

# Communication System Homework I (Spring 2020)

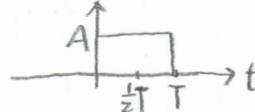
2.3

$$g(t) = g_e(t) + g_o(t)$$

$$g_e(t) = \frac{1}{2}[g(t) + g(-t)]$$

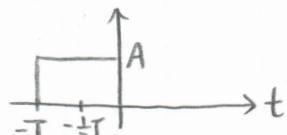
$$g_o(t) = \frac{1}{2}[g(t) - g(-t)]$$

(a)

$$g(t) = A \text{rect}\left(\frac{t}{T} - \frac{1}{2}\right) \rightarrow$$


$$\begin{aligned} g_e(t) &= \frac{1}{2}[g(t) + g(-t)] \\ &= \frac{A}{2} \text{rect}\left(\frac{t}{2T}\right) \end{aligned}$$

$$g(-t) = A \text{rect}\left(\frac{t}{T} + \frac{1}{2}\right) = A \text{rect}\left(\frac{t - (-\frac{1}{2}T)}{T}\right)$$



$$\begin{aligned} g_o(t) &= \frac{1}{2}[g(t) - g(-t)] \\ &= \frac{A}{2} \left[ \text{rect}\left(\frac{t - \frac{1}{2}T}{T}\right) - \text{rect}\left(\frac{t + \frac{1}{2}T}{T}\right) \right] \# \end{aligned}$$

(b)

By the time-scaling property  $g(t) \Leftrightarrow G(f)$

$$\begin{aligned} G_e(f) &= \frac{1}{2}[G(f) + G(-f)] \\ &= \frac{AT}{2} [\text{sinc}(fT) e^{-j\pi fT} + \text{sinc}(fT) e^{j\pi fT}] \end{aligned}$$

$$= AT \text{sinc}(fT) \cos(\pi fT) \text{ or } = AT \text{sinc}(2fT) \#$$

$$\begin{aligned} G_o(f) &= \frac{1}{2}[G(f) - G(-f)] \\ &= \frac{AT}{2} [\text{sinc}(fT) e^{-j\pi fT} - \text{sinc}(fT) e^{j\pi fT}] \\ &= -jAT \text{sinc}(fT) \sin(\pi fT) \# \end{aligned}$$

$$\begin{cases} \cos \theta = \frac{1}{2}(e^{j\theta} + e^{-j\theta}) \\ \sin \theta = \frac{1}{2j}(e^{j\theta} - e^{-j\theta}) \end{cases}$$

(a)

If  $g(t)$  is even and real, then

$$g(t) = \frac{1}{2}[g(t) + g(-t)]$$

and  $g(t) = g^*(t) \Rightarrow G(f) = G^*(-f)$  - ①

$$G^*(f) = \frac{1}{2}[G^*(f) + G^*(-f)]$$

$$\frac{1}{2}G^*(f) = \frac{1}{2}G^*(-f)$$

$$G^*(f) = G^*(-f)$$
 - ②

由①, ②得  $G^*(f) = G(f)$

$\therefore G(f)$  is all real \*

If  $g(t)$  is odd and real, then

$$g(t) = \frac{1}{2}[g(t) - g(-t)]$$

and  $g(t) = g^*(t) \Rightarrow G(f) = G^*(-f)$  - ③

$$G(f) = \frac{1}{2}[G(f) - G(-f)]$$

$$G^*(f) = \frac{1}{2}G^*(f) - \frac{1}{2}G^*(-f)$$

$$G^*(f) = -G^*(-f)$$
 - ④

由③, ④得  $G^*(f) = -G(f)$

$\therefore G(f)$  must be all imaginary \*

(b)

$$(-j\omega t)g(t) \rightleftharpoons \frac{d}{df}G(f)$$

$$t \cdot g(t) \rightleftharpoons \left(\frac{j}{\omega}\right) \frac{d}{df}G(f)$$

The previous step can be repeated  $n$  times so:

$$t^n g(t) \rightleftharpoons \left(\frac{j}{\omega}\right)^n G^{(n)}(f)$$
 得証 #

(c)

$$\text{Let } h(t) = t^n g(t)$$

$$H(f) = \left(\frac{1}{2\pi}\right)^n G^{(n)}(f)$$

$$\therefore \int_{-\infty}^{\infty} h(t) dt = H(0) = \left(\frac{j}{\omega}\right)^n G^{(n)}(0)$$
 得証 #

