The fundamental Humodynamic valation

First Law; dE = 5Q + 5W

(quinstate reversible process)

if priticle number can change: It: every change por porticle

$$dE = TdS - pdV + \mu dN$$

$$\Rightarrow E(S, V, N) \qquad T = \left(\frac{SE}{SV}\right)_{V,N} \qquad M = \left(\frac{SE}{SV}\right)_{SN}$$

$$T = \left(\frac{2E}{2E}\right)_{V,N} \qquad M = \left(\frac{2E}{NN}\right)_{V,N}$$

$$\left|dS = \frac{1}{T}dE + \frac{P}{T}dV - \frac{M}{T}dN\right| \Rightarrow S(E, V, N)$$

$$\frac{1}{T} = \begin{pmatrix} \frac{2s}{2E} \end{pmatrix}_{V,N} \qquad , \qquad \frac{P}{T} = \begin{pmatrix} \frac{2s}{2V} \end{pmatrix}_{E,N} \qquad , \qquad \frac{M}{T} = -\begin{pmatrix} \frac{2s}{2V} \end{pmatrix}_{E,N}$$

$$\frac{1}{T} = \left(\frac{2s}{2E}\right)_{v,N}$$

$$\frac{1}{T} = \left(\frac{23}{2V}\right)_{E_{iN}}$$

example: ideal pas

$$\frac{1}{T} = \frac{3Nk}{2E} \qquad \frac{P}{T} = \frac{Nk}{V}$$

$$\frac{P}{T} = \frac{Nk}{V}$$

$$dS = \frac{3Nk}{2} \frac{dE}{E} + Nk \frac{dV}{V}$$

often needed: S(T,V) = 3 Nk lu + Nk lux

sibbs - Duham relation

$$dS = \left(\frac{2S}{2E}\right)_{V,N} dE + \left(\frac{2S}{2V}\right)_{E,N} dV + \left(\frac{2S}{2V}\right)_{E,N} dN$$

$$dS = \frac{1}{T} dE + \frac{?}{T} dV - \frac{M}{T} dN$$

$$T = \left(\frac{\partial E}{\partial S}\right)_{V,N} \qquad P = \left(\frac{\partial E}{\partial V}\right)_{S,N} \qquad \mu = \left(\frac{\partial E}{\partial N}\right)_{S,N}$$

extensivity:
$$E(\lambda S, \lambda V, \lambda N) = \lambda E(S, V, N)$$
, $\forall \lambda \left(homotofleprot order \right)$

differentiate

$$\frac{\partial E}{\partial \Omega S} \cdot \frac{\partial \Omega S}{\partial A} + \frac{\partial E}{\partial \Omega V} \frac{\partial (AV)}{\partial A} + \frac{\partial E}{\partial \Omega W} \frac{\partial (AV)}{\partial A} = E(S, V, N)$$

$$\frac{\partial E}{\partial (\lambda S)} S + \frac{\partial E}{\partial (\lambda V)} V + \frac{\partial F}{\partial (\lambda W)} V = E(S, V, N)$$

than set $\lambda = 1$

The Third Law of Themodynamics lim S = 0 (with exaptions) Consequences; quoistatic change: $\frac{\delta Q}{T} = dS$ at constant volume: $SQ = C_V(T)dT$ $\int_{T}^{T_2} dS = \int_{T}^{T_2} \frac{SQ}{T} = \int_{T_1}^{T_2} \frac{C_V(T)}{T} dT$ $S(T_{1},V)-S(T_{1},V)=\int \frac{C_{V}(T)}{T}dT$ $S(T_{2},V) = \lim_{T \to 0} \int_{T}^{T_{2}} \frac{C_{1}(T)}{T} dT \implies \lim_{T \to 0} C_{1}(T) = 0$ since S(Tr,V) must be finite similarly, one con report the same for castut P lim Cp(T) =0 Generalized Thermodynamical Pokutials (equilibrium with constraints) at Tress 5 res Scomposite 5 + Stes The system of our intenst 15 comp = 15 + 15 res 20 in equilibrium find of (proporty). Junction of the system alone which is elwacterized by max or min.

