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CAMVIB originated in early 1980 as a program to transform Cartesian force constants (generated by the HONDO *ab initio* quantum chemistry package) to internal force constants. It was subsequently developed over several years at the University of Cambridge as a more general program for vibrational analysis. The original versions of subroutines BMAT and VIB were derived from programs RELK (L. B. Sims, 1975) and NCRDWDC (H. L. Sellers, L. B. Sims, L. Schafer & D. E. Lewis, *QCPE* 1977, 11, 339) which utilise analytical s-vector expressions (E. B. Wilson, J. C. Decius & P. C. Cross, *Molecular Vibrations*, McGraw-Hill, New York, 1955, pp 54-61) for B-matrix elements to solve the vibrational eigenvector/eigenvalue problem in mass-weighted Cartesian coordinates (W. D. Gwinn, *J. Chem. Phys.* 1971, 55, 477). The present version is dimensioned by using the external CAM_SIZE file, which can be edited to change the number of atoms.

```
! Header file for CAMVIB, CAMISO, LIPFR and UJISO to set array
! sizes as functions of the maximum number of atoms.
!
! 31 April 1997 - AJT
! 16 October 2016 - IHW

    parameter(MAXNAT =1000)
! These should not be touched:
    parameter(MAXNC = MAXNAT * 3)
    parameter(MAXNI = MAXNAT * 3 + MAXNAT / 2)
    parameter(MAXNINT= MAXNC - 6)
    parameter(MAXDIAG= MAXNC * (MAXNC + 1) / 2)
    parameter(MAXAPO = MAXNAT + 1)
! For CAMISO:
    parameter(MAXFCMS = MAXDIAG * 3)
    parameter(MAXXYZ = MAXNAT * 10)
```

Figure 1. The CAM_SIZE file, used to dimension the arrays in CAMVIB, LIPFR, and UJISO. Parameter MAXNAT (currently set at 1000) determines the maximum number of atoms. For most purposes a much smaller number may be chosen.

Many of the options (specified by "keywords") have been incorporated to deal with particular problems arising in the course of the IHW's research group (into force-constant calculations, prediction of vibrational spectra and computation of isotope effects) and will not be required by the "ordinary" user who may simply want to post-process the results of a Cartesian-force-constant calculation performed using some other (probably quantum-chemical) program. What follows consists of two parts. First, a description of the data and the various options available, item by item. Second, sample data files and corresponding output files selected to demonstrate aspects of the "normal" usage of the program. These have been annotated in the hope of clarifying their meaning.

(N.B. In this document the underlining symbol _ is used to denote a blank.).

Overview of CAMVIB input

١.

IPROG - Format (IA4)

May have the following values:

VIB to start a calculation

STOP to finish a calculation

2.

OPTIONS - Format (20(A4, IX)

The following keywords may be specified:

BOHR - Cartesian coordinate input is in atomic units instead of Angstroms.

REDU - a redundant set of valence coordinates is to be supplied, which implies that "symmetry" coordinates are also to be specified.

VALE - valence coordinates are to be input. (Not required if SYMM, REDU, RELX, ININ or INSY is specified.) Valence force constants are computed. If REDU or SYMM is specified, both valence and "symmetry" force constants are computed. Spurious translational and rotational contributions present in the supplied Cartesian force constants to be projected out; transformed Cartesian force constants are then re-computed from the internal force constants. (cf. I. H. Williams, Theochem - J. Mol. Struct. 1983, 11, 275-284).

SYMM - "symmetry" coordinates are to be constructed. (Not required if REDU or INSY is specified.)

IFCS - internal force constants (valence and/or symmetry) are printed out in units of: md/Å for stretching, md.Å /rad² for bending, and md/rad for stretch/bend interactions.

SCAL - valence force constants are to be scaled by a single value.

SCVD - diagonal valence force constants to be scaled individually.

SCVA - all valence force constants to be scaled by Pulay's method (see item 6; cf. P. Pulay, G. Fogarasi, G. Pongor, J. E. Boggs & A. Vargha, JACS, 1983, 105, 7037).

SCSD - diagonal symmetry force constants to be scaled individually (see item 6).

SCSA - all symmetry force constants to be scaled by Pulay's method (see item 6).

VECT - normal coordinates are to be printed out in Cartesian coordinates (both mass-weighted and unweighted). Additionally the normal coordinates are printed out in valence coordinates if VALE is specified or in "symmetry" coordinates if SYMM or REDU is specified, together with an approximate "potential energy distributions". If VECT is not specified frequencies only are computed and printed out.

RELX - compliance constants. relaxed force constants and interaction displacement coordinates are computed. (cf. I. H. Williams, Chem. Phys. Lett. 1982, 88, 462-466).

INCA - Cartesian force constant input: since it is the default, this option never needs to be specified explicitly.

ININ - valence force constant input.

INSY - symmetry force constant input.

OUTC - projected Cartesian force constants are written to channel 12. (Not required if keyword DISO is specified as an option.)

OUTI - valence force constants (unscaled) are written to channel 12.

OUTS - symmetry force constants (unscaled) are written to channel 12.

LINE - molecule is linear (with 3N-5 internal degrees of freedom for N atoms).

PRAX - geometrical coordinates are transformed to a principal-axis system with origin at the centre of mass. (Not normally required.)

MASS - non-standard atomic masses are to be supplied. (Not required if standard isotopic masses for H, Li, Be, B, C, N, O, F, Si, P, S Br Cl are to be used.)

FULL - full printout of all matrices and eigenvectors.

OBSD - calculated frequencies to be compared with supplied observed frequencies and the r.m.s. error computed.

AMPAC - geometry and force constants to be read from logical unit 9 assigned to a file (e.g. filename, RES) generated by a FORCE calculation with the AMPAC (or MOPAC) program.

CADPAC - geometry and force constants to be read from logical unit 9 assigned to a file generated by a SECDER calculation with the CADPAC program using the PUNCH option.

GAUS - Cartesian force constants from a Gaussian job to be read from the standard input using format (3E20.10).

6E16 - Cartesian force constants to be read from the standard input using format (6E16.8). (Not normally used now.)

GRAC - Cartesian force constants from a Grace job to be read from the standard input using format (1X, 3E20.12).

GAMS – Cartesian coordinates to be read from logical unit 73 assigned to a file generated by the GAMESS program. (Not normally used now.)

BREF - minimal printout

NOPR – skips unnecessary computation and printout when valence (or internal) coordinates are not being used in a calculation.

EXPL - symmetry coordinates are to be input explicitly (see item 11).

3.

TITLE - Format (20A4)

- anything you wish, its up to you!

4. Skip to item 5 unless keyword DISO is specified as an option.

IS, IG, IFFREQ - Format (312)

where

IS is the rotational symmetry number

IG is the electronic degeneracy

IFFREQ specifies the number of pre-calculated frequencies to be read (if desired).