(d)

$$\begin{aligned} \text{Let } g(t) = g_1(t)g_2^*(t) \Rightarrow G(f) &= \int_{-\infty}^{\infty} g(t) e^{-j\omega f t} dt \\ &\quad (G(0) = \int_{-\infty}^{\infty} g(t) dt) \end{aligned}$$

$$\mathcal{F}\{g(t)\} = \mathcal{F}\{g_1(t)g_2^*(t)\}$$

$$= \int_{-\infty}^{\infty} G_1(\lambda) G_2^*(\lambda - f) d\lambda$$

$$\therefore g_1(t)g_2^*(t) \rightleftharpoons \int_{-\infty}^{\infty} G_1(\lambda) G_2^*(\lambda - f) d\lambda$$
 得証 #

(e)

$$\text{由(d)可知 } g_1(t)g_2^*(t) \rightleftharpoons \int_{-\infty}^{\infty} G_1(\lambda) G_2^*(\lambda - f) d\lambda$$

$$\int_{-\infty}^{\infty} g_1(t)g_2^*(t) dt = G(0)$$

$$= \int_{-\infty}^{\infty} G_1(\lambda) G_2^*(\lambda - 0) d\lambda$$

replacing  $\lambda$  with  $f$

$$\Rightarrow \int_{-\infty}^{\infty} g_1(t)g_2^*(t) dt = \int_{-\infty}^{\infty} G_1(f) G_2^*(f) df$$
 得証 #

2.10

$$Y(f) = \int_{-\infty}^{\infty} X(\nu) X(f-\nu) d\nu$$

$$|X(\nu)| \neq 0, \text{ if } |\nu| \leq W$$

$$|X(f-\nu)| \neq 0, \text{ if } |f-\nu| \leq W$$

$$(f-\nu) \leq W \text{ for } f \leq W+\nu \text{ when } \nu \geq 0 \text{ and } \nu \leq W$$

$$(f-\nu) \geq -W \text{ for } f \leq -W+\nu \text{ when } \nu \leq 0 \text{ and } \nu \geq -W$$

$$\therefore (f-\nu) \leq W \text{ for } 0 \leq \nu \leq W \text{ when } f \leq 2W$$

$$(f-\nu) \geq -W \text{ for } -W \leq \nu \leq 0 \text{ when } f \geq -2W$$

$\therefore$  Over the range of integration  $[-W, W]$

the integral is non-zero if  $|f| \leq 2W$

2.14

(a)

$$\frac{dg(t)}{dt} \Leftrightarrow j2\pi f G(f), \text{ Let } g'(t) = \frac{dg(t)}{dt}$$

$$\text{By Rayleigh's theorem: } \int_{-\infty}^{\infty} |g(t)|^2 dt = \int_{-\infty}^{\infty} |G(f)|^2 df$$

$$\begin{aligned} W_{rms}^2 T_{rms}^2 &= \frac{\int_{-\infty}^{\infty} t^2 |g(t)|^2 dt \cdot \int_{-\infty}^{\infty} f^2 |G(f)|^2 df}{\left( \int_{-\infty}^{\infty} |g(t)|^2 dt \right)^2} \\ &= \frac{\int_{-\infty}^{\infty} t^2 |g(t)|^2 dt \cdot \int_{-\infty}^{\infty} g'(t) g'^*(t) dt}{4\pi^2 \left( \int_{-\infty}^{\infty} |g(t)|^2 dt \right)^2} \quad \left[ \begin{aligned} \int_{-\infty}^{\infty} f^2 |G(f)|^2 df &= \int_{-\infty}^{\infty} |f G(f)|^2 df \\ &= \int_{-\infty}^{\infty} \left| \frac{1}{j2\pi} \frac{d}{dt} g(t) \right|^2 dt \\ &= \frac{1}{4\pi^2} \int_{-\infty}^{\infty} |g'(t)|^2 dt \\ &= \frac{1}{4\pi^2} \int_{-\infty}^{\infty} g'(t) g'^*(t) dt \end{aligned} \right] \\ &\quad \because C + C^* = 2\operatorname{Re}\{C\} \leq 2|C|, \forall C \in \mathbb{C} \end{aligned}$$

