# MAE 438/538 Hybrid ODF Maglev Ball system Part 1

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# TABLE OF CONTENTS

Task #1 – System Choice

Task #2 – Linearized system model, transfer function, and state-space realization

Task #3 – Expected Performance

Task #4 – Preliminary Design Evaluation

Task #5 – Nonlinear Simulink system

### TASK 1 – SYSTEM CHOICE

The purpose of the system is to levitate a steel ball using magnetic forces. It is called a hybrid system because it consists of a permanent magnet and an electromagnet; the use of a permanent magnet means that less power is required for the electromagnet to raise and maintain the height of the ball, but it also means that there is a minimum nonzero distance between the ball and the top of the apparatus where the magnets are positioned, which is referred to as the minimum air gap. The height of the ball is controlled by the current through the coil of wire of the electromagnet (which is induced by applying a voltage across the terminals of the coil).

The two measured parameters are the command current and the height of the ball, which employs the use of two laser sensors. The nonlinear equations that describe the physical motion and the electrical behavior of the system are as follows:

$$\ddot{z} = -\frac{K_f}{m} \left[ \frac{a_1 + I}{a_2 + z} \right]^2 + g$$

$$K_a(I_c - I) = -RI + \dot{I} \frac{K_l}{(a_2 + z)} - (a_1 + I) \frac{K_l \dot{z}}{(a_2 + z)^2}$$

$$V(t)$$

$$V(t)$$

$$T_l = \text{minimum safe } z - \text{dist}$$

$$T_l = \text{minimum safe } z - \text{dist}$$

$$T_l = \text{minimum height}$$

$$T_l = m_l$$

z<sub>2</sub>= maximum z-dist

# PARAMETER VALUES

$$a_1 = 46.5894 Amps$$

$$a_2 = 0.007 \ m$$

$$K_f = 5.0678e - 6$$

$$K_a = 11.7858$$

$$K_l = 0.0065$$

$$m = 1.1 \text{ kg}$$

$$R = 1.1 ohms$$

$$g = 9.81 \text{ m/s}^2$$

### TASK 2 – Linearized System Model

 $z_o$  – equilibrium height

 $I_o$  – equilibrium current

$$\ddot{z} = \frac{\partial \ddot{z}}{\partial z} * z + \frac{\partial \ddot{z}}{\partial I} * I$$

$$\ddot{z} = \frac{2K_f}{m} \frac{(I_o + a_1)}{(z_o + a_2)^2} \left[ \frac{(I_o + a_1)}{(z_o + a_2)} * z - I \right]$$

$$\dot{I} = \frac{\partial \dot{I}}{\partial z}z + \frac{\partial \dot{I}}{\partial \dot{z}}\dot{z} + \frac{\partial \dot{I}}{\partial I}I + \frac{\partial \dot{I}}{\partial I_c}I_c$$

$$\frac{\partial \dot{i}}{\partial z} z = \frac{K_a (I_c - I_o) + I_o R - \frac{K_l (I_o + a_1)}{(a_2 + z_o)^2}}{K_l} z \qquad \qquad \frac{\partial \dot{i}}{\partial \dot{z}} \dot{z} = \frac{(I_o + a_1)}{(z_o + a_2)} \dot{z} 
\frac{\partial \dot{i}}{\partial l} I = \left[ \frac{R}{K_l} (z_{o+} a_2) + \frac{\dot{z}_o}{(z_{o+} a_2)} - \frac{K_a}{K_l} (z_{o+} a_2) \right] I \qquad \qquad \frac{\partial \dot{i}}{\partial I_c} I_c = \frac{K_a}{K_l} (z_o + a_2) I_c$$

### **State space representation:**

$$\dot{\vec{x}} = A\vec{x} + Bu$$
 where the transfer function is  $H(s) = \frac{Y(s)}{X(s)} = C(sI - A)^{-1}B + D$   
 $y = C\vec{x} + Du$ 

$$\mathbf{x} = \begin{pmatrix} \mathbf{z} \\ \dot{\mathbf{z}} \\ \mathbf{I} \end{pmatrix}$$
 ,  $\dot{\mathbf{x}} = \begin{pmatrix} \dot{\mathbf{z}} \\ \ddot{\mathbf{z}} \\ \dot{\mathbf{j}} \end{pmatrix}$  ,  $u = I_c$  ,  $y = z$ 

$$A = \begin{bmatrix} 0 & 1 & 0 \\ -\frac{1}{m}\frac{\partial \ddot{z}}{\partial z} & 0 & -\frac{1}{m}\frac{\partial \ddot{z}}{\partial I} \\ \frac{\partial \dot{i}}{\partial z} & \frac{\partial \dot{i}}{\partial \dot{z}} & \frac{\partial \dot{i}}{\partial I} \end{bmatrix}, B = \begin{bmatrix} 0 \\ 0 \\ \frac{\partial \dot{i}}{\partial I_c} \end{bmatrix}, C = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix}, D = \begin{bmatrix} 0 \end{bmatrix}$$