5. Skip to item 6 unless keyword MASS is specified as an option.

(Not normally used)

IA, IFK, X, Y, Z, WT - Format (A4, A1, 4F12.6)

where

IA is any symbol you want to denote an atom whose mass is given explicitly.

IFK is a symbol that serves no purpose in CAMVIB but is significant with program CUTOFF.

X,Y,Z are Cartesian coordinates in Ångström units, or in atomic units if BOHR is specified.

WT is a mass in atomic mass units.

*--- ends this section of the data. (N.B. this is a special value for the symbol IA.)

If keyword AMPAC or CADPAC has been specified, then only the isotopic symbols IA are required (one per line): the Cartesian coordinates are read from logical unit 9 and the contents of the present X,Y and Z fields are overwritten.

Skip to item 8 if keyword MASS is specified as an option.

6.

IA, IFK, X, Y, Z - Format (A4, A1, 3E20.10)

where

IA is any symbol you want to denote an atom whose mass is given explicitly.

IFK is a symbol that serves no purpose in CAMVIB but is significant with program CUTOFF.

X,Y,Z are Cartesian coordinates in Ångström units, or in atomic units if BOHR is specified.

*--- ends this section of the data. (N.B. this is a special value for the symbol IA.)

7. (Not normally used)

If keyword AMPA (for AMPAC) is specified as an option, then only the isotopic symbols IA are required (one per line): the Cartesian coordinates are read from logical unit 9 and the contents of the present X, Y and Z fields are overwritten.

TIME, IPT, REFH (Unformatted) – these serve no purpose in CAMVIB

X, Y, Z are Cartesian coordinates in Ångström units, one line for each atom specified in item 6.

Skip to item 10.

8. (Not normally used)

If keyword GAMS (for GAMESS) is specified as an option, then only the isotopic symbols IA are required (one per line): the Cartesian coordinates are read from logical unit 73 and the contents of the present X, Y and Z fields are overwritten.

X, Y, Z are Cartesian coordinates in Ångström units, one line for each atom specified in item 6. Skip to item 10.

9. (Not normally used)

If keyword CADP (for CADPAC) is specified, then only the isotopic symbols IA are required (one per line): the Cartesian coordinates are read from logical unit 9 and the contents of the present X, Y and Z fields are overwritten.

CADTIT - Format(A76) - is a title

SHDG - Format(IX,A4) - is a subheading with the value 'GEOM'

X, Y, Z are Cartesian coordinates in Ångström units, one line for each atom specified in item 6.

SHDG - Format(IX,A4) - is a subheading with the value 'GRAD'

Gx, Gy, Gz – Format(1X,3E20.12) – are components of the gradient, one line for each atom specified in item 6.

SHDG – Format(IX,A4) – is a subheading with the value 'CART'

10. Skip to item 11 unless any of the keywords VALE, REDU, SYMM, ININ, or INSY is specified as an option.

Specification of valence coordinates and implicit symmetry coordinates, one lines for each coordinate.

TYPE, (LIST(1)....LIST(4), SF, SLAB - Format (A1, 413, F10, 3, A4)

where

TYPE denotes the type of valence coordinate specified by the atoms in LIST, and may be one of the following.:

S - stretching of bond LIST(1) - LIST(2):

B - bending of angle LIST(1) - LIST(2) - LIST(3):

W - wagging of LIST(1) out of the plane LIST(2) - LIST(4) - LIST(3). LIST(1) is bonded to the central atom LIST(4). (cf. McIntosh et al., Can. J. Chem. 1978, 56, 1289).

L - bending of collinear atoms LIST(I) - LIST(2) - LIST(3) in the plane of LIST(4); a second valence coordinate for bending of the same three collinear atoms in the plane perpendicular to this is automatically generated. If the molecule itself is linear (rather than just a subsection of atoms being collinear) then keyword LINE must be specified to ensure the correct number of internal coordinates; the molecule must also be aligned along the z-axis. For the linear bending coordinate LIST(4) is given a number of greater than NAT (the number of atoms in the molecule). e.g. LIST(4) = 4 for CO_2 . The two valence coordinates generated are for bending in the xz and yz planes respectively.

T - torsion about bond LIST(1) = LIST(2). (cf. I.H. Williams, J. McKenna & L. B. Sims, J. Mol. Struct. **1979**, 55, 147-150; I. H. Williams, J. Mol. Spectrosc. **1977**, 66, 288-301) N.B. all torsional coordinates

must follow all stretching coordinates in the specification of the valence coordinates: this ensures the complete atomic connectivity table is available for use in generating the 8-matrix elements for torsional coordinates.

SF - is a scaling factor which is ignored unless one of the keywords SCAL, SCVD, SCVA, SCSD or SCSA has been specified. If left blank or input as zero, then a value of unity is printed and assumed. If SCAL has been specified, then only the value of SF associated with the first valence coordinate is significant: this is the factor by which the entire force-constant matrix is to be multiplied. (Note that this is equivalent to multiplying all the vibrational frequencies by the square root of SF.) If SCVD or SCVA has been specified, then the value of SF input for each valence coordinate is significant. SCVD multiplies each diagonal valence force constant by its associated SF value. SCVA not only causes the diagonal valence force constants to be scaled in this manner but also scales the off-diagonal valence force constants: the force constant F(i,j) coupling valence coordinates R(i) and R(j) is scaled by SQRT(SF(i)*SF(j)). This is equivalent to the scaling procedure recommended by Pulay (JACS 1983, 105, 7037).

SLAB - is a symmetry-coordinate label to be supplied if implicit generation of symmetry coordinates is required, *i.e.* if REDU, SYMM or INSY is specified but not EXPL. It is a four character label which may be anything convenient except that certain words, *viz*, TRIG, TET2, TET3 and TBPH, are significant and are interpreted as described under item 6. All three valence coordinates, from which a pair of TRIG symmetry coordinates are to be constructed, should be grouped consecutively (in the order given under item 10) each with SLAB = TRIG. Similarly, all six valence coordinates, from which a set of five TET2 or TET3 symmetry coordinates are to be constructed, should also be grouped consecutively in the order given under item 10.

* - ends this section of the data.

11. Skip to item 12 unless any of the keywords REDU, SYMM, or INSY are specified as options.

WORD, IROW(I)....IROW(NI) - Format(A4, 30I2)

[If necessary, up to four more continuation lines may be supplied:

IROW(I).....IROW(NI) - Format(3012)]

Word is a label for a "symmetry" coordinates constructed as a linear combination of valence coordinates with integral coefficients IROW(1), IROW(2), etc.; e.g. $SDEF_2-1-1$ There are presently four built-in options allowing for implicit generation of sets of symmetry coordinates from valence coordinates specified by unit coefficients in IROW:

TRIG generates coordinates appropriate for a trigonal planar centre, e.g. X=C(Y,Z).