$$\begin{aligned} \left\{ \int_{-\infty}^{\infty} [g_1^*(t) g_2(t) + g_1(t) g_2^*(t)] dt \right\}^2 &\leq \left[ \int_{-\infty}^{\infty} 2|g_1(t) g_2^*(t)| dt \right]^2 \\ &= 4 \left[ \int_{-\infty}^{\infty} |g_1(t) g_2^*(t)| dt \right]^2 \\ &\leq 4 \left[ \int_{-\infty}^{\infty} |g_1(t)| |g_2^*(t)| dt \right]^2 \\ &\leq 4 \int_{-\infty}^{\infty} |g_1(t)|^2 dt \int_{-\infty}^{\infty} |g_2(t)|^2 dt - \varnothing \end{aligned}$$

By C-S theorem

Let  $g_1(t) = t g(t)$ ,  $g_2(t) = g'(t)$

$$\Rightarrow \int_{-\infty}^{\infty} t^2 |g(t)|^2 dt \int_{-\infty}^{\infty} |g'(t)|^2 dt \geq \frac{\left\{ \int_{-\infty}^{\infty} t g^*(t) g'(t) + t g(t) g'^*(t) dt \right\}^2}{4} \quad (\text{By ①})$$

$$= \frac{\left\{ \int_{-\infty}^{\infty} t \frac{d}{dt} [g(t) g^*(t)] dt \right\}^2}{4}$$

By integration by parts

$$\begin{aligned} u &= t & dv &= \frac{d}{dt} [g(t) g^*(t)] dt \\ du &= dt & v &= |g(t)|^2 \end{aligned}$$

$$\left[ t |g(t)|^2 \Big|_{-\infty}^{\infty} - \int_{-\infty}^{\infty} |g(t)|^2 dt \right]^2 = \left[ \int_{-\infty}^{\infty} |g(t)|^2 dt \right]^2$$

$\left[ \begin{array}{l} \because \text{根據題目給的條件 } g(t) \text{ 比 } \frac{1}{t^2} \text{ 快 converge 到 } 0 \\ \text{在 } t \rightarrow \infty \text{ 及 } t \rightarrow -\infty \\ \therefore t |g(t)|^2 \Big|_{-\infty}^{\infty} = 0 \end{array} \right]$

$$= \frac{\left[ \int_{-\infty}^{\infty} |g(t)|^2 dt \right]^2}{4} \quad \text{②}$$

$$\therefore W_{rms}^2 T_{rms}^2 = \frac{\int_{-\infty}^{\infty} t^2 |g(t)|^2 dt \cdot \int_{-\infty}^{\infty} |g'(t)|^2 dt}{4\pi^2 (\int_{-\infty}^{\infty} |g(t)|^2 dt)^2}$$

$$\geq \frac{(\int_{-\infty}^{\infty} |g(t)|^2 dt)^2}{16\pi^2 (\int_{-\infty}^{\infty} |g(t)|^2 dt)^2} \quad (\text{By ②})$$

$$\geq \frac{1}{16\pi^2}$$

$$\Rightarrow W_{rms} T_{rms} \geq \frac{1}{4\pi} \text{ 得証} \#$$

(b)

$$\text{For } g(t) = \exp(-\pi t^2)$$

$$g(t) \rightleftharpoons \exp(-\pi f^2) = G(f)$$

$$\begin{aligned} \therefore W_{rms}^2 T_{rms}^2 &= \frac{\int_{-\infty}^{\infty} t^2 |g(t)|^2 dt \int_{-\infty}^{\infty} f^2 |G(f)|^2 df}{(\int_{-\infty}^{\infty} |g(t)|^2 dt)^2} \\ &= \frac{\int_{-\infty}^{\infty} t^2 \exp(-2\pi t^2) dt \int_{-\infty}^{\infty} f^2 \exp(-2\pi f^2) df}{(\int_{-\infty}^{\infty} \exp(-2\pi t^2) dt)^2} \\ &= \frac{\left( \frac{1}{4\pi} \sqrt{\frac{1}{2}} \right)^2}{\frac{1}{2}} = \left( \frac{1}{4\pi} \right)^2 \end{aligned}$$

$$\Rightarrow W_{rms} T_{rms} = \frac{1}{4\pi} \text{ 得証} \#$$

Using a table of integrals:

$$\int_0^\infty x^2 \exp(-ax^2) dx = \frac{1}{4a} \sqrt{\frac{\pi}{a}} \text{ for } a > 0$$

$$\therefore \int_{-\infty}^{\infty} t^2 \exp(-2\pi t^2) dt = \frac{1}{8\pi} \sqrt{\frac{\pi}{2\pi}} \cdot 2 = \frac{1}{4\pi} \sqrt{\frac{1}{2}}$$

$$\int_{-\infty}^{\infty} f^2 \exp(-2\pi f^2) df = \frac{1}{4\pi} \sqrt{\frac{1}{2}}$$

