Table 1 Selected Distances, Angles, and Torsions for $\bf 1$

Selected Distances (Å)			
Re(1)-C(16)	1.89(1)		
Re(1)- $C(17)$	1.934(8)		
Re(1)- $C(18)$	1.90(1)		
Re(1)- $N(1)$	2.162(6)		
Re(1)-N(2)	2.236(9)		
Re(1)- $Cl(1)$	2.496(2)		
Selected Angles (d	deg)		
C(16)-Re(1)-C(17)	87.6(4)		
C(16)-Re(1)-C(18)	88.3(4)		
C(17)-Re(1)- $C(18)$	87.3(4)		
C(16)-Re(1)-N(1)	96.4(3)		
C(17)-Re(1)-N(1)	174.9(3)		
C(18)-Re(1)-N(1)	95.9(3)		
C(16)-Re(1)-N(2)	169.3(3)		
C(17)-Re(1)-N(2)	101.1(3)		
C(18)-Re(1)-N(2)	98.3(3)		
N(2)-Re(1)-N(1)	74.5(3)		
C(16)-Re(1)-Cl(1)	91.7(3)		
C(17)-Re (1) -Cl (1)	91.7(3)		
C(18)-Re(1)-Cl(1)	179.9(3)		
N(1)-Re (1) -Cl (1)	84.0(2)		
N(2)-Re(1)-Cl(1)	81.6(2)		
O(1)-C(16)-Re(1)	179.6(9)		
O(2)-C(17)-Re(1)	176.0(8)		
O(3)-C(18)-Re(1)	177.3(9)		
Selected Torsions (deg)			
N(1)-C(5)-C(6)-N(2)	16(1)		
N(2)-C(10)-C(11)-N(3)	41(1)		

Table 2 Selected Distances, Angles, and Torsions for ${\bf 2}$

Selected Distances (Å)			
Re(1)-C(16)	1.926(9)		
Re(1)-C17)	1.975(10)		
Re(1)-N(1)	2.119(7)		
Re(1)-N(2)	2.080(7)		
Re(1)-N(3)	2.126(7)		
Re(1)- $Cl(1)$	2.489(3)		
N(1)-N(3)	4.14(1)		
Selected Angles	(deg)		
C(16)-Re(1)- $C(17)$	91.5(4)		
C(16)-Re(1)-N(2)	173.7(4)		
C(17)-Re(1)-N(2)	94.6(3)		
C(16)-Re(1)-N(1)	103.9(3)		
C(17)-Re(1)-N(1)	92.7(3)		
N(2)-Re(1)-N(1)	77.3(3)		
C(16)-Re(1)-N(3)	101.8(3)		
C(17)-Re(1)-N(3)	91.7(3)		
N(2)-Re(1)-N(3)	76.6(3)		
N(1)-Re(1)-N(3)	153.7(3)		
C(16)-Re (1) -Cl (1)	91.8(3)		
C(17)-Re (1) -Cl (1)	176.5(2)		
N(2)-Re(1)-Cl(1)	82.1(2)		
N(1)-Re (1) -Cl (1)	85.4(2)		
N(3)-Re(1)-Cl(1)	88.7(2)		
O(1)-C(16)-Re(1)	177.9(9)		
O(2)-C(17)-Re(1)	173.2(8)		
Selected Torsions (deg)			
N(1)- $C(5)$ - $C(6)$ - $N(2)$	1(1)		
N(2)- $C(10)$ - $C(11)$ - $N(3)$	-4(1)		

 ${\bf Table~3}$ Selected Distances, Angles, and Torsions for ${\bf 3}$

Selected Distances (Å)			
Re(1)-C(16)	1.911(3)		
Re(1)-C(17)	1.890(3)		
Re(1)-C(18)	1.921(4)		
Re(1)-N(1)	2.173(3)		
Re(1)-N(2)	2.232(2)		
Re(1)- $Br(1)$	2.6410(4)		
Selected Angles	(deg)		
C(16)-Re(1)-C(17)	89.1(1)		
C(16)-Re(1)- $C(18)$	85.9(1)		
C(16)-Re(1)-N(1)	97.9(1)		
C(17)-Re(1)-N(1)	92.5(1)		
C(18)-Re(1)-N(1)	175.4(1)		
C(16)-Re(1)-N(2)	171.2(1)		
C(17)-Re(1)-N(2)	96.0(1)		
C(18)-Re(1)-N(2)	101.3(1)		
N(1)-Re(1)-N(2)	74.7(1)		
C(16)-Re(1)-Br(1)	92.7(1)		
C(17)-Re(1)-Br(1)	177.6(1)		
C(18)-Re(1)-Br(1)	91.6(1)		
N(1)-Re (1) -Br (1)	85.74(7)		
N(2)-Re(1)-Br(1)	82.07(7)		
O(1)-C(16)-Re(1)	178.6(3)		
O(2)-C(17)-Re(1)	179.5(3)		
O(3)-C(18)-Re(1)	179.9(3)		
Selected Torsions (deg)			
N(1)-C(6)-C(1)-N(2)	-15.4(4)		
N(2)-C(5)-C(11)-N(3)	141.1(3)		

