

INSTITUT FRESNEL

PATRICK C. CHAUMET

DANIEL SENTENAC

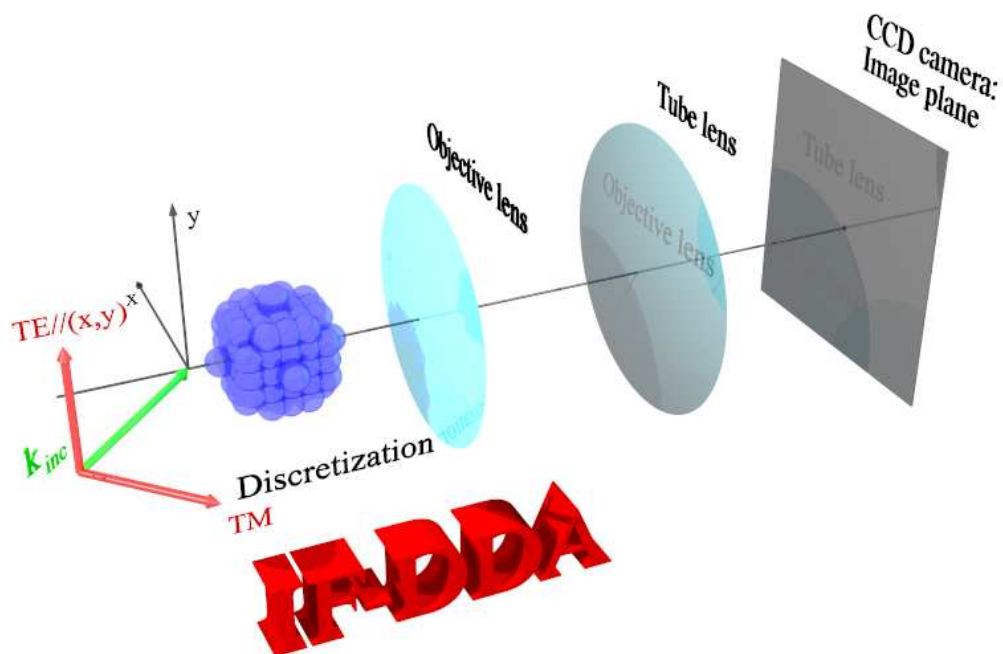
ANNE SENTENAC

---

## IF-DDA

Idiot Friendly-Discrete Dipole  
Approximation

---



---

# Contents

---

<b>List of figures</b>	<b>v</b>
<b>1 Generality</b>	<b>1</b>
1.1 Introduction . . . . .	1
1.2 The principle of discrete dipole approximation . . . . .	2
1.3 A word about the code . . . . .	3
1.4 How to compile the code . . . . .	3
1.5 A word about the authors . . . . .	4
1.6 Licence . . . . .	4
1.7 How to quote the code . . . . .	4
<b>2 Approximated method</b>	<b>6</b>
2.1 Introduction . . . . .	6
2.2 Approximated method . . . . .	8
2.2.1 Born . . . . .	8
2.2.2 Renormalized Born . . . . .	8
2.2.3 Born at the order 1 . . . . .	8
2.2.4 Rytov . . . . .	8
2.2.5 Renormalized Rytov . . . . .	8
2.2.6 Beam propagation method (BPM) . . . . .	9
2.2.7 Renormalized BPM . . . . .	9
<b>3 Numerical details</b>	<b>10</b>
3.1 Polarizability . . . . .	10
3.2 Correction to the tensor of susceptibility . . . . .	11
3.3 Solve the system of linear equation . . . . .	11
<b>4 Managing of the configurations</b>	<b>13</b>
4.1 Introduction . . . . .	13
4.2 Creation and saving of a new configuration . . . . .	13
4.3 Managing of the configurations . . . . .	13
<b>5 Properties of the illumination</b>	<b>14</b>
5.1 Introduction . . . . .	14
5.2 Beam . . . . .	14
5.2.1 Introduction . . . . .	14
5.2.2 Linear plane wave . . . . .	15

5.2.3	Circular plane wave	16
5.2.4	Multiplane wave	16
5.2.5	Antenna	16
5.2.6	Linear Gaussian	16
5.2.7	Circular Gaussian	17
5.2.8	Circular and linear Gaussian (FFT)	17
5.2.9	Linear Gaussian (para)	17
5.2.10	Circular Gaussian (para)	18
5.2.11	Arbitrary wave	18
<b>6</b>	<b>Definition of the object</b>	<b>20</b>
6.1	Introduction	20
6.2	Type of the object	20
6.2.1	Sphere	21
6.2.2	Inhomogeneous sphere	21
6.2.3	Random sphere (length)	22
6.2.4	Random sphere (meshsize)	22
6.2.5	Cube	23
6.2.6	Cuboid (length)	23
6.2.7	Cuboid (meshsize)	23
6.2.8	Inhomogeneous Cuboid (length)	24
6.2.9	Inhomogeneous Cuboid (meshsize)	24
6.2.10	Ellipsoid	24
6.2.11	Several spheres	25
6.2.12	Cylinder	25
6.2.13	concentric spheres	25
6.2.14	Arbitrary object	25
6.3	Choose the relative permittivity	26
6.4	Choose the discretization	27
<b>7</b>	<b>Possible study with the code</b>	<b>28</b>
7.1	Introduction	28
7.2	Study in far field	29
7.3	Microscopy	30
7.4	Study in near field	31
7.5	Optical force and torque	32
<b>8</b>	<b>Representation of the results</b>	<b>33</b>
8.1	Introduction	33
8.2	Digital exits	33
8.3	Graphics	34
8.3.1	Plot epsilon/dipoles	34
8.3.2	Far field and microscopy	34
8.3.2.1	Plot Poynting vector	34
8.3.2.2	Plot microscopy	35
8.3.3	Study of the near field	35
8.3.4	optical force and torque	35
<b>9</b>	<b>Ouput files for matlab, octave, scilab,...</b>	<b>36</b>
9.1	Introduction	36
9.2	List of all exit files	37

---

<b>10 Some examples</b>	<b>39</b>
10.1 Introduction . . . . .	39
10.2 Test1 . . . . .	39
10.3 Test2 . . . . .	43
10.4 Test3 . . . . .	46
10.5 Test4 . . . . .	47
<b>Bibliography</b>	<b>49</b>

---

# List of Figures

---

1.1	Principle of the DDA : the object under study (on the left) is discretized in a set of small dipoles (on the right)l. . . . .	2
5.1	Definition of the beam's direction . . . . .	15
5.2	Definition of the beam's polarization. . . . .	15
6.1	Definition of the angles of Euler according to the convention $Z - X - Z$ . Scheme taken from Wikipedia . . . . .	21
7.1	Simplified figure of the microscope. The object focus of the objective lens is at the origin of the frame. The axis of the lens is confounded with the $z$ axis and at the side of the positive $z$ . . . . .	30
10.1	Test1: configuration taken. . . . .	40
10.2	Modulus of the local field in $(x, y)$ plane. . . . .	40
10.3	Modulus of the macroscopic field in $(x, y)$ plane. . . . .	41
10.4	Modulus of the Poynting vector. . . . .	41
10.5	Optical force in the $(x, y)$ plane and in 3D. . . . .	42
10.6	Optical torque in the $(x, y)$ plane and in 3D. . . . .	42
10.7	Microscopy in transmission: Modulus of the diffracted field in the Fourier plane (left), modulus of the diffracted field in the image plane (middle), and modulus of the total field in the image plane (right). . . . .	42
10.8	Test2: configuration taken. . . . .	43
10.9	Object in 3D (left) and map of permittivity in the $(x, y)$ plane (right). . . .	43
10.10	Modulus of the incident field in $(x, y)$ plane. . . . .	44
10.11	Modulus of the local field in $(x, y)$ plane. . . . .	44
10.12	Modulus of the macroscopic field in $(x, y)$ plane. . . . .	45
10.13	Modulus of the Poynting vector. . . . .	45
10.14	Microscopy in reflection: Modulus of the diffracted field in the Fourier plane (left) and in image plane (right). . . . .	46
10.15	Test3: configuration taken. . . . .	46
10.16	Microscopy in transmission: incident taken to make the image (left). Modulus of the diffracted field in the image plane (middle), and modulus of the total field in the image plane (right). . . . .	47
10.17	Test4: configuration taken. . . . .	47
10.18	Microscope in reflection: incident taken to make the image (left). Modulus of the diffracted field in the image plane (right). . . . .	48

# Generality

---

## Contents

<b>1.1</b>	<b>Introduction</b>	<b>1</b>
<b>1.2</b>	<b>The principle of discrete dipole approximation</b>	<b>2</b>
<b>1.3</b>	<b>A word about the code</b>	<b>3</b>
<b>1.4</b>	<b>How to compile the code</b>	<b>3</b>
<b>1.5</b>	<b>A word about the authors</b>	<b>4</b>
<b>1.6</b>	<b>Licence</b>	<b>4</b>
<b>1.7</b>	<b>How to quote the code</b>	<b>4</b>

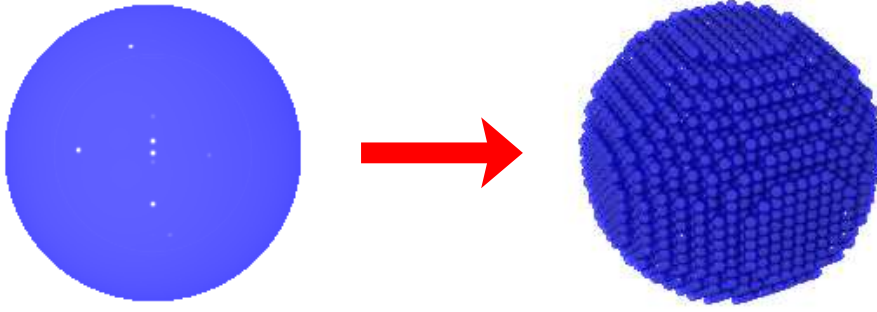
---

## 1.1 Introduction

This software computes the diffraction of an electromagnetic wave by a three-dimensional object. This interaction is taken into account rigorously by solving the Maxwell's equations, but can also do with the approximation of Born, Rytov or the BPM. The code has an user-friendly interface and allows you to choose canonical objects (sphere, cube, ...) as well as predefined incident waves (plane wave, Gaussian beam, ...) or arbitrary objects and incident waves. After by drop-down menus, it is easy to study cross sections, optical forces and torques, diffraction near field and far field as well as microscopy.

There are numerous methods that enable the study of the diffraction of an electromagnetic wave by an object of arbitrary form and relative permittivity. We are not going here to set up an exhaustive list of these methods, but the curious reader may refer to the article by F. M. Kahnert who details the advantages and weaknesses of the most common methods.<sup>1</sup>

The method we use is called coupled dipoles method (CDM) or the discrete dipole approximation (DDA). This method is a volume method, because the diffracted field is obtained from an integral, the support of which is the volume of the considered object. It had been introduced by E. M. Purcell and C. R. Pennypacker in 1973, in order to study the scattering of light by grains in interstellar medium.<sup>2</sup> The DDA has been subsequently widened to objects in presence of a plane substrate or in a multilayer system, see for instance Ref. [3]. These past few years, we endeavoured, on the one hand, to widen the DDA to more complex geometries (grating with or without any default) and, on the other hand, to increase its precision. These improvements tend to make this chapter a little technical, but they are going to be applied in the next chapters. Before studying more in details the last improvements of DDA, though, let us remind first of its principle.



**Figure 1.1 :** *Principle of the DDA : the object under study (on the left) is discretized in a set of small dipoles (on the right).*

## 1.2 The principle of discrete dipole approximation

Take an object of arbitrary form and relative permittivity in a homogeneous space that we suppose here being the vacuum. This object is submitted to an incident electromagnetic wave of wavelength  $\lambda$  ( $k_0 = 2\pi/\lambda$ ). The principle of the DDA consists in representing the object as a set of  $N$  small cubes of an edge  $a$  [by little, we mean smaller than the wavelength in the object :  $a \ll \lambda/\sqrt{\varepsilon}$  (Fig. 1.1)]. Each one of the small cubes under the action of the incident wave is going to get polarized, and as such, to acquire a dipolar moment, whose value is going to depend on the incident field and on its interaction with its neighbours. The local field of a dipole located at  $\mathbf{r}_i$ ,  $\mathbf{E}(\mathbf{r}_i)$ , is the sum of the incident wave and the field radiated by the other  $N - 1$  dipoles :

$$\mathbf{E}(\mathbf{r}_i) = \mathbf{E}_0(\mathbf{r}_i) + \sum_{j=1, i \neq j}^N \mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) \alpha(\mathbf{r}_j) \mathbf{E}(\mathbf{r}_j). \quad (1.1)$$

$\mathbf{E}_0$  is the incident wave,  $\mathbf{T}$  the linear susceptibility of the field in homogeneous space:

$$\mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) = e^{ik_0 r} \left[ \left( 3 \frac{\mathbf{r} \otimes \mathbf{r}}{r^2} - \mathbf{I} \right) \left( \frac{1}{r^3} - \frac{ik_0}{r^2} \right) + \left( \mathbf{I} - \frac{\mathbf{r} \otimes \mathbf{r}}{r^2} \right) \frac{k_0^2}{r} \right] \quad (1.2)$$

with  $\mathbf{I}$  the unity matrix and  $\mathbf{r} = \mathbf{r}_i - \mathbf{r}_j$ .  $\alpha$  is the polarizability of each discretization element obtained from the Clausius-Mossotti relation. Note that the polarizability  $\alpha$ , in order to respect the optical theorem, needs to contain a term called the radiative reaction term.<sup>4</sup> Equation (1.1) is valid for  $i = 1, \dots, N$ , and so represents a system of  $3N$  linear equations where the local fields,  $\mathbf{E}(\mathbf{r}_i)$ , being the unknowns. Once the system of linear equation is solved, the field scattered by the object at an arbitrary position  $\mathbf{r}$  is obtained by making the sum of all the radiated fields by each one of the dipoles :

$$\mathbf{E}(\mathbf{r}) = \sum_{j=1}^N \mathbf{T}(\mathbf{r}, \mathbf{r}_j) \alpha(\mathbf{r}_j) \mathbf{E}(\mathbf{r}_j). \quad (1.3)$$

When the object is in presence of a plane substrate or within a multilayer system, it is just necessary to replace  $\mathbf{T}$ , by the linear susceptibility of the referential system.

We have just presented the DDA as E. M. Purcell and C. R. Pennypacker had presented it earlier.<sup>2</sup> Note that another method very close to the DDA does exist. This method called

the method of the moments starts from the integral equation of Lippman Schwinger, which is strictly identical to the DDA. The demonstration of the equivalence between these two methods being a little technical, it is explained in Ref. <sup>5</sup>.

The advantages of the DDA are that it is applicable to objects of arbitrary forms, inhomogeneous (that is hardly achievable in case of surface method), and anisotropic (the polarizability associated to the mesh becomes a tensor). The outgoing wave condition is automatically satisfied through the linear susceptibility of the field. Finally, note that only the object is discretized unlike the methods of finite differences and finite elements. <sup>1</sup> The main inconvenience of the DDA consists in the fast increase of computation time together with the increase of the number of discretization elements, *i.e.*, the increase in size of the system of linear equations to be solved. There are ways to accelerate the resolution of a system of linear equations very important in size as the method of conjugated gradients, but, besides all, values of  $N > 10^6$  in homogeneous space are difficult to deal with.

### 1.3 A word about the code

The code is thought to have a user-friendly interface so that everyone can use it without any problems including non specialists. This allows undergraduate students to study, for example, the basics of microscopy (Rayleigh's criteria, notion of numerical aperture, ...) or diffraction without any problem; and researchers, typically biologists, having no notion of Maxwell's equations to simulate what gives a microscope (brightfield, phase microscope, dark field, ...) in function of the usual parameters and the object. Nevertheless, this code can also serve physicists specializing in electromagnetism in performing, for example, calculations of optical forces, diffraction, cross sections, near field and this with many incident beams.