Using a table of integrals:

$$\int_0^\infty \exp(-ax^2) dx = \frac{1}{2} \sqrt{\frac{\pi}{a}}$$

$$\therefore \int_{-\infty}^{\infty} \exp(-2\pi t^2) dt = \frac{1}{2} \sqrt{\frac{\pi}{2\pi}} \cdot 2 = \sqrt{\frac{1}{2}}$$

2.19

(a)

For the sake of convenience, let  $h(t)$  be the filter time-shifted so that it is symmetric about the region ( $t=0$ ).

$$\begin{aligned} H(f) &= \sum_{k=1}^{\frac{N-1}{2}} W_k \exp(-j2\pi f k) + \sum_{k=-1}^{-\frac{N-1}{2}} W_k \exp(-j2\pi f k) + W_0 \\ &= 2 \sum_{k=1}^{\frac{N-1}{2}} W_k \cos(2\pi f k) + W_0 \end{aligned}$$

Let  $G(f)$  be the filter returned to its correct position. Then

$$G(f) = H(f) \exp(-j2\pi f(\frac{N-1}{2})), \text{ which is a time-shift of } (\frac{N-1}{2}) \text{ samples.}$$

$$\therefore G(f) = \exp(-j\pi f(N-1)) 2 \sum_{k=1}^{\frac{N-1}{2}} W_k \cos(2\pi f k) + \exp(-j\pi f(N-1)) W_0 \#$$

(b)

By inspection, it is apparent that:

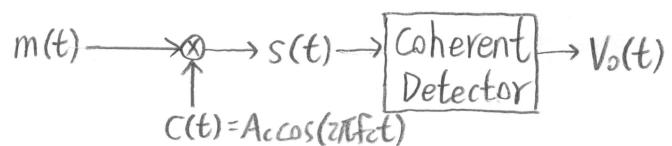
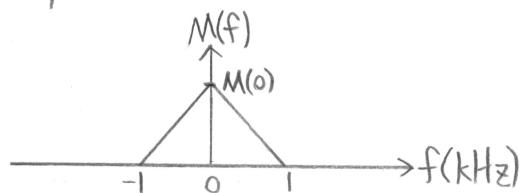
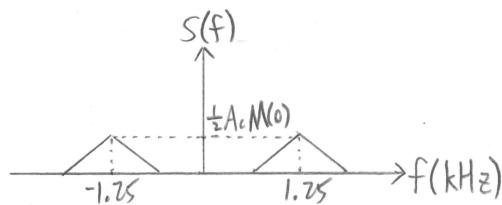
$$\nabla G(f) = \nabla \exp(-j\pi f(N-1))$$

This meets the definition of linear phase.  $\#$

3.8

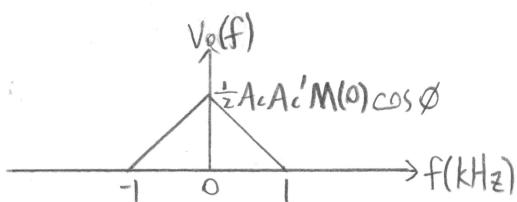
(a)

For  $f_c = 1.25 \text{ kHz}$ , the spectra of the message signal  $m(t)$ , the product modulator output  $s(t)$ , and the coherent detector output  $V_o(t)$  are as follows, respectively.