Table 4 Selected Distances and Angles for ${\bf 5}$

Selected Distances (Å)			
Re(2)-C(35)	1.138(9)		
Re(2)-C(36)	1.926(6)		
Re(2)-C(37)	1.954(7)		
Re(2)-C(38)	1.902(9)		
Re(2)-N(5)	2.242(7)		
Re(2)-N(6)	2.168(5)		
C(35)-N(8)	1.138(9)		
C(36)-O(4)	1.145(8)		
C(37)-O(5)	1.151(9)		
C(38)-O(6)	1.17(1)		
Selected Angles	(deg)		
C(16)-Re(1)-C(17)	91.5(4)		
C(16)-Re(1)-N(2)	173.7(4)		
C(17)-Re(1)-N(2)	94.6(3)		
C(16)-Re(1)-N(1)	103.9(3)		
C(17)-Re(1)-N(1)	92.7(3)		
N(2)-Re(1)-N(1)	77.3(3)		
C(16)-Re(1)-N(3)	101.8(3)		
C(17)-Re(1)-N(3)	91.7(3)		
N(2)-Re(1)-N(3)	76.6(3)		
N(1)-Re(1)-N(3)	153.7(3)		
C(16)-Re(1)-Cl(1)	91.8(3)		
C(17)-Re (1) -Cl (1)	176.5(2)		
N(2)-Re(1)-Cl(1)	82.1(2)		
N(1)-Re (1) -Cl (1)	85.4(2)		
N(3)-Re(1)-Cl(1)	88.7(2)		
O(1)-C(16)-Re(1)	177.9(9)		
O(2)-C(17)-Re(1)	173.2(8)		