The code thus has by default a simple interface where all numerical parameters are hidden and where many options are then chosen by default. But it's easy to access all Code options by checking the Advanced Interface option. This userguide explains how to use the advanced interface in starting with the different approaches used by the code to solve the Maxwell equations.

Note that the usability of the code is made to the detriment of the optimization of the RAM and the code can use large memory for large objects.

### 1.4 How to compile the code

The application is based on Qt-4.8 and gfortran. To install it you need : qt, qt-devel, gcc-c++ et gfortran. Notice that there is three versions of the code, the first one is sequential and uses FFTE (Fast Fourier Transform in the east), the second one uses FFTW (Fast Fourier Transform in the west) which needs openmp 4.5 minimum and the third uses HDF5 format to save data file. Then to compile:

Code par défaut	Code avec FFTW	Code avec FFTW et HDF5
qmake-qt4	qmake-qt4 "CONFIG+=fftw"	qmake-qt4 "CONFIG+=fftw hdf5"
make	make	make
make install	make install	make install

To run the application, cd bin, and ./cdm.

On linux system with the library FFTW, it requires to install FFTW packages with "dnf install \* fftw \*". For the version that uses HDF5 file you should install the following packages "dnf install hdf hdf5 hdf5-static hdf5-devel".



The code works on windows system but it is tricky to compile it if you want to use FFTW.

## 1.5 A word about the authors

- P. C. Chaumet is Professor at Fresnel Institute of Aix-Marseille University, and deals with the development of the fortran source code.
- A. Sentenac is research director at the CNRS, and works at Fresnel Institute of Aix-Marseille University, and participates to the development of the code connected to the far field diffraction.
- D. Sentenac develops the convivial interface of the code.
- G. Henry at Fresnel Institute of Aix-Marseille University works on the makefile and compilation on different linux system (Ubuntu, Fedora, etc).

## 1.6 Licence

Attribution-NonCommercial-ShareAlike 4.0 International (CC BY-NC-SA 4.0)

You are free to:

- Share - copy and redistribute the material in any medium or format
- Adapt - remix, transform, and build upon the material

The licensor cannot revoke these freedoms as long as you follow the license terms.

- Attribution - You must give appropriate credit, provide a link to the license, and indicate if changes were made. You may do so in any reasonable manner, but not in any way that suggests the licensor endorses you or your use.
- NonCommercial - You may not use the material for commercial purposes.
- ShareAlike - If you remix, transform, or build upon the material, you must distribute your contributions under the same license as the original.

## 1.7 How to quote the code

- If only the basic functions of the code are used:  
P. C. CHAUMET, A. SENTENAC, and A. RAHMANI,  
*Coupled dipole method for scatterers with large permittivity.*  
Phys. Rev. E **70**, 036606 (2004).
- If the calculation of the optical forces is used, then:  
P.C. CHAUMET, A. RAHMANI, A. SENTENAC, and G. W. BRYANT,  
*Efficient computation of optical forces with the coupled dipole method.*  
Phys. Rev. E **72**, 046708 (2005).
- If the calculation of optical couples is used:  
P. C. CHAUMET and C. BILLAUDEAU,  
*Coupled dipole method to compute optical torque: Application to a micropropeller.*  
J. Appl. Phys. **101**, 023106 (2007).

- If the rigorous Gaussian beam is used:  
P. C. CHAUMET,  
*Fully vectorial highly non paraxial beam close to the waist.*  
J. Opt. Soc. Am. A **23**, 3197 (2006).

# Approximated method

---

## Contents

<b>2.1</b>	<b>Introduction</b>	<b>6</b>
<b>2.2</b>	<b>Approximated method</b>	<b>8</b>
2.2.1	Born	8
2.2.2	Renormalized Born	8
2.2.3	Born at the order 1	8
2.2.4	Rytov	8
2.2.5	Renormalized Rytov	8
2.2.6	Beam propagation method (BPM)	9
2.2.7	Renormalized BPM	9

---

## 2.1 Introduction

In the previous chapter we have presented the DDA in a simple way where the object under study is a set of radiating dipole. In an approach more rigorous, with the Maxwell's equation, we get in Gaussian unit:

$$\nabla \times \mathbf{E}^m(\mathbf{r}) = i\frac{\omega}{c}\mathbf{B}(\mathbf{r}) \quad (2.1)$$

$$\nabla \times \mathbf{B}(\mathbf{r}) = -i\frac{\omega}{c}\varepsilon(\mathbf{r})\mathbf{E}^m(\mathbf{r}), \quad (2.2)$$

where  $\varepsilon(\mathbf{r})$  denotes the relative permittivity of the object and  $\mathbf{E}^m$  the macroscopic field inside the object, then we get

$$\nabla \times (\nabla \times \mathbf{E}^m(\mathbf{r})) = \varepsilon(\mathbf{r})k_0^2\mathbf{E}^m(\mathbf{r}), \quad (2.3)$$

with  $k_0 = \omega^2/c^2$ . Using the relationship  $\varepsilon = 1 + 4\pi\chi$ , where  $\chi$  denotes the linear field susceptibility, we have:

$$\nabla \times (\nabla \times \mathbf{E}^m(\mathbf{r})) - k_0^2\mathbf{E}^m(\mathbf{r}) = 4\pi\chi(\mathbf{r})k_0^2\mathbf{E}^m(\mathbf{r}). \quad (2.4)$$

To solve this equation one needs the Green function defined as:

$$\nabla \times (\nabla \times \mathbf{T}(\mathbf{r}, \mathbf{r}')) - k_0^2\mathbf{T}(\mathbf{r}, \mathbf{r}') = 4\pi k_0^2\mathbf{I}\delta(\mathbf{r} - \mathbf{r}'), \quad (2.5)$$

and the solution of Eq. (2.4) reads:

$$\mathbf{E}^m(\mathbf{r}) = \mathbf{E}_0(\mathbf{r}) + \int_{\Omega} \mathbf{T}(\mathbf{r}, \mathbf{r}') \chi(\mathbf{r}') \mathbf{E}^m(\mathbf{r}') d\mathbf{r}', \quad (2.6)$$

where  $\mathbf{E}^0$  is the incident field and  $\Omega$  the support of the object under study. When we solve Eq. (2.4) the field  $\mathbf{E}^m$  corresponds to macroscopic field inside the object. To solve Eq. (2.4) we discretize the object in a set of  $N$  subunits with a cubic meshsize  $d$ , then the integral equation becomes the sum of  $N$  integrals:

$$\mathbf{E}^m(\mathbf{r}_i) = \mathbf{E}^0(\mathbf{r}_i) + \sum_{j=1}^N \int_{V_j} \mathbf{T}(\mathbf{r}_i, \mathbf{r}') \chi(\mathbf{r}') \mathbf{E}^m(\mathbf{r}') d\mathbf{r}', \quad (2.7)$$

with  $V_j = d^3$ . Assuming the field, the Green function and the susceptibility constant over a subunit we get:

$$\mathbf{E}^m(\mathbf{r}_i) = \mathbf{E}^0(\mathbf{r}_i) + \sum_{j=1}^N \mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) \chi(\mathbf{r}_j) \mathbf{E}^m(\mathbf{r}_j) d^3. \quad (2.8)$$

Using, in first approximation (the radiative reaction term neglected)  $\int_{V_i} \mathbf{T}(\mathbf{r}_i, \mathbf{r}') d\mathbf{r}' = -4\pi/3^6$ , we get:

$$\mathbf{E}^m(\mathbf{r}_i) = \mathbf{E}^0(\mathbf{r}_i) + \sum_{j=1, i \neq j}^N \mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) \chi(\mathbf{r}_j) d^3 \mathbf{E}^m(\mathbf{r}_j) - \frac{4\pi}{3} \chi(\mathbf{r}_i) \mathbf{E}^m(\mathbf{r}_i), \quad (2.9)$$

then we can write

$$\mathbf{E}(\mathbf{r}_i) = \mathbf{E}^0(\mathbf{r}_i) + \sum_{j=1, i \neq j}^N \mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) \alpha_{\text{CM}}(\mathbf{r}_j) \mathbf{E}(\mathbf{r}_j) \quad (2.10)$$

$$\text{with } \mathbf{E}(\mathbf{r}_i) = \frac{\varepsilon(\mathbf{r}_i) + 2}{3} \mathbf{E}^m(\mathbf{r}_i) \quad (2.11)$$

$$\alpha_{\text{CM}}(\mathbf{r}_j) = \frac{3}{4\pi} d^3 \frac{\varepsilon(\mathbf{r}_i) - 1}{\varepsilon(\mathbf{r}_i) + 2}. \quad (2.12)$$

The field  $\mathbf{E}(\mathbf{r}_i)$  is the local field, *i.e.* the field at the position  $i$  in the absence of the subunit  $i$ . Then the linear system can be written formally as

$$\mathbf{E} = \mathbf{E}^0 + \mathbf{A} \mathbf{D}_{\alpha} \mathbf{E}, \quad (2.13)$$

where  $\mathbf{A}$  is a matrix which contains all the Green function and  $\mathbf{D}_{\alpha}$  is a tridiagonal matrix with the polarizabilities of each element of discretization. In the next chapter we detail how to solve Eq. (2.13) rigorously, but in this present chapter we detail different approached methods to avoid the tedious resolution of Eq. (2.13). The scattered field is computed through

$$\mathbf{E}^d(\mathbf{r}) = \sum_{j=1}^N \mathbf{T}(\mathbf{r}, \mathbf{r}_j) \alpha(\mathbf{r}_j) \mathbf{E}(\mathbf{r}_j). \quad (2.14)$$

## 2.2 Approximated method

### 2.2.1 Born

The most simple approximation is the Born approximation which consists to assume the field inside the object equal to the incident field for each element of discretization:

$$\mathbf{E}^m(\mathbf{r}_i) = \mathbf{E}^0(\mathbf{r}_i), \quad (2.15)$$

This approximation hold if the contrast is weak and the object small compare to the wavelength of illumination.

### 2.2.2 Renormalized Born

The renormalized Born approximation consists to assume the local field inside the object equal to the incident field :

$$\mathbf{E}(\mathbf{r}_i) = \mathbf{E}^0(\mathbf{r}_i). \quad (2.16)$$

In that case the macroscopic field reads:

$$\mathbf{E}^m(\mathbf{r}_i) = \frac{3}{\varepsilon(\mathbf{r}_i) + 2} \mathbf{E}^0(\mathbf{r}_i). \quad (2.17)$$

This approximation is better than the classical Born approximation when the permittivity is high.

### 2.2.3 Born at the order 1

To be more precise than the renormalized Born approximation, one can perform the Born series at the order one:

$$\mathbf{E}(\mathbf{r}_i) = \mathbf{E}^0(\mathbf{r}_i) + \sum_{j=1, i \neq j}^N \mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) \alpha(\mathbf{r}_j) \mathbf{E}^0(\mathbf{r}_j). \quad (2.18)$$

In that case we take into account the simple scattering.

### 2.2.4 Rytov

The Rytov approximation consist to take into account the phase variation inside the object:

$$E_\beta^m(\mathbf{r}_i) = E_\beta^0(\mathbf{r}_i) e^{E_\beta^d(\mathbf{r}_i)/E_\beta^0(\mathbf{r}_i)}, \quad (2.19)$$

with  $\beta = x, y, z$ . Notice that when a component of the incident field is null, then  $E_\beta^m = 0$ . This approximation permits to deal with large object compare to the wavelength of illumination, but always with low contrast of permittivity. The diffracted field reads:

$$\mathbf{E}^d(\mathbf{r}_i) = \sum_{j=1}^N \mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) \chi(\mathbf{r}_j) \mathbf{E}^0(\mathbf{r}_j), \quad (2.20)$$

### 2.2.5 Renormalized Rytov

The renormalized Rytov approximation deals with the local field:

$$E_\beta(\mathbf{r}_i) = E_\beta^0(\mathbf{r}_i) e^{E_\beta^d(\mathbf{r}_i)/E_\beta^0(\mathbf{r}_i)}, \quad (2.21)$$

and the diffracted field reads:

$$\mathbf{E}^d(\mathbf{r}_i) = \sum_{j=1, i \neq j}^N \mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) \alpha(\mathbf{r}_j) \mathbf{E}^0(\mathbf{r}_j). \quad (2.22)$$

### 2.2.6 Beam propagation method (BPM)

BPM is a class of algorithms designed for calculating the optical field distribution in space for very large object compare to the wavelength of illumination. BPM allows to obtain the electromagnetic field via alternating evaluation of diffraction and refraction steps handled in the Fourier and space domains. It is important to note that BPM ignores reflections, for more details see Ref. 7. In final the field reads

$$\mathbf{E}^m(x, y, z + d) = e^{ik_0 n(x, y, z + d)d} \mathcal{F}^{-1} \left[ \mathcal{F}[\mathbf{E}^m(x, y, z)] e^{-i(k_0 - k_z)d} \right], \quad (2.23)$$

where the field at the position  $(x, y, z + d)$  is computed with the permittivity at the same position and the field at the previous plane  $z$ . It is clear with this relation that the field is propagated only in the direction of the positive  $z$ . Note that the size of the FFT is given by the drop down menu and to avoid angle of incidence too high. Notice that the diffracted field is computed like the other methods which is more precise than the Kirchhoff's equation.

### 2.2.7 Renormalized BPM

We can do the same but with the local field:

$$\mathbf{E}(x, y, z + d) = e^{ik_0 n(x, y, z + d)d} \mathcal{F}^{-1} \left[ \mathcal{F}[\mathbf{E}(x, y, z)] e^{-i(k_0 - k_z)d} \right]. \quad (2.24)$$

# Numerical details

---

## Contents

<b>3.1</b>	<b>Polarizability</b> . . . . .	<b>10</b>
<b>3.2</b>	<b>Correction to the tensor of susceptibility</b> . . . . .	<b>11</b>
<b>3.3</b>	<b>Solve the system of linear equation</b> . . . . .	<b>11</b>

---

## 3.1 Polarizability

The DDA discretizes the object into a set of punctual dipoles, where a polarizability  $\alpha$  is associated to each punctual dipoles. There are different forms for this polarizability. The first to have been used, and the simplest, is the relation of Clausius Mossotti (CM)<sup>2</sup>:

$$\alpha_{\text{CM}} = \frac{3}{4\pi} \frac{\varepsilon - 1}{\varepsilon + 2} d^3 = \frac{\varepsilon - 1}{\varepsilon + 2} a^3, \quad (3.1)$$

where  $\varepsilon$  denotes the permittivity of the object,  $d$  the size of the cubic meshsize and  $a = \left(\frac{3}{4\pi}\right)^{\frac{1}{3}} d$  the radius of the sphere of the same volume than the cubic meshsize of the side  $d$ . Unfortunately, this relation does not keep the energy and, then, it is necessary to introduce a radiative reaction term that takes into account the fact that charges in movement lose energy, and the polarizability is, then, written as<sup>4</sup>:

$$\alpha_{\text{RR}} = \frac{\alpha_{\text{CM}}}{1 - \frac{2}{3} i k_0^3 \alpha_{\text{CM}}}. \quad (3.2)$$

After different forms of the polarizability have been established in order to improve the precision of the DDA and take into account the non-punctual character of the dipole, and we may quote, among the best known, the ones by Goedecke and O'Brien<sup>8</sup>,

$$\alpha_{\text{GB}} = \frac{\alpha_{\text{CM}}}{1 - \frac{2}{3} i k_0^3 \alpha_{\text{CM}} - k_0^2 \alpha_{\text{CM}} / a}, \quad (3.3)$$

by Lakhtakia<sup>9</sup>:

$$\alpha_{\text{LA}} = \frac{\alpha_{\text{CM}}}{1 - 2 \frac{\varepsilon - 1}{\varepsilon + 2} [(1 - i k_0 a) e^{i k_0 a} - 1]} \quad (3.4)$$

and Draine and Goodman<sup>10</sup>

$$\alpha_{\text{LR}} = \frac{\alpha_{\text{CM}}}{1 + \alpha_{\text{CM}} \left[ \frac{(b_1 + \varepsilon b_2 + \varepsilon b_3 S) k_0^2}{d} - \frac{2}{3} i k_0^3 \right]}, \quad (3.5)$$

with  $b_1 = -1.891531$ ,  $b_2 = 0.1618469$ ,  $b_3 = -1.7700004$  and  $S = 1/5$ .

