Simulating Variable Density Flows in the Low-Mach Number Limit with Incompact3D

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Outline

- Introduction
 - Motivation
 - The Low Mach Number (LMN) approximation
- QuasIncompact3D: LMN in Incompact3D
 - Algorithm to solve LMN
 - Treatment of pressure equation
- Results
 - Scaling on ARCHER and MARCONI
 - · 2D mixing layer
 - Non-Boussinesq gravity currents
- Conclusion

What problem are we trying to solve?

- Incompact3D provides powerful capabilities for solving incompressible flows...
- or flows with small density variations $(\Delta \rho \approx 0.01 \rho_0)$

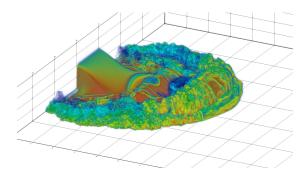


Figure: Gravity-driven flow simulated by Incompact3D¹

¹https://twitter.com/incompact3d

- If density variations are significant, needs to be treated as compressible flow
- Flow velocity may still be low $(\gamma M^2 \ll 1)$
- Results in ill-conditioned equations, e.g.

$$\gamma M^2 \rho \frac{D \boldsymbol{u}}{D t} = -\boldsymbol{\nabla} p + \frac{\gamma M^2}{Re} \boldsymbol{\nabla} \cdot \boldsymbol{\tau}$$

- Numerically this leads to requirement for very small timesteps
 - Inefficient!

The Low Mach Number Approximation

• Expand variables as power series using $\varepsilon = \gamma M^2$ as the small parameter and take lowest order terms (recall $\gamma M^2 \ll 1$)

 $u = u^{(0)} + \varepsilon u^{(1)} + \varepsilon^2 u^{(2)} + \varepsilon^2 u^{(2)}$

$$\begin{split} \boldsymbol{p}^{(0)} &= \boldsymbol{\rho}^{(0)} \boldsymbol{T}^{(0)} \\ \frac{\partial \boldsymbol{\rho}^{(0)}}{\partial t} + \boldsymbol{\nabla} \cdot \boldsymbol{\rho}^{(0)} \boldsymbol{u}^{(0)} &= 0 \\ \boldsymbol{0} &= \boldsymbol{\nabla} \boldsymbol{p}^{(0)} \\ \boldsymbol{\rho}^{(0)} \frac{\partial \boldsymbol{T}^{(0)}}{\partial t} + \boldsymbol{\rho}^{(0)} \boldsymbol{u}^{(0)} \cdot \boldsymbol{\nabla} \boldsymbol{T}^{(0)} &= \frac{\boldsymbol{\nabla} \cdot \boldsymbol{k} \boldsymbol{\nabla} \boldsymbol{T}^{(0)}}{Re Pr \boldsymbol{T}^{(0)}} + \frac{d \boldsymbol{p}^{(0)}}{dt} \\ \frac{\partial \boldsymbol{\rho}^{(0)} \boldsymbol{u}^{(0)}}{\partial t} + \boldsymbol{\nabla} \cdot \boldsymbol{\rho}^{(0)} \boldsymbol{u}^{(0)} \boldsymbol{u}^{(0)} &= -\boldsymbol{\nabla} \boldsymbol{p}^{(1)} + \frac{\boldsymbol{\nabla} \cdot \boldsymbol{\tau}^{(0)}}{Re} \end{split}$$

The Low Mach Number Approximation (cont.)

 Combining continuity and temperature equations yields velocity divergence constraint

$$\nabla \cdot \boldsymbol{u} = \frac{1}{p^{(0)}} \left(\frac{\nabla \cdot k \nabla T}{RePr} - \frac{dp^{(0)}}{dt} \right)$$

Boundary condition follows

$$\int_{\partial\Omega} \mathbf{u} \cdot \widehat{\mathbf{n}} dS = \frac{1}{p^{(0)}} \left(\frac{1}{RePr} \int_{\partial\Omega} k \nabla T \cdot \widehat{\mathbf{n}} dS - \frac{dp^{(0)}}{dt} V_{\Omega} \right)$$

Open domains

$$\frac{dp^{(0)}}{dt}=0\Rightarrow p^{(0)}=p_a$$

Overview

Advance density in time²

$$\rho^{k+1} = \rho^k + \Delta t \nabla \cdot (\rho \mathbf{u})^k$$

• Update temperature via EOS and compute $\nabla \cdot \boldsymbol{u}^{k+1}$

$$T^{k+1} = rac{
ho^{(0)}}{
ho^{k+1}} \Rightarrow oldsymbol{
abla} \cdot oldsymbol{u}^{k+1} = rac{oldsymbol{
abla} \cdot k oldsymbol{
abla} T^{k+1}}{
ho^{(0)} RePr}$$