Table 5 Selected Distances and Angles for 8.CH3CN

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Selected Distan	ces (Å)			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Re(1)-C(16)	1.889(4)			
$\begin{array}{c} {\rm Re}(1)\text{-N}(2) & 2.135(3) \\ {\rm Re}(1)\text{-N}(3) & 2.131(3) \\ {\rm Re}(1)\text{-N}(4) & 2.160(3) \\ \hline \\ {\rm Selected\ Angles\ (deg)} \\ \hline \\ {\rm C}(16)\text{-Re}(1)\text{-C}(17) & 87.69(16) \\ {\rm C}(16)\text{-Re}(1)\text{-N}(1) & 175.95(12) \\ {\rm C}(17)\text{-Re}(1)\text{-N}(1) & 96.35(12) \\ {\rm C}(16)\text{-Re}(1)\text{-N}(3) & 103.81(13) \\ {\rm C}(17)\text{-Re}(1)\text{-N}(3) & 94.03(12) \\ {\rm N}(1)\text{-Re}(1)\text{-N}(3) & 76.20(10) \\ {\rm C}(16)\text{-Re}(1)\text{-N}(2) & 103.58(13) \\ {\rm C}(17)\text{-Re}(1)\text{-N}(2) & 93.73(12) \\ {\rm N}(1)\text{-Re}(1)\text{-N}(2) & 75.99(10) \\ {\rm N}(3)\text{-Re}(1)\text{-N}(2) & 151.77(11) \\ {\rm C}(16)\text{-Re}(1)\text{-N}(4) & 90.50(14) \\ {\rm C}(17)\text{-Re}(1)\text{-N}(4) & 178.10(12) \\ {\rm N}(1)\text{-Re}(1)\text{-N}(4) & 85.46(10) \\ {\rm N}(3)\text{-Re}(1)\text{-N}(4) & 86.94(10) \\ {\rm N}(2)\text{-Re}(1)\text{-N}(4) & 86.15(10) \\ {\rm O}(1)\text{-C}(16)\text{-Re}(1) & 179.1(3) \\ \hline \end{array}$	Re(1)-C(17)	1.885(3)			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Re(1)- $N(1)$	2.091(3)			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Re(1)-N(2)	2.135(3)			
Selected Angles (deg) C(16)-Re(1)-C(17) 87.69(16) C(16)-Re(1)-N(1) 175.95(12) C(17)-Re(1)-N(1) 96.35(12) C(16)-Re(1)-N(3) 103.81(13) C(17)-Re(1)-N(3) 94.03(12) N(1)-Re(1)-N(3) 76.20(10) C(16)-Re(1)-N(2) 103.58(13) C(17)-Re(1)-N(2) 93.73(12) N(1)-Re(1)-N(2) 75.99(10) N(3)-Re(1)-N(2) 151.77(11) C(16)-Re(1)-N(4) 90.50(14) C(17)-Re(1)-N(4) 85.46(10) N(1)-Re(1)-N(4) 85.46(10) N(2)-Re(1)-N(4) 86.94(10) N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	Re(1)-N(3)	2.131(3)			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Re(1)-N(4)	2.160(3)			
$\begin{array}{llll} C(16)-Re(1)-N(1) & 175.95(12) \\ C(17)-Re(1)-N(1) & 96.35(12) \\ C(16)-Re(1)-N(3) & 103.81(13) \\ C(17)-Re(1)-N(3) & 94.03(12) \\ N(1)-Re(1)-N(3) & 76.20(10) \\ C(16)-Re(1)-N(2) & 103.58(13) \\ C(17)-Re(1)-N(2) & 93.73(12) \\ N(1)-Re(1)-N(2) & 75.99(10) \\ N(3)-Re(1)-N(2) & 151.77(11) \\ C(16)-Re(1)-N(4) & 90.50(14) \\ C(17)-Re(1)-N(4) & 178.10(12) \\ N(1)-Re(1)-N(4) & 85.46(10) \\ N(3)-Re(1)-N(4) & 86.94(10) \\ N(2)-Re(1)-N(4) & 86.15(10) \\ O(1)-C(16)-Re(1) & 179.1(3) \\ \end{array}$	Selected Angle	Selected Angles (deg)			
$\begin{array}{llll} C(17)\text{-Re}(1)\text{-N}(1) & 96.35(12) \\ C(16)\text{-Re}(1)\text{-N}(3) & 103.81(13) \\ C(17)\text{-Re}(1)\text{-N}(3) & 94.03(12) \\ N(1)\text{-Re}(1)\text{-N}(3) & 76.20(10) \\ C(16)\text{-Re}(1)\text{-N}(2) & 103.58(13) \\ C(17)\text{-Re}(1)\text{-N}(2) & 93.73(12) \\ N(1)\text{-Re}(1)\text{-N}(2) & 75.99(10) \\ N(3)\text{-Re}(1)\text{-N}(2) & 151.77(11) \\ C(16)\text{-Re}(1)\text{-N}(4) & 90.50(14) \\ C(17)\text{-Re}(1)\text{-N}(4) & 85.46(10) \\ N(3)\text{-Re}(1)\text{-N}(4) & 86.94(10) \\ N(2)\text{-Re}(1)\text{-N}(4) & 86.15(10) \\ O(1)\text{-C}(16)\text{-Re}(1) & 179.1(3) \\ \end{array}$	C(16)-Re(1)-C(17)	87.69(16)			
C(16)-Re(1)-N(3) 103.81(13) C(17)-Re(1)-N(3) 94.03(12) N(1)-Re(1)-N(3) 76.20(10) C(16)-Re(1)-N(2) 103.58(13) C(17)-Re(1)-N(2) 93.73(12) N(1)-Re(1)-N(2) 75.99(10) N(3)-Re(1)-N(2) 151.77(11) C(16)-Re(1)-N(4) 90.50(14) C(17)-Re(1)-N(4) 178.10(12) N(1)-Re(1)-N(4) 85.46(10) N(3)-Re(1)-N(4) 86.94(10) N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	C(16)-Re(1)-N(1)	175.95(12)			