Inside the code by default, it is  $\alpha_{RR}$  which is used. In the case when the permittivity is anisotropic only  $\alpha_{RR}$  is going to be used.

A last polarizability is introduced (PS) that only works for homogeneous spheres and is particularly precise for metals. This consists of making a change of the polarizability of the elements on the edge of the sphere taking into account the factor of depolarization of the sphere.<sup>11</sup>

## 3.2 Correction to the tensor of susceptibility

The tensor of susceptibility (or dyadic Green function) of the field connects the dipole to the position  $\mathbf{r}_j$  to the field radiated at the position  $\mathbf{r}_i$  by the relation :  $\mathbf{E}(\mathbf{r}_i) = \mathbf{T}(\mathbf{r}_i, \mathbf{r}_j)\mathbf{p}(\mathbf{r}_j)$ . But inside the DDA, considering the fact that the dipoles are associated with a certain volume, the following integration should be written<sup>5</sup>:

$$\mathbf{E}(\mathbf{r}_i) = \int_{V_j} \mathbf{T}(\mathbf{r}_i, \mathbf{r})\mathbf{p}(\mathbf{r})d\mathbf{r} \approx \left[ \int_{V_j} \mathbf{T}(\mathbf{r}_i, \mathbf{r})d\mathbf{r} \right] \mathbf{p}(\mathbf{r}_j), \quad (3.6)$$

supposing the meshsize small enough to be able to consider the field as being uniform in it. So, the tensor must be integrated upon the meshsize  $V_j$ . This integration is not analytic (it has to be done numerically and this takes time) and, in fact, it only serves for the dipoles which are the nearest to the observation, after that, the integration does not bring any more precision. So, in the code, we propose the possibility to integrate upon the nearest mesh sizes:

$$\int_{V_j} \mathbf{T}(\mathbf{r}_i, \mathbf{r})d\mathbf{r} \quad \text{if} \quad \frac{\|\mathbf{r}_i - \mathbf{r}_j\|}{d} \leq n \quad (3.7)$$

$$\mathbf{T}(\mathbf{r}_i, \mathbf{r}_j) \quad \text{if} \quad \frac{\|\mathbf{r}_i - \mathbf{r}_j\|}{d} > n. \quad (3.8)$$

$n$  may take the value entire 0 (by default) until 5.

## 3.3 Solve the system of linear equation

In order to know the electric field in the object, *i.e.* the field at the position of the  $N$  elements of discretization, we have to solve the following system of linear equation:

$$\mathbf{E} = \mathbf{E}_0 + \mathbf{A}D_\alpha\mathbf{E}, \quad (3.9)$$

where  $\mathbf{E}_0$  is a vector of size  $3N$  which contains the incident field at the discretization elements.  $\mathbf{A}$  is a matrix  $3N \times 3N$  which contains all the field tensor susceptibility and  $D_\alpha$  is a diagonal matrix  $3N \times 3N$ , if the object is isotropic, or diagonal block  $3 \times 3$  if the object is anisotropic.  $\mathbf{E}$  is the vector  $3N$  which contains the unknown electric local fields. The equation is solved by a non-linear iterative method. The code proposes numerous iterative methods, and the one used by default is GPBICG because it is the most efficient in most cases<sup>12</sup>. The code stops when the residue,

$$r = \frac{\|\mathbf{E} - \mathbf{A}D_\alpha\mathbf{E} - \mathbf{E}_0\|}{\|\mathbf{E}_0\|}, \quad (3.10)$$

is under the tolerance given by the user.  $10^{-4}$  is the tolerance used by default, because it is a good compromise between speed and precision. Please find below the different iterative method possible in the code:



- GPBICG1 : Ref. [13](#)
- GPBICG2 : Ref. [13](#)
- GPBICGsafe : Ref. [14](#)
- GPBICGAR1 : Ref. [13](#)
- GPBICGAR2 : Ref. [13](#)
- QMRCLA : Ref. [15](#)
- TFQMR : Ref. [15](#)
- CG : Ref. [15](#)
- BICGSTAB : Ref. [15](#)
- QMRBICGSTAB1 : Ref. [16](#)
- QMRBICGSTAB2 : Ref. [16](#)
- GPBICOR : Ref. [17](#)
- CORS : Ref. [18](#)
- BiCGstar-plus Ref. [19](#)

# Managing of the configurations

---

## Contents

---

<b>4.1</b>	<b>Introduction</b>	<b>13</b>
<b>4.2</b>	<b>Creation and saving of a new configuration</b>	<b>13</b>
<b>4.3</b>	<b>Managing of the configurations</b>	<b>13</b>

---

## 4.1 Introduction

The Code is launched by `./cdm` inside the `bin` folder for a Linux configuration. It has been created to be as convenient as possible and so needing few explanations for its use. However, certain conventions have been taken and need to be clarified.

## 4.2 Creation and saving of a new configuration

In order to start a new calculation, go to the tab *calculation* and *New*. A new configuration shows up with values by default. Once the new configuration is chosen, in order to be saved, the tab *Calculation* and *Save* have to be selected again. Then, we select the name of the configuration, and we may add a short description of the calculation that has been made. Another way to save a configuration is to click directly on the panel of the configuration *Save configuration*. Then, two fields appear, one for the name of the configuration and the second one for its description.

## 4.3 Managing of the configurations

In order to manage all the selected configurations, we have go to the tab *Calculation* and *Load*. So, a new window appears with all the saved configurations. For each configuration there is a short description that the user has entered, the date, when the configuration file has been saved, then the principal characteristics of the configuration (wave length, power, the beam's waist, object, material, discretization and tolerance of the iterative method). It is enough to click on a configuration and to click on *load* in order to load a configuration.

The *delete* button is used to delete a saved configuration and the *export* enables to export inside a file (name of the configuration.opt) all the characteristics of the configuration.

Note that by double clicking on the line, we can modify the description field.

# Properties of the illumination

---

## Contents

---

<b>5.1</b>	<b>Introduction</b>	<b>14</b>
<b>5.2</b>	<b>Beam</b>	<b>14</b>
5.2.1	Introduction	14
5.2.2	Linear plane wave	15
5.2.3	Circular plane wave	16
5.2.4	Multiplane wave	16
5.2.5	Antenna	16
5.2.6	Linear Gaussian	16
5.2.7	Circular Gaussian	17
5.2.8	Circular and linear Gaussian (FFT)	17
5.2.9	Linear Gaussian (para)	17
5.2.10	Circular Gaussian (para)	18
5.2.11	Arbitrary wave	18

---

## 5.1 Introduction

In the section properties of the illumination, the field *Wavelength* enables us to enter the using wavelength. This one is entered in nanometer. The field *P<sub>0</sub>* enables to enter the power of the laser beam in Watt. The field *W<sub>0</sub>* in nanometer enables to enter for a plane wave the radius of the laser beam and for a Gaussian beam, the waist of the beam.

## 5.2 Beam

### 5.2.1 Introduction

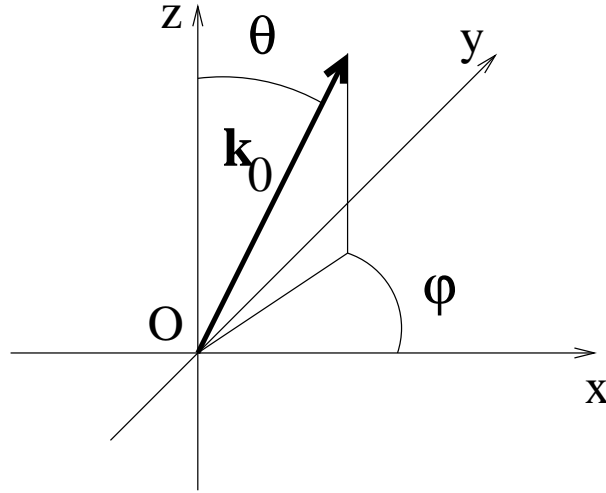
There are six beams predefined, their propagation direction is always defined in the same way, with two angles  $\theta$  and  $\varphi$ . They are connected to the given direction by the wave vector as follows:

$$k_x = k_0 \sin \theta \cos \varphi \quad (5.1)$$

$$k_y = k_0 \sin \theta \sin \varphi \quad (5.2)$$

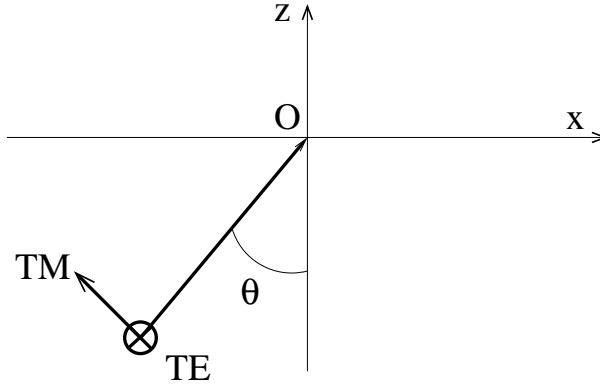
$$k_z = k_0 \cos \theta \quad (5.3)$$

where  $\mathbf{k}_0 = (k_x, k_y, k_z)$  is the wave vector parallel to the direction of the incident beam and  $k_0$  the wave number, see Fig. 5.1. For the polarization, we use the plane  $(x, y)$  as



**Figure 5.1 :** *Definition of the beam's direction*

referential surface. Then, we can determine a polarization TM ( $p$ ) and TE ( $s$ ) with the presence of a surface, see Fig. 5.2. The frame  $(x, y, z)$  is used as an absolute referential.



**Figure 5.2 :** *Definition of the beam's polarization.*

### 5.2.2 Linear plane wave

*Linear plane wave* is a plane wave linearly polarized. The first line is relative to  $\theta$  and the second to  $\varphi$ . The third line is connected to the polarization,  $\text{pola}=1$  en TM and  $\text{pola}=0$  in TE. Note that the polarization is not necessarily purely in TE or TM:  $\text{pola} \in [0, 1]$  such as  $E_{\text{TM}}^2 = \text{pola}^2 E^2$  and  $E_{\text{TE}}^2 = (1 - \text{pola}^2) E^2$ .

Note that the phase is always taken null at the origin of the frame:

$$\mathbf{E}(\mathbf{r}) = \mathbf{E}_0 e^{i\mathbf{k} \cdot \mathbf{r}}, \quad (5.4)$$

with Irradiance  $= P_0/S$  where  $S = \pi w_0^2$  is the surface of the beam and  $E_0 = \sqrt{2 \text{Irradiance} / c / \epsilon_0}$ .

### 5.2.3 Circular plane wave

*pwavircular* is a plane wave circularly polarized. The first line is relative to  $\theta$  and the second to  $\varphi$ . The third line is connected to the polarization that we can choose right (1) or left (-1) circular.

Note that the phase is taken null at the origin of the frame.

$$\mathbf{E}(\mathbf{r}) = \mathbf{E}_0 e^{i\mathbf{k} \cdot \mathbf{r}}, \quad (5.5)$$

with Irradiance =  $P_0/S$  where  $S = \pi w_0^2$  is the surface of the beam and  $E_0 = \sqrt{2\text{Irradiance}/c/\epsilon_0}$ .

### 5.2.4 Multiplane wave

*Multiplane wave* consists to take many planes waves. The first thing to do is to choose the number of plane wave, and then for each plane wave we choose  $\theta$  and  $\varphi$  and the polarization. We have to write also the complex magnitude of each plane wave. The sum of the power of all the plane wave is equal to  $P_0$ .

### 5.2.5 Antenna

The incident beam can be a dipole where the user defines the position and orientation. Notice that the antenna can be inside or outside the object. The magnitude is chosen such that the power radiated by the dipole is equal to  $P_0$ :

$$P_0 = \frac{1}{4\pi\epsilon_0} \frac{k^4 c}{3} \|\mathbf{p}\|^2. \quad (5.6)$$

### 5.2.6 Linear Gaussian

*Linear Gaussian* is a Gaussian wave polarized linearly. The first line is relative to  $\theta$  and the second to  $\varphi$ . The third line is connected to the polarization  $\text{pola}=1$  in TM and  $\text{pola}=0$  in TE. Note that the polarization is not necessarily in TE or TM:  $\text{pola} \in [0 \ 1]$  such as  $E_{\text{TM}}^2 = \text{pola}^2 E^2$  and  $E_{\text{TE}}^2 = (1 - \text{pola}^2) E^2$ .

The three following lines help to fix the position of the centre of the waist in nanometers in the frame  $(x, y, z)$ .

Note that this Gaussian beam may have a very weak waist, because it is calculated without any approximation through an angular spectrum representation. The definition of the waist, for a beam propagating along the  $z$  axis is :<sup>20</sup>

$$E(x, y, 0) = E_0 e^{-\rho^2/(2w_0^2)}, \quad (5.7)$$

with  $\rho = \sqrt{x^2 + y^2}$ . From this definition of the beam at  $z = 0$ , for a beam polarized along the  $x$  axis we get :<sup>21</sup>

$$E_x = E_0 \int_0^{k_0} w_0^2 \exp\left(-\frac{w_0^2(k_0^2 - k_z^2)}{2}\right) \exp(ik_z z) J_0\left(\rho \sqrt{k_0^2 - k_z^2}\right) k_z dk_z \quad (5.8)$$

$$E_z = -iE_0 \frac{x}{\rho} \int_0^{k_0} w_0^2 \exp\left(-\frac{w_0^2(k_0^2 - k_z^2)}{2}\right) \exp(ik_z z) J_1\left(\rho \sqrt{k_0^2 - k_z^2}\right) \sqrt{k_0^2 - k_z^2} dk_z \quad (5.9)$$

with  $J_1$  and  $J_0$  the Bessel's function. The irradiance is computed at the center of the Gaussian beam and the relationship between the power and the magnitude  $E_0$  is:

$$P_0 = \frac{\pi w_0^2}{4} c \epsilon_0 E_0^2 \left(1 + \frac{(k_0 w_0)^2 - 1}{k_0 w_0} \frac{\sqrt{\pi}}{2} \text{Im}[w(k_0 w_0)]\right) \quad (5.10)$$

$$\text{Irradiance} = \frac{E_0^2}{4} c \epsilon_0 \left(1 + \frac{(k_0 w_0)^2 - 1}{k_0 w_0} \frac{\sqrt{\pi}}{2} \text{Im}\left[w(k_0 w_0/\sqrt{2})\right]\right), \quad (5.11)$$

where  $w()$  denotes the Faddeeva's function. If we suppose  $w() \approx 0$ , we obtain  $P_0 = \pi w_0^2 \text{Irradiance}$  and we find the relation given for a plane wave.

### 5.2.7 Circular Gaussian

*Circular Gaussian* is a Gaussian wave circularly polarized. The first line is relative to  $\theta$  and the second to  $\varphi$ . The third line is connected to the polarization that we can choose right (1) or left (-1) circular.

The next three lines enable us to fix the position of the centre of the waist in nanometers in the frame  $(x, y, z)$ .

Note that this Gaussian wave may have a very weak waist, because it is calculated without any approximation through a plane wave spectrum.

### 5.2.8 Circular and linear Gaussian (FFT)

*Circular and linear Gaussian (FFT)* is a Gaussian wave based on the previous computation for the Circular and linear Gaussian, respectively. In this case, the incident wave is computed at the bottom of the object and then the beam is propagated with FFT as for the beam propagation method. This computation is quicker than the rigorous one. However, one needs to choose the number of points for the FFT enough large to not truncate the Gaussian beam and avoid periodicity problem.

### 5.2.9 Linear Gaussian (para)

*Linear Gaussian (para)* is a Gaussian wave polarized linearly. The first line is relative to  $\theta$  and the second to  $\varphi$ . The third line is connected to the polarization,  $\text{pola}=1$  with TM and  $\text{pola}=0$  with TE. Note that the polarization is not necessarily purely in TE or TM:  $\text{pola} \in [0, 1]$  such as  $E_{\text{TM}}^2 = \text{pola}^2 E^2$  and  $E_{\text{TE}}^2 = (1 - \text{pola}^2) E^2$ .