(S is mor, for an isolated uncontrolled system - I. Law)

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$$\Delta S_{ies} = -\frac{Q}{T_{res}}$$

$$\Delta S_{composite} = \Delta S - \frac{Q}{T_{res}}$$

$$\Delta E = Q + W = Q - P_{res} \Delta V$$

$$\Delta S_{comp} = \Delta S - \frac{Q}{T_{res}} = \Delta S - \frac{Q}{T_{res}}$$

$$\Delta S_{comp} = \Delta S - \frac{Q}{T_{res}} = \Delta S - \frac{\Delta E + P_{res} \Delta V}{T_{res}} > 0 \quad (I.L_{AUV})$$

$$T = T_{res}$$
, $\Delta V = O(V_{fixed}) \Rightarrow \Delta E - T \Delta S \times O$

$$S = -\left(\frac{2F}{2T}\right)_{VIN} \qquad P = -\left(\frac{2F}{2V}\right)_{TIN}$$

$$M = \begin{pmatrix} b + \\ 2N \end{pmatrix}_{T,V}$$

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Sependre Transpormetion

$$E(S,V,N)$$
 $T = \begin{pmatrix} 0E \\ 0S \end{pmatrix}_{V,N}$

$$F = E - 3\left(\frac{\partial E}{\partial S}\right)_{V,N} = E - TS$$

F(T,V,N)

$$S = -\begin{pmatrix} 2F \\ 0T \end{pmatrix}_{V_1N} \qquad P = \begin{pmatrix} 2F \\ 2V \end{pmatrix}_{T_1N} \qquad M = \begin{pmatrix} 2F \\ 2N \end{pmatrix}_{T_1V}$$

Segendre to replaced the extensive variable S by its intensive cognized themselve. variable T

$$E(S,V,N) \xrightarrow{S. tr.} F(T,V,N)$$

$$F = E - S(\frac{\partial E}{\partial S})_{V,N}$$

$$\begin{pmatrix} \frac{\partial G}{\partial T} \end{pmatrix} = -S \\
\frac{\partial G}{\partial P} = V \\
\frac{\partial G}{\partial N} = M$$

M: chemical potential

$$dg = \begin{pmatrix} 2g \\ 2T \end{pmatrix} dT + \begin{pmatrix} 2g \\ 2P \end{pmatrix} dP = -SdT + vdp$$

$$where \quad S = \frac{S}{N} \quad v = \frac{V}{N}$$

G= MN

Mathematical Note:

$$E = E(S, V, N)$$
 extensive nariables
 $E(1S, \lambda V, \lambda N) = \lambda E(S, V, N)$ homogeneous function
differentiate with respect to λ of the first order

 $\frac{\partial E}{\partial(\lambda S)}S + \frac{\partial E}{\partial(\lambda V)}V + \frac{\partial E}{\partial(\lambda N)}N = E$

$$G(T_iP_iN) = \mu(T_iP_i) \cdot N$$

 $g(T_iP) = \frac{G(T_iP_iN)}{N} = \mu(T_iP)$

Lundon or Grand Homodynamic potential Use notestion OTTIV,

= min. at fixed T, V, M

d. - dF - MdN - NdM =

= - SaT - pdV + udN - udN - Ndn =

= -SdT-PdV - NdM

using Gibbs - Duham:

useful to obtain equation of state

Thermodynamic Response Functions

$$C_{\nu} = \left(\frac{9E}{2T}\right)_{\nu}$$

$$C_{\rho} = \begin{pmatrix} 241 \\ 2T \end{pmatrix}_{\rho}$$

Are they independent?

Moxwell Relations and Applications

$$T = \begin{pmatrix} 0F \\ 2S \end{pmatrix}_V$$

$$\left(\frac{2T}{2V}\right)_{S} = \frac{3E}{2V2S} = \frac{3E}{2S2V} - \left(\frac{2P}{2S}\right)_{V}$$

example 1.
$$\left(\frac{27}{2V}\right)_s = -\left(\frac{5P}{2S}\right)_v$$

$$9 = -\left(\frac{2F}{2T}\right)_{V} \qquad P = -\left(\frac{2F}{2V}\right)_{T}$$

example 2.
$$\left(\frac{25}{2V}\right)_T = \left(\frac{2P}{2T}\right)_V$$

$$= > \left(\frac{25}{2P}\right) = -\left(\frac{2V}{2T}\right)_{P}$$

$$= > \frac{\left(\frac{\partial T}{\partial P}\right)}{\left(\frac{\partial F}{\partial S}\right)_{P}} = \frac{\left(\frac{\partial V}{\partial S}\right)_{P}}{\left(\frac{\partial F}{\partial S}\right)_{P}}$$

