rightarrow 3$$

$$\boxed{\frac{E_{12}}{I_2} = \frac{E_{21}}{I_1}} \rightarrow 4$$

Proof:- By Reciprocity theorem for antennas, the space b/w the Antenna 1 & Antenna 2 are replaced by a new of linear, passive and bilateral impedance.

$Z_{11}, Z_{22}$  = Self impedance Antenna 1 & Antenna 2

$Z_m$  = mutual impedance b/w 2<sup>nd</sup> Antennas

Now applying Kirchhoff's mesh law

from cut-1 :- dig from loop 2

$$(Z_{22} + Z_m) I_2 - Z_m I_1 = 0 \quad (\because \text{no voltage in loop 2})$$

$$I_2 = I_1 \frac{Z_m}{(Z_{22} + Z_m)} \rightarrow 5$$

for loop ~~loop 1~~ :-

$$(Z_{11} + Z_m) I_1 - Z_m I_2 = E_{12}$$

$$(Z_{11} + Z_m) I_1 - Z_m \left[ I_1 \left( \frac{Z_m}{Z_{22} + Z_m} \right) \right] = E_{12} \rightarrow 6$$

$$\Rightarrow I_1 \left[ \frac{(Z_{11} + Z_m)(Z_{22} + Z_m) - Z_m^2}{Z_{22} + Z_m} \right] = E_{12}$$

$$\Rightarrow I_1 \left[ \frac{Z_2 Z_{11} + Z_m Z_{11} + Z_{22} Z_m + Z_m^2 - Z_m^2}{(Z_{22} + Z_m)} \right] = E_{12}$$

(Q)  $I_1 = \frac{E_{12} (Z_{22} + Z_m)}{Z_{11} Z_{22} + Z_m (Z_{11} + Z_{22})} \rightarrow 7$

(34)

Substituting Eq (7) in Eq (6)

$$\hat{I}_2 = \frac{E_{12} (Z_{22} + Z_m) \cdot Z_m}{[Z_{11} \times Z_{22} + Z_m (Z_{11} + Z_{22})] \cdot (Z_{22} + Z_m)}$$

$$\hat{I}_2 = \frac{E_{12} \cdot Z_m}{Z_{11} \times Z_{22} + Z_m (Z_{11} + Z_{22})} \rightarrow (8)$$

Similarly  $\hat{I}_1$  on Ckt - 2 given by

$$\hat{I}_1 = \frac{E_{21} \cdot Z_m}{Z_{22} \cdot Z_{11} + Z_m (Z_{22} + Z_{11})} \rightarrow (9)$$

Clearly Eq (8) & (9) are same exact value of emf

As to theorem statement

$$E_{12} = E_{21} \text{ if } \hat{I}_1 = \hat{I}_2$$

$\therefore$  Applying Condition:-  $\hat{I}_1 = \hat{I}_2$

$$\frac{E_{12} Z_m}{[Z_{11}, Z_{22} + Z_m] (Z_{11} + Z_{22})} = \frac{E_{21} \cdot Z_m}{[Z_{11}, Z_{22} + Z_m] (Z_{11} + Z_{22})}$$

$\therefore E_{12} = E_{21}$

Hence Proved ..