$\begin{array}{llll} C(17)\text{-Re}(1)\text{-N}(3) & 94.03(12) \\ N(1)\text{-Re}(1)\text{-N}(3) & 76.20(10) \\ C(16)\text{-Re}(1)\text{-N}(2) & 103.58(13) \\ C(17)\text{-Re}(1)\text{-N}(2) & 93.73(12) \\ N(1)\text{-Re}(1)\text{-N}(2) & 75.99(10) \\ N(3)\text{-Re}(1)\text{-N}(2) & 151.77(11) \\ C(16)\text{-Re}(1)\text{-N}(4) & 90.50(14) \\ C(17)\text{-Re}(1)\text{-N}(4) & 178.10(12) \\ N(1)\text{-Re}(1)\text{-N}(4) & 85.46(10) \\ N(3)\text{-Re}(1)\text{-N}(4) & 86.94(10) \\ N(2)\text{-Re}(1)\text{-N}(4) & 86.15(10) \\ O(1)\text{-C}(16)\text{-Re}(1) & 179.1(3) \\ \end{array}$	C(17)-Re(1)-N(1)	96.35(12)			
N(1)-Re(1)-N(3) 76.20(10) C(16)-Re(1)-N(2) 103.58(13) C(17)-Re(1)-N(2) 93.73(12) N(1)-Re(1)-N(2) 75.99(10) N(3)-Re(1)-N(2) 151.77(11) C(16)-Re(1)-N(4) 90.50(14) C(17)-Re(1)-N(4) 178.10(12) N(1)-Re(1)-N(4) 85.46(10) N(3)-Re(1)-N(4) 86.94(10) N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	C(16)-Re(1)-N(3)	103.81(13)			
$\begin{array}{lll} C(16)\text{-Re}(1)\text{-N}(2) & 103.58(13) \\ C(17)\text{-Re}(1)\text{-N}(2) & 93.73(12) \\ N(1)\text{-Re}(1)\text{-N}(2) & 75.99(10) \\ N(3)\text{-Re}(1)\text{-N}(2) & 151.77(11) \\ C(16)\text{-Re}(1)\text{-N}(4) & 90.50(14) \\ C(17)\text{-Re}(1)\text{-N}(4) & 178.10(12) \\ N(1)\text{-Re}(1)\text{-N}(4) & 85.46(10) \\ N(3)\text{-Re}(1)\text{-N}(4) & 86.94(10) \\ N(2)\text{-Re}(1)\text{-N}(4) & 86.15(10) \\ O(1)\text{-C}(16)\text{-Re}(1) & 179.1(3) \\ \end{array}$	C(17)-Re(1)-N(3)	94.03(12)			
$\begin{array}{lll} C(17)\text{-Re}(1)\text{-N}(2) & 93.73(12) \\ N(1)\text{-Re}(1)\text{-N}(2) & 75.99(10) \\ N(3)\text{-Re}(1)\text{-N}(2) & 151.77(11) \\ C(16)\text{-Re}(1)\text{-N}(4) & 90.50(14) \\ C(17)\text{-Re}(1)\text{-N}(4) & 178.10(12) \\ N(1)\text{-Re}(1)\text{-N}(4) & 85.46(10) \\ N(3)\text{-Re}(1)\text{-N}(4) & 86.94(10) \\ N(2)\text{-Re}(1)\text{-N}(4) & 86.15(10) \\ O(1)\text{-C}(16)\text{-Re}(1) & 179.1(3) \\ \end{array}$	N(1)-Re(1)-N(3)	76.20(10)			
$\begin{array}{llll} N(1)\text{-Re}(1)\text{-N}(2) & 75.99(10) \\ N(3)\text{-Re}(1)\text{-N}(2) & 151.77(11) \\ C(16)\text{-Re}(1)\text{-N}(4) & 90.50(14) \\ C(17)\text{-Re}(1)\text{-N}(4) & 178.10(12) \\ N(1)\text{-Re}(1)\text{-N}(4) & 85.46(10) \\ N(3)\text{-Re}(1)\text{-N}(4) & 86.94(10) \\ N(2)\text{-Re}(1)\text{-N}(4) & 86.15(10) \\ O(1)\text{-C}(16)\text{-Re}(1) & 179.1(3) \\ \end{array}$	C(16)-Re(1)-N(2)	103.58(13)			
N(3)-Re(1)-N(2) 151.77(11) C(16)-Re(1)-N(4) 90.50(14) C(17)-Re(1)-N(4) 178.10(12) N(1)-Re(1)-N(4) 85.46(10) N(3)-Re(1)-N(4) 86.94(10) N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	C(17)-Re(1)-N(2)	93.73(12)			
C(16)-Re(1)-N(4) 90.50(14) C(17)-Re(1)-N(4) 178.10(12) N(1)-Re(1)-N(4) 85.46(10) N(3)-Re(1)-N(4) 86.94(10) N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	N(1)-Re(1)-N(2)	75.99(10)			
C(17)-Re(1)-N(4) 178.10(12) N(1)-Re(1)-N(4) 85.46(10) N(3)-Re(1)-N(4) 86.94(10) N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	N(3)-Re(1)- $N(2)$	151.77(11)			
N(1)-Re(1)-N(4) 85.46(10) N(3)-Re(1)-N(4) 86.94(10) N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	C(16)-Re(1)-N(4)	90.50(14)			
N(3)-Re(1)-N(4) 86.94(10) N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	C(17)-Re(1)-N(4)	178.10(12)			
N(2)-Re(1)-N(4) 86.15(10) O(1)-C(16)-Re(1) 179.1(3)	N(1)-Re(1)-N(4)	85.46(10)			
O(1)- $C(16)$ - $Re(1)$ 179.1(3)	N(3)-Re(1)-N(4)	86.94(10)			
	N(2)-Re(1)-N(4)	86.15(10)			
O(2)- $C(17)$ - $Re(1)$ 178.0(3)	O(1)-C(16)-Re(1)	179.1(3)			
	O(2)- $C(17)$ - $Re(1)$	178.0(3)			