TET2 generates coordinates appropriate for a methylenic centre, e.g. X-CH2-Y.

TET3 generates coordinates appropriate for methyl-like centre, e.g. X-CH3;

TBPH generates coordinates appropriate for a trigonal bipyramidal centre having a symmetry plane containing the equatorial atoms, e.g. A - C(E1,E2,E3) -A'.

If WORD is TRIG then a set of two "symmetry" coordinates is constructed from three valence coordinates in IROW for angle bending in the plane of a trigonal atom,

e.g. TRIG-----I_I_I.

These valence coordinates should be in the order Y-C-Z, X=C-Y, X=C-Z.

A "scissoring" combination and a "rocking" combination are constructed, equivalent to

SCIS-----2-1-1 ROCK-----1-1.

If WORD is TET2 or TET3 then a set of five "symmetry" coordinates is constructed for six valence coordinates in IROW for angle bending about a tetrahedral atom,

These valence coordinates should be in the order X-C-Y, X-C-HI, X-X-H2, Y-C-HI, Y-C-H2, HI-C-H2 for TET2 and X-C-HI, X-C-H2, X-X-H3, HI-C-H2, HI-C-H3, H2-C-H3 for TET3. The resulting "symmetry" coordinates are mutually orthogonal to the redundancy condition calculated for the actual molecular geometry.

Examples of TET2 and TET3 usage are in I. H. Williams, *Chem. Phys. Lett.* **1982**, *88*, 462-466; D. Spangler, I. H. Williams, G. M. Maggiora, *J. Comput. Chem.* **1983**, *4*, 524-541; J. S. Francisco & I. H. Williams, *Mol. Phys.* **1984**, *52*, 743-748.

These valence coordinates should be in the order A-C-El, A-C-E2, A-C-E3, A'-C-E1, A'-C-E2, A'-C-E3, E2-C-E3, E1-C-E3.

The resulting symmetry coordinates are mutually orthogonal to the two redundancy conditions calculated for the actual molecular geometry. Examples of TBPH usage are symmetrical transition structures $[H_2O-CH_3-OH_2]^+$ (I. H. Williams, *Bull. Soc. Chim. Belg.* **1982**, *91*, 356) and $[H_3N-CH_3-NH_3]^+$ (I. H. Williams, *JACS* **1984**, *106*, 7206-7212).

XTRA - calls a user-supplied subroutine (e.g. EX03) to generate a special set of symmetry coordinates (cf. J. S. Francisco & I. H. Williams, Chem. Phys. 1985, 95, 373). Not available in this version of CAMVIB.

If the number of valence coordinates exceeds 30 then the specification of each symmetry coordinate requires more than one line of data; second, third, fourth and fifth lines of data are read with FORMAT 30I2 to complete the array IROW if NI is ≤ 60 , ≤ 90 , ≤ 120 or ≤ 140 as necessary. The total number of symmetry coordinates specified (counting TRIG as two, TET2 and TET3 as five, and TBPH as seven) must equal NINT, the number of independent internal degrees of freedom.

12. Skip to item 13 unless ININ or INSY is specified.

(Not normally used.)

E(1)....E(NFI) - Format (6F12.6)

where

E is a linear array of dimension (3N-6)*(3N-5)/2 (where N is the number of atoms) into which is read the lower triangle of the matrix of valence or symmetry force constants (units of md/Å, md.Å /rad², etc.) generated by a prior run of CAMVIB with OUTI or OUTS specified.

Skip to item 14.

13.

E(1)....E(NFC) - Format (6E12.8) – unless an alternative format is specified, as below.

where

E is a linear array of dimensions 3N*(3N+1)/2 (where N is the number of atoms) into which is read the lower triangle of the Cartesian force constant matrix (units of hartree/bohr²), as computed by an electronic structure code such as GAUSSIAN, CADPAC or GAMESS.

If keyword GAUS (for GAUSSIAN) is specified as an option, then the format is (3E20.10).

If keyword GRAC (for GRACE) is specified as an option, then the format is (1X, 3E20.12).

If keyword 6E16 is specified as an option, then the format is (6E16.8).

14.

Skip to item 16 unless keyword OBSD is specified as an option.

IFR(1)..... IFR(NINT) - Format (2014)

where

IFR is an array containing the ordinal numbers of the calculated frequencies which are to be compared with observed frequencies. Remember that the first six calculated frequencies are the zeroes for translation and rotation, so the first genuine vibrational frequency is number seven.

15.

OBFR(I)....OBFR(NF) - Format (8F10.4)

where

OBFR is an array of values of observed frequencies input in the same order as the calculated frequencies specified by IFR. The number NF is determined by the number of non-zero elements in IFR. The units are cm⁻¹.

16. Go to item 1.

Implementation of the script run_camvib.sh

In order to facilitate the use of CAMVIB, the *run_camvib.sh* script was created. It takes its input from a file containing coordinate and Hessian information, for example, the fort.7 file output from a calculation in Gaussian with the keywords *punch=(coord,derivatives)* specified. Due to the nature of the script, it can be used with output from numerous electronic structure codes, only requiring minor editing in some circumstances.

run_camvib.sh requires the following files to be present, each of which will be described in turn:

fort.7 – the file containing the coordinates, gradient, and hessian from Gaussian.

symm_info.txt – text file with the internal coordinates for the molecule.

vib_header.txt – this text file contains the commands for CAMVIB and can be edited accordingly.

process_crd.awk - AWK script which parses the fort.7 file for coordinate data.

Process_hess.awk - AWK script which parses the fort.7 file for Hessian data.

The script produces the input for CAMVIB, and in the last action, runs the program. The directories used in the script itself will need to be changed in order to reflect those in the user's filesystem, however this is trivial.

Example CAMVIB input file (*.vib)