 $\Rightarrow$ 

$$S(t) = A_c \cos(2\pi f_c t) m(t)$$

$$S(f) = \frac{1}{2} A_c [M(f-f_c) + M(f+f_c)]$$

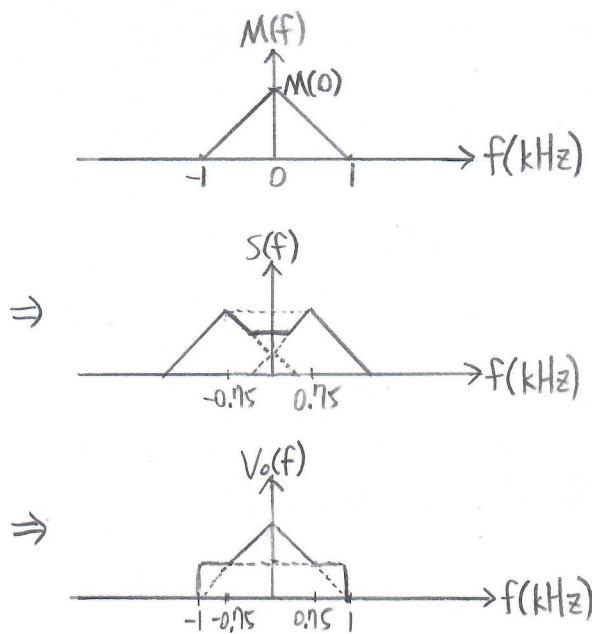
 $\Rightarrow$ 

$$\begin{aligned} V(t) &= \frac{1}{2} A_c A_c' \cos(4\pi f_c t + \phi) m(t) \\ &\quad + \frac{1}{2} A_c A_c' \cos \phi m(t) \end{aligned}$$

$$V_o(t) = \frac{1}{2} A_c A_c' \cos \phi m(t) \#$$

(b)

For the case when  $f_c = 0.75$ , the respective spectra are as follows:



To avoid sideband-overlap, the carrier frequency  $f_c$  must be greater than or equal to 1 kHz. The lowest carrier frequency is therefore 1 kHz for each sideband of the modulated wave  $S(t)$  to be inequality determined by  $m(t)$ .

3.9

The two AM modulator outputs are

$$S_1(t) = A_c [1 + k_a m(t)] \cos(2\pi f_c t)$$

$$S_2(t) = A_c [1 - k_a m(t)] \cos(2\pi f_c t)$$

Subtracting  $S_2(t)$  from  $S_1(t)$ :

$$S(t) = S_1(t) - S_2(t)$$

$= 2A_c k_a m(t) \cos(2\pi f_c t)$  which represents a DSB-SC modulated wave. #

3.11

(a) Multiplying the signal by the local oscillator gives:

$$\begin{aligned} S_1(t) &= A_c m(t) \cos(2\pi f_c t) \cos[2\pi(f_c + \Delta f)t] \\ &= \frac{A_c}{2} m(t) \{ \cos(2\pi \Delta f t) + \cos[2\pi(2f_c + \Delta f)t] \} \end{aligned}$$

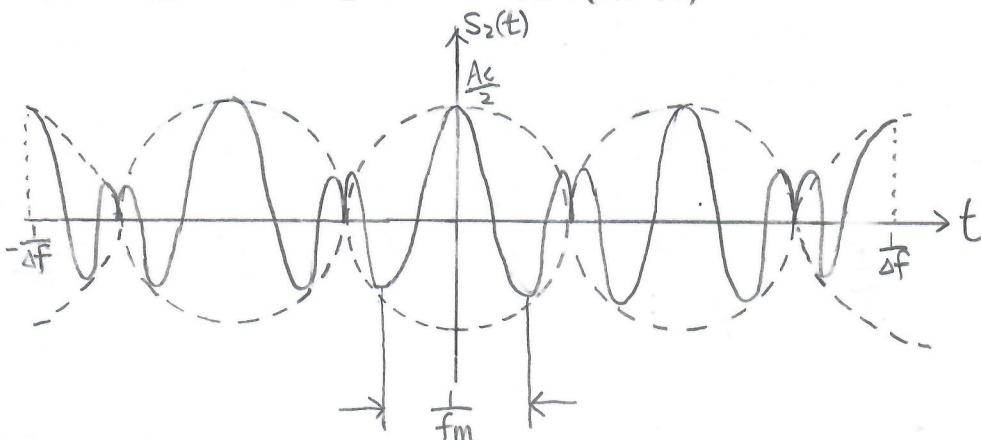
Low-pass filtering leaves:

$$S_2(t) = \frac{A_c}{2} m(t) \cos(2\pi \Delta f t)$$

Thus the output signal is the message signal modulated by a sinusoid of frequency  $\Delta f$ .