The next three lines enables us to fix the position of the centre of the waist in nanometers in the frame  $(x, y, z)$ .

Note that this Gaussian wave is calculated in accordance with the paraxial approximation and as such does not satisfy rigorously the Maxwell's equations. For a wave propagating along the  $z$  direction and polarized along the  $x$  axis we have:

$$E_x = E_0 \sqrt{2} \frac{w_0}{w} e^{-\rho^2/w^2} e^{ik_0 \rho^2 R(z)/2} e^{i(k_0 z + \eta)} \quad (5.12)$$

$$w = \sqrt{2} w_0 \sqrt{1 + \frac{z^2}{z_0^2}} \quad (5.13)$$

$$z_0 = k_0 w_0^2 \quad (5.14)$$

$$R(z) = \frac{z}{z^2 + z_0^2} \quad (5.15)$$

$$\eta = \tan^{-1}(z/z_0). \quad (5.16)$$

We remark that for  $z = 0$  the Gaussian beam has the same magnitude that those computed rigorously. The field and the irradiance at the center of the waist are computed through

$$E_0 = \sqrt{\frac{2P_0}{\pi c \epsilon_0 w_0^2}} \quad (5.17)$$

$$\text{irradiance} = c \epsilon_0 E_0^2 / 2 = \frac{P_0}{\pi w_0^2}. \quad (5.18)$$

### 5.2.10 Circular Gaussian (para)

*Circular Gaussian (para)* is a Gaussian wave polarized circularly. The first line is relative to  $\theta$  and the second to  $\varphi$ . The third line is connected to the polarization that we may choose right or left.

The next three lines enable us to fix the position of the centre of the waist in nanometers in the frame  $(x, y, z)$ .

Note that this Gaussian wave is calculated in accordance with the paraxial approximation and as such does not satisfy rigorously the Maxwell's equations.

### 5.2.11 Arbitrary wave

In the case of an arbitrary field, the characteristic are determined by the user. In other words, he has to create the field himself, and it is mandatory to create these files respecting the chosen conventions by the code.

The description of the discretization of the incident field is done within a file which is asked for when we click on *Props*. For example, for the real part of the component  $x$  of the field, it has to be constructed as follows:

```
nx,ny,nz
dx,dy,dz
xmin,ymin,zmin
```

- nx is the number of meshsize according to the axis  $x$
- ny is the number of meshsize according to the axis  $y$
- nz is the number of meshsize according to the axis  $z$
- dx is the step according to the axis  $x$
- dy is the step according to the axis  $y$
- dz is the step according to the axis  $z$
- xmin the smallest abscissa
- ymin the smallest ordinate
- zmin the smallest azimuth

Then, the files of the electric field are created as follows for each of the components of the real part and separated imaginary field:

```
open(11, file='Exr.mat', status='new', form='formatted', access='direct', recl=22)
do k=1,nz
  do j=1,ny
    do i=1,nx
      ii=i+nx*(j-1)+nx*ny*(k-1)
      write(11,FMT='(D22.15)',rec=ii) dreal(Ex)
    enddo
  enddo
enddo
```

---

Be careful, the mesh size of the discretization of the object has to be larger than the meshsize of the discretization of the field.



# Definition of the object

---

## Contents

<b>6.1</b>	<b>Introduction</b>	<b>20</b>
<b>6.2</b>	<b>Type of the object</b>	<b>20</b>
6.2.1	Sphere	21
6.2.2	Inhomogeneous sphere	21
6.2.3	Random sphere (length)	22
6.2.4	Random sphere (meshsize)	22
6.2.5	Cube	23
6.2.6	Cuboid (length)	23
6.2.7	Cuboid (meshsize)	23
6.2.8	Inhomogeneous Cuboid (length)	24
6.2.9	Inhomogeneous Cuboid (meshsize)	24
6.2.10	Ellipsoid	24
6.2.11	Several spheres	25
6.2.12	Cylinder	25
6.2.13	concentric spheres	25
6.2.14	Arbitrary object	25
<b>6.3</b>	<b>Choose the relative permittivity</b>	<b>26</b>
<b>6.4</b>	<b>Choose the discretization</b>	<b>27</b>

---

## 6.1 Introduction

The code proposes several predefined objects, and we are going to precise in this section how to enter their optogeometrical characteristics. Note that all the distances have to be entered in nanometers. The code is doing the conversion in meters.

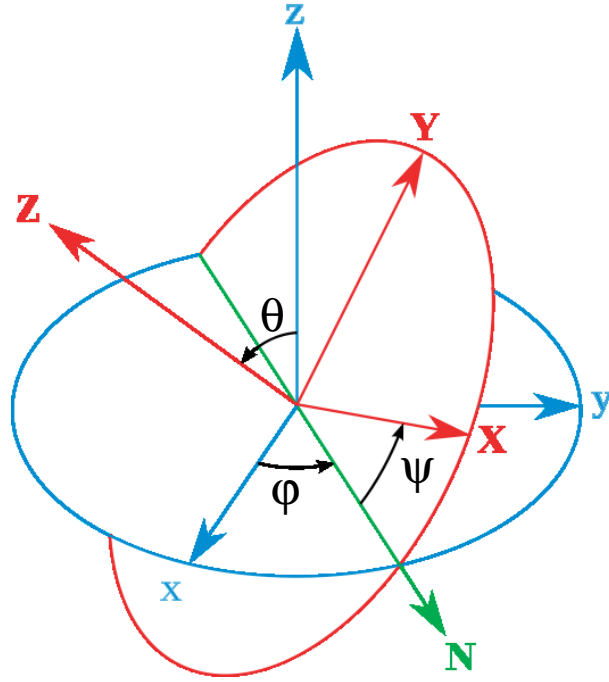
## 6.2 Type of the object

The list of the predefined objects is the following:

sphere, cube, cuboid, ellipsoid, several distinct spheres, cylinder, concentric spheres, inhomogeneous sphere and arbitrary object.

When the objects as the cube or the cuboid have their edges turned with respect to the axes of the system of coordinates, the angles of Euler are used as defined in Fig. 6.1. The rotation centre being the inertia centre of the object and the matrix of rotation reads:

$$\mathbf{A} = \begin{pmatrix} \cos(\psi) \cos(\varphi) - \sin(\psi) \cos(\theta) \sin(\varphi) & -\cos(\psi) \sin(\varphi) - \sin(\psi) \cos(\theta) \cos(\varphi) & \sin(\psi) \sin(\theta) \\ \sin(\psi) \cos(\varphi) + \cos(\psi) \cos(\theta) \sin(\varphi) & -\sin(\psi) \sin(\varphi) + \cos(\psi) \cos(\theta) \cos(\varphi) & -\cos(\psi) \sin(\theta) \\ \sin(\theta) \sin(\varphi) & \sin(\theta) \cos(\varphi) & \cos(\theta) \end{pmatrix}$$



**Figure 6.1 :** Definition of the angles of Euler according to the convention  $Z - X - Z$ .  
Scheme taken from Wikipedia

### 6.2.1 Sphere

For the sphere, there are four fields to be filled:

- The radius of the sphere in nanometer
- The abscissa of the centre of the sphere in nanometer
- The ordinate of the centre of the sphere in nanometer
- The azimuth of the centre of the sphere in nanometer

### 6.2.2 Inhomogeneous sphere

The permittivity of the sphere have a Gaussian noise with a correlation length  $l_c$ , standard deviation,  $A$  and an average  $\varepsilon_r$ .

For the inhomogeneous sphere there are seven fields to be filled:

- The radius of the sphere in nanometer

- The abscissa of the centre of the sphere in nanometer
- The ordinate of the centre of the sphere in nanometer
- The azimuth of the centre of the sphere in nanometer
- The seed
- The correlation length  $l_c$
- The magnitude of oscillation  $A$

### 6.2.3 Random sphere (length)

All the spheres are constituted with the same permittivity and the same radius but are distributed randomly in cuboid. There are nine fields to be filled:

- The edge of the cube in nanometer according to the axis  $x$
- The edge of the cube in nanometer according to the axis  $y$
- The edge of the cube in nanometer according to the axis  $z$
- The abscissa of the centre of the cuboid in nanometer
- The ordinate of the centre of the cuboid in nanometer
- The azimuth of the centre of the sphere in nanometer
- The seed
- The radius of the spheres
- The density of sphere, *i.e.*  $d = \text{volume of the sphere} / \text{volume of the cuboid}$ .  $d$  should satisfy the inequality  $0 < d < 0.5$ . If  $d$  is above 2, then it corresponds to the number of sphere in the box.

### 6.2.4 Random sphere (meshsize)

All the spheres are constituted with the same permittivity and the same radius but are distributed randomly in cuboid. There are ten fields to be filled:

- The abscissa of the centre of the cuboid in nanometer
- The ordinate of the centre of the cuboid in nanometer
- The azimuth of the centre of the sphere in nanometer
- Number of meshsize long  $x$
- Number of meshsize long  $y$
- Number of meshsize long  $z$
- meshsize in nanometer
- The radius of the spheres
- The seed

- The density of sphere, *i.e.*  $d = \text{volume of the sphere} / \text{volume of the cuboid}$ .  $d$  should satisfy the inequality  $0 < d < 0.5$ . If  $d$  is above 2, then it corresponds to the number of sphere in the box.

### 6.2.5 Cube

For the cube, there are seven fields to be filled:

- The edge of the cube in nanometer
- The abscissa of the centre of the sphere in nanometer
- The ordinate of the centre of the sphere in nanometer
- The azimuth of the centre of the sphere in nanometer
- First angle of Euler  $\psi$  by rotation around the axis  $z$
- Second angle of Euler  $\theta$  by rotation around the axis  $x$
- Third angle of Euler  $\varphi$  by rotation around the axis  $z$

### 6.2.6 Cuboid (length)

For the cuboid, there are nine fields to be filled:

- The edge of the cube in nanometer according to the axis  $x$
- The edge of the cube in nanometer according to the axis  $y$
- The edge of the cube in nanometer according to the axis  $z$
- The abscissa of the centre of the cuboid in nanometer
- The ordinate of the centre of the cuboid in nanometer
- The azimuth of the centre of the sphere in nanometer
- First angle of Euler  $\psi$  by rotation around the axis  $z$
- Second angle of Euler  $\theta$  by rotation around the axis  $x$
- Third angle of Euler  $\varphi$  by rotation around the axis  $z$

### 6.2.7 Cuboid (meshsize)

For the cuboid, there are seven fields to be filled:

- The abscissa of the centre of the cuboid in nanometer
- The ordinate of the centre of the cuboid in nanometer
- The azimuth of the centre of the sphere in nanometer
- Number of meshsize long  $x$
- Number of meshsize long  $y$
- Number of meshsize long  $z$
- Meshsize in nanometer

### 6.2.8 Inhomogeneous Cuboid (length)

The permittivity of the cuboid have a Gaussian noise with a correlation length  $l_c$ , standard deviation  $A$  and an average  $\varepsilon_r$ . For the cuboid, there are nine fields to be filled:

- The edge of the cube in nanometer according to the axis  $x$
- The edge of the cube in nanometer according to the axis  $y$
- The edge of the cube in nanometer according to the axis  $z$
- The abscissa of the centre of the cuboid in nanometer
- The ordinate of the centre of the cuboid in nanometer
- The azimuth of the centre of the sphere in nanometer
- The seed
- The correlation length  $l_c$
- The magnitude of oscillation  $A$

### 6.2.9 Inhomogeneous Cuboid (meshsize)

The permittivity of the cuboid have a Gaussian noise with a correlation length  $l_c$ , standard deviation  $A$  and an average  $\varepsilon_r$ . For the cuboid, there are nine fields to be filled:

- The abscissa of the centre of the cuboid in nanometer
- The ordinate of the centre of the cuboid in nanometer
- The azimuth of the centre of the sphere in nanometer
- Number of meshsize long  $x$
- Number of meshsize long  $y$
- Number of meshsize long  $z$
- Meshsize in nanometer
- The seed
- The correlation length  $l_c$
- The magnitude of oscillation  $A$

### 6.2.10 Ellipsoid

For the ellipsoid, there are nine fields to be fulfilled:

- The half axis in nanometer according to the axis  $x$
- The half axis in nanometer according to the axis  $y$
- The half axis in nanometer according to the axis  $z$
- The abscissa of the centre of the ellipse in nanometer

- The ordinate of the centre of the ellipse in nanometer
- The azimuth of the centre of the ellipse in nanometer
- First angle of Euler  $\psi$  by rotation around the axis  $z$
- Second angle of Euler  $\theta$  by rotation around the axis  $x$
- Third angle of Euler  $\varphi$  by rotation around the axis  $z$

### 6.2.11 Several spheres

For multiple spheres, it is convenient first to choose with the line from the under *number of objects* the number  $N$  of the expected spheres. Then, when we click on *Props N* windows, that we fill in the same way as for the unique sphere, appear. Beware, the spheres must be disconnected, otherwise, the code stops and shows error.

### 6.2.12 Cylinder

For the cylinder, there are eight fields to be fulfilled:

- The radius of the cylinder in nanometers
- The length of the cylinder in nanometer
- The abscissa of the centre of the cylinder in nanometer
- The ordinate of the centre of the cylinder in nanometer
- The azimuth of the centre of the cylinder in nanometer
- First angle of Euler  $\psi$  by rotation around the axis  $z$
- Second angle of Euler  $\theta$  by rotation around the axis  $x$
- Third angle of Euler  $\varphi$  by rotation around the axis  $z$

### 6.2.13 concentric spheres

For concentric spheres, it is convenient first to choose with the under line *number of objects* the number  $N$  of concentric spheres. Then, when we click on *Props N* windows appear. The first window is filled the same way as for the sphere, and for the next windows, it is enough to enter the radius in nanometer. The radii must be entered in increasing order, otherwise, the code shows the error.

### 6.2.14 Arbitrary object

In the case of an arbitrary object, it is defined by the user. In other words, he has to create the object himself, and then, it is convenient to create this entry file by respecting the conventions chosen by the code. *namefile* is the name of the file containing the arbitrary object and it is asked for when we choose the arbitrary object. It is coded in sequential and in ascii, and is necessarily described inside a cuboid box. Below are given the lines of the code enabling to create this file:

```
open(15,file=namefile,status='old',iostat=ierror)
write(15,*) nx,ny,nz
```

```

write(15,*) aretecube
do i=1,nz
  do j=1,ny
    do k=1,nx
      write(15,*) xs(i,j,k),ys(i,j,k),zs(i,j,k)
    enddo
  enddo
enddo
do i=1,nz
  do j=1,ny
    do k=1,nx
      if objet isotrope
        write(15,*) eps(i,j,k)
      elseif objet anisotrope
        do ii=1,3
          do jj=1,3
            write(15,*) epsani(ii,jj,i,j,k)
          enddo
        enddo
      endif
    enddo
  enddo
enddo
enddo

```

- nx : size of the cuboid according to the axis  $x$ .
- ny : size of the cuboid according to the axis  $y$ .
- nz : size of the cuboid according to the axis  $z$ .
- aretecube : size of the meshsize of discretization.
- x : abscissa of the mesh of discretization according the axis  $x$ .
- y : ordinate of the mesh of discretization according the axis  $y$ .
- z : azimuth of the mesh of discretization according the axis  $z$ .
- eps : epsilon of the object if isotropic
- epsani : epsilon of the object if anisotropic

### 6.3 Choose the relative permittivity

When the object or objects are chosen, it is then convenient to enter the relative permittivity. Apart from the arbitrary object, all the defined objects by default in the code are considered as being homogeneous. They may be isotropic or anisotropic. So, we choose *iso* or *aniso* and we click on *Epsilon*.

- *iso*: A board appears, where either we enter the relative permittivity by hand (real and imaginary part) or we choose a material in the data base.

- *aniso*: A board appears where we enter the relative permittivity by hand (real and imaginary part) for all the components of anisotropic tensor.