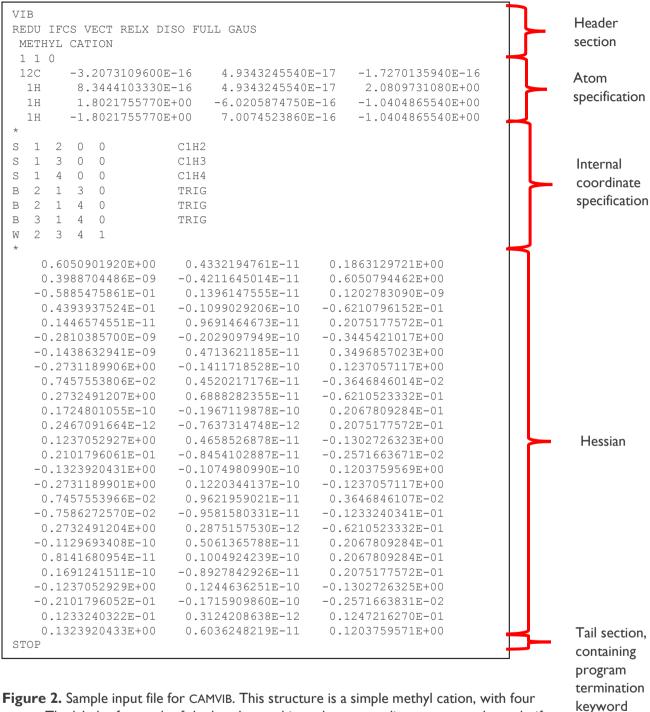


Figure 2. Sample input file for CAMVIB. This structure is a simple methyl cation, with four atoms. The labels after each of the bond-stretching valence coordinates serve only to clarify the output (FULL) of force constants (IFCS) and normal modes (VECT) in the valence-coordinate representation. The Cartesian coordinates and Hessian were obtained from a Gaussian calculation (GAUS) and output from this calculation will be used by UJISO or LIPFR (DISO). Owing to the trigonal planar geometry of this system, the three in-plane H-C-H angles are not independent. There is a local redundancy, which is eliminated by the use of symmetry combinations (rocking and scissoring) generated implicitly in consequence of the keyword REDU and the significant label TRIG after each of these valence coordinates. The sixth independent internal coordinate is the out-of-plane wagging coordinate. Relaxed force constants (and compliance constants) are calculated (RELX).

Overview of CAMVIB output

```
SIZE PRINTOUT
MAXAPO =
MAX ATOMS
               1000
MAX CRT-COORDS 3000
MAX INT-COORDS 3500
MAX DEG-FREE 2994
MAX DIAG/MATRX 4504500
 keywords
OPTIONS SPECIFIED . REDII IFCS VECT RELY DISC FILL GAIS
                                                                                                      title
 METHYL CATION
           MASS
                          X
                                       Y
                                                   7.
                                                        ANGSTROM
   ATOM
                                                                                   Cartesian coordinates
                                               0.000000
                     0.000000
0.000000
1.802176
      C 12.000000
                                   0.000000
0.000000
0.000000
                                      0.000000
 2
       Н
           1.007825
                                                  2.080973
          1.007825
                                                 -1.040487
                        -1.802176
           1.007825
                                      0.000000
                                                 -1.040487
INTERNAL COORDINATES, R
                                                                SCALING
                                                                FACTORS
                                                        no scaling factors specified, so default = 1.0
   1 S 1 STRETCH C 1 - H 2
                                                                    1.000
   2 S 2 STRETCH C 1 - H 3
                                                                    1 000
                    C 1 -
     S 3 STRETCH
                          H 4
                                                                    1.000
   4 B 1 BEND
                    H 2 - C 1 - H 3
                                                                    1.000
                    H 2 - C 1 - H 4
   5
     B 2 BEND
                                                                    1.000
   6 B 3 BEND
                    нз - с1 - н4
                                                                    1.000
      W 1 WAG
                    H 2 - C 1 OUT OF PLANE H 3 - C 1 - H 4
                                                                   1.000
B MATRIX (TRANSFORMATION FROM CARTESIANS TO INTERNALS : R = B * X )
                                                          6
                                                        1.000000
        0.000000 0.000000 -1.000000 0.000000
                                               0.000000
                                                                   0.000000
                                                                             0.000000
                                                                                       0.000000
                            0.500000
        -0.866025
                  0.000000
                                      0.000000
                                                0.000000
                                                         0.000000
                                                                   0.866025
                                                                             0.000000
                                                                                      -0.500000
         0.866025
                  0.000000
                            0.500000
                                      0.000000
                                                0.000000
                                                         0.000000
                                                                             0.000000
                                                                                       0.000000
                                                                   0.000000
         0.720817
                   0.000000
                            0.416164
                                     -0.480544
                                                0.000000
                                                          0.000000
                                                                   -0.240272
                                                                             0.000000
        -0.720817
                  0.000000
                            0.416164
                                      0.480544
                                                0.000000
                                                         0.000000
                                                                   0.000000
                                                                             0.000000
                                                                                       0.000000
                                                          0.000000
        0.000000
                 -1.441633
                            0.000000
                                     0.000000 0.480544
                                                        0.000000
                                                                   0.000000
                                                                             0.480544
                                                                                       0.000000
         0.000000
                  0.000000
                            0.000000
                   0.000000
         0.000000
                            0.000000
        -0.866025
                   0.000000
                            -0.500000
         0 000000
                   0.000000
                            0 000000
                   0.000000
                            -0.416164
        -0 240272
                   0.000000
         0.000000
                   0.480544
                            0.000000
REDUNDANCY CONDITION FOR COORDINATE 6 IS:
 0.0000000 0.0000000 0.0000000 1.0000000 1.0000000 0.0000000
                        elimination of local redundancy: all 3 HCH angles cannot increase together
SYMMETRY COORDINATES SPECIFIED IMPLICITLY
U MATRIX (TRANSFORMATION FROM INTERNAL TO SYMMETRY COORDINATES : S = U \star R )
                     2
                                      4
           C1H2
                 C1H3
                            C1H4
                                     SCIS
                                             ROCK
          1.0000 0.0000 0.0000 0.0000 0.0000
                                                     0.0000
                                   0.0000
S 2
           0.0000
                   1.0000
                            0.0000
                                             0.0000
                                                     0.0000
S 3
           0.0000
                   0.0000
                            1.0000
                                             0.0000
                                                     0.0000
в 1
           0.0000
                   0.0000
                            0.0000
                                    0.8165
                                             0.0000
                                                     0.0000
в 2
                            0.0000 -0.4082
                                            0.7071
           0.0000
                   0.0000
                                                     0.0000
           0.0000
                   0.0000
                            0.0000 -0.4082
                                            -0.7071
                                                     0.0000
В 3
                                   0.0000
           0.0000
                   0.0000
                            0.0000
                                            0.0000
W 1
                                                     1.0000
```