(b) If  $m(t) = \cos(2\pi f_m t)$

$$\text{then } S_2(t) = \frac{A_c}{2} \cos(2\pi f_m t) \cos(2\pi \Delta f t)$$



3.14

When the local carriers have a phase error  $\phi$ , we may write

$$\cos(2\pi f_c t + \phi) = \cos(2\pi f_c t) \cos \phi - \sin(2\pi f_c t) \sin \phi$$

In this case, we find that by multiplying the received signal  $r(t)$  by  $\cos(2\pi f_c t + \phi)$ , and passing the resulting output through a low-pass filter, the corresponding low-pass filter output in the receiver has a spectrum equal to  $\frac{A_c}{2} H(f-f_c)[\cos \phi M_1(f) - \sin \phi M_2(f)]$ . This indicates that there is cross-talk at the demodulator outputs.

3.15

The transmitted signal is given by

$$\begin{aligned} S(t) &= A_c m_1(t) \cos(2\pi f_c t) + A_c m_2(t) \sin(2\pi f_c t) \\ &= A_c [V_o + m_e(t) + m_r(t)] \cos(2\pi f_c t) + A_c [m_e(t) - m_r(t)] \sin(2\pi f_c t) \end{aligned}$$

(a)

$$S(t) \rightarrow \boxed{\text{Envelope Detector}} \rightarrow |\tilde{s}(t)| = y(t)$$

$$S(t) = \operatorname{Re}\{s(t)e^{j2\pi f_c t}\}$$

$$\tilde{s}(t) = A_c m_1(t) - j A_c m_2(t)$$

$$\begin{aligned} y(t) &= |\tilde{s}(t)| = \sqrt{A_c^2 (V_o + m_e(t) + m_r(t))^2 + A_c^2 (m_e(t) - m_r(t))^2} \\ &= A_c (V_o + m_e(t) + m_r(t)) \sqrt{1 + \left(\frac{m_e(t) - m_r(t)}{V_o + m_e(t) + m_r(t)}\right)^2} \end{aligned}$$

To minimize the distortion in the envelope detector output due to the quadrature component, we choose the DC offset  $V_o$  to be large. We may approximate  $y(t)$  as

$$y(t) \approx A_c (V_o + m_e(t) + m_r(t))$$

which except for the DC component  $A_c V_o$ , is proportional to the sum  $m_e(t) + m_r(t)$ .

(b)

$$\begin{aligned} V(t) &= S(t) A_c' \sin(2\pi f_c t) \\ &= A_c A_c' [m_1(t) \cos(2\pi f_c t) \sin(2\pi f_c t) + m_2(t) \sin(2\pi f_c t) \sin(2\pi f_c t)] \\ &= \frac{1}{2} A_c A_c' [m_1(t) \sin(4\pi f_c t) + m_1(t) \sin(0) + m_2(t) \cos(0) - m_2(t) \cos(4\pi f_c t)] \end{aligned}$$

Through Low-pass filter,

$$V_o(t) = \frac{1}{2} A_c A_c' m_2(t)$$

For coherent detection at the receiver, we need a replica of the carrier  $A_c \cos(2\pi f_c t)$ . This requirement can be satisfied by passing the received signal  $S(t)$  through a narrow-band filter of mid-band frequency  $f_c$ . However, to extract the difference  $m_e(t) - m_r(t)$ , we need  $\sin(2\pi f_c t)$ , which is obtained by passing the narrow-band filter output through a  $90^\circ$ -phase filter. Then multiplying  $S(t)$  by  $\sin(2\pi f_c t)$  and low-pass filtering, we can obtain a signal proportional to  $m_e(t) - m_r(t)$ .

(c)

① Equalize the outputs of the envelope detector and coherent detector.

② Pass the equalized outputs through an audio demixer to produce  $M_e(t)$  and  $M_r(t)$ .

The output from the envelop detector :  $V_{o1} = A_c M_1(t)$

The output from the coherent detector :  $V_{o2} = A_c M_2(t)$

$$\Rightarrow \begin{cases} V_{o1}' = \frac{V_{o1}}{A_c} - V_o \\ V_{o2}' = \frac{V_{o2}}{A_c} \end{cases} \Rightarrow \begin{cases} M_e(t) = \frac{1}{2}(V_{o1}' + V_{o2}') \\ M_r(t) = \frac{1}{2}(V_{o1}' - V_{o2}') \end{cases} \text{ are obtained.}$$