Integrate momentum via fractional step method³

$$(\rho \mathbf{u})^* = (\rho \mathbf{u})^k - \Delta t \left(\nabla \cdot (\rho \mathbf{u} \mathbf{u})^k - \frac{\nabla \cdot \tau^k}{Re} \right)$$
$$(\rho \mathbf{u})^{k+1} = (\rho \mathbf{u})^* - \Delta t \nabla \widetilde{\rho^{(1)}}^{k+1} \Rightarrow \mathbf{u}^{k+1} = \frac{(\rho \mathbf{u})^{k+1}}{\rho^{k+1}}$$

²Alternative algorithm updates temperature

³Chorin (1997)

Like incompressible approach, take divergence of momentum directly

$$\nabla^{2} \widetilde{p^{(1)}}^{k+1} = \frac{1}{\Delta t} \left(\boldsymbol{\nabla} \cdot (\rho \boldsymbol{u})^{*} - \boldsymbol{\nabla} \cdot (\rho \boldsymbol{u})^{k+1} \right)$$

- + Constant coefficient Poisson equation: direct solvers available
- Need an approximation for $\nabla \cdot (\rho \mathbf{u})^{k+1}$

$$\left| \nabla \cdot (\rho \boldsymbol{u})^{k+1} = -\left. \frac{\partial \rho}{\partial t} \right|^{k+1} \approx -\frac{\rho^{k+1} - \rho^k}{\Delta t} + \mathcal{O}\left(\Delta t\right)$$

Numerical Method

The Poisson Equation - Variable Coefficient

• Alternatively, $\nabla \cdot \boldsymbol{u}^{k+1}$ is available as a constraint⁴

$$\Rightarrow \boldsymbol{\nabla} \cdot \frac{1}{\rho} \widetilde{\boldsymbol{\nabla} \rho^{(1)}}^{k+1} = \frac{1}{\Delta t} \left(\boldsymbol{\nabla} \cdot \boldsymbol{u}^{\star} - \boldsymbol{\nabla} \cdot \boldsymbol{u}^{k+1} \right)$$

- Cannot solve directly using spectral solver
- Iterative solver

$$\begin{split} \nabla^2 \widetilde{\boldsymbol{p}^{(1)}}^{\nu+1} = & \nabla^2 \widetilde{\boldsymbol{p}^{(1)}}^{\nu} + \widetilde{\boldsymbol{\rho}} \left[\frac{1}{\Delta t} \left(\boldsymbol{\nabla} \cdot \boldsymbol{u}^{\star} - \boldsymbol{\nabla} \cdot \boldsymbol{u}^{k+1} \right) - \boldsymbol{\nabla} \cdot \frac{1}{\boldsymbol{\rho}} \boldsymbol{\nabla} \widetilde{\boldsymbol{p}^{(1)}}^{\nu} \right] \\ \left| \left| \Delta \widetilde{\boldsymbol{p}^{(1)}} \right| \right| \leq \text{tol} \end{split}$$

⁴*c.f.* incompressible flow: $\nabla \cdot \mathbf{u} = 0$

Numerical Method

The Poisson Equation - Discussion

Constant coefficient

- + Direct solver → fast solution
- Extrapolation is potential source of error
- Does not recover $\nabla \cdot \boldsymbol{u}^{k+1} = 0$ in inviscid case⁵

Variable coefficient

- + Obeys $\nabla \cdot \boldsymbol{u}^{k+1}$ constraint
- Iteration is potentially very expensive!

⁵Nicoud (2000)

Results Scalability tests

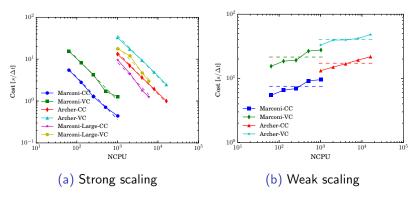


Figure: Strong and weak scaling of QuasIncompact3D, performed on ARCHER and MARCONI with periodic BCs

• Hyperbolic tangent velocity profile

$$u(y) = \frac{u_1 + u_2}{2} + \frac{u_1 - u_2}{2} \tanh\left(\frac{2y}{\delta}\right)$$
 $u_c = \frac{u_1\sqrt{T_2} + u_2\sqrt{T_1}}{\sqrt{T_1} + \sqrt{T_2}} = 0$
 $\frac{T_2}{T_1} = \frac{1}{2}, \frac{dp^{(0)}}{dt} = 0$

- Initial perturbation applied to velocity field to promote transition
- Periodic in x no-slip on y