	D SYMMETRY	FORCE CONS	TANTS	(MD/A FOR	STRETCHING,	MD.A/RAD**2	FOR BENDING)		
	1	2		3	4	5	6		
1 2	5.4443		214						
3		42 5.444 42 -0.029		E 444214					
4	0.0535			-0.107172	1.480353				
5	0.0928				-0.000028	1.480321			
6	0.0000				0.000000		1.395748		
JNSCALEI	D VALENCE	FORCE CONS	TANTS	(MD/A FOR	STRETCHING,	MD.A/RAD**2	FOR BENDING)		
	1	2		3	4	5	6	7	
1	5.4443			3	4	5	0	/	
2	-0.0291		314						
3		42 -0.029		5.444314					
4	0.0437			-0.087506	0.986902				
5	0.0437	53 -0.087	505	0.043741	-0.493467	0.986902			
6	-0.0875	0.043	765	0.043765	-0.493435	-0.493435	0.986870		
7	0.0000	0.000	000	0.000000	0.000000	0.000000	0.000000	1.395748	3
ROJECTI	ED CARTESI	AN FORCE CO	NSTAN'	IS (HARTREE	/BOHR**2)				
	1	2	3	4	5	6	7	8	9
1	0.605091								
2	0.000000	0.186316	0.60	5002					
4		0.000000			3914				
5					0.0207	02			
6					0.0000				
7	-0.273119	0.000000				00 -0.003647			
8 9							0.000000		0 100055
10	-0.273119						-0.132403 -0.007593		
11							0.000000		
12	-0.123706						0.012344		0.012490
	10	11	12						
10	0.273242	11	12						
11 12	0.000000	0.020702	0.12	0355					
					OF NORMAL MO	DES			
FREQUEN	CY		MASS-	-WEIGHTED C	ARTESIANS		UNWEIGH	TED CARTES:	IANS
	ATOM	X		Y	Z		X	Y	Z
0.0	0.00								
0.00	1	-0.03	16861	-0.195280	0.795578		-0.017238	-0.091322	0.37204
	2	-0.03		0.079721			-0.017238	0.128644	0.37204
	3		5334	0.019264			0.121564	0.120044	0.61245
	4		5334	-0.268763			0.121564	-0.433694	0.13163
					LINEAR COM		-0.159863	-0.846911	3.45034
	\$0.00 to	zana wali	i	diasts s	ANGULAR COM		-0.427160	-1.078179	0.52110
		-zero vall	162 IL	idicale a	OTTOMICIMOS	m of irans	slational an	u rolatio	nai motio
0.0				0 00::::	0.00000		0.000=00	0 00000	0.000
	1		6003	-0.074116			0.260502	-0.028990	-0.08144
	2		9780	0.289406			0.080685 0.350411	0.390608 0.172044	-0.08144 0.07428
	4		9623	-0.481312			0.350411	-0.649621	-0.23716
	7	0.23	,,,,,,	0.701312	0.113113		0.550411	0.043021	0.23/10
					LINEAR COM	IPONENTS	2.888389	-0.321433	-0.90299
					ANGULAR COM	IPONENTS	-0.974204	-0.834984	1.10141
0.00	000			0.014625	-0.109597		-0.102530	0.004500	-0.03372
0.00	000	-0.33	3223				0 000000	0 010056	0 00077
0.00		-0.33 -0.02		-0.201515	-0.031762		-0.022839	-0.213956	-0.03372
0.00	1	-0.02 -0.13	1511 14097	-0.201515 0.725693	-0.096763		-0.142376	0.770494	-0.10273
0.00	1 2	-0.02	1511 14097	-0.201515	-0.096763				-0.10273
0.0	1 2 3	-0.02 -0.13	1511 14097	-0.201515 0.725693	-0.096763		-0.142376	0.770494	-0.03372 -0.10273 0.03529

continued...

0.0000							
	1	-0.403511	-0.197144	-0.318114	-0.137569	-0.067213	-0.108455
	2	-0.550519	0.131211	-0.092190	-0.647645	0.154359	-0.108455
	3	0.099852	-0.193835	0.283302	0.117468	-0.228033	0.333283
	4	0.099852	-0.108774	-0.467682	0.117468	-0.127964	-0.550193
				LINEAR COMPONENTS	-1.749987	-0.854995	-1.379628
				ANGULAR COMPONENTS	-0.590202	-2.717378	-0.153894
0 0000							
0.0000	1	-0.184633	-0.559950	-0.079541	-0.065090	-0.197402	-0.028041
	2	0.244765	0.277308	-0.023051	0.297749	0.337336	-0.028041
	3	-0.202643	-0.389487	-0.281362	-0.246509	-0.473799	-0.342269
	4	-0.202643	-0.374645	0.235260	-0.246509	-0.455745	0.286187
	-	*******		*******			**
				LINEAR COMPONENTS	-0.800735	-2.428447	-0.344962
				ANGULAR COMPONENTS	-1.377497	1.869360	-0.026851
0.0000							
	1	-0.214206	0.634428	0.054031	-0.081052	0.240057	0.020444
	2	-0.003800	0.713382	0.015658	-0.004961	0.931433	0.020444
	3	-0.091216	-0.035040	-0.034812	-0.119097	-0.045751	-0.045452
	4	-0.091216	-0.126766	0.066128	-0.119097	-0.165512	0.086341
				LINEAR COMPONENTS	-0.928992	2.751455	0.234326
				ANGULAR COMPONENTS	-1.659341	0.365243	0.165951
				III.JODING COMI ONDINI D	1.000011	0.505245	0.100001
1386.0316							
	1	-0.000006	0.000000	0.298533	-0.000002	0.000000	0.090279
	2	0.000014	0.000000	0.087577	0.000015	0.000000	0.091387
	3	-0.373211	0.000000	-0.558845	-0.389446	0.000000	-0.583156
	4	0.373215	0.000000	-0.558859	0.389451	0.000000	-0.583170
				LINEAR COMPONENTS	0.000000	0.000000	0.000000
				ANGULAR COMPONENTS	0.000000	0.000000	0.000000
				zero values	indicate pur	e vibration	al motion
1386.0614							
	1	0.298531	0.000000	0.000006	0.090279	0.000000	0.000002
	2	-0.774327	0.000000	0.000002	-0.808011	0.000000	0.000002
	3	-0.127904	0.000000	-0.373227	-0.133468	0.000000	-0.389463
	4	-0.127890	0.000000	0.373206	-0.133453	0.000000	0.389441
				LINEAR COMPONENTS	0.000000	0.000000	0.00000
				ANGULAR COMPONENTS	0.000000	0.000000	0.000000
1400 1000							
1428.1288	1	0.000000	-0.448609	0.000000	0.000000	-0.143952	0.000000
	2	0.000000	0.515994	0.000000	0.000000	0.571337	0.000000
	3	0.000000	0.515994	0.000000	0.000000	0.571337	0.000000
	4	0.000000	0.515994	0.000000	0.000000	0.571337	0.000000
	4	3.00000	0.010004	0.00000	0.00000	0.0/100/	3.00000
				LINEAR COMPONENTS	0.000000	0.000000	0.000000
				ANGULAR COMPONENTS	0.000000	0.000000	0.000000
3012.3790							
	1	0.000000	0.000000	-0.000006	0.000000	0.000000	-0.000002
	2	0.000000	0.000000	-0.577334	0.000000	0.000000	-0.577334
	3	-0.500008	0.000000	0.288677	-0.500008	0.000000	0.288677
	4	0.500008	0.000000	0.288677	0.500008	0.000000	0.288677
				LINEAR COMPONENTS	0.000000	0.000000	0.000000
				ANGULAR COMPONENTS	0.000000	0.000000	0.000000
				III.OODIII. COMI ONDNI 5	0.00000	0.00000	0.000000
3218.9221							
	1	-0.000116	0.000000	0.334855	-0.000036	0.000000	0.102445
	2	0.000000	0.000000	-0.769371	0.000000	0.000000	-0.812213
	3	0.332922	0.000000	-0.193160	0.351461	0.000000	-0.203916
	4	-0.332521	0.000000	-0.192929	-0.351037	0.00000	-0.203672
				LINEAR COMPONENTS	0.000000	0.000000	0.000000
				ANGULAR COMPONENTS	0.000000	0.000000	0.000000
2010 0000							
3218.9230	1	_0 >>40=7	0 000000	_0 000116	_0 100446	0 000000	_0_000036
	2	-0.334857 0.000952	0.000000	-0.000116 0.000267	-0.102446 0.001005	0.000000	-0.000036 0.000282
	3	0.000952	0.000000	-0.332663	0.001005	0.000000	-0.351187
	4	0.577142	0.000000	0.332797	0.609523	0.000000	0.351329
	4	0.3//3/3	0.00000	0.552151	0.007525	0.00000	0.001029
				LINEAR COMPONENTS	0.000000	0.000000	0.000000
				ANGULAR COMPONENTS	0.000000	0.000000	0.000000
i .							