## 6.4 Choose the discretization

The number  $N_c$  entered in the field of the discretization corresponds to the number of layers forming the object in its largest direction.

A few examples:

- For an ellipse of half axis  $(a, b, c)$ , it is going to be the greatest half axis  $a$  that is going to be selected and the edge of discretization is going to be of  $2a/N_c$ .
- For a cube the number of meshsize is so going to be of  $N = N_c^3$ .



# Possible study with the code

---

## Contents

<b>7.1</b>	<b>Introduction</b>	<b>28</b>
<b>7.2</b>	<b>Study in far field</b>	<b>29</b>
<b>7.3</b>	<b>Microscopy</b>	<b>30</b>
<b>7.4</b>	<b>Study in near field</b>	<b>31</b>
<b>7.5</b>	<b>Optical force and torque</b>	<b>32</b>

---

## 7.1 Introduction

To determine the object with the appropriate orientation is not an easy task. That is why the first option *Only dipoles with epsilon*, enables us to check quickly if the object entered is well the one intended without any calculation being launched. Once this has been done, there are three great fields: the study in far field, the study in near field and the optical forces.

Important: Note that in the DDA the computation that takes the longest time is the calculation of the local field due to the necessity to solve the system of linear equations. One option has been added which consists in reading again the local field starting with a file. When this option is selected, the name of a file is asked for; either we enter an old file or a new name:

- If this is a new name, the calculation of the local field is going to be accomplished, then, stored together with the chosen configuration.
- - If this is an old name, the local field is going to be read again with a checking that the configuration has not been changed between the writing and the second reading. This makes it easier to relaunch calculations very quickly for the same configuration but for different studies.

Note also that if the calculation asked has a large number of discretization and that we are not interested by the output files in .mat (needs to use matlab), then we have the option “Do not write mat file”. This requires the code to write no .mat file, and allows the code to go faster, less fill the hard drive and be better parallelized.

## 7.2 Study in far field

When the option far field is selected, three possibilities appear:

- *Cross section*: This option enables us to calculate the extinction ( $C_{\text{ext}}$ ), absorbing ( $C_{\text{abs}}$ ) and scattering cross section ( $C_{\text{sca}}$ ). The scattering cross section is obtained through  $C_{\text{sca}} = C_{\text{ext}} - C_{\text{abs}}$ . The extinction and absorption cross sections may be evaluated as:

$$C_{\text{ext}} = \frac{4\pi k_0}{\|\mathbf{E}_0\|^2} \sum_{j=1}^N \text{Im} [\mathbf{E}_0^*(\mathbf{r}_j) \cdot \mathbf{p}(\mathbf{r}_j)] \quad (7.1)$$

$$C_{\text{abs}} = \frac{4\pi k_0}{\|\mathbf{E}_0\|^2} \sum_{j=1}^N \left[ \text{Im} [\mathbf{p}(\mathbf{r}_j) \cdot (\alpha^{-1}(\mathbf{r}_j))^* \mathbf{p}^*(\mathbf{r}_j)] - \frac{2}{3} k_0^3 \|\mathbf{p}^*(\mathbf{r}_j)\|^2 \right] \quad (7.2)$$

- *Cross section+Poynting*: This option calculates also the scattering cross section from the integration of the far field diffracted by the object upon  $4\pi$  steradians, the asymmetric factor and calculates differential cross section, *i.e.*  $\langle \mathbf{S} \rangle \cdot \mathbf{n} R^2$  with  $\mathbf{S}$  the Poynting vector,  $\mathbf{n}$  the direction of observation, which is going to be represented in 3D. The values  $N\theta$  and  $N\phi$  enable us to give the number of points used in order to calculate the scattering cross and to represent the Poynting vector. The larger the object is, the larger  $N\theta$  and  $N\phi$  must be, which leads to time consuming calculations for objects of several wavelengths.

$$C_{\text{sca}} = \frac{k_0^4}{\|\mathbf{E}_0\|^2} \int \left\| \sum_{j=1}^N [\mathbf{p}(\mathbf{r}_j) - \mathbf{n}(\mathbf{n} \cdot \mathbf{p}(\mathbf{r}_j))] e^{-ik_0 \mathbf{n} \cdot \mathbf{r}_j} \right\|^2 d\Omega \quad (7.3)$$

$$g = \frac{k_0^3}{C_{\text{sca}} \|\mathbf{E}_0\|^2} \int \mathbf{n} \cdot \mathbf{k}_0 \left\| \sum_{j=1}^N [\mathbf{p}(\mathbf{r}_j) - \mathbf{n}(\mathbf{n} \cdot \mathbf{p}(\mathbf{r}_j))] e^{-ik_0 \mathbf{n} \cdot \mathbf{r}_j} \right\|^2 d\Omega \quad (7.4)$$

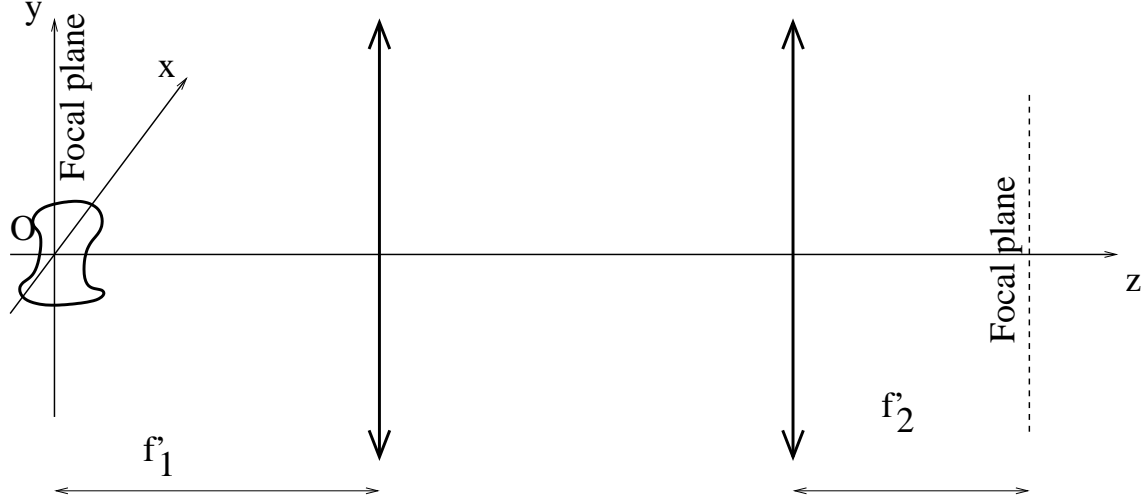
$$\langle \mathbf{S} \rangle \cdot \mathbf{n} R^2 = \frac{ck_0^4}{8\pi} \left\| \sum_{j=1}^N [\mathbf{p}(\mathbf{r}_j) - \mathbf{n}(\mathbf{n} \cdot \mathbf{p}(\mathbf{r}_j))] e^{-ik_0 \mathbf{n} \cdot \mathbf{r}_j} \right\|^2 \quad (7.5)$$

Another solution in order to go faster (option *quick computation*) and to pass by FFT for the calculation of the diffracted field. In this case, of course, it is convenient to discretize keeping in mind that the relation  $\Delta x \Delta k = 2\pi/N$  connects the mesh size of the discretization with the size of the FFT. The  $N$  chosen for the moment is  $N = 256$ . This is convenient for objects larger than the wavelength. Indeed,  $L = N\Delta x$  corresponds to the size of the object which gives  $\Delta k = 2\pi/L$ , and if the size of the object is too small, then, the  $\Delta k$  is too large, and the quadrature is imprecise. Note that since the integration is performed on two planes parallel to the plane  $(x, y)$ , is not convenient if the incident makes an angle more than 70 degrees with the  $z$  axis. The 3D representation of the vector of Poynting is done as previously, *i.e.* with  $N\theta$  and  $N\phi$  starting with an interpolation upon the calculated points with the FFT.

- *Energy Conservation*. This study computes the reflectance, transmittance and absorptance. If the object under study is no absorbing then the absorptance should be zero. Then it traduces the level of energy conservation of our solver. It can depend of the precision of the iterative method and of the polarizability chosen.

### 7.3 Microscopy

This option permits to compute the image obtained for different microscope (holographic, brightfield, darkfield and phase). It asks for the numerical aperture of the objective lens (necessarily between 0 and 1), then, calculates the field diffracted by the object and the picture obtained through the microscope. By default, the lenses are placed parallel to the plane  $(x, y)$  and at the side of the positive  $z$ . The focus of the microscope is placed to the origin of the frame but can be changed via the field “Position of the focal plane”. (Fig. 7.1). The magnification of the microscope is  $G$  and should be above 1.



**Figure 7.1 :** *Simplified figure of the microscope. The object focus of the objective lens is at the origin of the frame. The axis of the lens is confounded with the  $z$  axis and at the side of the positive  $z$ .*

The calculation for the diffracted field may be completed starting with the sum of the radiation of the dipoles (very long when the object has a lot of dipoles) or with FFT (option *quick computation*) with a value  $N = 128$  by default here as well. In this case,  $\Delta x \Delta k = 2\pi/N$  with  $\Delta x$  the mesh size of discretization of the object which corresponds also to the discretization of the picture plane. Consequently, this one has a size of  $L = N\Delta x$ .

The diffracted field in far field at a distance  $r$  of the origin can be written as  $\mathbf{E} = \mathbf{S}(k_x, k_y, \mathbf{r}_{\text{object}}) \frac{e^{ikr}}{r}$ . The field after the first lens is then defined as:  $\mathbf{E}^f = \frac{\mathbf{S}(k_x, k_y, \mathbf{r}_{\text{object}})}{-2i\pi\gamma}$  with  $\gamma = \sqrt{k_0^2 - k_x^2 - k_y^2}$  and the image through the microscope is given by its Fourier transform,  $\mathbf{E}^i = \mathcal{F}(\mathbf{E}^f)$ .

To take into account the magnification of the microscope in the image we perform a rotation of the vector  $\mathbf{E}^f$  before its Fourier transform as:

$$\mathbf{E}^i = \mathcal{F}(R(\theta)\mathbf{E}^f) \quad (7.6)$$

$$\text{with } R(\theta) = \begin{pmatrix} u_x^2 + \cos\theta(1 - u_x^2) & u_x u_y(1 - \cos\theta) & u_y \sin\theta \\ u_x u_y(1 - \cos\theta) & u_y^2 + \cos\theta(1 - u_y^2) & -u_x \sin\theta \\ -u_y \sin\theta & u_x \sin\theta & \cos\theta \end{pmatrix} \quad (7.7)$$

$$\theta = \sin^{-1}[\sin(-\beta)/G] - \beta \quad (7.8)$$

$$\beta = \cos^{-1}(k_z/k_0) \quad (7.9)$$

$$u_x = -k_y/k_{\parallel} \quad (7.10)$$

$$u_y = k_x/k_{\parallel}. \quad (7.11)$$

Note that we can simulate a microscope in transmission ( $k_z > 0$ ) or in reflexion ( $k_z < 0$ ). We can notice, for a microscope in transmission, that when the total field is computed in the Fourier plane (scattered plus incident field *i.e.* specular), in the case of the plane wave, a Dirac in the Fourier space is placed at the pixel the closest of the incident wave vector.

- *Holographic*: This option computes the diffracted field (Fourier plane) with the incident field defined in the section illumination properties. It computes the image plane with or without the presence of the incident field.
- *Brightfield*: This microscope uses a condenser lens, which focuses light from the light source onto the sample with a numerical aperture defined below the magnification. It consists to sum many incident field inside this numerical aperture with different polarizations, hence it can take time as it needs to solve many direct problem. The result is given in the image plane with the incident field (a kind of dark field) and with the incident field (brightfield).
- *Darkfield & phase*: In darkfield microscopy the condenser is designed to form a hollow cone of light with a numerical aperture equal to the condenser lens, as apposed to brightfield microscopy that illuminates the sample with a full cone of light. The result is given in the image plane (scattered field). In the phase microscopy the ring-shaped illuminating light that passes the condenser annulus is focused on the specimen by the condenser exactly as in the dark field microscope and then the incident field with a phase shifted of  $\pi/2$  is added to the scattered field.

## 7.4 Study in near field

When the option near field is selected, two possibilities appear:

- *Local field*: This option enables us to draw the local field to the position of each element of discretization. The local field being the field at the position of each element of discretization in absence of itself.
- *Macroscopic field*: This option enables us to draw the macroscopic field to the position of each element of discretization. The connection between the local field and the macroscopic field is given Ref. <sup>5</sup> :

$$\mathbf{E}_{\text{macro}} = 3 \left( \varepsilon + 2 - i \frac{k_0^3 d^3}{2\pi} (\varepsilon - 1) \right)^{-1} \mathbf{E}_{\text{local}} \quad (7.12)$$

The last option enables us to choose the mesh in which the local and macroscopic fields are represented.

- *Object*: Only the field in the object is represented. Notice that when FFT is used for the beam or for the computation of the diffracted field then this option is passed in the option *Cube*. This is same for the computation of the emissivity, the reread option and the use of the BPM(R).
- *Cube*: The field is represented within a cube containing the object.
- *Wide field*: The field is represented within a box greater than the object. The size of the box correspond to the size of the object plus the Additional sideband ( $x, y$  ou  $z$ )

on each side. For example for a sphere with a radius  $r = 100$  nm and discretization of 10, *i.e.* a meshsize of 10 nm, with an Additional sideband  $x$  of 2, 3 for  $y$  and 4 for  $z$ , we get a box of size:

$$l_x = 100 + 2 \times 2 \times 10 = 140 \text{ nm} \quad (7.13)$$

$$l_y = 100 + 2 \times 3 \times 10 = 160 \text{ nm} \quad (7.14)$$

$$l_z = 100 + 2 \times 4 \times 10 = 180 \text{ nm} \quad (7.15)$$

$$(7.16)$$

## 7.5 Optical force and torque

When the force option is selected, four possibilities appear:

- *Optical force*: Calculation of the optical force exerting on one or more objects.
- *Optical force density*: Enables us to draw the density of the optical force.
- *Optical torque*: Calculation of the optical torque exerting on one or more objects. The torque is computed for an origin placed in the gravity center of the object.
- *Optical torque density*: Enables us to draw the density of the optical force torque.

The net optical force and troque experienced by the object are computed with [22,23](#):

$$\mathbf{F} = (1/2) \sum_{j=1}^N \text{Re} \left( \sum_{v=1}^3 p_v(\mathbf{r}_j) \frac{\partial (E_v(\mathbf{r}_j))^*}{\partial u} \right) \quad (7.17)$$

$$\mathbf{\Gamma} = \sum_{j=1}^N \left[ \mathbf{r}_j \times \mathbf{F}(\mathbf{r}_j^g) + \frac{1}{2} \text{Re} \{ \mathbf{p}(\mathbf{r}_j) \times [\mathbf{p}(\mathbf{r}_j) / \alpha_{\text{CM}}(\mathbf{r}_j)]^* \} \right]. \quad (7.18)$$

where  $u$  or  $v$ , stand for either  $x$ ,  $y$ , or  $z$ . The symbol  $*$  denotes the complex conjugate.  $\mathbf{r}_j^g$  is the vector bewteen  $j$  and the center of masse of the object.

# Representation of the results

## Contents

<b>8.1 Introduction</b>	<b>33</b>
<b>8.2 Digital exits</b>	<b>33</b>
<b>8.3 Graphics</b>	<b>34</b>
8.3.1 Plot epsilon/dipoles	34
8.3.2 Far field and microscopy	34
8.3.3 Study of the near field	35
8.3.4 optical force and torque	35

## 8.1 Introduction

Three windows enable us to manage and represent the requested results. The one on the top enables us to manage the different figures; the one at the bottom on the left present the digital values requested, and the one at the bottom on the right is kept for the graphic representations.

## 8.2 Digital exits

All the results are given in the SI system.

- *Object subunits*: Number of elements of discretization of the object under study.
- *Mesh subunits* : Number of elements of discretization of the cuboid containing the object under study.
- *Mesh size* : Size of the element of discretization.
- $\lambda/(10n)$  : In order to obtain a good precision, it is advised to have a discretization under the value of  $\lambda/10$  in the considered material of optical index  $n$ .
- $k_0$  :Wave number.
- *Irradiance*: Beam irradiance, for a Gaussian beam, it is estimated at the center of the waist.