Table 6 Selected Distances, Angles, and Torsions for $\kappa^2(\text{terpy})\text{Mn(CO)}_3\text{Br}$ from Compain et. al.

Selected Distances (Å)			
Mn(1)-N(1)	2.045(1)		
Mn(1)-N(2)	2.105(2)		
N(1)-N(2)	2.636(2)		
Selected Angles (deg)			
N(1)-Mn(1)-N(2)	78.84(6)		
Selected Torsions (deg)			
N(1)-C(8)-C(9)-N(2)	-16.5(2)		
N(2)-C(13)-C(14)-N(3)	143.2(2)		

Table 7 Crystal data and structure refinement for compounds 1, 3, 5, and 7

7	5	3	1	Compound
$C_{22}H_{14}N_4O_6F_3SRe$	$C_{20}H_{11}N_4O_3Re$	$C_{19}H_{11}N_3O_3ReBr$	$C_{19}H_{11}N_3O_3ReCl$	Empirical formula
693.63	530.04	583.41	538.96	Formula weight (g/mol)
200	200	200	200(2)	Temperature (K)
0.71073	0.71073	0.71073	0.71073	Wavelength (Å)
	Triclinic	Monoclinic	Triclinic	Crystal System
	P-1	C2/c	P-1	Space Group
	9.9196(9)	31.1537(7)	9.8736(4)	a (Å)
	14.9902(14)	7.1176(2)	14.8202(4)	b (Å)
	16.5187(15)	16.8519(4)	16.3472(4)	c (Å)
	68.363(2)	90.000	69.2890(10)	$\alpha \text{ (deg)}$
	80.929(2)	111.0230(10)	80.801(2)	β (deg)
	79.975(2)	90.000	79.836(2)	$\gamma \; (\deg)$
	2236.6(4)	3488.00	2190.00(12)	Volume (\mathring{A}^3)
	2, 1.927	8, 2.222	2, 1.997	$Z, r (calc) (Mg/m^3)$
	5.821	9.282	6.063	Absorption coefficient (mm ⁻¹)
	Semi-empirical from equivalents			Absorption correction
	R1 = 0.0390, wR2 = 0.0921	R1 = 0.0232, wR2 = 0.0614	R1 = 0.0397, wR2 = 0.0839	Final R indices $[I \ge 2\sigma(I)]$
		R1 = 0.0285, wR2 = 0.0642	R1 = 0.0604, WR2 = 0.0951	R indices (all data)

Table 8 Crystal data and structure refinement for compounds $\mathbf{2},\,\mathbf{4},\,\mathbf{6},\,$ and $\mathbf{8}$

Compound	2	4	6	8
Empirical formula	$\frac{\mathrm{C_{18}H_{11}N_{3}O_{2}ReCl}}$	$\mathrm{C_{18}H_{11}N_3O_2ReBr}$	$C_{19}H_{11}N_4O_2Re$	$\overline{\mathrm{C_{21}H_{14}N_4O_5F_3SRe}}$
Formula weight (g/mol)	510.95	530.04	502.04	665.61
Temperature (K)	200(2)	200	200	200
Wavelength (Å)	0.71073	0.71073	0.71073	0.71073
Crystal System	Triclinic			Triclinic
Space Group	P-1			P-1
a (Å)	8.5275(3)			8.5745(4)
b (Å)	14.2421(5)			11.9805(5)
c (Å)	17.4637(6)			13.0970(5)
$\alpha \text{ (deg)}$	77.948(2)			79.748(2)
β (deg)	85.684(2)			81.106(2)
γ (deg)	79.890			88.091(2)
Volume $(Å^3)$	2041.79(12)			1307.99(10)
$Z, r (calc) (Mg/m^3)$	4, 2.050			2, 1.993
Absorption coefficient (mm ⁻¹)	6.494			5.094
Absorption correction		Semi-empirical fr	om equivalents	
Final R indices $[I \ge 2\sigma(I)]$	R1 = 0.0636, wR2 = 0.1018			R1 = 0.0294, wR2 = 0.0673
R indices (all data)	R1 = 0.0985, wR2 = 0.1110			R1 = 0.0366, wR2 = 0.0700