EQUENCY	(CM-1)	: 0	.00	(0.00	0	.00	0.	.00	C	0.00	(0.00
		VECTOR	P.E.D.	VECTOR	P.E.D.	VECTOR	P.E.D.	VECTOR	P.E.D.	VECTOR	P.E.D.	VECTOR	P.E.I
1	C1H2	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.0
2	C1H3	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.0
3	C1H4	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.
4 5	SCIS ROCK	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.0
6	ROCK	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.00	0.000	0.
REQUENCY	(CM-1)): 138	6.03	138	86.06	142	8.13	3012	2.38	321	18.92	321	18.92
		VECTOR	P.E.D.	VECTOR	P.E.D.	VECTOR	P.E.D.	VECTOR	P.E.D.	VECTOR	P.E.D.	VECTOR	P.E.
1	C1H2	0.001	0.00	0.000	0.00	0.000	0.00	-0.575	0.34	-0.863	0.66	0.000	0.
2	C1H3	-0.001	0.00	0.001	0.00	0.000	0.00	-0.575	0.34	0.432	0.17	0.747	0.
3	C1H4	-0.001	0.00	-0.001	0.00	0.000	0.00	-0.575	0.34	0.431	0.17	-0.748	0.
4	SCIS	0.437	0.25	0.757		0.000	0.00	0.000	0.00	0.050	0.00	-0.086	0.
5 6	ROCK	0.757	0.75	-0.437 0.000	0.25 0.00	0.000 0.928	0.00	0.000	0.00	0.086	0.00	0.050	0.
	RY COM							2/MD.A FOI					
		1	2	- (/	3	4		5	6				
1		.183947	4		J	4		J	O				
			0 10	2010									
2		.000859		3948	0 100040								
3		.000859		0859	0.183948								
4		.006628	-0.00		0.013255		76954						
5	-0	.011480		1480	0.000002		00013	0.67696					
6	0	.000000	0.00	00000	0.000000	0.0	00000	0.00000	ο.	716462			
					STANTS (D ES (OFF-D								
INTERAC	CTION I	DISPLACI 1							6				
INTERAC	CTION 1	DISPLACE 1 .436340	EMENT CC	ORDINATE	ES (OFF-D	IAGONAL		TS)	6				
INTERAC 1 2	CTION 1 5 0	DISPLACE 1 .436340 .004668	EMENT CC 2 5.43	OORDINATE	ES (OFF-D	IAGONAL 4		TS)	6				
INTERAC 1 2 3	5 0	DISPLACE 1 .436340 .004668 .004668	2 5.43 0.00	00RDINATE 36320 94670	3 5.436320	IAGONAL 4	ELEMEN'	TS)	6				
INTERAC 1 2 3 4	5 0 0 -0	DISPLACE 1 .436340 .004668 .004668	5.43 0.00	00RDINATE 86320 94670 99787	3 5.436320 0.019580	IAGONAL 4 1.4	ELEMEN'	TS) 5					
INTERAC 1 2 3 4 5	5 0 0 -0	1 .436340 .004668 .004668 .009791 .016957	5.43 0.00 -0.00 0.01	6320 4670 9787 6958	3 5.436320 0.019580 0.000004	1.4 0.0	ELEMEN' 77206 00019	5 5 1.47717	3				
1 2 3 4 5 6	5 0 0 -0 -0	1 .436340 .004668 .004668 .009791 .016957	5.43 0.00 -0.00 0.01	36320 94670 99787 6958	3 5.436320 0.019580 0.000004 0.000000	1.4 0.0 0.0	ELEMEN' 77206 00019	5 1.477173 0.000000	3 1.	395748			
1 2 3 4 5 6	5 0 0 -0 -0 0 COMP:	1 .436340 .004668 .004668 .009791 .016957 .000000	5.43 0.00 -0.00 0.01 0.00	36320 94670 99787 6958	S.436320 0.019580 0.000004 0.000000 FOR STRE	1.4 0.0 0.0	ELEMEN' 77206 00019	5 1.47717; 0.000000	3 0 1. BENDIN	395748 G)	7		
1 2 3 4 5 6	5 0 0 0 0 0 COMP	1 .436340 .004668 .004668 .009791 .016957 .000000	5.43 0.00 -0.00 0.01	36320 94670 99787 6958	3 5.436320 0.019580 0.000004 0.000000	1.4 0.0 0.0	ELEMEN' 77206 00019	5 1.477173 0.000000	3 1.	395748 G)	7		
1 2 3 4 5 6 ALENCE	5 0 0 0 0 0 COMP:	1 .436340 .004668 .004668 .009791 .016957 .000000 LIANCE (1 .183947	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT	36320 04670 19787 6958 10000 CS (A/MD	S.436320 0.019580 0.000004 0.000000 FOR STRE	1.4 0.0 0.0	ELEMEN' 77206 00019	5 1.47717; 0.000000	3 0 1. BENDIN	395748 G)	7		
1 2 3 4 5 6 ALENCE 1 2	5 0 0 0 0 COMP:	1 .436340 .004668 .004668 .009791 .016957 .000000 LIANCE (1 .183947 .000859	2 5.43 0.000 -0.00 0.01 0.00 CONSTANT 2 0.18	36320 14670 19787 16958 10000 CS (A/MD	3 5.436320 0.019580 0.000004 0.000000 FOR STRE	1.4 0.0 0.0 TCHING,	ELEMEN' 77206 00019	5 1.47717; 0.000000	3 0 1. BENDIN	395748 G)	7		
1 2 3 4 5 6 ALENCE 1 2 3	5 0 0 0 0 COMP:	1 .436340 .004668 .009791 .016957 .000000 LIANCE (1 .183947 .000859 .000859	2 5.43 0.000 -0.000 0.01 0.000 CONSTANT 2 0.18 0.000	86320 94670 99787 6958 90000 PS (A/MD	3 5.436320 0.019580 0.000004 0.000000 FOR STRE 3 0.183948	1.4' 0.0' 0.0' TCHING,	77206 00019 00000 RAD**2	5 1.47717; 0.000000	3 0 1. BENDIN	395748 G)	7		
1 2 3 4 5 6 ALENCE 1 2 3 4 4	5 0 0 0 0 0 COMP:	1 .436340 .004668 .009791 .016957 .000000 LIANCE (1 .183947 .000859 .000859 .005412	5.43 0.000 -0.000 0.01 0.000 CONSTANT 2 0.18 0.000 -0.000	86320 94670 99787 6958 90000 CS (A/MD	3 5.436320 0.019580 0.000000 FOR STRE 3 0.183948 0.010823	1.4' 0.00 TCHING, 4	77206 00019 00000 RAD**2	5 1.47717; 0.0000000/MD.A FOR 5	3 0 1. BENDIN	395748 G)	7		