- *Field modulus*: Modulus of the field, for a Gaussian beam, it is estimated at the center of the waist.
- *Tolerance obtained*: Tolerance obtained for the chosen iterative method. Logically under the requested value.
- *Number of products  $Ax$  (iterations)*: Number of matrix vector products completed by the iterative method. Between brackets the iteration number of the iterative method.
- *Extinction cross section*: Value of the extinction cross section.
- *Absorbing cross section*: Value of the absorbing cross section.
- *Scattering cross section*: Value of the scattering cross section obtained by = extinction cross section- absorbing cross section.
- *Scattering cross section with integration*: Value of the scattering cross section obtained by integration of the far field field radiated by the object.
- *Scattering asymmetric parameter*: Asymmetric factor.
- *Optical force  $x$* : Optical force according to the axis  $x$ .
- *Optical force  $y$* : Optical force according to the axis  $y$ .
- *Optical force  $z$* : Optical force according to the axis  $z$ .
- *Optical force modulus*: Modulus of the optical force.
- *Optical torque  $x$* : Optical torque according to the axis  $x$ .
- *Optical torque  $y$* : Optical torque according to the axis  $x$ .
- *Optical torque  $z$* : Optical torque according to the axis  $x$ .
- *Optical torque modulus*: Modulus of the optical torque.

## 8.3 Graphics

### 8.3.1 Plot epsilon/dipoles

The button *Plot epsilon/dipoles* enables us to see the position of each element of discretization. The colour of each point is associated with the value of the permittivity of the considered meshsize.

### 8.3.2 Far field and microscopy

#### 8.3.2.1 Plot Poynting vector

*Plot Poynting*: enables us to draw the modulus of the Poynting vector in 3D.

### 8.3.2.2 Plot microscopy

*Plot microscopy* enables us to draw the diffracted field in far field by the object may this be either of the modulus of the field or of the  $x$ ,  $y$  or  $z$ . Then, the vectorial field on the picture plane is represented by considering a magnification  $G$  for the microscope.

The diffracted field is represented upon a regular mesh in  $\Delta k_x = \Delta k_y$  such as  $\sqrt{k_x^2 + k_y^2} \leq k_0$  NA with the origin of the phase at the origin of the frame  $(x, y, z)$ . If the computation is done by radiation of the dipoles, then, the obtained picture has a size  $k_0 NA$  and discretized as  $\Delta k_x = 2k_0 NA/N$ , and if this one is done with Fourier transform, then, the size of the picture is fixed by discretization of the object  $\Delta x$  with the relation  $\Delta x \Delta k = 2\pi/N$ .

The field inside the picture plane is calculated with Fourier transform. So, we have with the calculation by radiation of the dipoles:

$$\Delta x \Delta k_x = \frac{2\pi}{N} \quad (8.1)$$

$$\Delta x 2k_0 NA = 2\pi \quad (8.2)$$

$$\Delta x = \frac{\lambda}{2NA} \quad (8.3)$$

The size of the picture is then  $\lambda/(2NA)$ .

If the calculation of the diffracted field has been made by FFT, then, the discretization is that of the mesh.

For the holographic microscope we present the Fourier plane (with and without the incident field) and the image plane (with and without the incident field). For the brightfield options we present the image plane with the incident field (brightfield) and without the incident field (a kind of darkfield). For the darkfield & phase option we present the image plane without the incident (darkfield) and with the incident phase shifted of  $\pi/2$  (phase).

### 8.3.3 Study of the near field

- The first button *Field* enables us to choose to represent the incident field, local field or macroscopic field.
- The button *Type* enables us to represent the modulus or the component  $x$ ,  $y$  or  $z$  of the studied field.
- The button *Cross section  $x$*  ( $y$  or  $z$ ) enables us to choose the abscissa of the cut (ordinate or dimension). *Plot  $x$*  ( $y$  or  $z$ ) draws the cut in plane  $x$ . *Plot all  $x$*  draws all the cut at once.

### 8.3.4 optical force and torque

- The first button *Field* enables us to choose to represent the optical force or the optical torque.
- The button *Type* enables us to choose to represent the modulus or the component  $x$ ,  $y$  or  $z$  of the studied field.
- The button *Cross section  $x$*  ( $y$  or  $z$ ) enables us to choose the abscissa of the cut (ordinate or azimuth). *Plot  $x$*  ( $y$  or  $z$ ) draws the cur. *Plot all  $x$*  draws all the cuts at once.



# Output files for matlab, octave, scilab,...

---

## Contents

---

<b>9.1 Introduction</b>	<b>36</b>
<b>9.2 List of all exit files</b>	<b>37</b>

---

## 9.1 Introduction

It is not necessary to use the graphic interface of the program to watch the results. For the scalar, all the results are in the output file and for the pictures, it is possible to use directly the exit files in ascii and to read them through other softwares such as Matlab, Octave, Scilab,...For example in the directory bin the field ifdda.m uses matlab to represent the different data.

When the advanced option is chosen, it is possible to choose to save the data either in separate .mat files or in a single hdf5 file.

- In the case of the hdf5 file, there are six created groups: option (the options chosen by the user), near field (the near field data), microscopy (data from the microscopy), far field (data from the far field option), and dipole (position of the elements of discretization and permittivity).
- In the case of .mat file, all the output are formatted in the form of a unique column vector or two column vectors if the number is a complex (the real part being associated with the first column and the imaginary part with the second column).
- In the hdf5 file all the data are formatted under the form of a single column vector and with two separate tables in the case of complex numbers.
- In the case where the file contains three-dimensional data, these ones are always stored as follows:

```
do i=1,nz
  do j=1,ny
    do k=1,nx
      write(*,*) data(i,j,k)
```

**enddo**  
**enddo**  
**enddo**

Three-dimensional data are going to be recognized by 3D at the beginning of the line.

## 9.2 List of all exit files

- $x, y, z$  represent the different used coordinates.
- (3D)  $\epsilon$  contain the permittivity of the object.
- (3D)  $x_c, y_c, z_c$  contain the coordinates of all the points of the mesh.
- (3D)  $x_{wf}, y_{wf}, z_{wf}$  contain the coordinates of all the points of the mesh in which the near field is calculated when the wide field option (wide field) is used.
- (3D complex)  $\text{incidentfield}_x(x, y)$  contains the component  $x(y, z)$  of the incidental field only inside the object.
- (3D)  $\text{incidentfield}$  contains the modulus of the incident field only inside the object.
- (3D complexe)  $\text{macroscopicfield}_x(x, y)$  contains the component  $x(y, z)$  of the macroscopic field only inside the object.
- (3D) contains the modulus of the macroscopic field only inside the object.
- (3D complexe)  $\text{mlocalfield}_x(x, y)$  contains the component  $x(y, z)$  of the local field only inside the object.
- (3D)  $\text{localfield}$  contains the modulus of the local field only inside the object.
- (3D complexe)  $\text{incidentfield}_{xwf}(x, y)$  contains the component  $x(y, z)$  of the incident field inside the box of near field in wide field.
- (3D)  $\text{incidentfield}_{wf}$  contains the modulus of the incidental field inside the box of near field in wide field.
- (3D complexe)  $\text{macroscopicfield}_{xwf}(x, y)$  contains the component  $x(y, z)$  of the macroscopic field inside the box of near field in wide field.
- (3D)  $\text{macroscopicfield}_{wf}$  contains the modulus of the macroscopic field inside the box of near field in wide field.
- (3D complexe)  $\text{localfield}_{xwf}(x, y)$  contains the component  $x(y, z)$  of the local field inside the box of near field in wide field.
- (3D)  $\text{localfield}_{wf}$  contains the modulus of the local field inside the box of near field in wide field.
- $\theta$  is a board which contains all the  $\theta$  angles corresponding to all the directions in which the vector of Poynting is calculated. Its size is  $(N_{\theta}+1)*N_{\phi}$ .
- $\phi$  is a board which contains all the  $\theta$  angles corresponding to all the directions in which the vector of Poynting is calculated. Its size is  $(N_{\theta}+1)*N_{\phi}$ .

- poynting pointing contains the modulus of the vector of Poynting in theta and phi direction of size  $(N_{\theta}+1)*N_{\phi}$ .
- (3D) forcex (y,z) contains the  $x$  component of the optical force only inside the object.
- (3D) torquex (y,z) contains the  $x$  component of the optical torque force only inside the object.
- (2D) fourier(x,y,z) contains the diffracted field in the fourier plane in modulus (x,y,z).
- (2D) fourierinc(x,y,z) contains the total field in the fourier plane in modulus (x,y,z).
- kxfourier contains the coordinates of the Fourier plane.
- (2D) image(x,y,z) contains the diffracted field in the image plane in modulus (x,y,z).
- (2D) imageinc(x,y,z) contains the total field in the image plane in modulus (x,y,z).
- (2D) imagebf(x,y,z) contains the diffracted field in the image plane in modulus (x,y,z) for a dark field.
- (2D) imageincbf(x,y,z) contains the total field in the image plane in modulus (x,y,z) for a brightfield microscope.
- (2D) imagedf(x,y,z) contains the diffracted field in the image plane in modulus (x,y,z) for a dark field.
- (2D) imageincdf(x,y,z) contains the total field in the image plane in modulus (x,y,z) for a phase microscope.
- Poynting contains the Poynting modulus for the direction  $\theta$  and  $\phi$ .
- theta and phi contains the direction  $\theta$  and  $\phi$  for Poynting.
- poyntingneg and poyntingpos contain the Poynting modulus for  $k_z < 0$  and  $k_z > 0$  respectively in the plane  $(k_x, k_y)$ .
- kx and ky contain the coordinates for poyntingneg and poyntingpos.

---

# Some examples

---

## Contents

---

<a href="#">10.1 Introduction</a>	39
<a href="#">10.2 Test1</a>	39
<a href="#">10.3 Test2</a>	43
<a href="#">10.4 Test3</a>	46
<a href="#">10.5 Test4</a>	47

---

## 10.1 Introduction

In bin/tests there is the file options.db3. You should copy it in the directory bin as "cp options.db3. /.", and then you launch the code after the load four test configurations appear that allow you to see all the options in action.

## 10.2 Test1

The aim of test1 is to test a simple case and many options of the code to validate them. Figure [10.1](#) shows the options of the chosen configuration.

Start calculation

Save configuration

Calculation options

rigorous

Read local field from file

Database file

Save in HDF5 file

Name h5 file

ifdda.h5

Advanced interface

☒

Wavelength (nm)

632.8

Power (W)

1

Waist (nm)

6328

Beam

Linear plane wave

Props

Number of plane waves

1

Object properties

Object

sphere

Props

Number of objects

1

Anisotropy

iso

Epsilon

Discretization

20

Study

Only dipoles

☐

Far field

☒

Cross section

☒

Poynting + asymmetry factor

☒

Quick computation (FFT)

☒

Ntheta:

36

Nphi:

72

Energy conservation

☒

Microscopy

☒

Microscope

Holographic

Side of observation

kz>0 (transmis:)

Quick computation (FFT)

☒

Numerical aperture [0,1] (objective lens)

0.9

Magnification

100

Focal plane position (nm)

200

Optical Force

☒

Optical force

☒

Optical force density

☒

Optical torque

☒

Optical torque density

☒

Near field

☒

Local field

☒

Macroscopic field

☒

Range of study

Wide field

Additional sideband x

1

Additional sideband y

2

Additional sideband z

3

Numerical parameters

Iterative Method Tolerance

0.0001

Iterative Method

GPBICG1

Polarizability

RR

Integration Green function

2

FFT size for far field

512

Figure 10.1 : Test1: configuration taken.

The following figures show the results obtained. The plots are done with Matlab and these are directly the eps files from the ifdda.m script that are used. The advantage of matlab in this case is to give all the figures in one go.

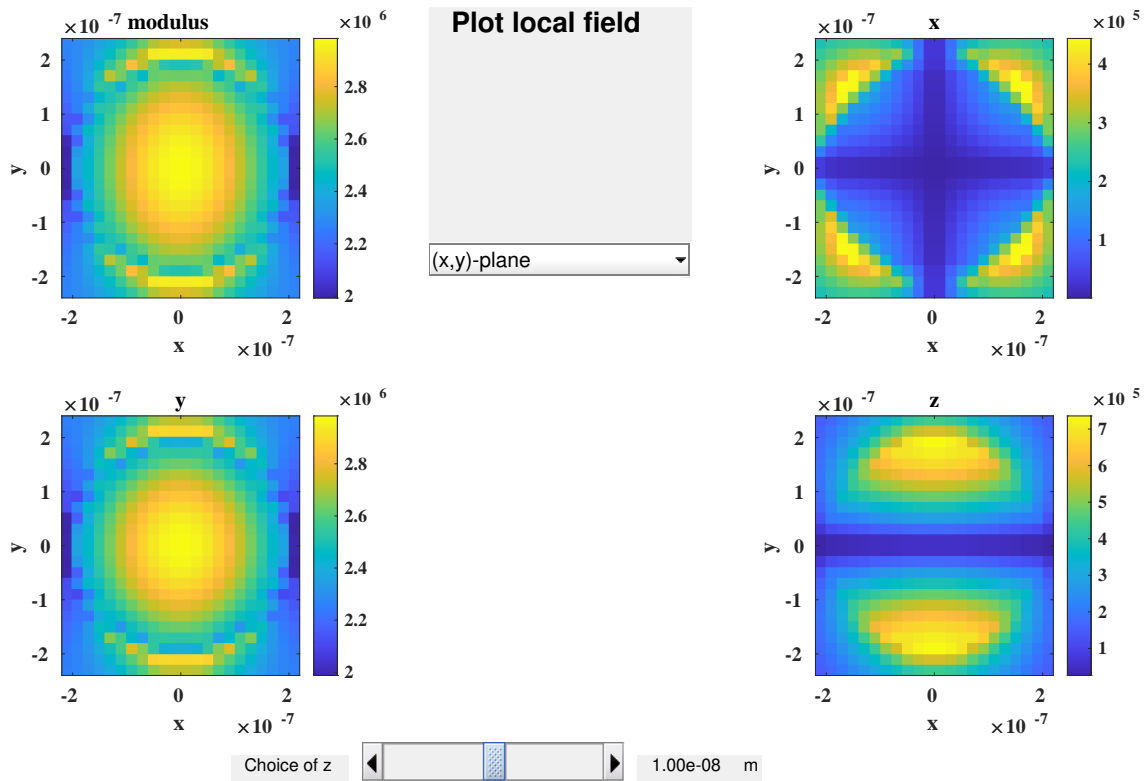


Figure 10.2 : Modulus of the local field in (x,y) plane.