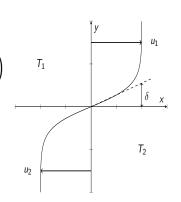


Figure: Diagram of non-isothermal mixing layer

Results

2D Non-Isothermal Mixing Layer - Results (Vorticity)

CC	VC $ ho_0$	VC $ ho_h$	G2005

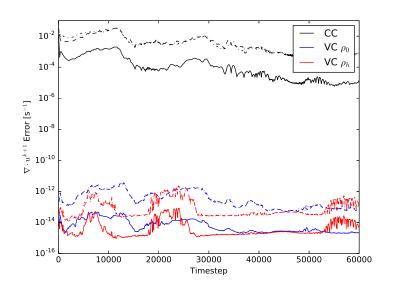
Results

2D Non-Isothermal Mixing Layer - Results (Density)

СС	VC $ ho_0$	VC $ ho_h$	G2005

Results

2D Non-Isothermal Mixing Layer - Results (Error in $\nabla \cdot \boldsymbol{u}^{k+1}$)



Results

2D Non-Isothermal Mixing Layer - Results (Performance Comparison)

Poisson Eq.	CPU / Δ <i>t</i> [s]
CC	4.48×10^{-2}
	$6.16 imes 10^{-1}$
VC ρ_h	3.53×10^{-1}
	Cost (normalised)
CC	1
VC $ ho_0$	13.75
VC ρ_h	7.88
Time (its) in Poisson [%]	
CC	23.4 (1)
VC $ ho_0$	94.2 (34.1)
$VC \rho_h$	89.9 (18.8)

2D Non-Boussinesq Lock-Exchange Problem⁶

- Two fluids of different densities $\rho_2>\rho_1$ horizontally separated in a vertical gravity field
- $\nu_1 = \nu_2 \Rightarrow$ test of variable viscosity implementation
- Results to be validated against data of Birman et al. (2005)

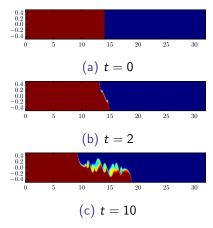


Figure: Lock-exchange $\frac{\rho_2}{\rho_1} = 0.998$

⁶Anecdotally, this case highlights the importance of the guess for $p^{\nu=0}$!

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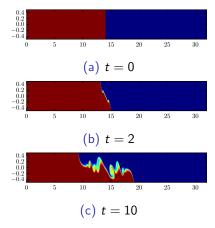


Figure: Lock-exchange
$$\frac{\rho_2}{\rho_1} = 0.92$$

⁷Anecdotally, this case highlights the importance of the guess for $p^{\nu=0}$!

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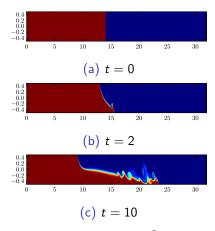


Figure: Lock-exchange $\frac{\rho_2}{\rho_1} = 0.2$

⁸Anecdotally, this case highlights the importance of the guess for $p^{\nu=0}$!

Conclusion and Future Work

- LMN implemented in Incompact3D
- Implemented constant and variable coefficient Poisson solvers
- Proposed new formulation for variable coefficient Poisson solver

- Complete simulation of buoyant, turbulent jets
- Complete validation of non-Boussinesq lock-exchange in 2D
- Investigate 3D non-Boussinesq lock-exchange problem

Thanks for listening!

The Poisson Equation - Variable Coefficient, Choice of $\widetilde{\rho}$

- Free choice of $\widetilde{\rho}$
- Choice of $\widetilde{\rho}$ will affect convergence
- ullet Typical choices are an average or minimum value, $\widetilde{
 ho}=
 ho_0$
 - Stems from 'brute force' derivation of iteration equation
- Chain-rule suggests $\widetilde{\rho}$ should vary in space

$$\nabla \cdot \frac{1}{\rho} \nabla \widetilde{\rho^{(1)}} = \frac{1}{\rho} \nabla^2 \widetilde{\rho^{(1)}} + \nabla \frac{1}{\rho} \cdot \nabla \widetilde{\rho^{(1)}}$$
$$= \frac{1}{\rho} \nabla^2 \widetilde{\rho^{(1)}} + \left(\nabla \cdot \frac{1}{\rho} \nabla \widetilde{\rho^{(1)}} - \frac{1}{\rho} \nabla^2 \widetilde{\rho^{(1)}} \right)$$
$$\Rightarrow \widetilde{\rho} = \left(\frac{1}{\rho} \right)^{-1}$$

+ Harmonic average is proportional to local minimum - promoting stability