1 2 3 4 5 6 ALENCE 1 2 3	5 0 0 0 0 0 COMP:	1 .436340 .004668 .009791 .016957 .000000 LIANCE (1 .183947 .000859 .000859	5.43 0.000 -0.000 0.01 0.000 CONSTANT 2 0.18 0.000 -0.000	86320 94670 99787 6958 90000 CS (A/MD	3 5.436320 0.019580 0.000004 0.000000 FOR STRE 3 0.183948	1.4' 0.00 TCHING, 4	77206 00019 00000 RAD**2	5 1.47717; 0.000000	3 0 1. BENDIN	395748 G)	7		
1 2 3 4 5 6 ALENCE 1 2 3 4 4	5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 .436340 .004668 .009791 .016957 .000000 LIANCE (1 .183947 .000859 .000859 .005412	5.43 0.000 -0.000 0.01 0.000 CONSTANT 2 0.18 0.000 -0.000	06320 44670 99787 6958 00000 CS (A/MD	3 5.436320 0.019580 0.000000 FOR STRE 3 0.183948 0.010823	1.4 0.0 0.0 TCHING, 4	77206 00019 00000 RAD**2	5 1.47717; 0.0000000/MD.A FOR 5	3 1. BENDIN 6	395748 G)	7		
1 2 3 4 5 6 ALENCE 1 2 3 4 5 5	COMP: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 .436340 .004668 .009791 .016957 .000000 LIANCE (1 .183947 .000859 .000842 .005412 .010823	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT 2 0.18 0.00 -0.00 0.01 -0.00	36320 44670 99787 6958 990000 CS (A/MD 33948 99859 95410 9823	3 5.436320 0.019580 0.000004 0.000000 FOR STRE 3 0.183948 0.010823 -0.005410 -0.005413	1.4 0.0 0.0 TCHING, 4	77206 00019 00000 RAD**2	5 1.47717: 0.000000 /MD.A FOR 5	3 1. BENDIN 6	395748 G)		462	
1 2 3 4 5 6 ALENCE 1 2 3 4 5 6 7 RELAXEI	CTION 1 5 0 0 -0 0 COMP: 0 0 0 0 0 0 0 0 0 0 0 0 0	1 .436340 .004668 .009791 .016957 .000000 .LIANCE (1 .183947 .000859 .005412 .005412 .010823 .000000 .ARY VALI	2 5.43 0.000 -0.000 0.01 0.000 CONSTANT 2 0.18 0.000 -0.000 0.01 -0.000 0.01 -0.000	36320 04670 19787 6958 00000 2S (A/MD 33948 10859 15410 10823 15413	3 5.436320 0.019580 0.000004 0.000000 FOR STRE 3 0.183948 0.010823 -0.005410 -0.005413	1.4' 0.0' 0.0' TCHING, 4 0.4' -0.2' -0.2' 0.0'	77206 00019 00000 RAD**2 51302 225644 25659 00000 ELEMEN'	1.47717: 0.000000 /MD.A FOR 5 0.45130: -0.22565: 0.000000 TS) AND	3 1. BENDIN 6	395748 G) 451317		462	
1 2 3 4 5 6 ALENCE 1 2 3 4 4 5 6 7 RELAXEI	COMP: CO	1 .436340 .004668 .009791 .016957 .000000 .11ANCE (1.183947 .000859 .0005412 .005412 .010823 .000000 .ARY VALIDISPLACE	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT 2 0.18 0.00 -0.00 0.01 -0.00 0.01 -0.00 0.00 2 ENCE FC	36320 04670 19787 6958 00000 2S (A/MD 33948 10859 15410 10823 15413	3 5.436320 0.019580 0.000000 FOR STRE 3 0.183948 0.010823 -0.005413 0.000000 STANTS (D	1.4' 0.0' 0.0' TCHING, 4 0.4' -0.2' -0.2' 0.0'	77206 00019 00000 RAD**2 51302 225644 25659 00000 ELEMEN'	1.47717: 0.000000 /MD.A FOR 5 0.45130: -0.22565: 0.000000 TS) AND	3 1. BENDIN 6	395748 G) 451317 000000		462	
INTERAC 1 2 3 4 5 6 ALENCE 1 2 3 4 5 6 7 RELAXEI INTERAC	COMP: CO	DISPLACE 1 .436340 .004668 .009791 .016957 .000000 LIANCE (1 .183947 .000859 .005412 .005412 .005412 .005412 .010823 .000000 ARY VALIDISPLACE 1 .436340	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT 2 0.18 0.00 -0.00 0.01 -0.00 0.00 0.00 ENCE FC	36320 14670 19787 16958 100000 100000 100000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 1000000 1000000 100000 100000 100000 10000000 1000000 100000 1000	3 5.436320 0.019580 0.000000 FOR STRE 3 0.183948 0.010823 -0.005410 0.000000 STANTS (DES (OFF-D	1.4 0.0 0.0 TCHING, 4 0.4 -0.2 -0.2 0.0	77206 00019 00000 RAD**2 51302 225644 25659 00000 ELEMEN'	1.47717; 0.000000 /MD.A FOR 5 0.45130; -0.22565; 0.000000	3 1. BENDIN 6	395748 G) 451317 000000	0.716	462	
1 2 3 4 5 6 ALENCE 1 2 3 4 5 6 7 RELAXEI INTERAC	COMP: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 .436340 .004668 .004668 .009791 .016957 .000000 .11ANCE (1 .183947 .000859 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .000000 .005412 .000000 .000000 .000000 .000000 .000000	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT 2 0.18 0.00 -0.00 0.01 -0.00 0.01 -2.00 0.00 CONSTANT 2 5.43	36320 36320 364670 99787 .6958 30000 CS (A/MD 33948 30823 .55413 .0000 CRCE CONS ORDINATE	SES (OFF-D 3 5.436320 0.019580 0.000004 0.000000 FOR STRE 3 0.183948 0.010823 -0.005410 -0.005413 0.000000 STANTS (D ES (OFF-D 3	1.4 0.0 0.0 0.0 TCHING, 4 0.4 -0.2 -0.2 0.0 1AGONAL 1AGONAL	77206 00019 00000 RAD**2 51302 225644 25659 00000 ELEMEN'	1.47717; 0.000000 /MD.A FOR 5 0.45130; -0.22565; 0.000000	3 1. BENDIN 6	395748 G) 451317 000000	0.716	462	