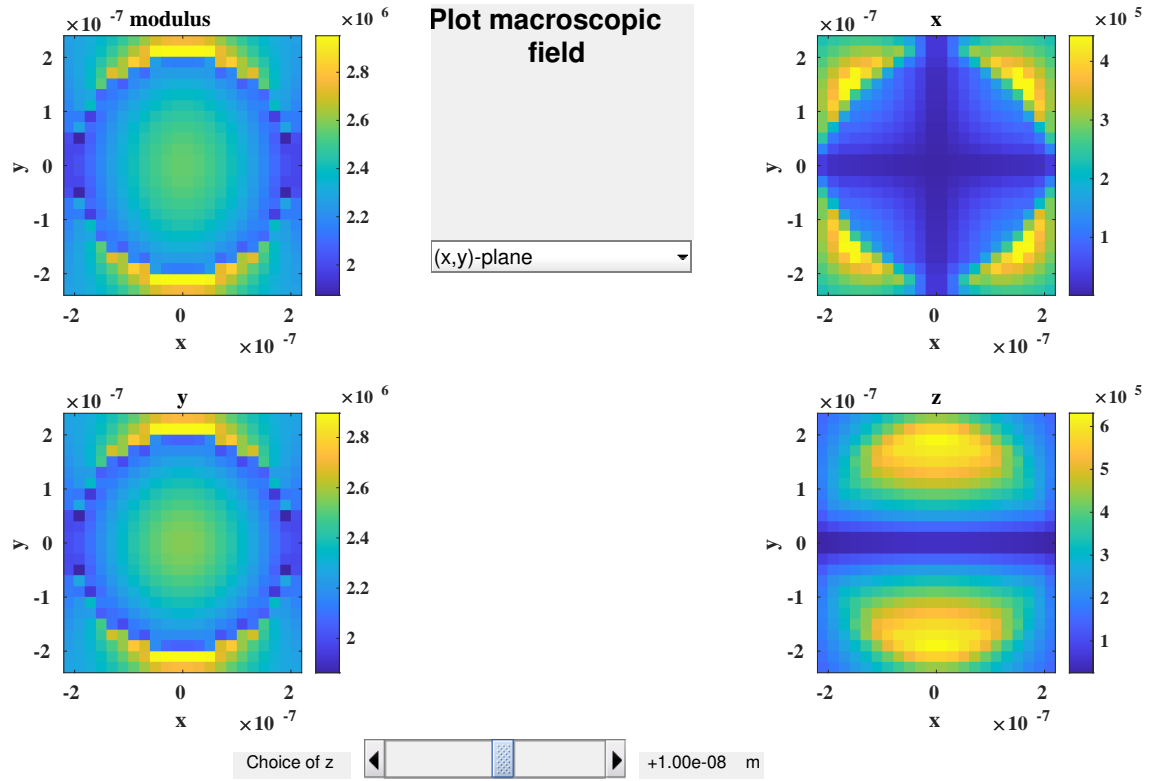


Figure 10.3 : Modulus of the macroscopic field in  $(x,y)$  plane.

Because the incident field is polarized along the  $y$  direction (TE), hence the  $y$  component of the field inside the sphere is the largest.

Poynting Modulus in  $k_x$  and  $k_y$  plane

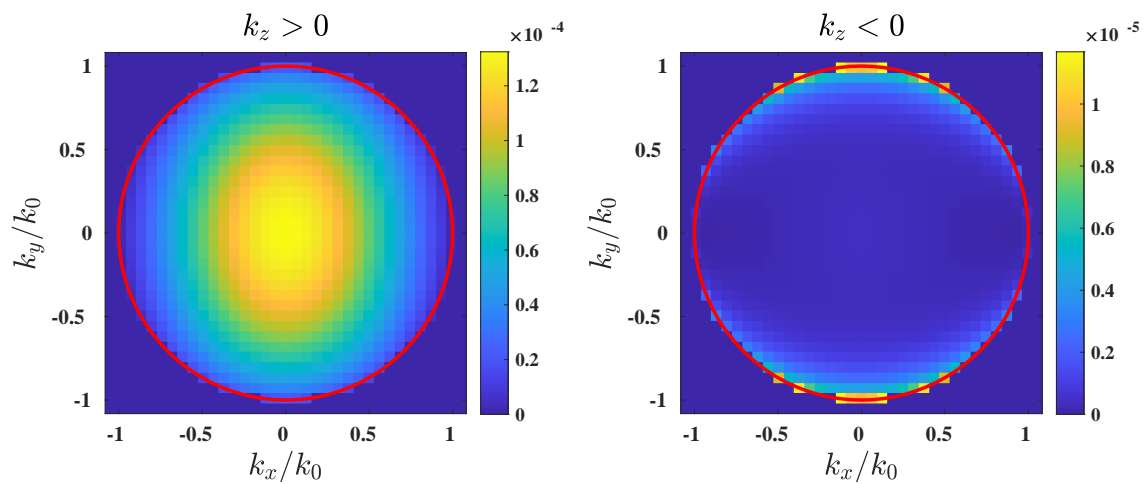


Figure 10.4 : Modulus of the Poynting vector.

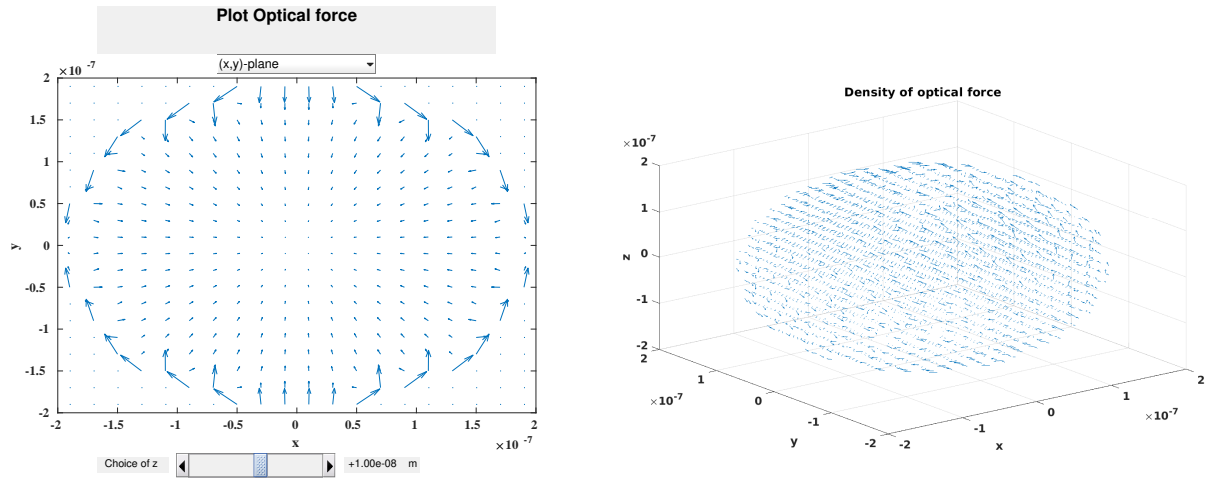


Figure 10.5 : Optical force in the  $(x,y)$  plane and in 3D.

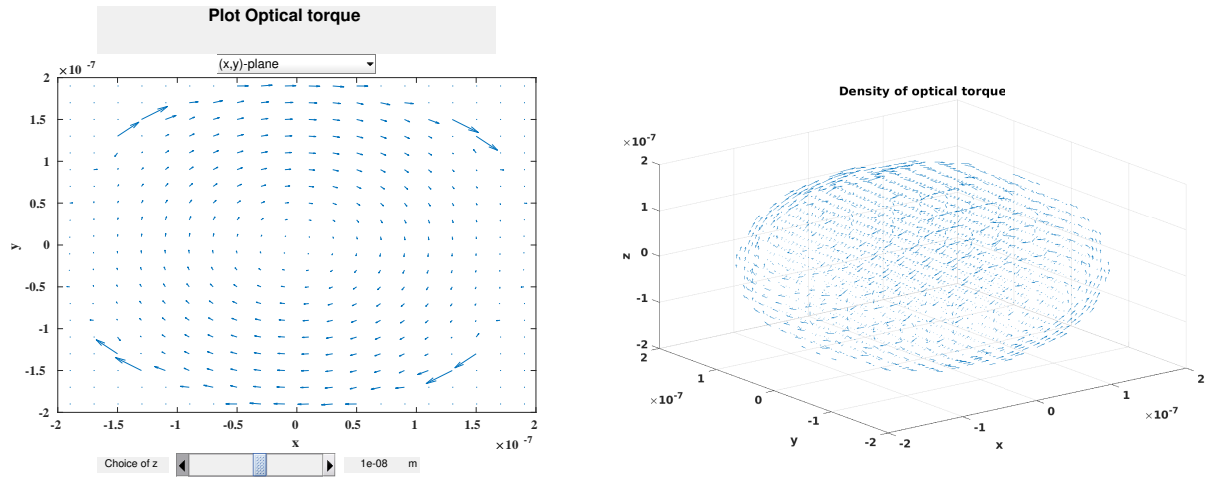


Figure 10.6 : Optical torque in the  $(x,y)$  plane and in 3D.

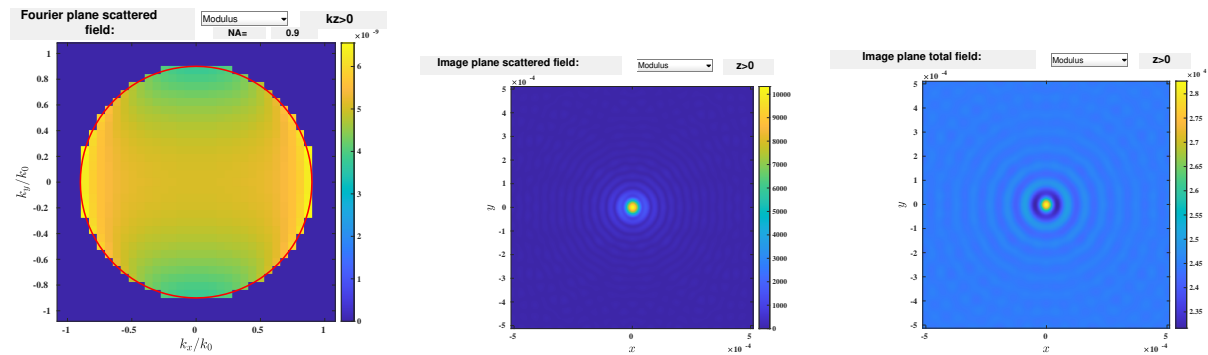


Figure 10.7 : Microscopy in transmission: Modulus of the diffracted field in the Fourier plane (left), modulus of the diffracted field in the image plane (middle), and modulus of the total field in the image plane (right).

## 10.3 Test2

The aim of the test2 is to test a simple case and many options code to validate them. Figure 10.8. shows the options of the chosen configuration. The illumination is done by two plane waves.

Figure 10.8 : Test2: configuration taken.

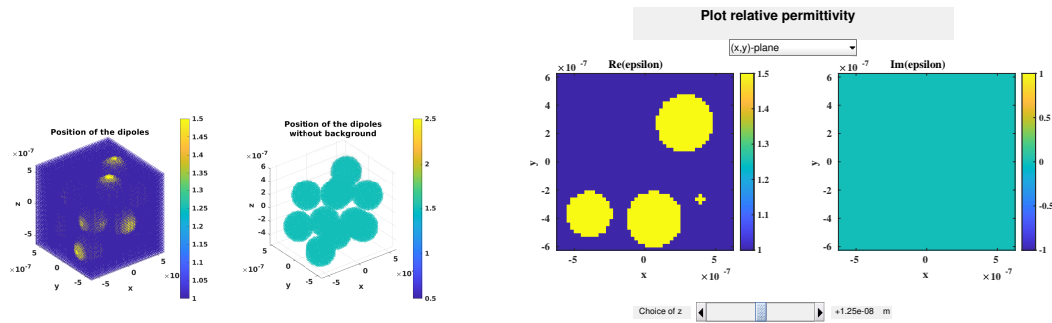


Figure 10.9 : Object in 3D (left) and map of permittivity in the  $(x,y)$  plane (right).

The following figures show the results obtained.



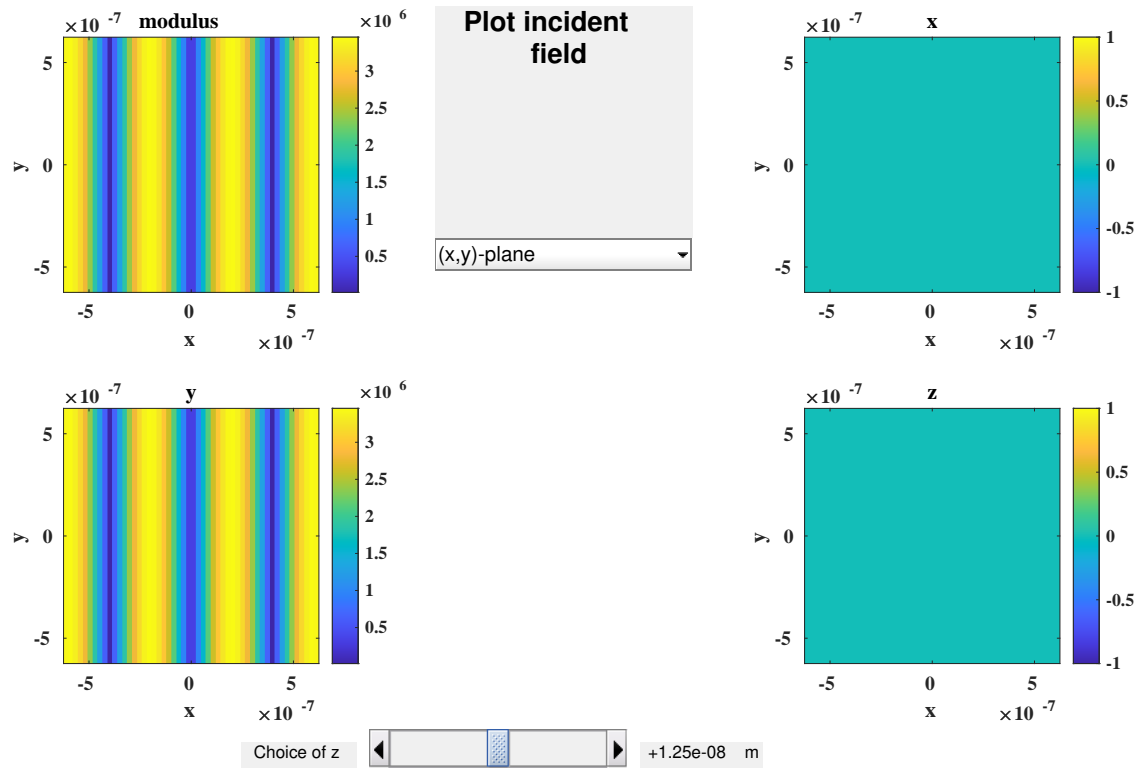


Figure 10.10 : Modulus of the incident field in  $(x,y)$  plane.

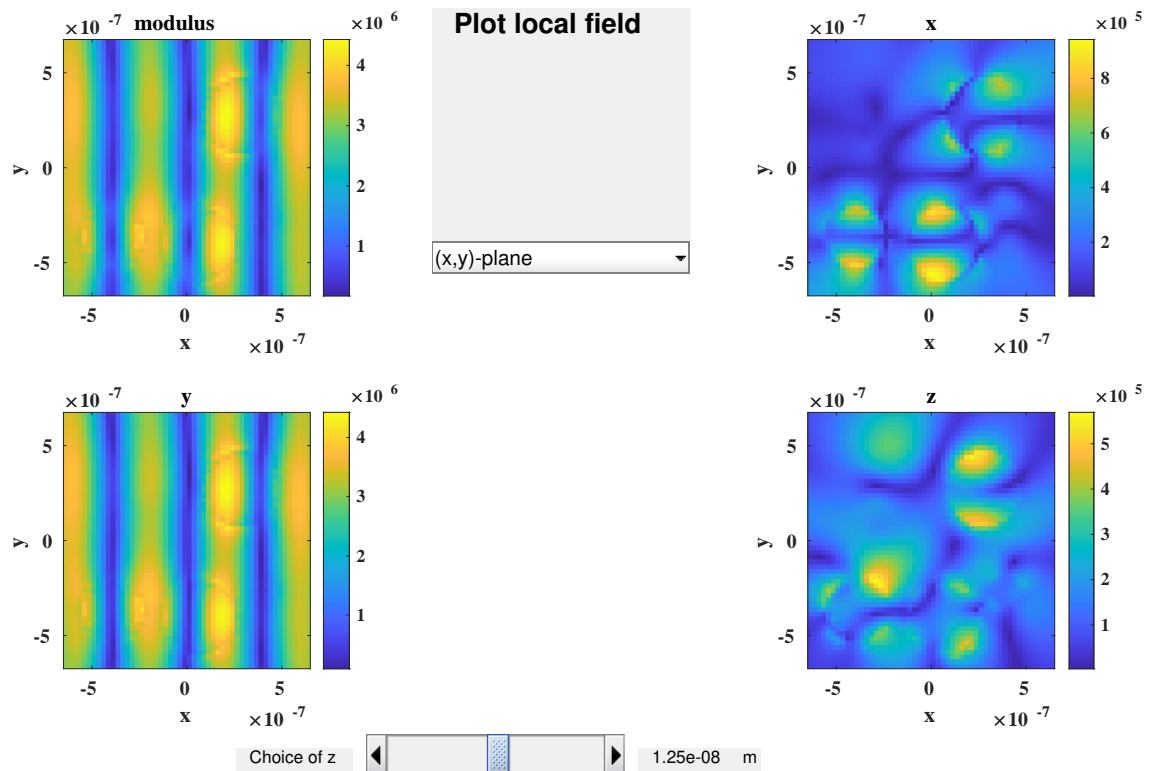


Figure 10.11 : Modulus of the local field in  $(x,y)$  plane.