 $z_o$  is related to  $I_o$  through the first equation. Since they are both equilibrium constants, we have:

$$\dot{z_0} = 0$$
,  $\dot{z_0} = 0$ 

Rearranging equation 1 for  $I_o$  yields the following expression:

$$I_{o} = \sqrt{\frac{mg}{K_{f}}}(z_{o} + a_{2}) - a_{1}$$

From measurement documentation, z\_o is selected to be 0.0252 m [3]. Therefore:

$$I_0 = 0.3975$$

The transfer function is the ratio of the output to the input. For this system, the input is the *command* current (not the excitation current) and the output is the height of the ball. Both are functions of time, so they can be transformed into the Laplace domain.

Since the partial derivatives for the linear model are with respect to the equilibrium conditions, they are constant values  $(z_0, I_0, a_1, a_2, I_{c_0})$ . Therefore to make the equations more easier to read, the symbol 'k' will be used to refer to a particular linear constant, with an identifying subscript linking it to a partial derivative

$$k_{z} = \frac{\partial \ddot{z}}{\partial z}, k_{I} = \frac{\partial \ddot{z}}{\partial I}$$

$$k_{i_{z}} = \frac{\partial \dot{I}}{\partial z}, k_{i_{z}} = \frac{\partial \dot{I}}{\partial \dot{z}}, k_{i_{c}} = \frac{\partial \dot{I}}{\partial I_{c}}, k_{i_{I}} = \frac{\partial \dot{I}}{\partial I}$$

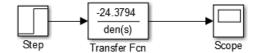
$$\frac{output}{input} = \frac{z}{I_{c}} = \frac{\frac{-k_{i}}{m} * k_{i_{c}}}{s^{3} - k_{i_{i}} * s^{2} + \left(\frac{k_{i}}{m} * k_{i_{z}} + \frac{k_{z}}{m}\right) * s - k_{i_{i}} * \frac{k_{z}}{m}}$$

$$-\frac{2K_{f}}{m} \frac{K_{a}}{K_{l}} \frac{(I_{o} + a_{1})}{(z_{o} + a_{2})^{2}} (z_{o} + a_{2})$$

$$\frac{z}{I_{c}} = \frac{s^{3} - \frac{1}{K_{l}} [(K_{a} - R)(z_{o} + a_{2})]s^{2} - \frac{2K_{f}}{mK_{l}} \frac{(I_{o} + a_{1})^{2}}{(z_{o} + a_{2})^{3}} [(K_{a} - R)(z_{o} + a_{2})]}$$

$$\frac{z}{I_c} = \frac{-24.3794}{s^3 + 52.9258s^2 - 32254.6763}$$

# **Linear Simulink Model**



# **Linear Response**



## TASK 3 – Expected performance

Zeros: None

**Poles:** 

20.9019

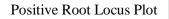
Gain: -24.379

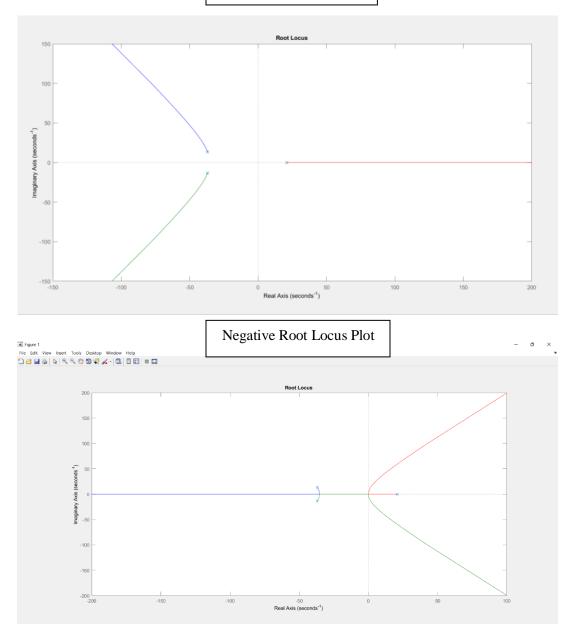
Zero-Pole-Gain form:

tf = 
$$\frac{-24.379}{(s - 20.9)(s^2 + 73.83s + 1543)}$$
  
 $\omega_n = \sqrt{1543} = 39.2810$   
 $\zeta = \frac{73.83}{\omega_n} = 1.8795$   
 $\phi = \tan^{-1}\left(\frac{\sqrt{1 - \zeta^2}}{\zeta}\right) = 1.2444j$   
 $\omega_d = \omega_n * \sqrt{1 - \zeta^2} = 62.5114j$   
Risetime:  $t_r = \frac{\pi - \phi}{\omega_d} = -0.0199 - 0.0503j$   
 $\%OS = 100 * e^{\left(\frac{-\zeta pi}{\sqrt{1 - \zeta^2}}\right)} = -84.2567 - 53.8592j$ 

\*It is important to note that using the 'stepinfo()' MATLab function for the transfer function, all pole-zero specifications returned either NaN or inf

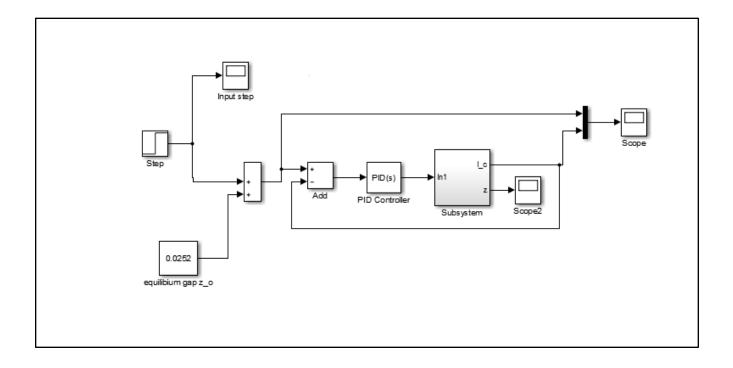
TASK 4 – Preliminary Design Evaluation

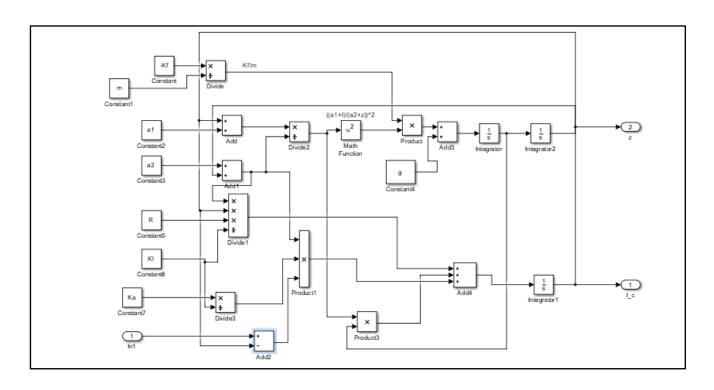


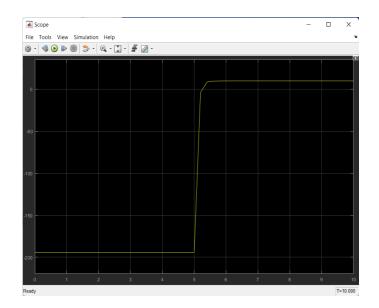


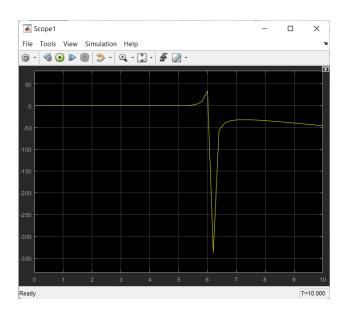
Since the system is unstable, P-control alone will not be enough to achieve the desired design parameters. The pole in the right-hand plane shows that Integral and derivative control are necessary as well. With P-control alone, the system will oscillate undesirably for an extended period of time when one position is required.

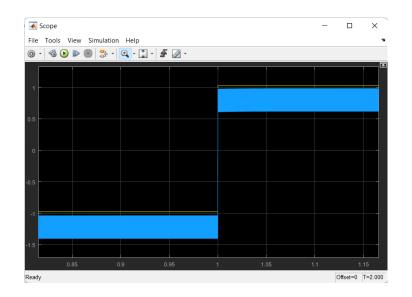
TASK 5 – Nonlinear Simulink model











### References

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