1 2 3 4 5 6 ALENCE 1 2 3 4 4 5 6 7 RELAXEI	COMP: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 .436340 .004668 .004668 .009791 .016957 .000000 .11ANCE (1 .183947 .000859 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .010823 .000000 .005412 .000000 .005412 .000000 .000000 .000000 .000000 .000000	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT 2 0.18 0.00 -0.00 0.01 -0.00 0.01 -2.00 0.00 CONSTANT 2 5.43	36320 36320 364670 99787 .6958 30000 CS (A/MD 33948 30823 .55413 .0000 CRCE CONS ORDINATE	3 5.436320 0.019580 0.000000 FOR STRE 3 0.183948 0.010823 -0.005410 0.000000 STANTS (DES (OFF-D	1.4 0.0 0.0 0.0 TCHING, 4 0.4 -0.2 -0.2 0.0 1AGONAL 1AGONAL	77206 00019 00000 RAD**2 51302 225644 25659 00000 ELEMEN'	1.47717; 0.000000 /MD.A FOR 5 0.45130; -0.22565; 0.000000	3 1. BENDIN 6	395748 G) 451317 000000	0.716	462	
1 2 3 4 5 6 ALENCE 1 2 3 4 5 5 6 7 RELAXEI INTERAC	COMP: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 .436340 .004668 .009791 .016957 .000000	2 5.43 0.000 0.01 0.00 0.00 0.01 0.00 0.00 0.	36320 14670 19787 16958 100000 100000 100000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 1000000 100000 100000 100000 1000000 1000000 100000 100000 100000 10000000 1000000 100000 1000	SES (OFF-D 3 5.436320 0.019580 0.000004 0.000000 FOR STRE 3 0.183948 0.010823 -0.005410 -0.005413 0.000000 STANTS (D ES (OFF-D 3	1.4' 0.00 0.00 TCHING, 4 0.40.20.2. 0.00 IAGONAL 1AGONAL	77206 00019 00000 RAD**2 51302 25644 25659 00000 ELEMEN' ELEMEN'	1.47717; 0.000000 /MD.A FOR 5 0.45130; -0.22565; 0.000000	3 1. BENDIN 6	395748 G) 451317 000000	0.716	462	
1 2 3 4 5 6 ALENCE 1 2 3 4 5 6 6 7 RELAXEI INTERAC	COMP: CO	1 .436340 .004668 .009791 .016957 .000000	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT 2 0.18 0.00 0.01 -0.00 0.01 -0.00 0.01 -0.00 0.01 -0.00 0.00	00RDINATE 06320 04670 09787 06958 00000 0S (A/MD 083948 00859 05410 00823 05413 00000 0RCE CONS 00RDINATE	3 5.436320 0.019580 0.000000 FOR STRE 3 0.183948 0.010823 -0.005410 0.005413 0.000000 STANTS (DES (OFF-D 3 5.436320 0.023981	1.4' 0.0' 0.0' TCHING, 4 0.4' -0.2' -0.2' 0.0' IAGONAL IAGONAL 4 2.2'	77206 00019 00000 RAD**2 51302 25644 25659 00000 ELEMEN' ELEMEN'	1.47717; 0.000000 /MD.A FOR 5 0.45130; -0.22565; 0.000000	3 0 1. BENDIN 6 2 9 0. 0 0.	395748 G) 451317 000000	0.716	462	
1 2 3 4 5 6 ALENCE 1 2 3 4 4 5 6 6 7 RELAXEI INTERAC	COMP: CO	1 .436340 .004668 .009791 .016957 .000000 .1ANCE (1 .183947 .000859 .0005412 .010823 .000000 .ARY VALID DISPLACE .010823 .0004668 .004668 .004668 .001991 .011991	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT 2 0.18 0.00 -0.00 0.01 -0.00 0.01 -0.00 2 ENCE FC 2 5.43 0.00 -0.01 0.02	33948 30859 35410 308CE CONS 300RDINATE	STANTS (DES (OFF-D 3 3)	1.4 0.0 0.0 TCHING, 4 0.4 -0.2 -0.2 0.0 IAGONAL 1AGONAL 4	77206 00019 00000 RAD**2 51302 25644 25659 00000 ELEMEN' ELEMEN'	1.47717; 0.000000 /MD.A FOR 5 0.45130; -0.22565; 0.000000 TS) AND TS) 5	3	395748 G) 451317 000000	0.716	462	
1 2 3 4 5 6 ALENCE 1 2 3 4 5 6 7 7 RELAXEI INTERAC	COMP: CO	1 .436340 .004668 .009791 .016957 .000000 .1ANCE (1 .183947 .000859 .0005412 .010823 .000000 .ARY VALI .010823 .000000 .436340 .004668 .004668 .004668 .004991 .011991 .023981	2 5.43 0.00 -0.00 0.01 0.00 CONSTANT 2 0.18 0.00 -0.00 0.01 -0.00 0.01 -0.00 2 5.43 0.00 -0.01 0.02 -0.01	36320 44670 99787 6958 90000 7S (A/MD 33948 90859 95410 90823 95413 900000 900000 900000 90000 90000 90000 90000 90000 90000 90000 90000 90000 90000 900000 90000 90000 90000 90000 90000 90000 90000 90000 90000 900000 900000 900000 9000000	SES (OFF-D 3 5.436320 0.019580 0.000004 0.000000 FOR STRE 3 0.183948 0.010823 -0.005410 -0.005413 0.000000 STANTS (D ES (OFF-D 3 5.436320 0.023981 -0.011987 -0.011994	1.4 0.0 0.0 TCHING, 4 0.4 -0.2 -0.2 0.0 IAGONAL 1AGONAL 4	77206 00019 00000 RAD**2 51302 25644 25659 00000 ELEMEN' 15809 99984 00000	1.47717: 0.000001 /MD.A FOR 5 0.45130: -0.22565: 0.0000001 TS) AND TS)	3 0 1. BENDIN 6 2 9 0. 0 0.	395748 G) 451317 000000	0.716· 7		

Figure 3. Annotated sample output file for CAMVIB calculation on methyl cation corresponding to the input file shown in Figure 2.