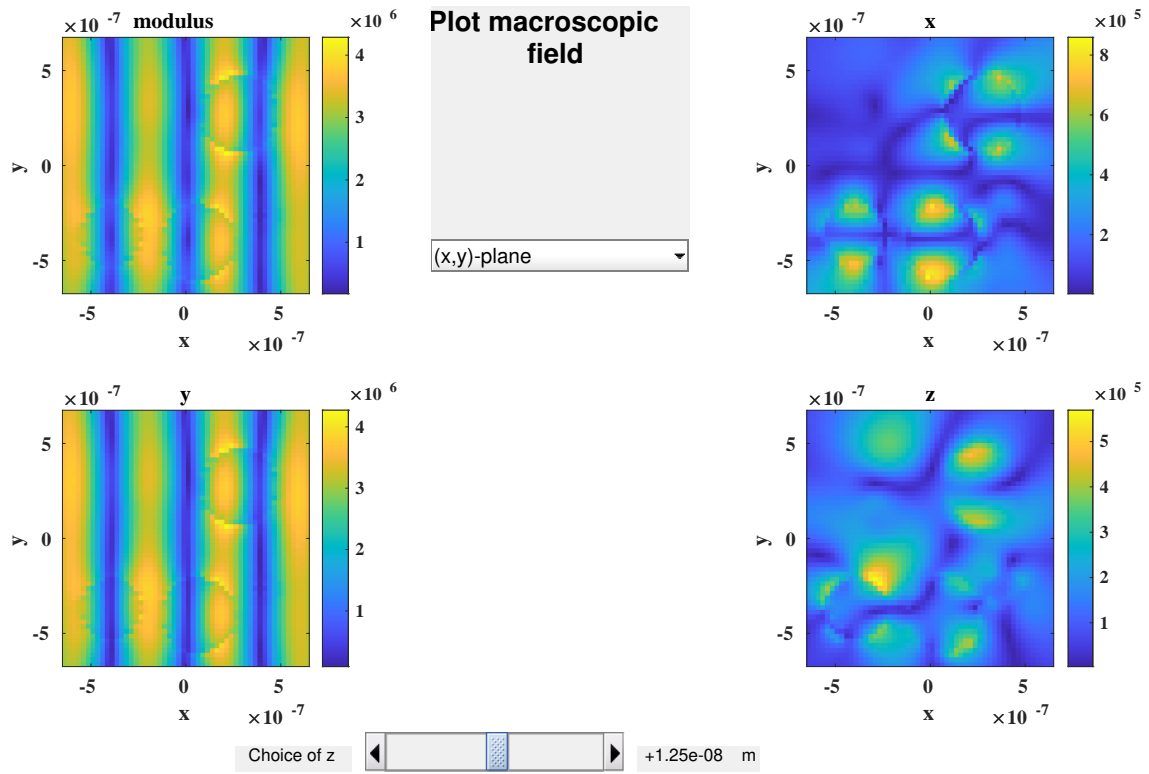


Figure 10.12 : Modulus of the macroscopic field in  $(x, y)$  plane.

Poynting Modulus in  $k_x$  and  $k_y$  plane

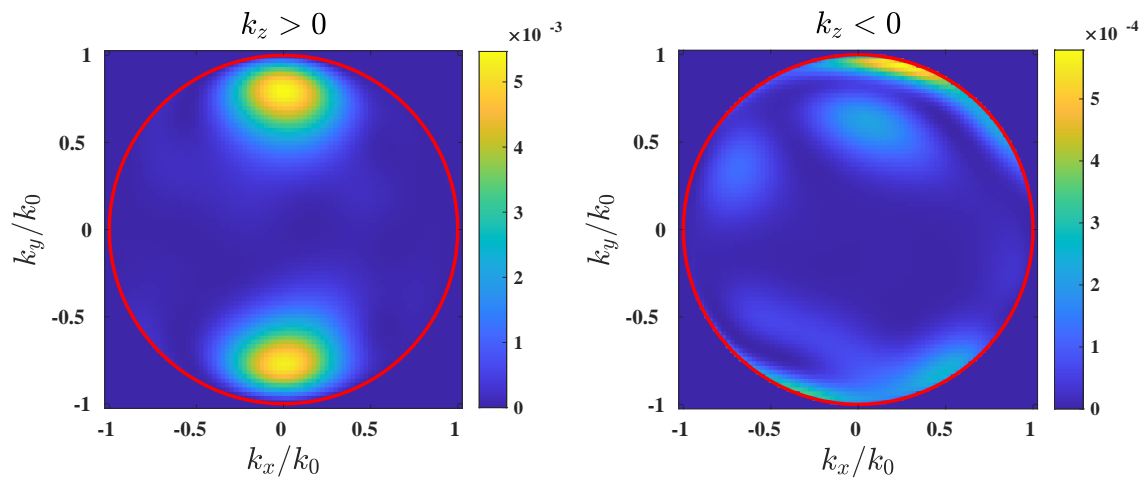
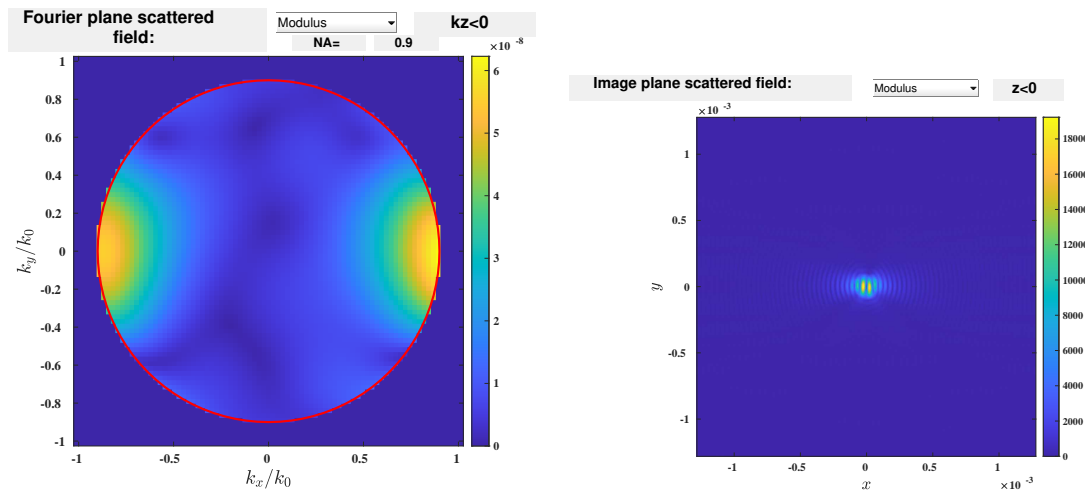


Figure 10.13 : Modulus of the Poynting vector.



**Figure 10.14 :** *Microscopy in reflection: Modulus of the diffracted field in the Fourier plane (left) and in image plane (right).*

## 10.4 Test3

The aim of the test3 is to test the microscopy in dark field and bright field in transmission. One studies a sphere with a radius of 500 nm and permittivity 1.5.

Start calculation

Save configuration

Calculation options

rigorous

Read local field from file

☐

Database file

Save in HDF5 file

Name h5 file

ifdda.h5

Advanced interface

☒

Wavelength (nm)

632.8

Power (W)

1

Waist (nm)

300

Beam

Linear plane wave

Props

Number of plane waves

1

+

-

Object

sphere

Props

Number of objects

1

+

-

Anisotropy

iso

Epsilon

Discretization

40

Only dipoles

☐

Far field

☐

Microscopy

☒

Microscope

Brightfield

Side of observation

kz>0 (transmis:)

Quick computation (FFT)

☒

Numerical aperture [0,1] (objective lens)

0.9

Magnification

100

Focal plane position (nm)

0

Numerical aperture [0,1] (condenser lens)

0.8

Optical Force

☐

Near field

☐

Iterative Method Tolerance

0.0001

Iterative Method

GPBICG1

Polarizability

LA

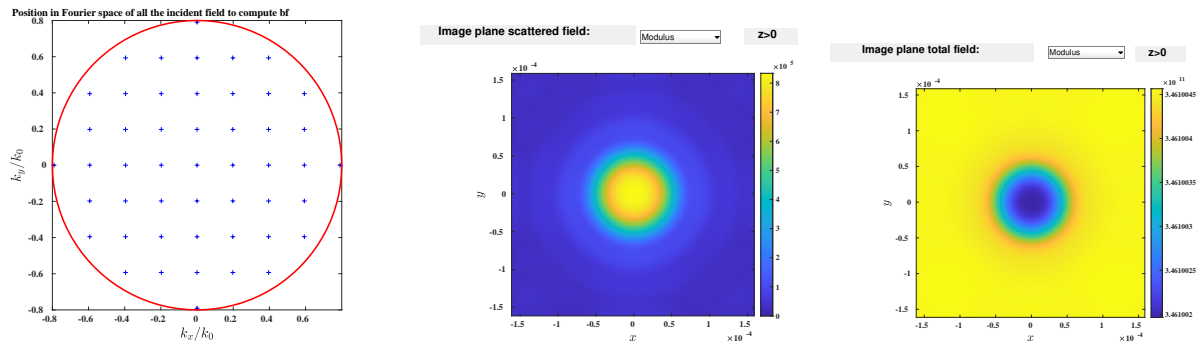
Integration Green function

0

FFT size for far field

128

**Figure 10.15 :** *Test3: configuration taken.*



**Figure 10.16 :** *Microscopy in transmission: incident taken to make the image (left). Modulus of the diffracted field in the image plane (middle), and modulus of the total field in the image plane (right).*

## 10.5 Test4

Same configuration as in test3 for a dark field microscope.

Start calculation

Save configuration

Calculation options

rigorous

Read local field from file

☐

Database file

Save in HDF5 file

Name h5 file

ifdda.h5

Advanced interface

☒

**Illumination properties**

Wavelength (nm)

632.8

Power (W)

1

Waist (nm)

6328

Beam

Linear plane wave

Props

Number of plane waves

1

**Object properties**

Object

sphere

Props

Number of objects

1

Anisotropy

iso

Epsilon

Discretization

40

**Study**

Only dipoles

☐

Far field

☐

Microscopy

☒

Microscope

Darkfield & pha

Side of observation

kz<0 (reflexion)

Quick computation (FFT)

☒

Numerical aperture [0,1] (objective lens)

0.9

Magnification

100

Focal plane position (nm)

500

Numerical aperture [0,1] (condenser lens)

0.8

Optical Force

☐

Near field

☐

**Numerical parameters**

Iterative Method Tolerance

0.0001

Iterative Method

GPBICG1

Polarizability

LA

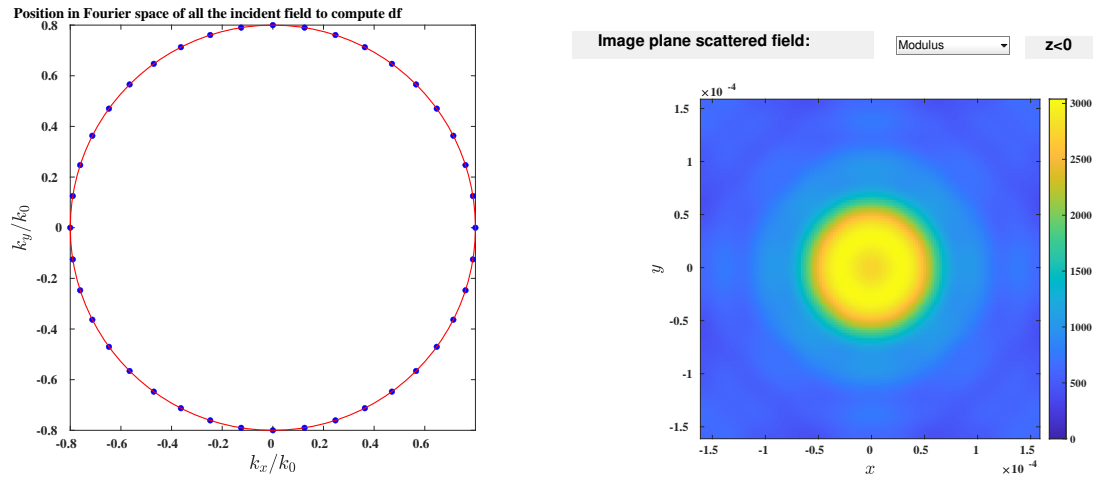
Integration Green function

0

FFT size for far field

128

**Figure 10.17 :** *Test4: configuration taken.*



**Figure 10.18 :** *Microscope in reflection: incident taken to make the image (left). Modulus of the diffracted field in the image plane (right).*

---

# Bibliography

---

- [1] F. M. Kahnert, J. Quant. Spect. Rad. Transf. **79-80**, 775 (2003).
- [2] E. M. Purcell and C. R. Pennypacker, Astrophys. J. **186**, 705 (1973).
- [3] A. Rahmani, P. C. Chaumet, F. de Fornel, and C. Girard, Phys. Rev. A **56**, 3245 (1997).
- [4] B. T. Draine, Astrophys. J. **333**, 848 (1988).
- [5] P. C. Chaumet, A. Sentenac, and A. Rahmani, Phys. Rev. E **70**, 036606 (2004).
- [6] A. D. Yaghjian, Proceedings of the IEEE **68**, 248 (1980), ISSN 0018-9219.
- [7] U. S. Kamilov, I. N. Papadopoulos, M. H. Shoreh, A. Goy, C. Vonesch, M. Unser, and D. Psaltis, IEEE Transactions on Computational Imaging **2**, 59 (2016), ISSN 2333-9403.
- [8] G. H. Goedecke and S. G. O'Brien, Appl. Opt. **27**, 2431 (1988).
- [9] A. Lakhtakia, Int. J. Mod. Phys. C **3**, 583 (1992).
- [10] B. T. Draine and J. Goodman, Astrophys. J. **405**, 685 (1993).
- [11] A. Rahmani, P. C. Chaumet, and G. W. Bryant, Astrophys. J. **607**, 873 (2004).
- [12] P. C. Chaumet and A. Rahmani, Opt. Lett. **34**, 917 (2009).
- [13] M. Thuthu, S. Fujino, and Y. Onoue, IMECS **1** (2009).
- [14] S. Fujino and T. Sekimoto, IMECS **2** (2012).
- [15] R. D. Da Cunha and T. Hopkins, Appl. Numer. Math. **19**, 33 (1995).
- [16] T. F. Chan, E. Gallopoulos, V. Simoncini, T. Szeto, and C. H. Tong, SIAM J. Sci. Comput. **15**, 338 (1994).
- [17] L. Zhao, T.-Z. Huang, Y.-F. Jing, and L.-J. Deng, Computers & Mathematics with Applications **66**, 1372 (2013), ISSN 0898-1221.
- [18] B. Carpentieri, Y.-F. Jing, T.-Z. Huang, W.-C. Pi, and X.-Q. Sheng, Computational Electromagnetics International Workshop pp. 85–90 (2011).
- [19] S. Fujino and K. Iwasato, Proc. of the World Congress on Engineering **1** (2015).

- [20] G. P. Agrawal and D. N. Pattanayak, J. Opt. Soc. Am. A **69**, 575 (1979).
- [21] P. C. Chaumet, J. Opt. Soc. Am. A **23**, 3197 (2006).
- [22] P. C. Chaumet and M. Nieto-Vesperinas, Opt. Lett. **25**, 1065 (2000).
- [23] P. C. Chaumet and C. Billaudeau, J. Appl. Phys. **101**, 023106 (2007).