Application: Relationship between
$$Cp.Cv.M_T.and L$$
 $Cp = Cv + \begin{pmatrix} \frac{\partial V}{\partial T} \end{pmatrix}_p \begin{bmatrix} \frac{\partial E}{\partial V} \\ \frac{\partial V}{\partial T} \end{bmatrix}_p + P \end{bmatrix}$ (from earlier)

 $dE = TdS - pdV$ (for N)

 $\begin{pmatrix} \frac{\partial E}{\partial V} \end{pmatrix}_T = T \begin{pmatrix} \frac{\partial S}{\partial V} \end{pmatrix}_T - P$
 $T \begin{pmatrix} \frac{\partial S}{\partial V} \end{pmatrix}_T = \begin{pmatrix} \frac{\partial E}{\partial V} \end{pmatrix}_T + P$
 $Cp = Cv + \begin{pmatrix} \frac{\partial V}{\partial T} \end{pmatrix}_P \cdot T \begin{pmatrix} \frac{\partial S}{\partial V} \end{pmatrix}_T$
 $using (a) Markeell relation, example 2)$
 $Cp = Cv + \begin{pmatrix} \frac{\partial V}{\partial T} \end{pmatrix}_P T \begin{pmatrix} \frac{\partial P}{\partial V} \end{pmatrix}_V$
 $use identity: \begin{pmatrix} \frac{\partial V}{\partial T} \end{pmatrix}_P \begin{pmatrix} \frac{\partial P}{\partial V} \end{pmatrix}_V \cdot \begin{pmatrix} \frac{\partial P}{\partial V} \end{pmatrix}_T = -1$ (follows from the excitence of exposure $Cp = Cv - T \begin{pmatrix} \frac{\partial P}{\partial V} \end{pmatrix}_T \begin{pmatrix} \frac{\partial V}{\partial T} \end{pmatrix}_P$
 $using definition:$

$$C_p = C_v + V T \frac{d^2}{K_T}$$

 $C_{\rho} > C_{\nu}$

Thermodynamic Processes

Equilibrium belween Phases (Phase Coexistence)

$$G(T,P,N)$$
 $g=\frac{G}{N}=g(T,P)=G=Ng$

$$G = N_1 g_1 + N_2 g_2$$
 $N = N_1 + N_2 = court$ $dN_2 = dN_1$

$$dG = g, dN, + g_2 dN_2 = (g, -g_2) dN, = 0$$
 at equilibrium

The Clausius - Clapsyron equation

Slangthe coexistance cure: $\Delta g_1 = \Delta g_2$ -3, $\Delta T + V, \Delta P = -3, \Delta T + V_2 \Delta P$ $\Delta P = -3, \Delta T = -3, \Delta T + V_3 \Delta P$ $\Delta P = -3, \Delta T = -3, \Delta T + V_3 \Delta P$ $\Delta P = -3, \Delta T = -3, \Delta T + V_3 \Delta P$ $\Delta P = -3, \Delta T = -3, \Delta T + V_3 \Delta P$ $\Delta P = -3, \Delta T = -3, \Delta T = -3, \Delta T + V_3 \Delta P$ $\Delta P = -3, \Delta T = -3, \Delta$

$$C-C: \frac{\Delta P}{\Delta T} = \frac{S_2 - S_1}{V_2 - N_1}$$

P.f.
$$V_2 - V_1 = V_2 - V_3 \approx V_3$$

$$V_3 \approx \frac{kT}{P_{grs}}$$

$$\frac{dP}{dT} = \frac{q_{ext}}{TkT} \Rightarrow \frac{dP}{P} = \frac{q_{ext}}{k} \frac{dT}{T^2} \Rightarrow \lim_{p \to \infty} \frac{q_e}{kT} + co.$$